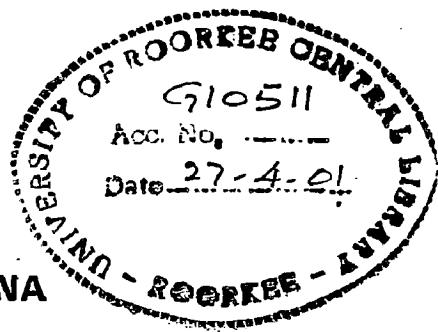


RESERVOIR OPERATION STUDY FOR PUMPED STORAGE SCHEME -A CASE STUDY

A DISSERTATION

**submitted in partial fulfillment of the
requirements for the award of the degree
of
MASTER OF ENGINEERING
in
WATER RESOURCES DEVELOPMENT**

**By
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January, 2001

10

Allah, who taught (the use of) the Pen
Taught man that, Which Allah knew not
(Qur'an: Al Alaq 4-5)

For their love, support, and advice,
this dissertation is dedicated to
my parents, my wife Desi, my son Pandu (Papas),
and my family.
They are with me always
and is my highest inspiration

CANDIDATE'S DECLARATION

I hereby certify that the work which is being presented in the dissertation entitled "**RESERVOIR OPERATION STUDY FOR PUMPED STORAGE SCHEME - A CASE STUDY**" in partial fulfilment of the requirement for the award of the Degree of **Master of Engineering in Water Resources Development (Civil)** submitted in the Water Resources Development Training Centre of the University is an authentic record of my own work carried out during a period from July, 2000 to January, 2001 under the supervision of Dr. B.N. ASTHANA, Emeritus Fellow at WRDTC, University of Roorkee, Roorkee, India.

The matter embodied in this dissertation has not been submitted by me for the award of any other degree.

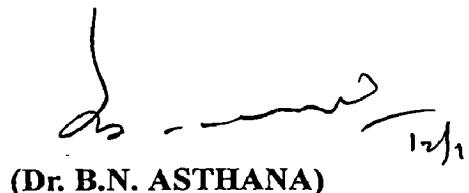
Place: Roorkee

Date: January , 2001



(DINNY SURYAKENCANA)

This is to certify that the above statement made by the candidate is correct to the best of my knowledge.



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(DINNY SURYAKENCANA)

ABSTRACT

In the modern industrialized society, there has been tremendous increase in the requirement of electricity. On one hand and at same time, management of greater variations in the energy used between day and night, weekdays and weekends or holidays and on the other hand, daily, weekly and yearly maximum loads pose serious problems to the electricity supply industries to deal with. If sufficient generating capacity is provided to meet the maximum system load, it requires heavy expenditure on plants with very little earning of revenue from it.

The electrical energy as such cannot be stored in large quantities. Energy storage system in the form of pumped storage can reduce the overall cost of power by reducing the amount of generating capacity required by absorbing energy during off-peak period and delivering it during peak load. The use of hydro pumped storage facilities to meet peaking capacity has been growing at an increasing rate in some countries. It has been adopted recently in India.

Reservoir operation study is very useful part of the project and should not be over looked. A correctly prepared operation schedule can show how the reservoir should be operated to derive maximum benefits.

Optimizing of reservoir operation of a pumped storage scheme is complex. Since computers are available as fast calculating tools, the problem of reservoir operation in small periods (such as hourly period for pumped storage scheme) can be easily solved. Computer program for such a study has been developed in this dissertation and its applicability has been illustrated in case of Tehri Hydro Electric Project. The study has shown that slight variations in project operation schedule of Tehri Pumped Storage Scheme have resulted in better irrigation facilities from the project and substantial increase in power generation.

CONTENTS

| | Page |
|--|-------------|
| CANDIDATE'S DECLARATION | i |
| ACKNOWLEDGEMENT | ii |
| ABSTRACT | iii |
| CONTENTS | v |
| LIST OF TABLES | vii |
| LIST OF FIGURES | ix |
| CHAPTER-1: INTRODUCTION | 1 |
| CHAPTER -2: RESERVOIR OPERATION STUDY ON PUMPED | |
| STORAGE SCHEME | 5 |
| 2.1 Pumped Storage Scheme | 5 |
| 2.1.1 Definition of Pumped Storage | 5 |
| 2.1.2 Type of Pumped Storage | 6 |
| 2.1.3 Role of Pumped Storage Schemes | 7 |
| 2.1.4 Development Pumped Storage in India | 12 |
| 2.1.4.1 Trend of Development | 12 |
| 2.1.4.2 Future Development | 12 |
| 2.1.5 World Scenario of Pumped Storage Scheme | |
| Development | 13 |
| 2.2 Reservoir Operation Study | 14 |
| 2.3 Decision on Operating Criteria | 15 |
| CHAPTER -3: DEVELOPMENT OF INPUT-OUTPUT MODEL | 17 |
| 3.1 The Model | 17 |
| 3.2 Input | 18 |
| 3.3 Output | 18 |
| 3.4 Computation Procedure | 19 |
| 3.5 Computer Program | 20 |
| 3.6 Explanation of Program Output | 20 |

CHAPTER -4: APPLICATION OF MODEL IN CASE OF TEHRI

| | |
|---|----|
| HYDRO ELECTRIC PROJECT | 25 |
| 4.1 Tehri Hydro Electric Project | 25 |
| 4.2 Project Data | 28 |
| 4.3 Proposed Operation Schedule | 34 |
| 4.3.1 Trial Combination of Peaking and Non-Peaking Hours | 34 |
| 4.3.2 Trial with Maximum Water to be Released or Pumped in Each Step Combination of Peaking And Non-Peaking Hours | 41 |

CHAPTER -5: DISCUSSION OF RESULT 53

| | |
|--|----|
| 5.1 Project Data | 53 |
| 5.2 Proposed Operation Schedule | 54 |

CHAPTER -6: CONCLUSION 61**REFERENCES** 65**APPENDIX I : PROJECT DATA****APPENDIX II : DROPS (D_Reservoir Operation of Pumped Storage Scheme)**

Program

- Definition of Variables
- Flowchart
- Listing of Computer Program
- Instruction for User

APPENDIX III :

- Input of Program
- Output of Program

LIST OF TABLES

| Title | Page |
|--|------|
| Table 4.1 Result of Reservoir Operation Study Model with Project Operation Schedule. RESULT OF DROPS: SROINT1.OUT (WITH PROJECT DATA) | 30 |
| Table 4.2 Ten Daily Schedule of Generating and Pumping at Tehri Reservoir | 31 |
| Table 4.3 Result of Reservoir Operation Study Model with Input Basic Duration of Peaking and Non-peaking Hour Time. RESULT OF DROPS: SROBAS1.OUT (WITH BASIC DURATION TIME DATA, STAGE I) | 37 |
| Table 4.4 Ten Daily Schedule of Generating and Pumping (Input and output for Stage I Process) | 38 |
| Table 4.5.a Result of Reservoir Operation Study Model with 9 Combination of Peaking and Non-peaking Hour. RESULT OF DROPS: COMBINAT.OUT (STAGE II) | 43 |
| Table 4.5.b Input Data to Develop Curve of % Meeting Irrigation Demand – Average Annual System Energy Generated | 43 |
| Table 4.6 Result of Reservoir Operation Study Model with Proposed Peaking and Non-peaking Hour with Maximum Water Releasing and Pumping. RESULT OF DROPS: SROMAX1.OUT (STAGE III) | 45 |
| Table 4.7 Ten Daily Schedule of Generating and Pumping (Input and output for Stage III Process) | 46 |
| Table 4.8 Result of Reservoir Operation Study Model with Proposed Operation Schedule. RESULT OF DROPS: SROPRF1.OUT (WITH PROPOSED DATA, STAGE IV) | 49 |

| | |
|---|-----------|
| Table 4.9 Proposed of Ten Daily Schedule of Generating and Pumping at Tehri Reservoir | 50 |
| Table 5.1 Calculation of Dependable Annual Energy Generated with Project Schedule Operation | 59 |
| Table 5.2 Calculation of Dependable Annual Energy Generated with Proposed Schedule Operation | 60 |

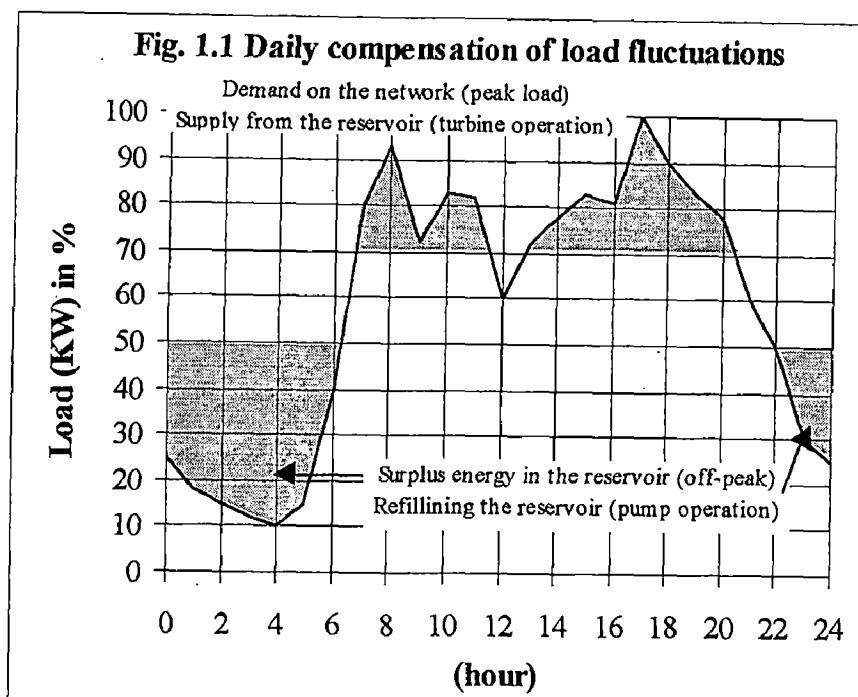
LIST OF FIGURES

| Title | Page |
|---|-------------|
| Fig. 1.1 Daily compensation of load fluctuations | 1 |
| Fig. 2.1.a Re-Circulating Type of Pumped Storage Scheme | 6 |
| Fig. 2.1.b Multi-use Type of Pumped Storage Scheme | 6 |
| Fig. 2.1.c Water Transfer Type of Pumped Storage Scheme | 7 |
| Fig. 4.1 Location Map of Tehri Hydro Electric Project | 26 |
| Fig. 4.2 Tehri Dam (Lay out of works) | 27 |
| Fig. 4.3 Reservoir flow condition : | |
| Fig. 4.3.1 First Peak Hour Condition | 34 |
| Fig. 4.3.2 First Non-peak Hour Condition | 35 |
| Fig. 4.3.3 Second Peak Hour Condition | 35 |
| Fig. 4.3.4 Second Non-peak Hour Condition | 35 |
| Fig. 4.3.5 Break Hour Condition | 36 |
| Fig. 4.4 Curve showing of | |
| % of Meeting Irrigation Demand vs Average Annual System Energy Generated | 44 |
| Fig. 5.1 Relation of Generator-motor capacity vs pump turbine performance | 53 |
| Fig. 5.2 Comparison of Project & Proposed Schedule Operation (in Yearly Basis) | 57 |
| Fig. 5.3 Comparison of Project & Proposed Schedule Operation (in Daily Basis) | 58 |

Chapter 1

INTRODUCTION

In the modern industrialized society, there has been tremendous increase in the requirements of electricity. On one hand and at same time, management of greater variations in the energy used between day and night, weekdays and weekends or holidays, and on the other hand, daily, weekly and yearly maximum loads pose serious problems to the electricity supply industries to deal with. If sufficient generating capacity is provided to meet the maximum system load, it requires heavy expenditure on plant with very little earning of revenue from it.



Since electrical energy cannot be stored in large quantities, the production of electricity must be adopted for whole time so that it corresponds at any given moment to the immediate consumption. Thus, sufficient generating capacity must be constructed to meet the peak load.

Technically this problem has been tackled by two ways either by storing energy generated by the base load power plants during off-peak hours, or by installing special peak load power plants having low fixed charges. One method of storing energy is by pumping water from lower reservoir downstream to upper reservoir, at times when the general demand for power is low and then by utilizing

the water stored in upper reservoir to generate hydroelectric power during the peak load periods. This is the concept of Pumped Storage Scheme.

One of the important things in Water Resources Planning, especially in a project of storage reservoir, is Reservoir Operation Study. This study can show us the behavior of reservoir during operation, and give a operation schedule which may optimize the utilization of storage.

To evaluate the behavior of reservoirs in a pumped storage scheme, we have to study the operation during each time step on hourly basis. It involves a huge amount of calculation if we have to process the time series data for the last 20 – 30 years.

This problem can be solved with the aid of computers. Capability of a computer recently is very amazing, so we can make a detailed study of the behavior of reservoir, and make operation schedule for the reservoir to optimize the benefits.

Reservoir Operation Study of Pumped Storage scheme has objectives as follow :

Design Stage :

- a. to determine the storage capacity and therefore the height of the dams
- b. to determine install capacity of pumped storage plant.

Operation Stage :

- a. to determine the yield, of the mean volume that could be released from the reservoir to fulfil its purposes;
- b. to optimize the operating schedule (schedule of generation time and pumping time) by simulating the reservoir operation using the series project data of the last 20 - 30 years.

In this dissertation, the objective is to develop a computer program for reservoir operation of a pumped storage scheme. The program is validated with the data of Tehri project, and the existing operating schedule or working table of Tehri stage II Hydro Electric project has been optimized by trial and errors of several combinations.

The dissertation has following chapters:

Chapter 2 presents the definition, principle, and types of pumped storage scheme and development of such schemes in India.

Chapter 3 presents literature review of reservoir operation study in general, and for pumped storage scheme.

Chapter 4 presents development of the input and output program DROPS (D_Reservoir Operations of Pumped Storage Scheme). It includes the steps of calculation.

Chapter 5 deals with application of model or program in case of Tehri Hydro electric Project and gives analysis and results of model runs for optimizing operation schedule.

Chapter 6 it deals with conclusions.

Appendices are Program Flowchart, listing of DROPS Program, example input and output of case study, and original project data.

Chapter 2

RESERVOIR OPERATION STUDY ON PUMPED STORAGE SCHEME

2.1 Pumped Storage Scheme

The advent of an ever-increasing number of large base-load generating units and the growth of high peak load demand has greatly increased the need for flexible peak load generating capacity. This peak load generating capacity could be provided by either quick start generating units such as combustion turbines, combined cycle units, diesels, and small common header compressed air, and batteries.³

Another effective alternative is to convert low cost surplus off peak electric power into peak power. Pumped hydro is one of the methods to do this conversion, although it is relatively expensive to install and the number of suitable sites is also limited.¹⁴

The use of hydro pumped storage facilities to meet peaking capacity has been growing at an increasing rate in some countries. In addition, these schemes can contribute to the overall electric power system by performing the function of load regulation, quick response reserve capacity to off-set short term generation or transmission outage and increase overall system energy.¹⁵

Because of their high effectiveness in utilization of power system, large capacity, high head, high speed, pumped storage power plants (PSPP) are now being constructed in the world. It is also gaining momentum in India.

2.1.1 Definition of Pumped Storage:

Pumped storage scheme is a combined pumping and generating plant; hence it is not a primary producer of electrical power but, by means of the conversions, stores the surplus power of the network and returns it in peak load periods.¹⁴

In this scheme water generates power during peak demand, while the same water is pumped back in the reservoir during lean demand period. The provision is based on economics of operation and the availability of enough spare capacity in the grid to operate the machines as pump in the low load period.⁸

2.1.2 Type of Pumped Storage Scheme⁸

- a. **Storage or Re-Circulating type**, water from reservoir A (Fig. 2.1.a) is used to produce power at station P and the discharge through tailrace is stored in reservoir B. During lean periods, the water from reservoir B is pumped back to A which later produces energy in time of need.

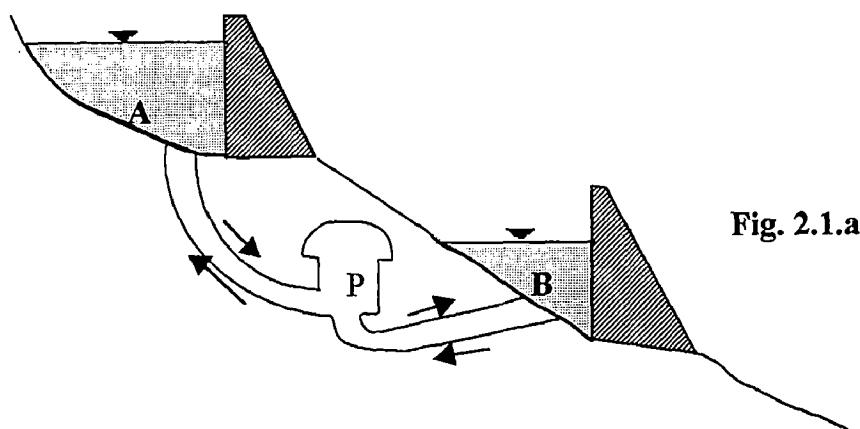


Fig. 2.1.a

- b. **Pondage or Multi-use type** in addition to the pumping back of reservoir B to reservoir A for producing peak power at station P_1 , some water of reservoir B is also used to produce power at station P_2 in the downstream (Fig. 2.1.b). Releases from P_2 will meet other water needs in the downstream.

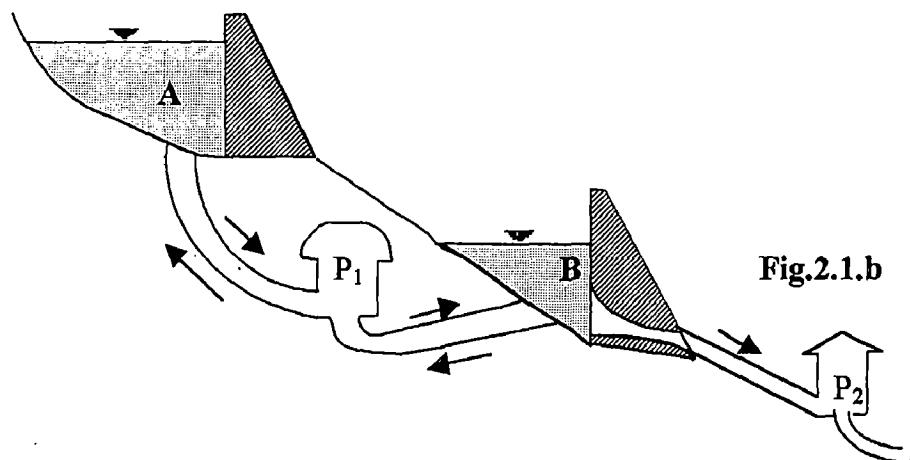


Fig. 2.1.b

- c. **Part Head or Water Transfer** type water of reservoir B is pumped to an elevated reservoir A in another valley. The water of reservoir A is utilized to produce power at station P in a third valley (Fig. 2.1.c).

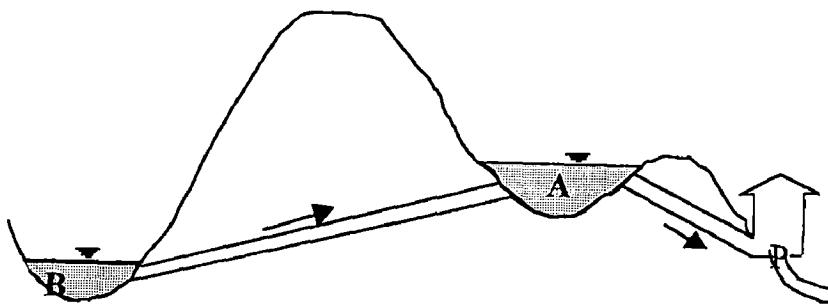


Fig.2.1.c

In this dissertation we consider the type of Multi-use Pumped Storage, It means there are some release from down stream reservoir to meet the requirement of several other interests. This type of pumped storage schemes is more common.

2.1.3 Role of Pumped Storage Schemes¹⁵

The role of pumped storage schemes in a power system is described in the following paragraph. These have all the merits of a hydropower station plus some additional advantages as is evident from the following.

Most Efficient and Practical means for Storing Large Quantity of Energy

Pumped storage hydroelectric schemes have proved technologically the most attractive method of storing excess system thermal energy during off peak hours and returning it to the system during peak hours. Although net extra energy production is not involved in pumped storage schemes, the conversion of otherwise excess night energy into high productive peak energy has provided the economic base for these schemes. Thus these schemes provide the most efficient and practical means for storing large quantity of energy. These plants spread in value between base power and peak power.

Reduction in System Minimum Loading

During off peak hours, when the load is low, some of the base load units may have to run at part load. If the minimum load is low enough, the sum of minimum operating levels of the committed base load units may still exceed the minimum load level. In this situation, the base load energy will be dumped or is forced to sell to the neighboring utilities at very low rates. If pumped storage scheme is available in the system, this dump energy can be used for pumping operation. Even if the system does not need that stored energy during the peak, having stored that energy allows the utility to sell it on peak to utilities at a profit.

Improvement in Efficiency and Economy of the Thermal Power Stations

The operation of thermal and nuclear power plants at very low load (during off peak period) would adversely affect the efficiency of the power system, power plant life and fuel consumption per KWh generated. Thus increasing number of large base load thermal and nuclear power plants, which cannot be operated at low loads due to economic reasons would need construction of pumped storage power projects. The pumped storage schemes improve the plant load factor, efficiency and durability of thermal units and reduce severe cycling of these units and hence they improve the operational performance of thermal power plants. These allow thermal generating units to operate at nearly constant output all the time and at the best efficiency instead of ramping up and down for the daily load cycle. This translates into lower thermal and mechanical stresses on the boiler and turbine. Reduction in wear and tear on an expensive base load unit can prolong its life, lower its maintenance costs, and improve its availability. All these benefits can result into significant cost savings. Frequent starting and stopping of thermal generating unit's results in the economic losses as well as adverse effects of the equipments. Thus the pumped storage hydroelectric schemes help in improving the operational and economic performances of thermal plants by creating favorable conditions in the power system, which facilitate base load operation of thermal/nuclear power plants.

Spinning Reserve Benefits

Spinning reserve benefits come from the fact that pumped storage schemes have a fast response time. Spinning reserve provided by thermal units is costly

because it forces a thermal unit to be operated at part load, which is inefficient, when pumped storage system is not generating at full load, its unused generating capacity can be used to meet the utility's spinning reserve requirements. Efficiency for pumped storage is not as sensitive to part load as that of thermal plant. Even if the pumped storage units are not generating, as long as there is water in the upper reservoir, the full rating of storage generating capacity is credited towards spinning reserve.

Thus, these schemes provide system-spinning reserve at no cost by operating the installation at partial load. When operated in this manner, the PSPP in many cases can achieve overall power system savings by reducing the portion of the required spinning reserves assigned to operating units and standby in steam electric plants. These schemes serve extremely well with their reserve capacity to maintain the power supply in case of failure of thermal and nuclear generating units or in case where there is an unanticipated high demand for electric power due to the availability to come rapidly on line at full load from no-load synchronized spinning reserve in as little as 15 seconds.

Power Generation Load Leveling

As there may be severe fluctuations in the daily power consumption patterns, it has become increasingly necessary to optimize the various type of electric power generation in order to achieve the most cost efficient supply of electricity. Pumped storage hydroelectric schemes can make this possible by utilizing power from thermal and nuclear generation facilities at night (off peak hours) to pump water from lower reservoir to upper reservoir, where it can repeatedly be used to generate power during peak demand hours.

In a power system without pumped storage generation, electricity power generation like thermal and nuclear are also primarily to meet peak demand. When the fluctuation in the demand becomes severe, the repeated start up and shut down required to make the required generation output adjustment result in high fuel costs and lower performance level for these power plants.

In a power system with PSPP, the power needs during peak demand periods can be met by these pumped storage schemes. In this way the system enables to modify the high and low extremes in operating levels of thermal and nuclear power

plants, thus facilitating a load leveling effect, which may result in an increased operating efficiency and reduced costs. Therefore, although the pumped storage schemes consume more energy than they generate and do not increase power system energy supply unless there is natural inflow into upper reservoir, these schemes level the peak and valleys of a typical electricity utility load curve and provide emergency power. These schemes create an artificial demand in the power system at low load periods by pumping water from lower pond to upper pond, which is then utilized to generate power to meet peak demands.

Voltage and Power Factor Correction

Voltage and power factor correction are additional operating benefits of pumped storage schemes, when the pumped storage units can operate in a voltage regulation mode like a synchronous condenser and can reduce losses as well as maintain the quality of services to customers.

Improved System Reliability

System operating reliability can be improved by having a pumped storage scheme in the system. The availability of a pumped storage plant is much higher than that of combustion turbines. The speed at which a reversible unit can be brought on line makes it ideal for covering for forced outages of thermal units in the system.

Output Adjustment Capabilities

Another continually growing importance/role of the pumped storage hydroelectric schemes is there availability for providing a quick employable reserve source of power and possibility for enabling load frequency regulations. Electricity is normally supplied at a frequency of 50 Hz. However this frequency is not constant, as it declines when supply capacity falls short of demand and increases in demand when supply is in excess of demand in the power system. Failure to keep supply and demand of the electricity can have an adverse effect on electrical and electronic equipment connected as the loads and may even cause power failures. Therefore the adjustment of generation output in response to demand fluctuations is an important way of ensuring the supply of high quality power at suitable

frequency. The important characteristics of PSPP (to reach maximum output within a very short period, say 3 to 5 minutes of start up and adjustment in their output within a matter of seconds) make them more flexible than thermal and nuclear power plants.

Environmentally Friendly

Pumped storage hydroelectric schemes are environmentally friendly. These schemes generate electric power by regulating water between upper and lower regulating reservoir. Once the water has been stored, it can be used repeatedly without changes in water levels downstream, except during the initial filling of the reservoirs. Thus the pumped storage hydroelectric schemes have got very limited, if any adverse effect on environment of the region and help in reducing pollution and others adverse effects which are otherwise likely to results from the development of alternative sources of energy for meeting the peak requirements. Further configuration of pumped storage schemes in mountain regions often provides for underground location of powerhouse and other key elements of the system, thus avoiding disruption of scenery and minimizing the esthetic impact of the new structure.

Other Attributes Offered by Pumped Storage Power Plants

The pumped storage hydroelectric schemes are economically advantageous because they convert low value, low cost, off peak energy to high value, on peak capacity energy and highly flexible peaking power. In addition these schemes are comparatively more flexible from the considerations of selection of their sites. These schemes require much less capital investment. Low investment, ruggedness in nature, easiness in maintenance due to simplicity in mechanism, flexibility in operation and design (short term peaking, spinning or ready reserve), high reliability, and hydrologic independence etc. are other attributes offered by PSPP.

2.1.4 Development Pumped Storage in India¹⁵

2.1.4.1 Trend of Development

It was Sixth Plan, when the first pumped storage hydroelectric scheme Nagarjunasagar (7×100 MW) in Andhra Pradesh was installed in India. First six units of 100 MW each of the project were commissioned in the Sixth Five Year Plan in the existing conventional Nagarjunasagar powerhouse (having one conventional unit of 110 MW already in operation). However, the units of the scheme are being operated as conventional units due to non-availability of the tail pond dam. Paithon(1×12 MW) in Maharashtra was the second pumped storage hydroelectric scheme installed in India during the same Plan. Thus, the total Hydro installed capacity under pumped storage schemes was 612 MW at the end of Sixth Five Year Plan.

The seventh unit of 100 MW at Nagarjunasagar pumped storage scheme and all the four units of Kadamparai pumped storage scheme (4×100 MW) in Tamil Nadu, aggregating to 500 MW were commissioned during Seventh Five Year Plan. Thus, the total hydroelectric installed capacity under pumped storage schemes was stepped up to 1112 MW at the end of Seventh Five Year Plan.

Kadana Stage I (2×60 MW) pumped storage scheme in Gujarat and reversible Panchet Hill second unit of 40 MW under Damodar Valley Corporation in Bihar were commissioned in 1990-91. Thus the total hydroelectric installed capacity under pumped storage schemes in operation as on 31st March 1992 (at the end of the Annual Plans 1990-91 and 1991-92) rose to 1272 MW.

During the Eight Five Year Plan, two pumped storage scheme, viz. – Ujjani (1×12 MW, commissioned), Bhira PSS (1×150 MW, rolled on 29th March 1995) and unit of 1 of 60 MW of Kadana Stage II (rolled on 31st March 1996). These on adding raising pumped storage installed capacity to 1494 MW on 31st March 1997.

2.1.4.2 Future Development.

Four sanctioned pumped storage schemes and unit 2 of 60 MW Kadana Stage II in the existing Kadana Stage I PSS in Gujarat with an aggregate installed capacity of 3310 MW are under various stages of construction in India. These schemes are Ghatgar (2×125 MW) in Maharashtra, Sardar Sarovar RBPH (6×200

MW) in Gujarat, Srisailam LBPH (6 x 150 MW) in Andhra Pradesh, Purulia PSS (4 x 225 MW) in West Bengal.

In addition to these Central Electricity Authority has cleared two pumped storage scheme, viz.- Bhivpuri PSS (1 x 90 MW) in Maharashtra and Tehri Stage II (4 x 250 MW) in Uttar Pradesh with an aggregate installed capacity of 1090 MW.

Further, Central Electricity Authority has identified 56 additional potential sites for development of pumped storage schemes with a probable installed capacity of 93,920 MW.

2.1.5 World Scenario of Pumped Storage Schemes Development¹⁵

Pumped storage hydroelectric schemes has its beginning in Switzerland, where the first pure pumped storage plant was constructed in 1904. This system of pumped storage power generation had separate turbine/generator and pump motor installation. The generator-motor system (tandem type) for combined usage as generator and motor was developed in 1910 and used in Italy.

In country like Germany where thermal power was main, the pumped storage power schemes were completed for the purpose of daily or weekly regulations so as to make effective the midnight surplus capacities of thermal power station and of imparting adaptability to be quick coping with fluctuations in power demand.

In 1925 a plant having greater capacity began operating in Federal Republic of Germany. In 1930s the first pumped storage plant in Japan was built.

To improve the economics of PSPP, reversible pump-turbines were developed in 1930s. Research and development of this type were carried out in various countries resettled in the introduction of high efficiency, high head, large capacity of pumped storage power stations. Today practically all pumped storage power stations have adopted this type.

The first significant progress in pumped storage (the beginning of single runner reversible pump/turbine development) was identified on the early 1940s in Brazil. The early 1950s saw the advent of the era of increased pumped storage construction. Canadian power authority developed the Niagara Falls installations, the first truly daily/nightly cycle pumped storage plants with reversible units. This

plant was converted from existing hydroelectric installations demonstrating the technological advancement in pumped storage developments.

Before 1960, there were about 40 PSPP with an aggregate approximate installed capacity of 2700 MW. At the end of 1974 additional 90 number of pumped storage power plants with a combined total installed capacity 10 times greater were in operation and many were in various stages of construction.

There are 290 PSPP with an aggregate installed capacity of about 82800 MW in operation in the world. USA has the credit of having the largest numbers of PPSP (38 number with 18091 MW total installed capacity). The second largest numbers of PSPP in operation are in Japan (38 number with 17005 MW total installed capacity). The third largest producer of PSPP is Italy (20 number with 6449 MW total installed capacity), followed by Germany (35 number with 5688 MW total installed capacity).

The unit capacity-wise, World's largest capacity of pump-turbine unit (398 MW) is installed at Helms PSPP in USA, installed in 1984. The second largest unit size (386 MW) is also in USA at Racoons Mountain installed in 1979.

There are 42 PSPP with an aggregate installed capacity of about 27400 MW in various stage of construction in the World. Maximum numbers of PSPP under construction are in Japan (8 number with 5480 MW total installed capacity).

About 550 number of PSPP aggregating to about 392,000 MW installations have been planned all over the world. Japan has planned the largest number of PSPP (440 number with 329,116 MW total installed capacity) for future development.

2.2 Reservoir Operation Study

The reservoir operation table is the result of reservoir operation study, which is also termed as working table shows the pattern of the inflow of water into the reservoir, and demand for the corresponding period, surplus to be stored or released during period. This is to be studied for the optimum utilization of the runoff. A correctly prepared operation table can show at a glance how the reservoir is going to behave after it has been put into operation. Operation table is very useful part of the project and should not be overlooked. It will also prove the adequacy of the capacity of the reservoir tentatively fixed earlier.⁸

The reservoir operation plan is devised to achieve the greatest value or benefit from the storage capacity. The plan must be based on ^{ed} 7.

- a. Knowledge of the flow characteristic of the stream.
- b. The purpose or purposes of the reservoir must be analyzed to determine, how the hydrograph of flow should be altered to produce the greatest benefits.
- c. Special considerations, such as the effect of sudden releases of stream flows and long sustained flows from the reservoir on agricultural developments and other interests in the valley below the reservoir.

The cooperation of two or more water uses generally permit savings large enough to make multi purpose storage reservoir economically attractive.

(Q1) The manner in which the coordination of different purposes is realized is controlled by the most important utilization of storage in the reservoir. The character of the sites determines this in turn. For instance, power generation is usually considered a secondary benefit in comparison to the other uses, but in some instances, power is the main objective. In such cases, the flood moderation capacity is provided as the surcharge capacity, so that any restriction on power generation should be precluded.

Fehm

A multi purpose operation does not differ essentially from the single purpose one. Identical principles apply to each water use without any regard to other uses, which are served by the same reservoir. The main difference is the necessity of allocating the specific capacity for each of the uses served. ⁷

For pumped storage power project, operation is based on the principle of power generation by exchange of the water between two impoundment. These impoundments are often man made, resulting from the damming of a free flowing stream. This scheme uses the energy of stored water to generate and store electric power. ¹⁵

2.3 Decision on Operating Criteria ¹⁵

The success of the pumped storage power development depends on the availability of the pumping up energy. Therefore the pumping up energy should be carefully studied to ensure the availability of it.

When total firm output of the base load power stations linked to the power system exceeds the off period demand, the difference becomes the availability of pumping up energy.

The pumping energy resources can be calculated based on demand projection, the power development projects and daily load curve on the typical highest load days and the lowest load days and the lean period. The difference between the daily loads curved produced for future demand and the base load during the night can be evaluated as pumping energy resources. 9

From projected typical daily load curve characteristic and availability of electric power, decision can be taken regarding:

- The hours during which and time when the surplus energy would be available in a day for pumping water from lower reservoir to the upper reservoir utilizing this surplus energy and therefore to decide number of pumping hours.
- The load curve would also indicate the deficit energy duration in hours and its period in order to use the available amount of water for the peak power generation.

Chapter 3

DEVELOPMENT OF INPUT-OUTPUT MODEL

3.1 The Model.

The proposed model is meant to be simple and easy to operate. It provides for each time step (that is each period of peak hour or non-peak hour), the water balance of Pumped Storage Reservoir System. It can be stated as follows.

$$\begin{aligned} & \text{[Inflow to the System]} - \text{[Outflow from the System]} = \text{[Change in Storage} \\ & \quad \text{System]} \end{aligned}$$

In case of Pumped Storage Scheme with two reservoir (Mixed use type):

$$\text{Reservoir A : } S_i = S_{i-1} + Q_i + P_i + Q_{pi} - E_i - I_i - Q_{ai} - S_p$$

$$\text{Reservoir B : } S_i = S_{i-1} + Q_i + P_i + Q_{ai} - Q_{pi} - E_i - I_i - Q_{ai} - S_p - D_i$$

Where, S_i = Storage at the end of the period i

Q_i = Inflow during the period i

P_i = Precipitation over the reservoir during the period i

Q_{pi} = Pumping flow during the period i

E_i = Evaporation from the reservoir during the period i

I_i = Infiltration under the reservoir during the period i

Q_{ai} = Release through power tunnel from reservoir A to reservoir B
during the period i

S_p = Spill from the reservoir during the period i

D_i = Release from B during the period i to meet downstream demand

Q_{pi} = 0 at peak hour } 9

Q_{ai} = 0 at non-peak hour } .

S_{i-1} = define it.

In this study the precipitation over the reservoir and infiltration through reservoir have been neglected, so water balance formula has been rewritten as below:

$$\text{Reservoir A : } S_i = S_{i-1} + Q_i + Q_{pi} - E_i - Q_{ai} - S_p$$

$$\text{Reservoir B : } S_i = S_{i-1} + Q_i + Q_{ai} - Q_{pi} - E_i - Q_{ai} - S_p - D_i$$

3.2 I n p u t

Input to computer program (DROPS program) of reservoir operation model consist of the storage-elevation curve and the area-elevation curve for each reservoir (File name “RACAP.DAT” and “RBCAP.DAT”), and value of S_{max} and S_{min} of each reservoir, data of physical construction (File name “SCHEME.DAT”) are read in. This program also facilitated with interactive input of physical construction data if needed.

The following input data available on monthly basis has been computerized:

1. Inflow into. (File name is “INTEHRI.DAT”)
2. Evaporation losses. (File name “EVAP.DAT”)
3. Irrigation demand. (File name “IRRDM.DAT”)

This data has been converted into ten daily bases, as the proposed project operation schedule is also on ten daily bases.

3.3 O u t p u t

Outputs from the reservoir operation model are:

1. Water elevation and volume of water in storage as a function of time for the operation period, for each reservoir, volume of water into the reservoirs and water release for irrigation demand. (File name “ROAXXXx.OUT”, and “ROBXXXx.OUT”)
2. Gross head, net head, discharge for energy generation on upper and lower powerhouses, corresponding to volume of water release for irrigation demand, percentage of irrigation supply and total energy generated from whole system. (File name “ENGXXXx.OUT”)
3. Annual water balance showing the monthly inflow, evaporation, yield and spilling of each reservoir. (File name “SROXXX0.OUT”)
4. Average annual energy generated for full series of inflow data, average percentage of meeting irrigation demand. (File name “SROXXX1.OUT”)
5. Average 10 daily percentage of meeting irrigation demand for full series of inflow data. (File name “SROXXX1.OUT”)

3.4 Computation Procedure

The water balance study is subject to the following assumptions:

1. Inflow/runoff, irrigation demand, and evaporation losses are uniform in hourly basis. Actually is depending on the data we have.
2. SA_0 , initial storage at upper reservoir (upper reservoir = 'A'), corresponding to HA_0 , initial elevation at reservoir A = FRL (Full Reservoir Level) at the end of monsoon period (1st October). SB_0 , initial storage at lower reservoir (lower reservoir = 'B'), corresponding to HB_0 , initial elevation at reservoir B = MDDL (Minimum Draw Down Level).
3. All water release in operation of reservoir A and B is through powerhouse during non-monsoon period.

Calculation in each step period:

a. General

1. All calculations of water releasing and pumping, are subject to condition the water level in the both reservoir will in no case fall below MDDL.
2. Maximum amount of water release from A is equal to live storage capacity of the reservoir B that is smaller storage capacity.
3. Amount of water release from A shall meet irrigation demand, evaporation loss and shall fill reservoir B upto FRL. Spilling from B is minimized. Except in monsoon period, when inflow is too much, i.e. more than storage capacity of both reservoirs.
4. If S_i is greater than S_{max} , the storage capacity, then :

$$Sp_i = S_i - S_{max}, S_i = S_{max}$$

This condition states that the storage in the reservoir should not exceed S_{max} . ✓

5. Pumping of water from B to A, is restricted to the maximum water release from A or to the amount of water available above the MDDL at B, or to the amount of water which will fill A up to FRL.
6. Release from B to meet the irrigation demand subject to 24 hours release.

- b. In case of optimization of operation schedule of existing pumped storage scheme, there are some additional constraints to be considered for above calculation:

1. Maximum capacity of water conductor.
2. Maximum capacity of turbine in generating mode or pumping mode.
3. Maximum installed capacity.
4. Period for pumping back of water.

3.5 Computer Program

Beside the DROPS program (D_Reservoir Operation of Pumped Storage Scheme) where details are given in Appendix I, Another computer program DROPSC program (D_Reservoir Operation of Pumped Storage Scheme with different Combination of peaking and non-peaking hours) has been developed. Basically it is same as DROPS but looping for each combination of peaking and non-peaking hours for all 35 years series data, and not all OUTPUT of DROPS program has been taken in files. It is for reducing the time of Program running and reducing memory consumption. In DROPSC only the summary of the reservoir operation, to see the relation between Percentage of Success of Irrigation Demand and Total Energy Generated is taken on file name COMBINAT.OUT.

3.6 Explanation of Program Output

Outputs of the program are in form of tables and the program will be automatically divide the output file in every 8 years data,

ROAXXXx : ROA = Reservoir Operation at A (upper reservoir),

XXX = Three initial first letter from input of Inflow data file

x = Number of file automatically given by program, start from 0

In ROA file, there are the name of month, year of operation and 11 columns, the value of flow is +ve if into the reservoir and -ve if out from reservoir

Column 1, DATE: Date of operation

Column 2, PERIOD: Condition of period (Peak or non-peak hours)

Column 3, DURATION: Duration of period in hours

Column 4, INFLA: Natural inflow to the reservoir A in M³

Column 5, QPUMP: Volume of water pumping from lower reservoir in M³

Column 6, EVAPLA: Evaporation Losses of reservoir A in M³

Column 7, QA: Volume of water releases from reservoir A, through power tunnel in M^3

Column 8, SPILLA: Volume of water spills from reservoir A in M^3

Column 9, STOREA: Volume of water stores in reservoir A in M^3

Column 10, AREA: Area of water surfaces in reservoir A in M^3

Column 11, EL.A: Elevation of water surface in reservoir A in M

ROBXXXXx : ROB = Reservoir Operation at B (lower reservoir),

XXX = Three initial first letter from input of Inflow data file

x = Number of file automatically given by program, start from 0

In ROB file, there are the name of month, year of operation and 12 columns, the value of flow is +ve if into the reservoir and -ve if out from reservoir

Column 1, DATE: Date of operation

Column 2, PERIOD: Condition of period (Peak or non-peak hours)

Column 3, DURATION: Duration of period in hours

Column 4, INFLB: Natural inflow + Spill from reservoir A to the reservoir

B in M^3

Column 5, QA: Volume of water release from reservoir A to reservoir B, through power tunnel in M^3

Column 6, IRRS: Volume of water release from B to meet irrigation demand in M^3

Column 7, EVAPLB: Evaporation Losses of reservoir B in M^3

Column 8, QPUMP: Volume of water pumping to upper reservoir in M^3

Column 9, SPILLB: Volume of water spills from reservoir B in M^3

Column 10, STOREB: Volume of water stores in reservoir B in M^3

Column 11, BREA: Area of water surfaces in reservoir B in M^3

Column 12, EL.B: Elevation of water surface in reservoir B in M

After end of month, there is summation of spilling water from reservoir B in M^3

ENGXXXx : ENG = Total Energy Generated,

XXX = Three initial first letter from input of Inflow data file

x = Number of file automatically given by program, start from 0

In ENG file, there are the name of month, year of operation and 13 columns.

Column 1, DATE: Date of operation

Column 2, PERIOD: Condition of period (Peak or non-peak hours)

Column 3, DURATION: Duration of period in hours

Column 4, GROSSH: Gross Head in M

Column 5, NETTH: Net Head = Gross Head – Friction head loss in M

Column 6, Q: Discharge through power tunnel of U/S powerhouse in M^3/sec

Column 7, STARTP: Power Generated at start period in MW

Column 8, ENDP: Power Generated at end period in MW

Column 9, AV.ENERGY: Average Energy Generated at U/S powerhouse in
MWh

Column 10, QD: Discharge through D/S powerhouse in M^3/sec

Column 11, ENERGY: Energy Generated at D/S powerhouse in MWh

Column 12, TOT.ENERGY: Total Energy Generated at U/S and D/S
powerhouse in MWh

Column 13, IRR.: Percentage Irrigation Supply inn each period

SROXXXx : SRO = Summary of Reservoir Operation,

XXX = Three initial first letter from input of Inflow data file

x = Number of file automatically given by program, 0 and 1

SROXXX0 = File Summary of Reservoir Operation in Every Year (monthly basis)

In SROXXX0 file, there are the year of operation and 12 columns

Column 1, MONTH: Month of operation

Column 2, RUNOFF A: Summary of Inflow to Reservoir A in M^3

Column 3, RUNOFF B: Summary of Inflow to Reservoir B in M^3

Column 4, TOTAL: RUNOFF A + RUNOFF B in M^3

Column 5, IRRIG.DEMAND: Total Irrigation Demand in M^3

Column 6, EVAP.LOSS: Evaporation Losses of reservoir in mm/day

Column 7, IRRIG.SUPPLY: Total Irrigation Supply in M^3

Column 8, IRRIG.DEMAND STATUS: Status of Percentage Meeting
Irrigation Demand. Succeed = 100%

Column 9, AV.POWER START: Average Power Generated at start period
in MW

Column 10, AV.POWER END: Average Power Generated at end period in
MW

Column 11, AV.ENERGY GENERATED: Total Average Energy
Generated in MWh at U/S powerhouse

Column 12, SPILL AT B: Total Volume of water spills from reservoir B in
 M^3

After end of year, there is summation of all parameters, and the minimum elevation
occur in reservoir A and reservoir B

SROXXX1 = File Summary of Reservoir Operation in 35 Years (yearly basis)

In SROXXX1 file, there are 2 tables with 10 and 4 columns respectively

In first table, it is Summary of Reservoir Operation in 35 Years (yearly basis)

Column 1, YEAR: Year of operation

Column 2, TOTAL INFLOW: TOTAL RUNOFF on this year in M^3

Column 3, IRRIG.DEMAND: Total Irrigation Demand on this year in M^3

Column 4, IRRIG.SUPPLY: Total Irrigation Supply on this year in M^3

Column 5, IRRIG.DEMAND STATUS: Status of Percentage Meeting
Irrigation Demand.

Column 6, AV.ENERGY GENERATED: Total Average Energy Generated
in MWh at U/S powerhouse on this year

Column 7 SPILL AT B: Total Volume of water spills from reservoir B on
this year in M^3

Column 8, HA MIN: Minimum Elevation Occurs in reservoir A in M

Column 9, HB MIN: Minimum Elevation Occurs in reservoir B in M

Column 10, TOT. SYSTEM EN. GENERATE: Total System Energy
Generated in MWh on this year

After end of 35 years operation, there are Average Percentage Meeting Irrigation Demand, Average Annual of Energy Generated, and the minimum elevation occur in reservoir A and reservoir B

Second table is Summary of ten daily Average Percentage Meeting Irrigation Demand;

Column 1, MONTH: Name of month

Column 2: Average Percentage Meeting Irrigation Demand in first 10 daily
for all 35 years operation on this month.

Column 3: Average Percentage Meeting Irrigation Demand in second 10
daily for all 35 years operation on this month

Column 4: Average Percentage Meeting Irrigation Demand in third 10 daily
for all 35 years operation on this month

Chapter 4

APPLICATION OF MODEL IN CASE OF TEHRI HYDRO ELECTRIC PROJECT

4.1 Tehri Hydro Electric Project^{9,15}

Tehri Hydro Electric Project is located at Tehri, Uttaranchal. The project is under construction across river Bhagirathi, a tributary of river Ganga it is a project to meet irrigation requirements and hydropower development. A location map of the scheme is given at Figure 4.1

Upper Reservoir

The scheme envisages creation of an upper reservoir by constructing a dam across Bhagirathi River in Tehri Garhwal district of Uttaranchal. It is an earth and rockfill type 260.5 m high and dam, with a live storage capacity of 2615 MCM.

Lower Reservoir

The lower reservoir for the scheme would be at Koteshwar, which is to be created by constructing a dam across Bhagirathi River with a live storage capacity of 36 MCM. It is about 4 km downstream of upper reservoir. It has FRL equal to TWL of upper reservoir i.e. 612.0 M and MDDL at the riverbed level below upper dam i.e. 598.5 M.

Water Conductor System

Water conductor system of the scheme would have two submerged type intakes at the left bank of Bhagirathi River, two headrace tunnels and four penstocks for one power house of four units.

Powerhouse

The underground powerhouse complex at Tehri comprises of eight machines of 250 MW each. Four of these machines housed in one cavity are conventional type having an installed capacity of 1000 MW (4×250 MW). The other four machines are reversible machines and these can operate in turbine as well

as pumping mode. The capacity of each reversible machine is also 250 MW and these are installed in another cavity called the PSP. Apart from this, there is another surface powerhouse at Koteshwar with an installed capacity of 400 MW (4×100 MW). The layout of the project is shown in Figure 4.2

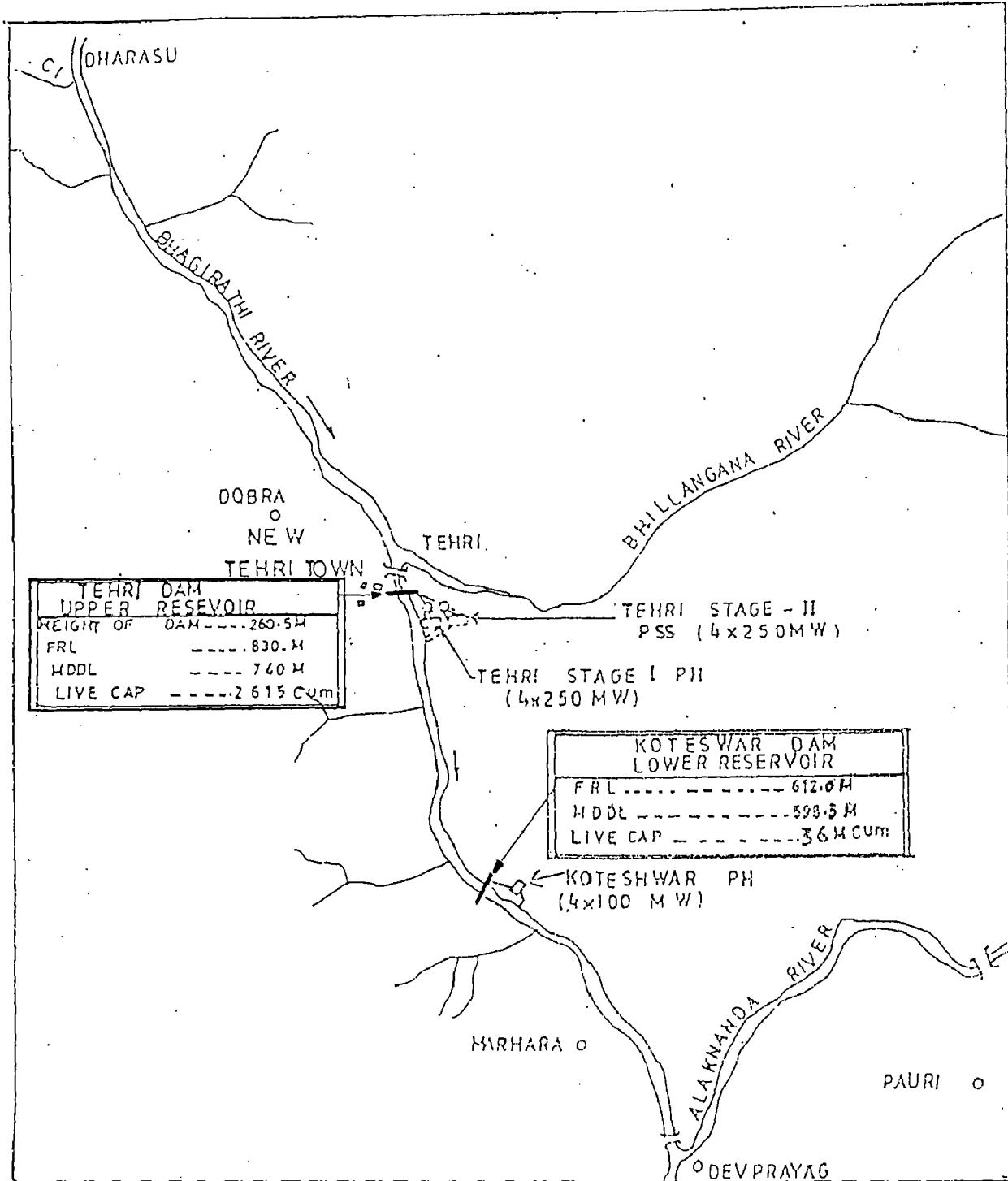


Fig. 4.1 Location Map of Tehri Hydro Electric Project

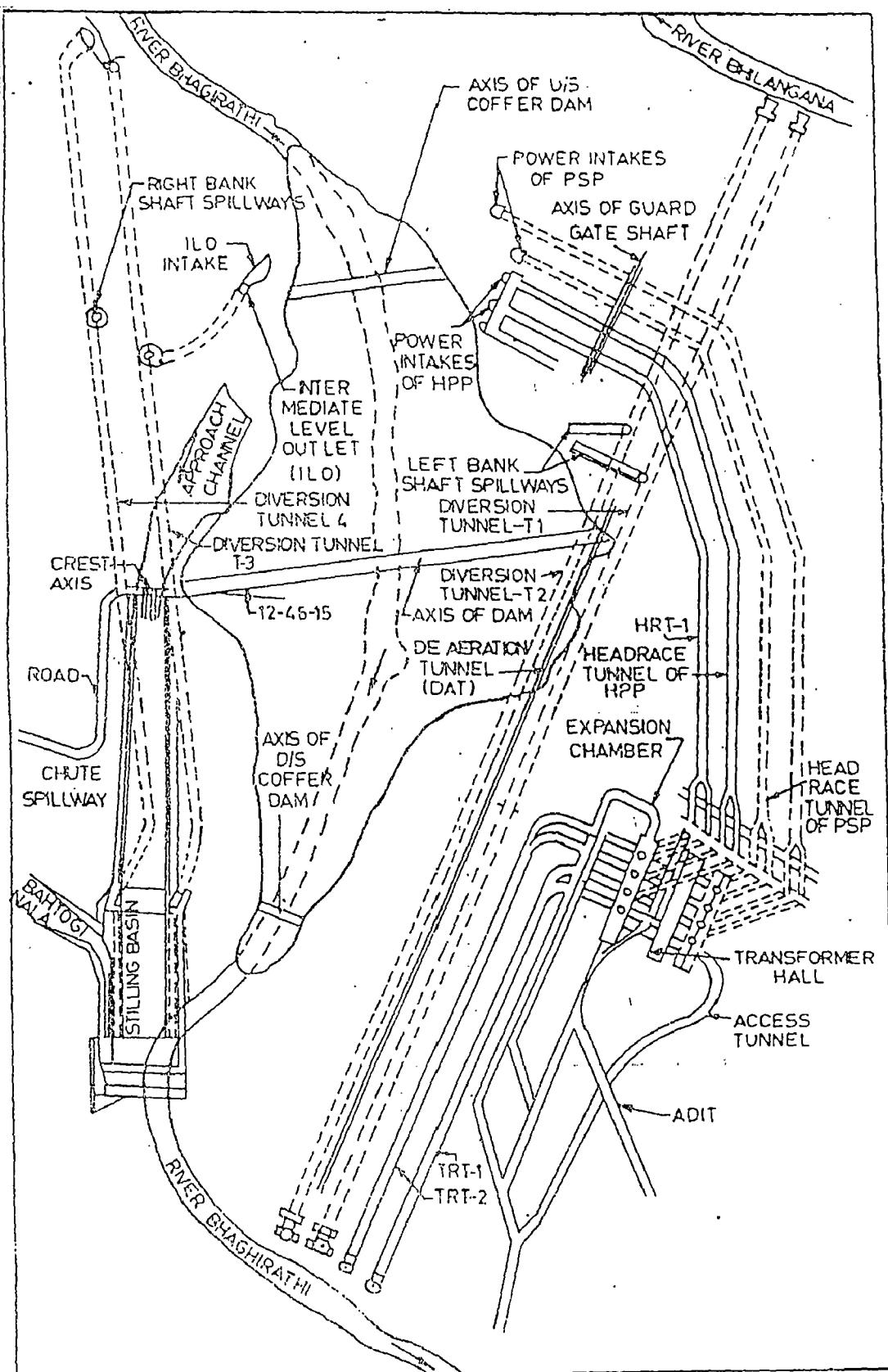


Fig. 4.2 Tehri Dam (Lay out of works)

4.2 Project Data

Detail of the project data can be seen in Appendix II. These are briefly summarized below:

- Inflow runoff data series to Tehri reservoir (upper reservoir i.e. Reservoir A) on monthly basis is available for 35 years, from 1963 – 1997. No additional inflow to Koteswar reservoir (lower reservoir i.e. Reservoir B), except releases is expected from the intervening catchments from reservoir A.
- Evaporation losses on monthly basis.
- Irrigation demand downstream of reservoir B on monthly basis. There is no irrigation demand from this project in July, August, and September months.
- Area-capacity data of Tehri reservoir and Koteswar reservoir are available.
- FRL at A = 830 M
- MDDL at A = 740 M
- FRL at B = 612 M
- MDDL at B = 598.5 M
- Install capacity at Tehri (upper powerhouse) 8 x 250 MW, with 4 machines reversible type and 4 machines conventional type.
- All assumption in section 3.4 are applicable
- Additional physical constraint based on project data:

1. Maximum discharge capacity of turbine in generating mode has been worked out from the maximum release shown in project operation schedule. It is on 1st ten daily of January: Maximum volume of water release = 17.79 MCM

$$\frac{17.79 \text{ MCM}}{4 \text{ hr}} = \frac{17.19 \times 10^6}{4 \times 3600} = 1235.42 \frac{\text{M}^3}{\text{sec}} \text{ for 8 machines or } 154.43 \frac{\text{M}^3}{\text{sec}}$$

each machine.

2. Maximum discharge capacity of turbine in pumping mode has been worked out from the releases on 2nd ten daily of June of project operation schedule:

$$\frac{2.36 \text{ MCM}}{1.1 \text{ hr}} = \frac{2.36 \times 10^6}{1.1 \times 3600} = 595.96 \frac{\text{M}^3}{\text{sec}} \text{ for 4 machines or } 148.99 \frac{\text{M}^3}{\text{sec}}$$

each machine. Maximum capacity for pumping by 4 machines in 8 hours

$$= 595.96 \frac{\text{M}^3}{\text{sec}} \times 8 \text{ hr} \times 3600 \text{ sec} = 17.16 \text{ MCM}$$

3. Power tunnel ¹⁵: 2 nos., diameter, D = 8.5 M, length, L = 1100 M

4. Other assumptions:

- Efficiency of turbine and machine, $\eta = 0.85$
- Coefficient of friction, f = 0.02
- Net head of Koteswar powerhouse $H_n = 75 \text{ M}$
- Head losses, $H_l = \frac{fLv^2}{2gD}$

5. Maximum discharge capacity through Koteswar powerhouse:

$$Q = \frac{P}{9.81H_n\eta} = \frac{400 \times 10^3}{9.81 \times 75 \times 0.85} = 625.39 \frac{\text{M}^3}{\text{sec}}$$

6. Availability period for pumping up water at night from 10.00 pm. to 06.00 am.

7. The combination of peaking and non-peaking hours and net inflows are taken as given in project operation schedule. It will become the maximum limit of water releasing or pumping.

Using the input data based on project data the DROPS program was run for 35 years inflow series to work out the percentage of success to meeting irrigation demand and generation of energy. The results are given in table 4.1 and table 4.2

TABLE 4.1 SUMMARY OF TOTAL RESERVOIR OPERATION

| YEAR OF | TOTAL INFLOW (M3) | IRRIG. DEMAND (M3) | IRRIG. SUPPLY (M3) | IRRIG. AV. ENERGY DEMAND GENERATED STATUS | SPILL (MWh) | HA MIN (M) | HB MIN EN.GENERATE (M) | TOT. SYSTEM (MWh) |
|------------------|-------------------------|--------------------------|--------------------------|---|----------------|------------------|------------------------------|----------------------|
| 1963 | .9010E+09 | .9832E+09 | .9299E+09 | 94.58% | .621E+06 | .222E+09 | 823.08 | 598.50 .782E+06 |
| 1964 | .5643E+10 | .4606E+10 | .4450E+10 | 96.61% | .354E+07 | .151E+10 | 747.71 | 598.50 .432E+07 |
| 1965 | .7066E+10 | .4606E+10 | .4431E+10 | 96.21% | .345E+07 | .226E+10 | 740.07 | 598.50 .422E+07 |
| 1966 | .8281E+10 | .4606E+10 | .4538E+10 | 98.52% | .366E+07 | .366E+10 | 759.19 | 598.50 .445E+07 |
| 1967 | .6760E+10 | .4606E+10 | .4496E+10 | 97.61% | .362E+07 | .226E+10 | 753.99 | 598.50 .440E+07 |
| 1968 | .6859E+10 | .4606E+10 | .4527E+10 | 98.28% | .356E+07 | .226E+10 | 753.06 | 598.50 .435E+07 |
| 1969 | .7090E+10 | .4606E+10 | .4560E+10 | 98.99% | .353E+07 | .246E+10 | 740.58 | 598.50 .433E+07 |
| 1970 | .7501E+10 | .4606E+10 | .4521E+10 | 98.15% | .360E+07 | .299E+10 | 752.53 | 598.50 .439E+07 |
| 1971 | .7100E+10 | .4606E+10 | .4403E+10 | 95.59% | .365E+07 | .267E+10 | 773.16 | 598.50 .441E+07 |
| 1972 | .7346E+10 | .4606E+10 | .4475E+10 | 97.16% | .350E+07 | .282E+10 | 740.07 | 598.50 .428E+07 |
| 1973 | .7128E+10 | .4606E+10 | .4497E+10 | 97.64% | .365E+07 | .259E+10 | 764.60 | 598.50 .443E+07 |
| 1974 | .7481E+10 | .4606E+10 | .4455E+10 | 96.73% | .348E+07 | .298E+10 | 761.77 | 598.50 .425E+07 |
| 1975 | .6439E+10 | .4606E+10 | .4129E+10 | 89.64% | .332E+07 | .229E+10 | 740.05 | 598.50 .404E+07 |
| 1976 | .9728E+10 | .4606E+10 | .4487E+10 | 97.42% | .372E+07 | .513E+10 | 770.95 | 598.50 .450E+07 |
| 1977 | .1192E+11 | .4606E+10 | .4606E+10 | 100.00% | .373E+07 | .727E+10 | 753.86 | 600.01 .453E+07 |
| 1978 | .1099E+11 | .4606E+10 | .4444E+10 | 96.48% | .358E+07 | .658E+10 | 740.10 | 598.50 .436E+07 |
| 1979 | .8547E+10 | .4606E+10 | .4503E+10 | 97.76% | .352E+07 | .402E+10 | 740.12 | 598.50 .430E+07 |
| 1980 | .7977E+10 | .4606E+10 | .4525E+10 | 98.23% | .360E+07 | .340E+10 | 755.16 | 598.50 .438E+07 |
| 1981 | .6130E+10 | .4606E+10 | .4507E+10 | 97.86% | .347E+07 | .154E+10 | 760.92 | 598.50 .425E+07 |
| 1982 | .7302E+10 | .4606E+10 | .4530E+10 | 98.34% | .350E+07 | .272E+10 | 741.95 | 598.50 .428E+07 |
| 1983 | .5631E+10 | .4606E+10 | .4190E+10 | 90.96% | .330E+07 | .150E+10 | 740.08 | 598.50 .403E+07 |
| 1984 | .8785E+10 | .4606E+10 | .4438E+10 | 96.35% | .351E+07 | .424E+10 | 749.83 | 598.50 .428E+07 |
| 1985 | .8798E+10 | .4606E+10 | .4484E+10 | 97.34% | .358E+07 | .426E+10 | 747.10 | 598.50 .436E+07 |
| 1986 | .5945E+10 | .4606E+10 | .4383E+10 | 95.16% | .339E+07 | .155E+10 | 769.38 | 598.50 .415E+07 |
| 1987 | .8491E+10 | .4606E+10 | .4514E+10 | 98.00% | .355E+07 | .386E+10 | 741.52 | 598.50 .433E+07 |
| 1988 | .7139E+10 | .4606E+10 | .4415E+10 | 95.85% | .356E+07 | .273E+10 | 765.29 | 598.50 .433E+07 |
| 1989 | .7205E+10 | .4606E+10 | .4504E+10 | 97.80% | .362E+07 | .262E+10 | 753.40 | 598.50 .440E+07 |
| 1990 | .6484E+10 | .4606E+10 | .4524E+10 | 98.21% | .351E+07 | .190E+10 | 744.62 | 598.50 .430E+07 |
| 1991 | .8231E+10 | .4606E+10 | .4556E+10 | 98.91% | .358E+07 | .363E+10 | 759.33 | 598.50 .437E+07 |
| 1992 | .6705E+10 | .4606E+10 | .4529E+10 | 98.33% | .348E+07 | .215E+10 | 740.08 | 598.50 .426E+07 |
| 1993 | .9172E+10 | .4606E+10 | .4474E+10 | 97.14% | .360E+07 | .461E+10 | 766.71 | 598.50 .438E+07 |
| 1994 | .7031E+10 | .4606E+10 | .4524E+10 | 98.21% | .354E+07 | .249E+10 | 750.32 | 598.50 .433E+07 |
| 1995 | .7264E+10 | .4606E+10 | .4551E+10 | 98.81% | .347E+07 | .261E+10 | 740.14 | 598.50 .426E+07 |
| 1996 | .8222E+10 | .4606E+10 | .4462E+10 | 96.87% | .360E+07 | .370E+10 | 784.87 | 598.50 .437E+07 |
| 1997 | .9878E+10 | .4606E+10 | .4556E+10 | 98.92% | .363E+07 | .513E+10 | 766.22 | 598.50 .442E+07 |
| AVERAGE ANNUAL = | | | | 97.11% | .354E+07 | .317E+10 | | .432E+07 |

MIN. ELEVATION AT A = 740.05 M
 MIN. ELEVATION AT B = 598.50 M

10 DAYS % AVERAGE MEETING IRR. DEMAND

| MONTH | 1st | 2nd | 3rd |
|-----------|--------|--------|--------|
| JANUARY | 100.00 | 100.00 | 100.00 |
| FEBRUARY | 100.00 | 100.00 | 100.00 |
| MARCH | 100.00 | 100.00 | 100.00 |
| APRIL | 100.00 | 99.98 | 99.82 |
| MAY | 98.02 | 95.01 | 92.59 |
| JUNE | 99.26 | 99.56 | 98.99 |
| JULY | .00 | .00 | .00 |
| AUGUST | .00 | .00 | .00 |
| SEPTEMBER | .00 | .00 | .00 |
| OCTOBER | 100.00 | 100.00 | 99.96 |
| NOVEMBER | 91.64 | 78.90 | 78.66 |
| DECEMBER | 99.81 | 99.84 | 99.59 |

Table 4.2-1 Ten Daily Schedule of Generating and Pumping at Tehri Reservoir

| PERIOD | PARAMETERS | 06-08 hrs | 08-12 hrs | 12-18 hrs | 18-22 hrs | 22-06 hrs | Net D/S release | % Irrigation Supply | |
|-------------|-----------------------------------|-----------|-----------|-----------|-----------|-----------|-----------------|---------------------|---------------------|
| | | 2 hrs | 4 hrs | 6 hrs | 4 hrs | 8 hrs | D/S release | Theoretical | Reservoir Op. Study |
| JAN (1-10) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 3 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 13.30 | | 17.79 | -10.13 | 20.96 | 99.47 | 100.00 |
| JAN (11-20) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 3.5 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 15.15 | | 17.51 | -10.71 | 21.95 | 104.17 | 100.00 |
| JAN (21-31) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 3.8 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 16.35 | | 17.28 | -11.17 | 22.46 | 106.59 | 100.00 |
| FEB (1-10) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 7 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.05 | | 17.05 | -10.25 | 23.85 | 104.44 | 100.00 |
| FEB (11-20) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 3.5 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 14.63 | | 16.82 | -12.1 | 19.35 | 84.74 | 100.00 |
| FEB (21-28) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 7.8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 16.47 | | 16.47 | -12.29 | 20.65 | 90.43 | 100.00 |
| MAR (1-10) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 7.1 | | | |
| | Net inflow in D/S reservoir (MCM) | | 16.24 | | 16.24 | -11.66 | 20.82 | 106.26 | 100.00 |
| MAR (11-20) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 15.9 | | 15.9 | -10.89 | 20.91 | 106.72 | 100.00 |
| MAR (21-31) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 6.8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 15.65 | | 15.65 | -12.09 | 19.21 | 98.04 | 100.00 |
| APR (1-10) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 7.4 | | | |
| | Net inflow in D/S reservoir (MCM) | | 15.32 | | 15.32 | -13.36 | 17.28 | 92.74 | 100.00 |
| APR (11-20) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 6.7 | | | |
| | Net inflow in D/S reservoir (MCM) | | 15.09 | | 15.09 | -12.3 | 17.88 | 95.96 | 99.98 |
| APR (21-30) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 4.8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 14.86 | | 14.86 | -9.07 | 20.65 | 110.82 | 99.82 |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. Study % Irrigation Supply = Average of 35 years reservoir operation simulation study

Table 4.2-2 Ten Daily Schedule of Generating and Pumping at Tehri Reservoir

| PERIOD | PARAMETERS | 06-08 hrs | 08-10 hrs | 12-14 hrs | 14-22 hrs | 22-06 hrs | Net | % Irrigation Supply | |
|-------------|--|-----------|-----------|--------------------|-------------------|------------------|---------------------|---------------------|---------------------|
| | | 2 hrs | 2 hrs | 3 hrs | 4 hrs | 8 hrs | D/S release | Theoretical | Reservoir Op. Study |
| MAY (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 4 14.51 | | 8T 4 14.51 | 4P 2.7 -5.26 | 23.76 | 107.65 98.02 |
| MAY (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 4 14.17 | | 8T 4 14.17 | 4P 3.4 -6.74 | 21.6 | 97.87 95.01 |
| MAY (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 4 14.05 | | 8T 4 14.05 | 4P 2.5 -5.03 | 23.07 | 104.53 92.59 |
| JUN (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 4 13.71 | | 8T 4 13.71 | 4P 1.8 -3.83 | 23.59 | 147.59 99.26 |
| JUN (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 4 13.36 | | 8T 4 13.36 | 4P 1.1 -2.36 | 24.36 | 152.41 99.56 |
| JUN (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 4 13.36 | | 8T 4 13.36 | 4P 5.5 -11.79 | 14.93 | 93.41 98.99 |
| JUL (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 4 13.59 | | 8T 4 13.59 | 4P 5.9 12.32 | 39.5 | |
| JUL (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 4 14.17 | | 8T 4 14.17 | 4P 7.4 -14.52 | 13.82 | |
| JUL (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 2.6 10.38 | | 8T 4 15.67 | 4P 8 -13.82 | 12.23 | |
| AUG (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 1.2 5.16 | | 8T 4 17.28 | 4P 8 -11.29 | 11.15 | |
| AUG (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 0.5 1.96 | | 8T 4 17.39 | 4P 8 -9.33 | 10.02 | |
| AUG (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | | 8T 4 16.93 | 8T 1.1 4.76 | 8T 4 16.93 | | 38.62 | |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. Study % Irrigation Supply = Average of 35 years reservoir operation simulation study

Table 4.2-3 Ten Daily Schedule of Generating and Pumping at Tehri Reservoir

| PERIOD | PARAMETERS | 16-18 hrs | 18-22 hrs | 12-14 hrs | 18-22 hrs | 22-06 hrs | Net | % Irrigation Supply | |
|-------------|-----------------------------------|-----------|-----------|-----------|-----------|-----------|-------------|---------------------|---------------------|
| | | 2 hrs | 4 hrs | 6 hrs | 4 hrs | 8 hrs | D/S release | Theoretical | Reservoir Op. Study |
| SEP (1-10) | Units running | | | 8T | | 8T | | | |
| | Hrs of running | | | 4 | | 4 | | | |
| | Net inflow in D/S reservoir (MCM) | | | 16.62 | | 16.82 | | 33.44 | |
| SEP (11-20) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 3.8 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 15.92 | | 16.82 | -8.64 | 24.1 | |
| SEP (21-30) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 2.4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 10.05 | | 16.82 | -8.64 | 18.23 | |
| OCT (1-10) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 2.1 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 9.01 | | 16.82 | -8.64 | 17.19 | 302.43 |
| | | | | | | | | | 100.00 |
| OCT (11-20) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 2.2 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 9.16 | | 16.93 | -8.64 | 17.45 | 307.01 |
| | | | | | | | | | 100.00 |
| OCT (21-30) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 1 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 4.29 | | 17.05 | -8.64 | 12.7 | 223.44 |
| | | | | | | | | | 99.96 |
| NOV (1-10) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 0.6 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 2.65 | | 17.05 | -8.64 | 11.06 | 97.25 |
| | | | | | | | | | 91.64 |
| NOV (11-20) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 0.7 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 3.02 | | 17.05 | -8.75 | 11.32 | 99.53 |
| | | | | | | | | | 78.90 |
| NOV (21-30) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 0.8 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 3.3 | | 17.16 | -8.75 | 11.71 | 102.96 |
| | | | | | | | | | 78.66 |
| DEC (1-10) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 2.3 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 10.92 | | 17.16 | -8.99 | 19.09 | 127.05 |
| | | | | | | | | | 99.81 |
| DEC (11-20) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 2.7 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 11.73 | | 17.39 | -9.33 | 19.79 | 131.71 |
| | | | | | | | | | 99.84 |
| DEC (21-31) | Units running | | | 8T | | 8T | 4P | | |
| | Hrs of running | | | 2.02 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | | 9 | | 17.72 | -5.61 | 21.11 | 140.49 |
| | | | | | | | | | 99.59 |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. Study % Irrigation Supply = Average of 35 years reservoir operation simulation study

4.3 Proposed Operation Schedule

To achieve the objective of study i.e., to optimize the project operation schedule trial and error procedure is adopted. To develop and propose an optimized operation, we have done trial on two parameters of operation schedule, i.e.:

1. Combination of peaking and non-peaking hours in 24 hours in every ten daily basis period of operation schedule. These are called Stage I and II process.
2. Maximum water to be released or pumped (Net inflow) in each step combination of peaking and non-peaking hours, in every ten daily basis period of operation schedule. These are called Stage III and IV process.

4.3.1 Trial Combination of Peaking and Non-Peaking Hours

The combination of hours is denoted as below in the program:

DT(1) = first peak hour, there will be releases from A and also from B.

DT(2) = first non-peak hour, there will be no releases from A but there will be releases from B.

DT(3) = second peak hour, there will be releases from A and also from B.

DT(4) = second non-peak hour, there will be pumping to A and also releases from B.

DT(5) = break hour, there will be no releases or pumping but there may be releases from B.

In all above time combinations there is inflow to A and also release from B to meet the irrigation demands down stream of the project, to simplify the problem for the first trial we use the same combination of peaking and non-peaking hours in each time step of operation schedule.

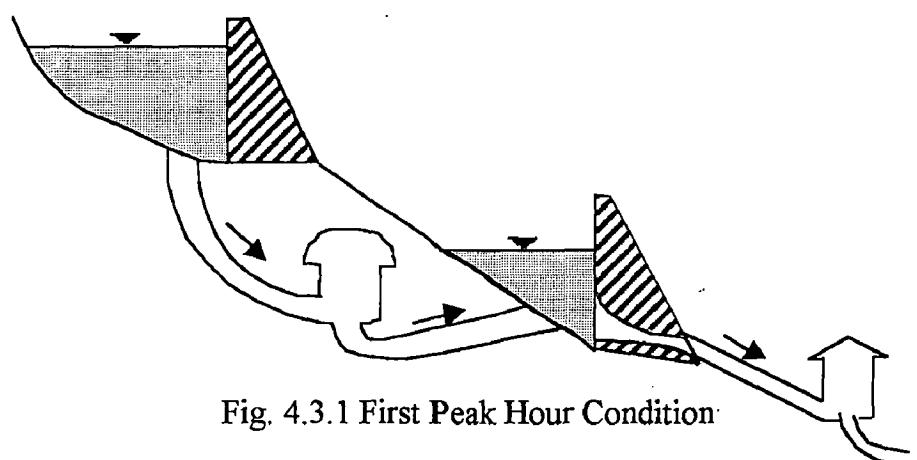


Fig. 4.3.1 First Peak Hour Condition

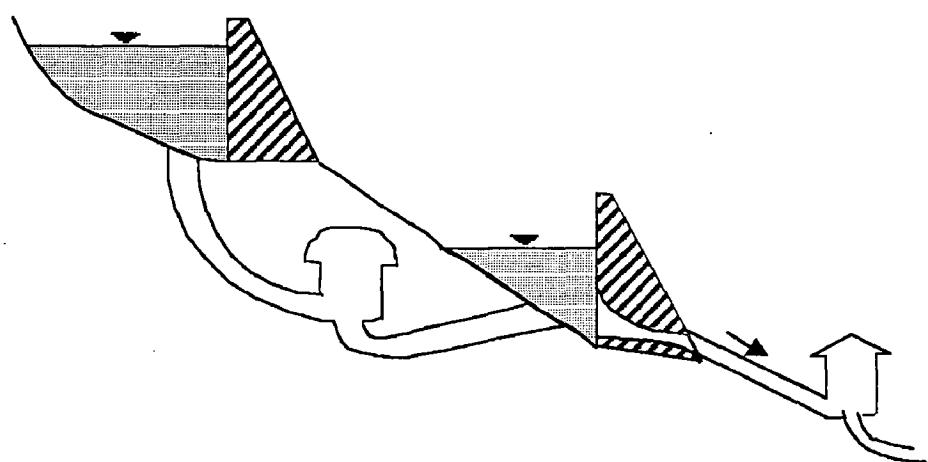


Fig 4.3.2 First Non-peak Hour Condition

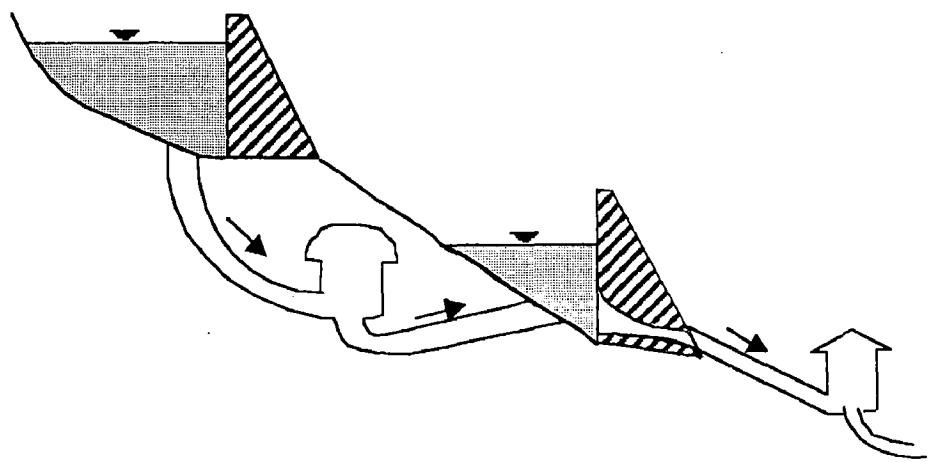


Fig.4.3.3 Second Peak Hour Condition

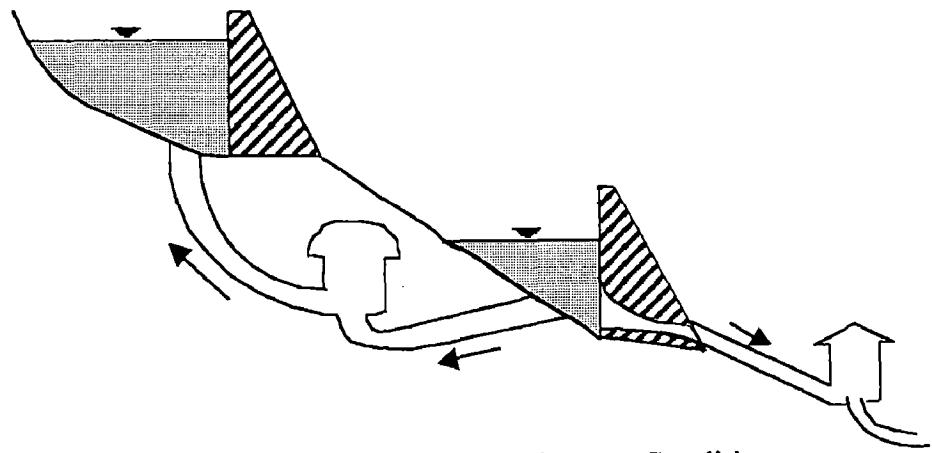


Fig. 4.3.4 Second Non-peak Hour Condition

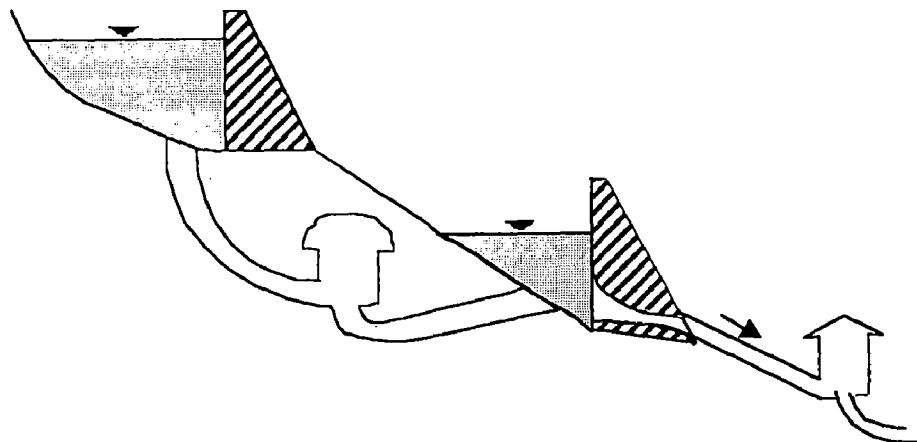


Fig. 4.3.5 Break Hour Condition

Stage I (using DROPS program); DROPS program is run with input of following combination of peaking and non-peaking hours. It is called “base duration time” combination; it is same as in project data.

- DT(1) = First peak hour from 08.00 to 12.00 (4 hours)
- DT(2) = First non peak hour from 12.00 to 18.00 (6 hours)
- DT(3) = Second peak hour from 18.00 to 22.00 (4 hours)
- DT(4) = Second non peak hour from 22.00 to 06.00 (8 hours)
- DT(5) = Break hour from 06.00 to 08.00 (2 hours)

In this case maximum value of water releasing and pumping has been allowed in all ten dailies. The results are given in table 4.3 and table 4.4. The results as compared to table 4.1 and table 4.2 show that energy generation has increased but irrigation requirements are not met during April, May and June.

TABLE 4.3 SUMMARY OF TOTAL RESERVOIR OPERATION

| YEAR | TOTAL OF INFLOW (M3) | IRRIG. DEMAND (M3) | IRRIG. SUPPLY (M3) | IRRIG. DEMAND STATUS | AV. ENERGY GENERATED (MWh) | SPILL AT B (M3) | HA MIN (M) | HB MIN (M) | TOT. EN. GENERATE (MWh) | SYSTEM (MWh) |
|------|-------------------------------|--------------------------|--------------------------|----------------------------|----------------------------------|-----------------------|------------------|------------------|-------------------------------|-----------------|
| 1963 | .9010E+09 | .9832E+09 | .9832E+09 | 100.00% | .148E+07 | .670E+09 | 809.28 | .600.97 | .165E+07 | |
| 1964 | .5643E+10 | .4606E+10 | .4259E+10 | 92.47% | .414E+07 | .169E+10 | 740.08 | .598.50 | .488E+07 | |
| 1965 | .7066E+10 | .4606E+10 | .4105E+10 | 89.13% | .438E+07 | .279E+10 | 740.06 | .598.50 | .509E+07 | |
| 1966 | .8281E+10 | .4606E+10 | .4316E+10 | 93.71% | .461E+07 | .378E+10 | 740.10 | .598.50 | .536E+07 | |
| 1967 | .6760E+10 | .4606E+10 | .4305E+10 | 93.48% | .454E+07 | .251E+10 | 740.11 | .598.50 | .529E+07 | |
| 1968 | .6859E+10 | .4606E+10 | .4228E+10 | 91.79% | .442E+07 | .253E+10 | 740.06 | .598.50 | .513E+07 | |
| 1969 | .7090E+10 | .4606E+10 | .4034E+10 | 87.59% | .443E+07 | .294E+10 | 740.06 | .598.50 | .532E+07 | |
| 1970 | .7501E+10 | .4606E+10 | .4294E+10 | 93.23% | .458E+07 | .323E+10 | 740.11 | .598.50 | .549E+07 | |
| 1971 | .7100E+10 | .4606E+10 | .4606E+10 | 100.00% | .469E+07 | .250E+10 | 743.65 | .600.97 | .549E+07 | |
| 1972 | .7346E+10 | .4606E+10 | .3991E+10 | 86.65% | .435E+07 | .327E+10 | 740.06 | .598.50 | .505E+07 | |
| 1973 | .7128E+10 | .4606E+10 | .4563E+10 | 99.07% | .469E+07 | .255E+10 | 740.14 | .598.50 | .549E+07 | |
| 1974 | .7481E+10 | .4606E+10 | .4341E+10 | 94.24% | .450E+07 | .289E+10 | 740.05 | .598.50 | .525E+07 | |
| 1975 | .6439E+10 | .4606E+10 | .3873E+10 | 84.10% | .432E+07 | .275E+10 | 740.04 | .598.50 | .499E+07 | |
| 1976 | .9728E+10 | .4606E+10 | .4606E+10 | 100.00% | .495E+07 | .491E+10 | 744.48 | .600.97 | .575E+07 | |
| 1977 | .1192E+11 | .4606E+10 | .4421E+10 | 95.99% | .499E+07 | .719E+10 | 740.11 | .598.50 | .576E+07 | |
| 1978 | .1099E+11 | .4606E+10 | .4374E+10 | 94.96% | .494E+07 | .689E+10 | 740.10 | .598.50 | .570E+07 | |
| 1979 | .8547E+10 | .4606E+10 | .4183E+10 | 90.81% | .461E+07 | .433E+10 | 740.07 | .598.50 | .534E+07 | |
| 1980 | .7977E+10 | .4606E+10 | .4490E+10 | 97.49% | .473E+07 | .357E+10 | 740.14 | .598.50 | .551E+07 | |
| 1981 | .6130E+10 | .4606E+10 | .4362E+10 | 94.71% | .401E+07 | .185E+10 | .740.09 | .598.50 | .477E+07 | |
| 1982 | .7302E+10 | .4606E+10 | .3940E+10 | 85.54% | .429E+07 | .309E+10 | 740.04 | .598.50 | .498E+07 | |
| 1983 | .5631E+10 | .4606E+10 | .3842E+10 | 83.42% | .401E+07 | .211E+10 | 740.04 | .598.50 | .468E+07 | |
| 1984 | .8785E+10 | .4606E+10 | .3905E+10 | 84.77% | .439E+07 | .440E+10 | 740.03 | .598.50 | .507E+07 | |
| 1985 | .8798E+10 | .4606E+10 | .4357E+10 | 94.61% | .471E+07 | .459E+10 | 740.11 | .598.50 | .547E+07 | |
| 1986 | .5945E+10 | .4606E+10 | .4558E+10 | 98.96% | .399E+07 | .164E+10 | 740.19 | .598.50 | .478E+07 | |
| 1987 | .8491E+10 | .4606E+10 | .3807E+10 | 82.65% | .429E+07 | .424E+10 | 740.04 | .598.50 | .495E+07 | |
| 1988 | .7139E+10 | .4606E+10 | .4549E+10 | 98.76% | .460E+07 | .265E+10 | 740.19 | .598.50 | .539E+07 | |
| 1989 | .7205E+10 | .4606E+10 | .4317E+10 | 93.73% | .457E+07 | .290E+10 | 740.08 | .598.50 | .532E+07 | |
| 1990 | .6484E+10 | .4606E+10 | .4056E+10 | 88.06% | .425E+07 | .239E+10 | 740.05 | .598.50 | .495E+07 | |
| 1991 | .8231E+10 | .4606E+10 | .4335E+10 | 94.12% | .451E+07 | .365E+10 | 740.09 | .598.50 | .526E+07 | |
| 1992 | .6705E+10 | .4606E+10 | .4124E+10 | 89.54% | .441E+07 | .253E+10 | 740.05 | .598.50 | .513E+07 | |
| 1993 | .9172E+10 | .4606E+10 | .4606E+10 | 100.00% | .487E+07 | .447E+10 | 740.22 | .600.97 | .567E+07 | |
| 1994 | .7031E+10 | .4606E+10 | .4374E+10 | 94.95% | .455E+07 | .278E+10 | 740.10 | .598.50 | .531E+07 | |
| 1995 | .7264E+10 | .4606E+10 | .4025E+10 | 87.38% | .434E+07 | .306E+10 | 740.05 | .598.50 | .504E+07 | |
| 1996 | .8222E+10 | .4606E+10 | .4606E+10 | 100.00% | .483E+07 | .355E+10 | 762.40 | .600.97 | .563E+07 | |
| 1997 | .9878E+10 | .4606E+10 | .4606E+10 | 100.00% | .501E+07 | .477E+10 | 743.97 | .601.11 | .581E+07 | |

AVERAGE ANNUAL = 93,033 - 452E+07 - 388E+10 527E+07

MIN. ELEVATION AT A = 740.03 M

MIN. ELEVATION AT A = 740.00 M
MIN. ELEVATION AT B = 598.50 M

10 DAYS % AVERAGE MEETING IRR. DEMAND

| MONTH | 1st | 2nd | 3rd |
|-----------|--------|--------|--------|
| JANUARY | 100.00 | 100.00 | 100.00 |
| FEBRUARY | 100.00 | 100.00 | 100.00 |
| MARCH | 100.00 | 100.00 | 97.26 |
| APRIL | 94.68 | 90.10 | 77.22 |
| MAY | 70.86 | 62.54 | 60.65 |
| JUNE | 97.37 | 98.53 | 98.53 |
| JULY | .00 | .00 | .00 |
| AUGUST | .00 | .00 | .00 |
| SEPTEMBER | .00 | .00 | .00 |
| OCTOBER | 100.00 | 100.00 | 100.00 |
| NOVEMBER | 100.00 | 100.00 | 100.00 |
| DECEMBER | 100.00 | 100.00 | 100.00 |

Table 4.4-1 Ten Daily Schedule of Generating and Pumping (Stage I)

| PERIOD | PARAMETERS | 06:08 hrs | 08:12 hrs | 12:18 hrs | 18:22 hrs | 20:06 hrs | Net D/S release | Theoretical % Irrigation Supply |
|-------------|-----------------------------------|-----------|-----------|-----------|-----------|-----------|-----------------|---------------------------------|
| | | hrs | hrs | hrs | hrs | hrs | D/S | % Irr. |
| JAN (1-10) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 87.42 |
| JAN (11-20) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 87.42 |
| JAN (21-31) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 87.42 |
| FEB (1-10) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 80.66 |
| FEB (11-20) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 80.66 |
| FEB (21-28) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 80.66 |
| MAR (1-10) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 94.01 |
| MAR (11-20) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 94.01 |
| MAR (21-31) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 94.01 |
| APR (1-10) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 98.86 |
| APR (11-20) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 98.86 |
| APR (21-30) | Units running | | 8T | | 8T | 4P | | |
| | Hrs of running | | 4 | | 4 | 8 | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -17.16 | 18.42 | 98.86 |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. study % of Irrigation Supply = Average of 35 years reservoir operation simulation study

Table 4.4-2 Ten Daily Schedule of Generating and Pumping (Stage I)

| PERIOD | PARAMETERS | 06-08 hrs 2 hrs | 08-12 hrs 4 hrs | 12-18 hrs 6 hrs | 18-22 hrs 4 hrs | 22-06 hrs 8 hrs | Net D/S Release | Theoretical % Irrigation Supply |
|-------------|--|--------------------|--------------------|--------------------|--------------------|--------------------|-----------------|---------------------------------|
| MAY (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 83.46 |
| MAY (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 83.46 |
| MAY (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 83.46 |
| JUN (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 115.25 |
| JUN (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 115.25 |
| JUN (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 115.25 |
| JUL (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| JUL (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| JUL (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| AUG (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| AUG (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| AUG (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | 2 | 8T 4 17.79 | 4P 0 0 | 48.87 | |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. study % of Irrigation Supply = Average of 35 years reservoir operation simulation study

Table 4.4-3 Ten Daily Schedule of Generating and Pumping (Stage I)

| PERIOD | PARAMETERS | 06-08 hrs 2 hrs | 08-12 hrs 4 hrs | 12-18 hrs 6 hrs | 18-22 hrs 4 hrs | 22-06 hrs 8 hrs | Net D/S release | Theoretical % Irrigation Supply |
|-------------|--|--------------------|--------------------|--------------------|--------------------|--------------------|-----------------|---------------------------------|
| SEP (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| SEP (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| SEP (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| OCT (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 324.07 |
| OCT (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 324.07 |
| OCT (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 324.07 |
| NOV (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 161.96 |
| NOV (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 161.96 |
| NOV (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 161.96 |
| DEC (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 122.59 |
| DEC (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 122.59 |
| DEC (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 122.59 |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. study % of Irrigation Supply = Average of 35 years reservoir operation simulation study

Stage II (using DROPSC program);

With this program, we carried out the study to determine the effect of irrigation supply on total energy generated. Irrigation supplies changing by changing the combination hours of duration time.

The combinations of hours have been generate by reducing and increasing the first peak hour duration (DT(1)) with 0.5 hour difference. We have explored this possibility of the variation seem in first peak hour period in project operation schedule. The second peak hour period is constant during in project operation schedule, the pumping period of 8 hours is kept constant in all combinations, so the change in first peak hour duration has caused corresponding change in break hour period i.e. DT(5). The results of these runs are given in table 4.5 and fig.4.4. The results of these runs have helped in generating a trade off curve between the percentage of meeting irrigation demand and the energy generated. It's shown in table 4.5.b and fig.4.4

4.3.2 Trial with Maximum Water to be Released or Pumped in Each Step

Combination of Peaking And Non-Peaking Hours

Stage III (using again DROPS program); DROPS program is run with only proposed combination of peaking and non-peaking hours and input of maximum possibility value in water releasing and pumping.

To increase the percentage of meeting irrigation demands trial runs are made by reducing the duration of first peak hour (DT(1)) in the period of 3rd ten daily of July to 2nd ten daily of August and from 3rd ten daily of September to the end of December. In this period the first peak hour on project operation schedule is less than 4 hour.

The basis of selecting proposed operation schedule, may depend on the following aspects:

- a. The irrigation supply is meeting irrigation demand 100%
- b. The maximum energy generation
- c. Theoretical % irrigation supply (Table 4.7), it should more and nearly 100%

From table 4.6 and table 4.7 the year operation that fulfils all above aspects is year of 1977. We take this year operation, as basis of the proposed operation schedule.

Next step is rounded the value of net inflow of year 1977 to 0.01 MCM and,

Stage IV (using DROPS program); DROPS program is run with proposed combination of peaking and non-peaking hours and proposed net inflow (after rounded the net inflow in operation of year 1977). The results of these runs are given in table 4.8 and table 4.9.

Table 4.5.a RESULT OF DROPSC: COMBINAT.OUT

| COMB | DT(1) | DT(2) | DT(3) | DT(4) | DT(5) | AVIRR | AVERAGE ANNUAL | |
|------|-------|-------|-------|-------|-------|--------|----------------|--------------|
| | | | | | | | EN.GEN | SYS.EN.GEN |
| 1 | 2.00 | 6.00 | 4.00 | 8.00 | 4.00 | 88.81% | .287E+07 | .358E+07 |
| 2 | 2.50 | 6.00 | 4.00 | 8.00 | 3.50 | 97.70% | .337E+07 | .416E+07 |
| 3 | 3.00 | 6.00 | 4.00 | 8.00 | 3.00 | 98.26% | .395E+07 | .473E+07 |
| 4 | 3.50 | 6.00 | 4.00 | 8.00 | 2.50 | 97.07% | .446E+07 | .523E+07 |
| 5 | 4.00 | 6.00 | 4.00 | 8.00 | 2.00 | 93.03% | .452E+07 | .527E+07 *** |
| 6 | 4.50 | 6.00 | 4.00 | 8.00 | 1.50 | 93.03% | .459E+07 | .533E+07 |
| 7 | 5.00 | 6.00 | 4.00 | 8.00 | 1.00 | 93.03% | .464E+07 | .538E+07 |
| 8 | 5.50 | 6.00 | 4.00 | 8.00 | .50 | 93.03% | .468E+07 | .542E+07 |
| 9 | 6.00 | 6.00 | 4.00 | 8.00 | .00 | 93.02% | .471E+07 | .546E+07 |

ENERGY MAX GENERATED= .546E+07 MWh

% MAX. IRR. SUPPLY = 98.26 %

Note: *** Combination of "Base Duration Time"

Table 4.5.b Input Data to Develop Curve of % Meeting Irrigation Demand vs Average Annual System Energy Generated

| COMBINATION | AV. % MEETING IRRIGATION DEMAND | AV. ANNUAL SYS. EN. GENERATED (x 10 ⁹ KWh) | REMARK |
|-------------|---------------------------------------|---|------------|
| 1 | 88.81% | 3.58 | Proj. Data |
| 2 | 97.70% | 4.16 | |
| | 97.10% | 4.32 | |
| 3 | 98.26% | 4.73 | |
| | 98.50% | 5.22 | |
| 4 | 97.07% | 5.23 | Propose |
| 5 | 93.03% | 5.27 | |
| 6 | 93.03% | 5.33 | |
| 7 | 93.03% | 5.38 | |
| 8 | 93.03% | 5.42 | |
| 9 | 93.02% | 5.46 | |

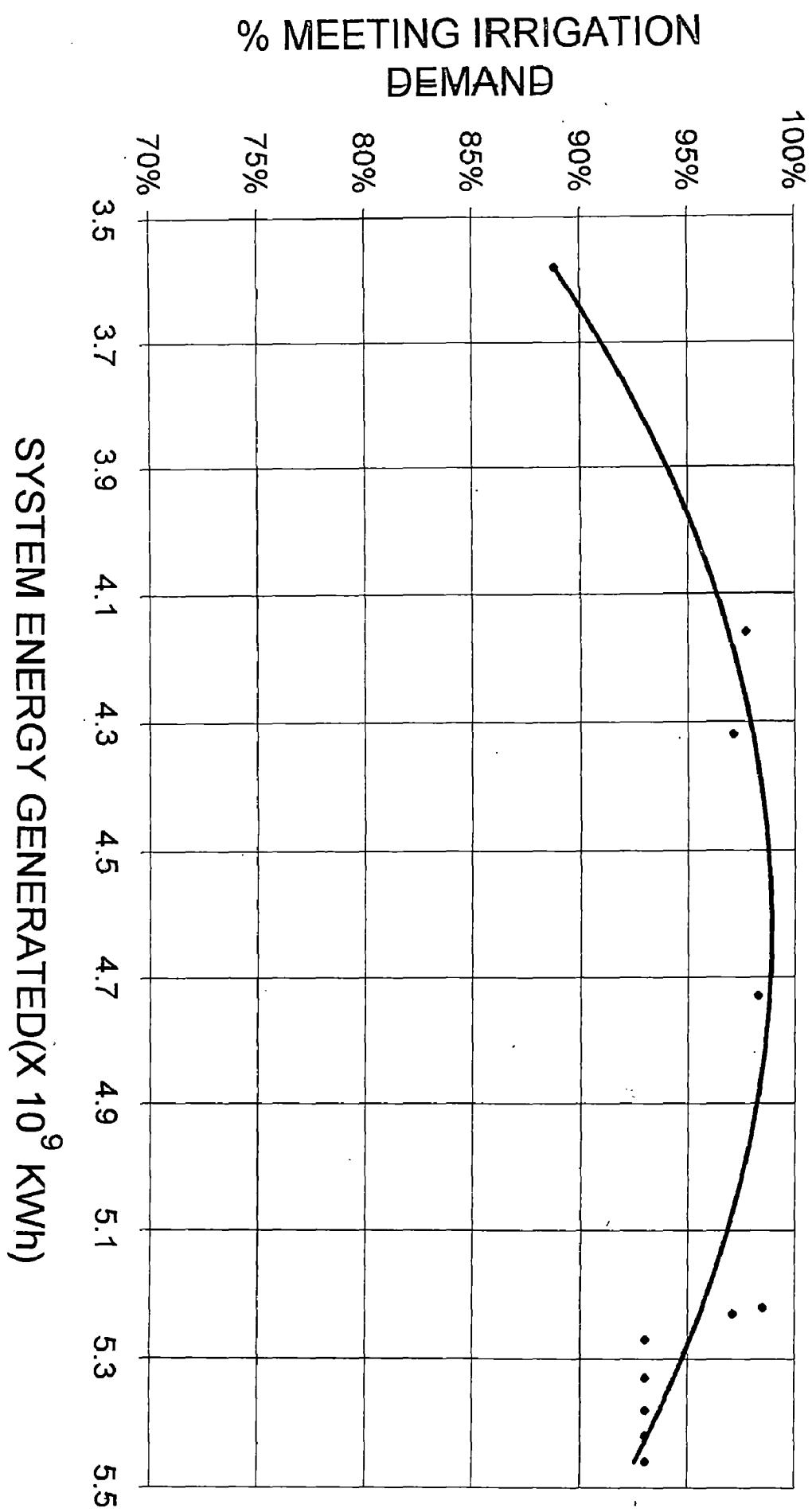


Fig.4.4 % MEETING IRRIGATION DEMAND - ANNUAL SYSTEM ENERGY GENERATED

TABLE 4.6 SUMMARY OF TOTAL RESERVOIR OPERATION

| YEAR OF | TOTAL INFLOW (M3) | IRRIG. DEMAND (M3) | IRRIG. SUPPLY (M3) | IRRIG. DEMAND STATUS | AV. ENERGY GENERATED (MWh) | SPILL AT B (M3) | HA MIN (M) | HB MIN EN. (M) | TOT. SYSTEM GENERATE (MWh) |
|------------------|-------------------------|--------------------------|--------------------------|----------------------------|----------------------------------|-----------------------|------------------|----------------------|----------------------------------|
| 1963 | .9010E+09 | .9832E+09 | .9832E+09 | 100.00% | .104E+07 | .255E+09 | 820.61 | 600.42 | .121E+07 |
| 1964 | .5643E+10 | .4606E+10 | .4606E+10 | 100.00% | .439E+07 | .156E+10 | 743.08 | 600.42 | .519E+07 |
| 1965 | .7066E+10 | .4606E+10 | .4292E+10 | 93.19% | .416E+07 | .232E+10 | 740.07 | 598.50 | .490E+07 |
| 1966 | .8281E+10 | .4606E+10 | .4605E+10 | 99.98% | .442E+07 | .347E+10 | 749.70 | 598.50 | .522E+07 |
| 1967 | .6760E+10 | .4606E+10 | .4606E+10 | 100.00% | .457E+07 | .219E+10 | 750.22 | 600.42 | .537E+07 |
| 1968 | .6859E+10 | .4606E+10 | .4606E+10 | 100.00% | .432E+07 | .215E+10 | 746.69 | 600.42 | .512E+07 |
| 1969 | .7090E+10 | .4606E+10 | .4534E+10 | 98.45% | .431E+07 | .245E+10 | 740.04 | 598.50 | .510E+07 |
| 1970 | .7501E+10 | .4606E+10 | .4606E+10 | 100.00% | .456E+07 | .295E+10 | 749.70 | 600.42 | .536E+07 |
| 1971 | .7100E+10 | .4606E+10 | .4606E+10 | 100.00% | .458E+07 | .249E+10 | 765.89 | 600.42 | .538E+07 |
| 1972 | .7346E+10 | .4606E+10 | .4453E+10 | 96.69% | .433E+07 | .284E+10 | 740.07 | 598.50 | .510E+07 |
| 1973 | .7128E+10 | .4606E+10 | .4606E+10 | 100.00% | .458E+07 | .248E+10 | 759.13 | 600.42 | .538E+07 |
| 1974 | .7481E+10 | .4606E+10 | .4599E+10 | 99.85% | .422E+07 | .277E+10 | 750.76 | 598.50 | .502E+07 |
| 1975 | .6439E+10 | .4606E+10 | .4184E+10 | 90.83% | .418E+07 | .231E+10 | 740.05 | 598.50 | .491E+07 |
| 1976 | .9728E+10 | .4606E+10 | .4606E+10 | 100.00% | .455E+07 | .497E+10 | 765.52 | 600.42 | .535E+07 |
| 1977 | .1192E+11 | .4606E+10 | .4606E+10 | 100.00% | .475E+07 | .719E+10 | 750.08 | 600.97 | .555E+07 |
| 1978 | .1099E+11 | .4606E+10 | .4563E+10 | 99.06% | .460E+07 | .661E+10 | 740.10 | 598.50 | .539E+07 |
| 1979 | .8547E+10 | .4606E+10 | .4462E+10 | 96.87% | .436E+07 | .404E+10 | 740.12 | 598.50 | .514E+07 |
| 1980 | .7977E+10 | .4606E+10 | .4606E+10 | 100.00% | .439E+07 | .328E+10 | 748.97 | 600.42 | .519E+07 |
| 1981 | .6130E+10 | .4606E+10 | .4606E+10 | 100.00% | .416E+07 | .155E+10 | 751.37 | 600.42 | .496E+07 |
| 1982 | .7302E+10 | .4606E+10 | .4452E+10 | 96.65% | .415E+07 | .270E+10 | 740.12 | 598.50 | .492E+07 |
| 1983 | .5631E+10 | .4606E+10 | .4239E+10 | 92.03% | .410E+07 | .160E+10 | 740.08 | 598.50 | .484E+07 |
| 1984 | .8785E+10 | .4606E+10 | .4414E+10 | 95.83% | .419E+07 | .409E+10 | 740.15 | 598.50 | .496E+07 |
| 1985 | .8798E+10 | .4606E+10 | .4606E+10 | 100.00% | .454E+07 | .420E+10 | 742.74 | 600.42 | .534E+07 |
| 1986 | .5945E+10 | .4606E+10 | .4606E+10 | 100.00% | .419E+07 | .149E+10 | 760.17 | 600.42 | .499E+07 |
| 1987 | .8491E+10 | .4606E+10 | .4346E+10 | 94.37% | .428E+07 | .385E+10 | 740.11 | 598.50 | .503E+07 |
| 1988 | .7139E+10 | .4606E+10 | .4606E+10 | 100.00% | .445E+07 | .254E+10 | 756.58 | 600.42 | .525E+07 |
| 1989 | .7205E+10 | .4606E+10 | .4606E+10 | 100.00% | .455E+07 | .254E+10 | 747.29 | 600.42 | .535E+07 |
| 1990 | .6484E+10 | .4606E+10 | .4556E+10 | 98.93% | .421E+07 | .183E+10 | 740.10 | 598.50 | .500E+07 |
| 1991 | .8231E+10 | .4606E+10 | .4606E+10 | 100.00% | .438E+07 | .355E+10 | 754.77 | 600.42 | .518E+07 |
| 1992 | .6705E+10 | .4606E+10 | .4516E+10 | 98.05% | .421E+07 | .217E+10 | 740.08 | 598.50 | .499E+07 |
| 1993 | .9172E+10 | .4606E+10 | .4606E+10 | 100.00% | .444E+07 | .446E+10 | 758.76 | 600.42 | .524E+07 |
| 1994 | .7031E+10 | .4606E+10 | .4606E+10 | 100.00% | .434E+07 | .245E+10 | 746.93 | 600.42 | .514E+07 |
| 1995 | .7264E+10 | .4606E+10 | .4487E+10 | 97.41% | .417E+07 | .263E+10 | 740.07 | 598.50 | .495E+07 |
| 1996 | .8222E+10 | .4606E+10 | .4606E+10 | 100.00% | .446E+07 | .355E+10 | 779.04 | 598.56 | .526E+07 |
| 1997 | .9878E+10 | .4606E+10 | .4606E+10 | 100.00% | .460E+07 | .508E+10 | 764.46 | 599.44 | .540E+07 |
| AVERAGE ANNUAL = | | | | 98.52% | .437E+07 | .311E+10 | | | .516E+07 |

MIN.ELEVATION AT A = 740.04 M
 MIN.ELEVATION AT B = 598.50 M

| 10 DAYS % AVERAGE MEETING IRR. DEMAND | | | |
|---------------------------------------|--------|--------|--------|
| MONTH | 1st | 2nd | 3rd |
| JANUARY | 100.00 | 100.00 | 100.00 |
| FEBRUARY | 100.00 | 100.00 | 100.00 |
| MARCH | 100.00 | 100.00 | 100.00 |
| APRIL | 100.00 | 100.00 | 100.00 |
| MAY | 97.70 | 91.28 | 83.96 |
| JUNE | 97.82 | 98.53 | 98.53 |
| JULY | .00 | .00 | .00 |
| AUGUST | .00 | .00 | .00 |
| SEPTEMBER | .00 | .00 | .00 |
| OCTOBER | 100.00 | 100.00 | 100.00 |
| NOVEMBER | 99.96 | 100.00 | 100.00 |
| DECEMBER | 100.00 | 100.00 | 100.00 |

Table 4.7-1 Ten Daily Schedule of Generating and Pumping (Stage III)

| PERIOD | PARAMETERS | 06-08 hrs | 08-12 hrs | 12-18 hrs | 18-22 hrs | 22-06 hrs | Net D/S release | Theoretical % Irrigation Supply |
|----------------|---|-----------|------------------|-----------|------------------|-------------------|--------------------|---------------------------------|
| | | 2 hrs | 4 hrs | 6 hrs | 4 hrs | 8 hrs | | |
| JAN (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 87.42 |
| JAN (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 87.42 |
| JAN (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 87.42 |
| FEB (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 80.66 |
| FEB (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 80.66 |
| FEB (21-28) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 80.66 |
| MAR (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 94.01 |
| MAR (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 94.01 |
| MAR (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 94.01 |
| APR (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 98.86 |
| APR (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 98.86 |
| APR (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 98.86 |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. Study % Irrigation Supply = Average of 35 years reservoir operation simulation study

Table 4.7-2 Ten Daily Schedule of Generating and Pumping (Stage III)

| PERIOD | PARAMETERS | 06-08 hrs | 08-12 hrs | 12-18 hrs | 18-22 hrs | 22-06 hrs | Net D/S release | Theoretical % Irr. Supply |
|-------------|--|-----------|------------------|------------------|------------------|-------------------|-----------------|---------------------------|
| | | 2 hrs | 4 hrs | 6 hrs | 4 hrs | 8 hrs | | |
| MAY (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 83.46 |
| MAY (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 83.46 |
| MAY (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 83.46 |
| JUN (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 115.25 |
| JUN (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 115.25 |
| JUN (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 115.25 |
| JUL (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| JUL (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| JUL (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| AUG (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| AUG (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| AUG (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | 8T 6 13.29 | 8T 4 17.79 | 4P 0 0 | 48.87 | |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. Study % Irrigation Supply = Average of 35 years reservoir operation simulation study

Table 4.7-3 Ten Daily Schedule of Generating and Pumping (Stage III)

| PERIOD | PARAMETERS | 06:08 hrs 2 hrs | 08:12 hrs 4 hrs | 12:18 hrs 6 hrs | 18:22 hrs 4 hrs | 22:06 hrs 8 hrs | Net D/S release | Theoretical % Irrigation Supply |
|-------------|--|--------------------|--------------------|--------------------|--------------------|--------------------|-----------------|---------------------------------|
| SEP (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| SEP (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| SEP (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | |
| OCT (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 324.07 |
| OCT (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 324.07 |
| OCT (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 324.07 |
| NOV (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 161.96 |
| NOV (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 161.96 |
| NOV (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 161.96 |
| DEC (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 122.59 |
| DEC (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 122.59 |
| DEC (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | 122.59 |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. Study % Irrigation Supply = Average of 35 years reservoir operation simulation study

TABLE 4.8 SUMMARY OF TOTAL RESERVOIR OPERATION

| YEAR OF | TOTAL INFLOW (M3) | IRRIG. DEMAND (M3) | IRRIG. SUPPLY (M3) | IRRIG. STATUS | AV. ENERGY DEMAND GENERATED (MWh) | SPILL AT B (M3) | HA MIN (M) | HB MIN (M) | TOT. EN. GENERATE (MWh) | SYSTEM |
|------------------|-------------------------|--------------------------|--------------------------|------------------|--|-----------------------|------------------|------------------|----------------------------|--------|
| 1963 | .9010E+09 | .9832E+09 | .9832E+09 | 100.00% | .117E+07 | .255E+09 | 820.49 | 603.16 | .134E+07 | |
| 1964 | .5643E+10 | .4606E+10 | .4606E+10 | 100.00% | .437E+07 | .157E+10 | 742.93 | 601.11 | .517E+07 | |
| 1965 | .7066E+10 | .4606E+10 | .4290E+10 | 93.13% | .414E+07 | .232E+10 | 740.07 | 598.50 | .488E+07 | |
| 1966 | .8281E+10 | .4606E+10 | .4606E+10 | 100.00% | .455E+07 | .347E+10 | 749.55 | 601.11 | .535E+07 | |
| 1967 | .6760E+10 | .4606E+10 | .4606E+10 | 100.00% | .455E+07 | .219E+10 | 750.04 | 601.11 | .535E+07 | |
| 1968 | .6859E+10 | .4606E+10 | .4606E+10 | 100.00% | .445E+07 | .215E+10 | 746.53 | 601.11 | .525E+07 | |
| 1969 | .7090E+10 | .4606E+10 | .4532E+10 | 98.39% | .443E+07 | .245E+10 | 740.08 | 598.50 | .522E+07 | |
| 1970 | .7501E+10 | .4606E+10 | .4606E+10 | 100.00% | .455E+07 | .295E+10 | 749.54 | 601.11 | .535E+07 | |
| 1971 | .7100E+10 | .4606E+10 | .4606E+10 | 100.00% | .457E+07 | .249E+10 | 765.77 | 601.11 | .537E+07 | |
| 1972 | .7346E+10 | .4606E+10 | .4451E+10 | 96.63% | .431E+07 | .284E+10 | 740.07 | 598.50 | .508E+07 | |
| 1973 | .7128E+10 | .4606E+10 | .4606E+10 | 100.00% | .457E+07 | .248E+10 | 759.00 | 601.11 | .537E+07 | |
| 1974 | .7481E+10 | .4606E+10 | .4599E+10 | 99.85% | .435E+07 | .277E+10 | 750.63 | 598.50 | .515E+07 | |
| 1975 | .6439E+10 | .4606E+10 | .4181E+10 | 90.77% | .417E+07 | .231E+10 | 740.05 | 598.50 | .490E+07 | |
| 1976 | .9728E+10 | .4606E+10 | .4606E+10 | 100.00% | .467E+07 | .497E+10 | 765.40 | 601.11 | .547E+07 | |
| 1977 | .1192E+11 | .4606E+10 | .4606E+10 | 100.00% | .473E+07 | .719E+10 | 749.94 | 601.51 | .553E+07 | |
| 1978 | .1099E+11 | .4606E+10 | .4558E+10 | 98.96% | .457E+07 | .661E+10 | 740.10 | 598.50 | .537E+07 | |
| 1979 | .8547E+10 | .4606E+10 | .4462E+10 | 96.87% | .435E+07 | .404E+10 | 740.12 | 598.50 | .512E+07 | |
| 1980 | .7977E+10 | .4606E+10 | .4606E+10 | 100.00% | .451E+07 | .328E+10 | 748.81 | 601.11 | .531E+07 | |
| 1981 | .6130E+10 | .4606E+10 | .4606E+10 | 100.00% | .428E+07 | .155E+10 | 751.24 | 601.11 | .508E+07 | |
| 1982 | .7302E+10 | .4606E+10 | .4449E+10 | 96.60% | .428E+07 | .270E+10 | 740.02 | 598.50 | .505E+07 | |
| 1983 | .5631E+10 | .4606E+10 | .4236E+10 | 91.97% | .409E+07 | .160E+10 | 740.08 | 598.50 | .483E+07 | |
| 1984 | .8785E+10 | .4606E+10 | .4414E+10 | 95.84% | .431E+07 | .409E+10 | 740.15 | 598.50 | .508E+07 | |
| 1985 | .8798E+10 | .4606E+10 | .4606E+10 | 100.00% | .453E+07 | .420E+10 | 742.58 | 601.11 | .533E+07 | |
| 1986 | .5945E+10 | .4606E+10 | .4606E+10 | 100.00% | .418E+07 | .150E+10 | 760.05 | 601.11 | .498E+07 | |
| 1987 | .8491E+10 | .4606E+10 | .4344E+10 | 94.31% | .426E+07 | .385E+10 | 740.11 | 598.50 | .502E+07 | |
| 1988 | .7139E+10 | .4606E+10 | .4606E+10 | 100.00% | .443E+07 | .254E+10 | 756.45 | 601.11 | .523E+07 | |
| 1989 | .7205E+10 | .4606E+10 | .4606E+10 | 100.00% | .454E+07 | .254E+10 | 747.13 | 601.11 | .534E+07 | |
| 1990 | .6484E+10 | .4606E+10 | .4554E+10 | 98.87% | .434E+07 | .183E+10 | 740.10 | 598.50 | .513E+07 | |
| 1991 | .8231E+10 | .4606E+10 | .4606E+10 | 100.00% | .451E+07 | .355E+10 | 754.64 | 601.11 | .531E+07 | |
| 1992 | .6705E+10 | .4606E+10 | .4514E+10 | 98.00% | .433E+07 | .217E+10 | 740.08 | 598.50 | .511E+07 | |
| 1993 | .9172E+10 | .4606E+10 | .4606E+10 | 100.00% | .457E+07 | .446E+10 | 758.63 | 601.11 | .537E+07 | |
| 1994 | .7031E+10 | .4606E+10 | .4606E+10 | 100.00% | .447E+07 | .245E+10 | 746.77 | 601.11 | .527E+07 | |
| 1995 | .7264E+10 | .4606E+10 | .4484E+10 | 97.35% | .430E+07 | .263E+10 | 740.02 | 598.50 | .508E+07 | |
| 1996 | .8222E+10 | .4606E+10 | .4606E+10 | 100.00% | .456E+07 | .355E+10 | 778.94 | 601.11 | .536E+07 | |
| 1997 | .9878E+10 | .4606E+10 | .4606E+10 | 100.00% | .472E+07 | .508E+10 | 764.34 | 601.11 | .552E+07 | |
| AVERAGE ANNUAL = | | | | 98.50% | .443E+07 | .311E+10 | | | .522E+07 | |

MIN. ELEVATION AT A = 740.02 M
 MIN. ELEVATION AT B = 598.50 M

| 10 DAYS % AVERAGE MEETING IRR. DEMAND | | | |
|---------------------------------------|--------|--------|--------|
| MONTH | 1st | 2nd | 3rd |
| JANUARY | 100.00 | 100.00 | 100.00 |
| FEBRUARY | 100.00 | 100.00 | 100.00 |
| MARCH | 100.00 | 100.00 | 100.00 |
| APRIL | 100.00 | 100.00 | 100.00 |
| MAY | 97.64 | 91.21 | 83.70 |
| JUNE | 97.82 | 98.53 | 98.53 |
| JULY | .00 | .00 | .00 |
| AUGUST | .00 | .00 | .00 |
| SEPTEMBER | .00 | .00 | .00 |
| OCTOBER | 100.00 | 100.00 | 100.00 |
| NOVEMBER | 100.00 | 100.00 | 100.00 |
| DECEMBER | 100.00 | 100.00 | 100.00 |

Table 4.9-1 Proposed of Ten Daily Schedule of Generating and Pumping at Tehri Reservoir

| PERIOD | PARAMETERS | 06-08 hrs | 08-12 hrs | 12-15 hrs | 18-22 hrs | 22-26 hrs | Net D/S Release | % Irrigation Supply | |
|-------------|-----------------------------------|-----------|-----------|-----------|-----------|-----------|-----------------|---------------------|---------------------|
| | | 2 hrs | 4 hrs | 6 hrs | 4 hrs | 6 hrs | | Theoretical | Reservoir Op. Study |
| JAN (1-10) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 3 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 13.34 | | 13.34 | -5.61 | 21.07 | 100.00 | 100.00 |
| JAN (11-20) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 17.79 | -14.51 | 21.07 | 100.00 | 100.00 |
| JAN (21-31) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 14.34 | -11.06 | 21.07 | 100.00 | 100.00 |
| FEB (1-10) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 14.49 | -9.44 | 22.84 | 100.02 | 100.00 |
| FEB (11-20) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 14.49 | -9.44 | 22.84 | 100.02 | 100.00 |
| FEB (21-28) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 14.49 | -9.44 | 22.84 | 100.02 | 100.00 |
| MAR (1-10) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 14.21 | -12.4 | 19.6 | 100.03 | 100.00 |
| MAR (11-20) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 14.21 | -12.4 | 19.6 | 100.03 | 100.00 |
| MAR (21-31) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 14.21 | -12.4 | 19.6 | 100.03 | 100.00 |
| APR (1-10) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 14.13 | -13.27 | 18.65 | 100.09 | 100.00 |
| APR (11-20) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 14.13 | -13.27 | 18.65 | 100.09 | 100.00 |
| APR (21-30) | Units running | | 8T | | 8T | 4P | | | |
| | Hrs of running | | 4 | | 4 | 8 | | | |
| | Net inflow in D/S reservoir (MCM) | | 17.79 | | 14.13 | -13.27 | 18.65 | 100.09 | 100.00 |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. Study % Irrigation Supply = Average of 35 years reservoir operation simulation study

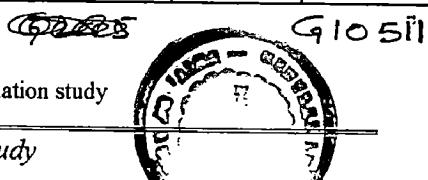


Table 4.9-2 Proposed of Ten Daily Schedule of Generating and Pumping at Tehri Reservoir

| PERIOD | PARAMETERS | 06-08 hrs | 08-12 hrs | 12-18 hrs | 18-22 hrs | 22-06 hrs | Net D/S release | % Irrigation Supply | |
|-------------|--|-----------|------------------|------------|------------------|-------------------|-----------------|---------------------|---------------------|
| | | 2 hrs | 4 hrs | 6 hrs | 4 hrs | 6 hrs | | Theoretical | Reservoir Op. Study |
| MAY (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 14.41 | 4P 8 -10.12 | 22.08 | 100.04 | 97.64 |
| MAY (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 14.41 | 4P 8 -10.12 | 22.08 | 100.04 | 91.21 |
| MAY (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 14.41 | 4P 8 -10.12 | 22.08 | 100.04 | 83.70 |
| JUN (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 12.28 | 4P 8 -14.08 | 15.99 | 100.04 | 97.82 |
| JUN (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 12.27 | 4P 8 -14.07 | 15.99 | 100.04 | 98.53 |
| JUN (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 12.26 | 4P 8 -14.06 | 15.99 | 100.04 | 98.53 |
| JUL (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | | |
| JUL (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | | |
| JUL (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -17.16 | 9.52 | | |
| AUG (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -17.16 | 9.52 | | |
| AUG (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -17.16 | 9.52 | | |
| AUG (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | 2 13.29 | 8T 4 17.79 | 4P 0 0 | 48.87 | | |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. Study % Irrigation Supply = Average of 35 years reservoir operation simulation study

Table 4.9-3 Proposed of Ten Daily Schedule of Generating and Pumping at Tehri Reservoir

| PERIOD | PARAMETERS | 06-08 hrs | 08-12 hrs | 12-18 hrs | 18-22 hrs | 22-06 hrs | Net D/S release | % Irrigation Supply | |
|-------------|--|-----------|------------------|-----------|------------------|-------------------|-----------------|---------------------|---------------------|
| | | 2 hrs | 4 hrs | 6 hrs | 4 hrs | 8 hrs | D/S release | Theoretical | Reservoir Op. Study |
| SEP (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | | |
| SEP (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 4 17.79 | | 8T 4 17.79 | 4P 8 -17.16 | 18.42 | | |
| SEP (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -17.16 | 9.52 | | |
| OCT (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -17.16 | 9.52 | 167.49 | 100.00 |
| OCT (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -17.16 | 9.52 | 167.49 | 100.00 |
| OCT (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -17.16 | 9.52 | 167.49 | 100.00 |
| NOV (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -15.3 | 11.38 | 100.06 | 100.00 |
| NOV (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -15.3 | 11.38 | 100.06 | 100.00 |
| NOV (21-30) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -15.3 | 11.38 | 100.06 | 100.00 |
| DEC (1-10) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -11.65 | 15.03 | 100.03 | 100.00 |
| DEC (11-20) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -11.65 | 15.03 | 100.03 | 100.00 |
| DEC (21-31) | Units running Hrs of running Net inflow in D/S reservoir (MCM) | | 8T 3 13.34 | | 8T 4 13.34 | 4P 8 -11.65 | 15.03 | 100.03 | 100.00 |

Note:

* Theoretical % Irrigation Supply = Net D/S release : Irrigation Demand in that period

** Reservoir Op. Study % Irrigation Supply = Average of 35 years reservoir operation simulation study

Chapter 5

DISCUSSION OF RESULTS

5.1 Project Data (Output of DROPS program)

$$1. \text{ Efficiency of reversible pump turbine} = \frac{\text{Capacity pumping mode}}{\text{Capacity generating mode}} =$$

$$\frac{148.99 \text{ M}^3/\text{sec}}{154.43 \text{ M}^3/\text{sec}} = 96.5\% \text{ or ratio of turbine maximum discharge to pump}$$

$$\text{maximum discharge} = \frac{Q_{T \max}}{Q_{P \max}} = \frac{154.43 \text{ M}^3/\text{sec}}{148.99 \text{ M}^3/\text{sec}} = 1.04, \text{ from reference 14,}$$

page 828; and if *ratio of turbine maximum head to pump maximum head* is

$$1.0, \text{ it means } \alpha = 1.3, \text{ where } \alpha = \frac{\text{Motor Capacity (KW)}}{\text{Generator Capacity (KVA)}}, \text{ so, motor}$$

capacity (KW) is substantially more than generator capacity (KVA)

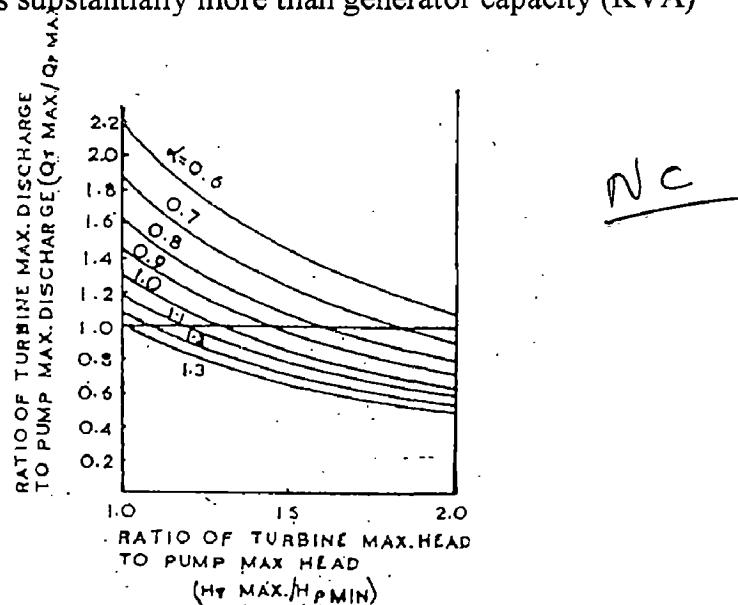


Fig. 5.1 Relation of generator-motor capacity vs pump turbine performance

2. The average percentage of meeting irrigation demands with the project data obtained by simulating 35 years inflows runs is 97.10% and Annual energy generated of the system in 35 years is 4.32×10^9 KWh. The minimum average percentage irrigation demands occurs in the month of November

(Table 4.1 and Table 4.2). The percentage irrigation demands are met 100 % in the year i.e. 1977

5.2 Proposed Operation Schedule

Stage I Project Data of Construction, Base Duration Time and Maximum Possible Value of Water Release or Pumping. (Output DROPS program)

The average percentage of meeting irrigation demands with this data for all 35 years data is 93.03% and Annual energy generated of the system in 35 years is 5.27×10^9 KWh. The minimum average percentage irrigation demands occurs in the month of May (Table 4.3 and Table 4.4). This operation schedule yields more energy generation but lesser percentage of meeting irrigation demands as compared to project operation schedule.

Stage II Project Data of Construction, Changing Duration Time and Maximum Possible Value of Water Release or Pumping (Output DROPSC program)

On reducing first peak hour DT(1) from "base duration time of 4 hours", the percentage of meeting irrigation demands has increased but energy generated reduce, when first peak period is reduced to 2 hours, the percentage of meeting irrigation demands decreased along with the decrease in energy generation.

Similarly when the peak hour DT(1) is increased, the percentage of meeting irrigation demands remained practically constant but energy generation increased

From these results of stage II and the project operation schedule, attempt was made to increase the percentage of meeting irrigation demands. Model runs have shown that by reducing the duration of first peak hour (DT(1)) in 3rd ten daily of July to 2nd ten daily of August and from 3rd ten daily of September to the end of December, to 3 hour. Maximum percentage of meeting irrigation demands of 98.26% could be achieved. (Table 4.5 and Fig.4.4).

Stage III Project Data of Construction, Proposed Duration Time and Maximum Possible Value of Water Release or Pumping. (Output DROPS program)

The average percentage of meeting irrigation demands with this data for all 35 years data is 98.52% and Annual energy generated of the system in 35 years is 5.16×10^9 KWh. The minimum average percentage irrigation demands occurs in the month of May (Table 4.6 and Table 4.7). This operation schedule yields more energy generation and more percentage of meeting irrigation demands as compared to project operation schedule.

The result of year where the irrigation demands is 100% and maximum energy generated is year of 1977.

To obtain proposed net inflow in optimized operation schedule we take this year 1977 operation, as basic of the proposed operation schedule of net inflow and rounded it to 0.01 MCM.

Stage IV Project Data of Construction, Proposed Duration Time and Proposed Net Inflow (after rounded the value to 0.01 MCM). (Output DROPS program)

The average percentage of meeting irrigation demands with this data for all 35 years data is 98.50% and Annual energy generated of the system in 35 years is 5.22×10^9 KWh. The minimum average percentage irrigation demands occurs in the month of May (Table 4.8 and Table 4.9). This operation schedule yields more energy generation and more percentage of meeting irrigation demands as compared to project operation schedule, but less in percentage of meeting irrigation demand than result in Stage III.

Comparison between Project and Proposed Schedule Operation

1. From the curve between Annual Average Energy Generated vs. Years, shown in Fig. 5.2 it can be seen that in each year the Annual Average Energy Generated through proposed operation schedule is more than the Annual Average Energy Generated by project operation schedule.
2. From the curve between Annual Volume of Water Spill from B vs. Year, shown in Fig. 5.2 it can be seen that each year the Annual Volume of Water

Spill from B in proposed operation schedule is slightly less than the Annual Volume of Water Spill from B in project operation schedule.

3. From Fig. 5.3 the difference in generating and pumping duration hours is in first peak hour and second non-peak hour (pumping hour) i.e.:

- In months of March to July duration of first peak hour is same, but pumping hours of the project schedule are less duration than proposed schedule in this period.
- And in months of August to February duration of second non-peak hour (pumping hour) is same, but first peak hours of the project schedule are less than these proposed schedule in this period.

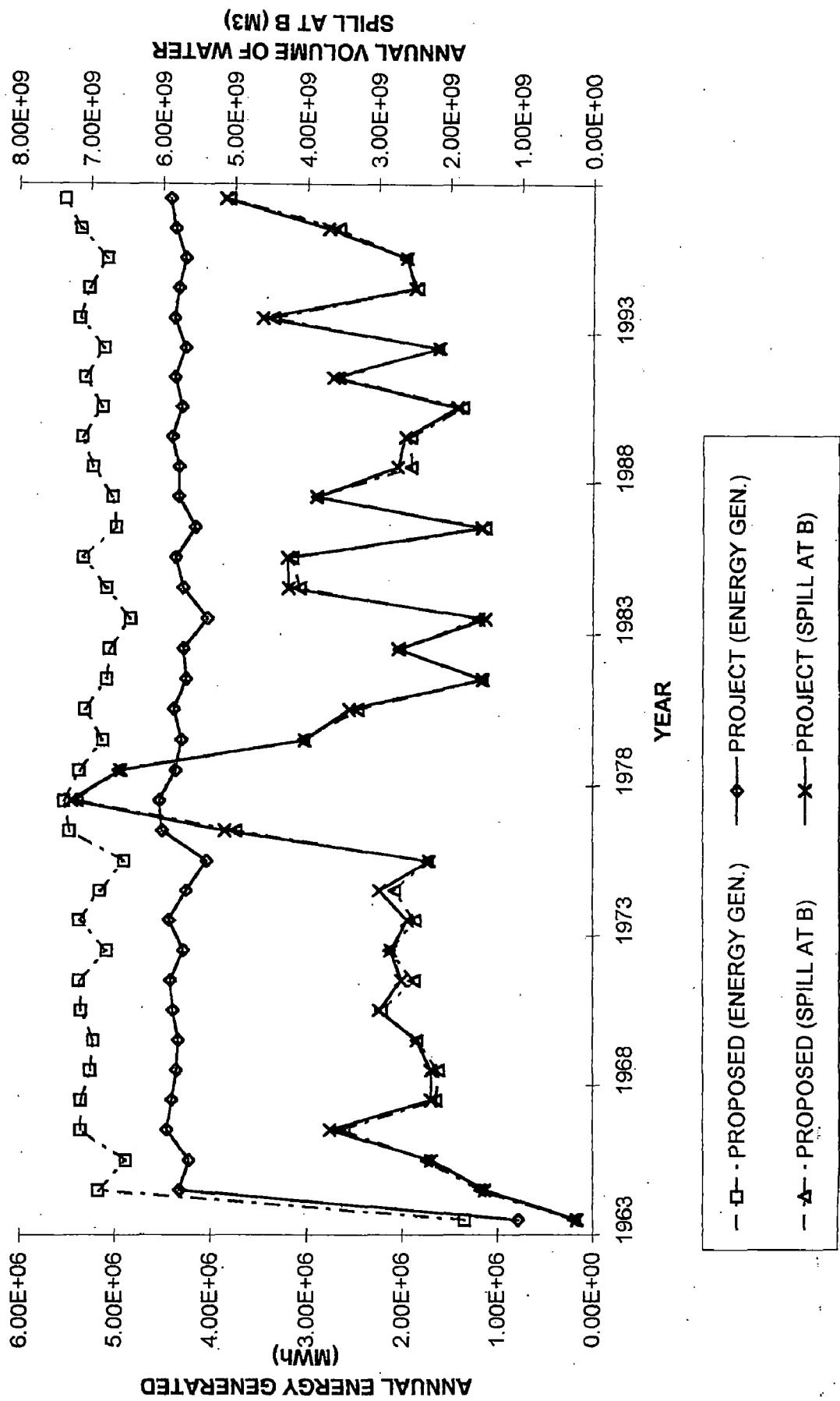
4. From Fig. 5.3 the differences of volume of water released and pumped are as below:

- In first peak hour it can be seen that in whole year volume of water released in proposed operation schedule is more than project operation schedule.
- In second peak hour, from September to April the volume of water released in proposed operation schedule is less than project operation schedule and the other months the trend is reversed.
- In second non-peak hour (pumping hour), almost in the whole year the volume of water pumped in proposed operation schedule is more than project operation schedule.

5. From tables 5.1 and 5.2, 70% dependable annual energy generated is as below:

- Project operation schedule: $4.28 \times 10^9 \text{ KWh}$
- Proposed operation schedule: $5.08 \times 10^9 \text{ KWh}$
- Difference: $0.8 \times 10^9 \text{ KWh}$ or 18.69%

**Fig. 5.2 Comparison of Project & Proposed Schedule Operation
(In Yearly Basis)**



**Fig. 5.3 Comparison of Project & Proposed Schedule Operation
(In Monthly Basis)**

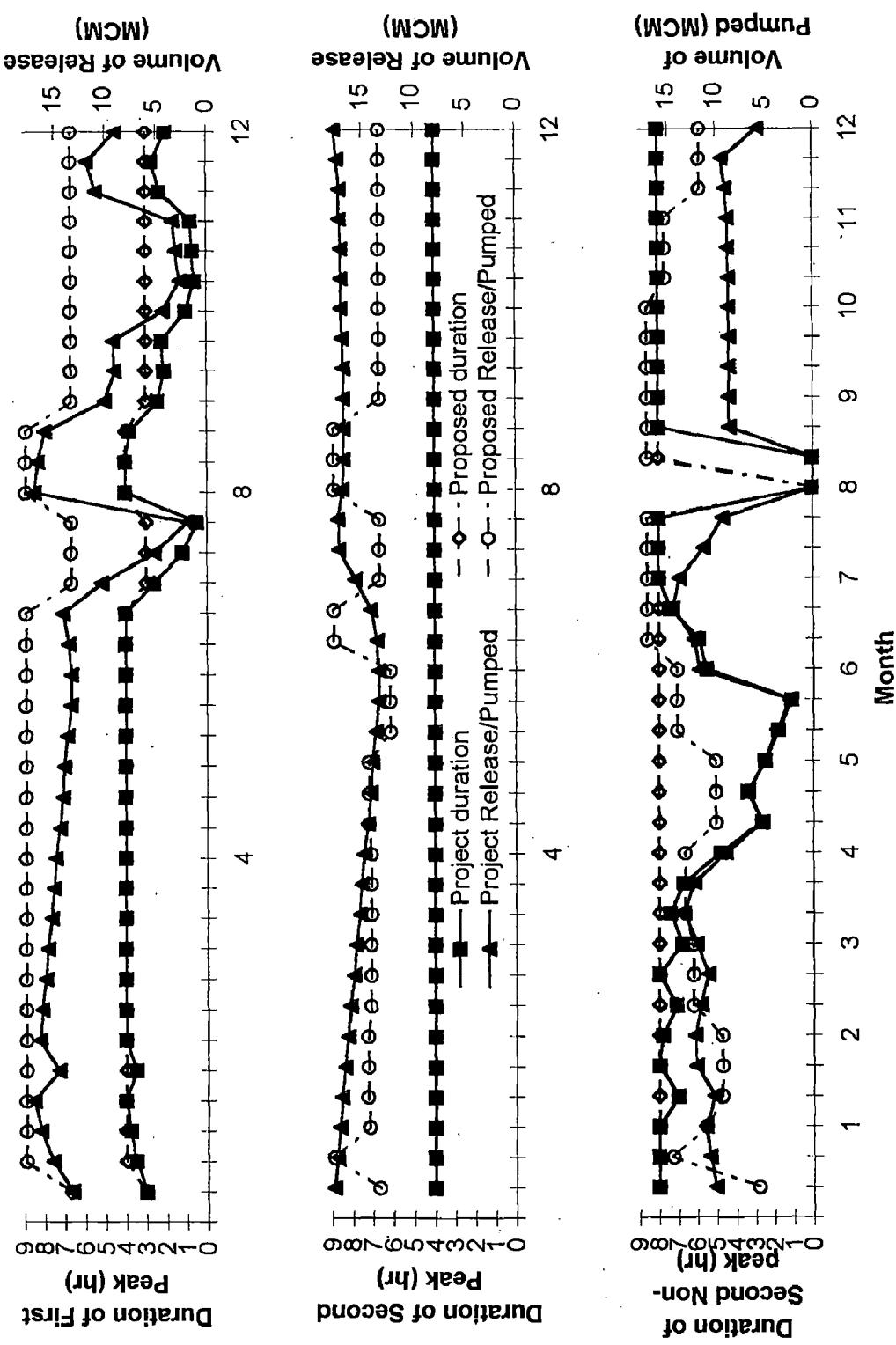


Table 5.1 Calculation Dependable Annual Energy Generated with Project Schedule Operation

| n | YEAR | ENERGY GENERATED (MWh) | PROBABILITY |
|-------|------|------------------------|-------------|
| 0.25 | 1963 | 7.82E+05 | 99.29% |
| 1.25 | 1983 | 4.03E+06 | 96.45% |
| 2.25 | 1975 | 4.04E+06 | 93.62% |
| 3.25 | 1986 | 4.15E+06 | 90.78% |
| 4.25 | 1965 | 4.22E+06 | 87.94% |
| 5.25 | 1974 | 4.25E+06 | 85.11% |
| 6.25 | 1981 | 4.25E+06 | 82.27% |
| 7.25 | 1992 | 4.26E+06 | 79.43% |
| 8.25 | 1995 | 4.26E+06 | 76.60% |
| 9.25 | 1972 | 4.28E+06 | 73.76% |
| 10.25 | 1982 | 4.28E+06 | 70.92% |
| 11.25 | 1984 | 4.28E+06 | 68.09% |
| 12.25 | 1979 | 4.30E+06 | 65.25% |
| 13.25 | 1990 | 4.30E+06 | 62.41% |
| 14.25 | 1964 | 4.32E+06 | 59.57% |
| 15.25 | 1969 | 4.33E+06 | 56.74% |
| 16.25 | 1987 | 4.33E+06 | 53.90% |
| 17.25 | 1988 | 4.33E+06 | 51.06% |
| 18.25 | 1994 | 4.33E+06 | 48.23% |
| 19.25 | 1968 | 4.35E+06 | 45.39% |
| 20.25 | 1978 | 4.36E+06 | 42.55% |
| 21.25 | 1985 | 4.36E+06 | 39.72% |
| 22.25 | 1991 | 4.37E+06 | 36.88% |
| 23.25 | 1996 | 4.37E+06 | 34.04% |
| 24.25 | 1980 | 4.38E+06 | 31.21% |
| 25.25 | 1993 | 4.38E+06 | 28.37% |
| 26.25 | 1970 | 4.39E+06 | 25.53% |
| 27.25 | 1967 | 4.40E+06 | 22.70% |
| 28.25 | 1989 | 4.40E+06 | 19.86% |
| 29.25 | 1971 | 4.41E+06 | 17.02% |
| 30.25 | 1997 | 4.42E+06 | 14.18% |
| 31.25 | 1973 | 4.43E+06 | 11.35% |
| 32.25 | 1966 | 4.45E+06 | 8.51% |
| 33.25 | 1976 | 4.50E+06 | 5.67% |
| 34.25 | 1977 | 4.53E+06 | 2.84% |

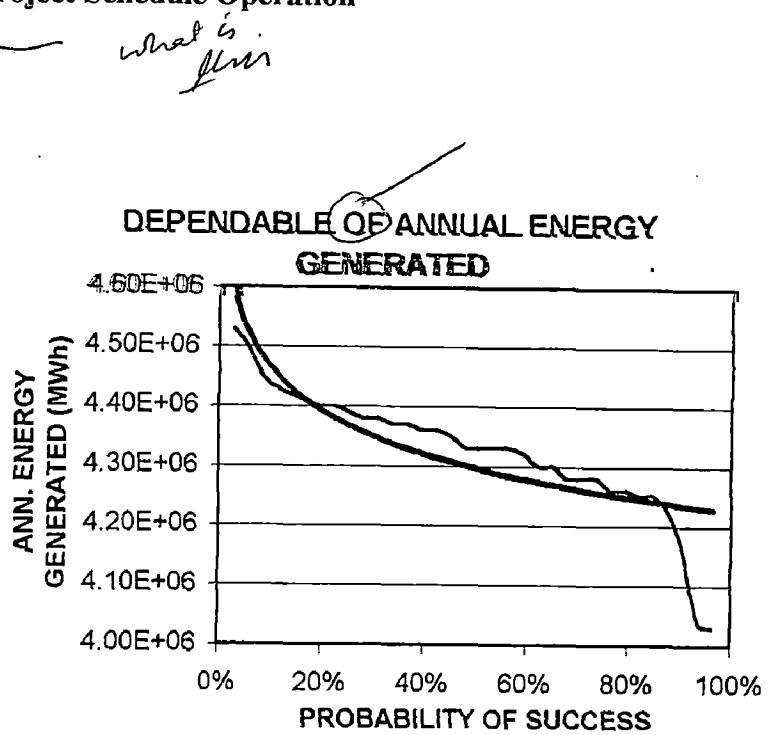
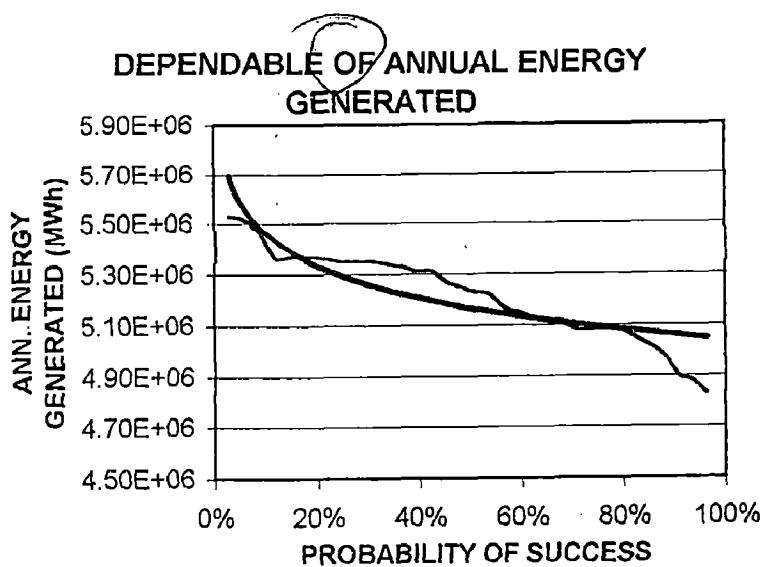


Table 5.2 Calculation of Dependable Annual Energy Generated with Proposed Schedule Operation

| n | YEAR | ENERGY GENERATED | (1-n/(m+1)) |
|-------|-------------|------------------|---------------|
| 0.25 | 1963 | 1.34E+06 | 99.29% |
| 1.25 | 1983 | 4.83E+06 | 96.45% |
| 2.25 | 1965 | 4.88E+06 | 93.62% |
| 3.25 | 1975 | 4.90E+06 | 90.78% |
| 4.25 | 1986 | 4.98E+06 | 87.94% |
| 5.25 | 1987 | 5.02E+06 | 85.11% |
| 6.25 | 1982 | 5.05E+06 | 82.27% |
| 7.25 | 1972 | 5.08E+06 | 79.43% |
| 8.25 | 1981 | 5.08E+06 | 76.60% |
| 9.25 | 1984 | 5.08E+06 | 73.76% |
| 10.25 | 1995 | 5.08E+06 | 70.92% |
| 11.25 | 1992 | 5.11E+06 | 68.09% |
| 12.25 | 1979 | 5.12E+06 | 65.25% |
| 13.25 | 1990 | 5.13E+06 | 62.41% |
| 14.25 | 1974 | 5.15E+06 | 59.57% |
| 15.25 | 1964 | 5.17E+06 | 56.74% |
| 16.25 | 1969 | 5.22E+06 | 53.90% |
| 17.25 | 1988 | 5.23E+06 | 51.06% |
| 18.25 | 1968 | 5.25E+06 | 48.23% |
| 19.25 | 1994 | 5.27E+06 | 45.39% |
| 20.25 | 1980 | 5.31E+06 | 42.55% |
| 21.25 | 1991 | 5.31E+06 | 39.72% |
| 22.25 | 1985 | 5.33E+06 | 36.88% |
| 23.25 | 1989 | 5.34E+06 | 34.04% |
| 24.25 | 1966 | 5.35E+06 | 31.21% |
| 25.25 | 1967 | 5.35E+06 | 28.37% |
| 26.25 | 1970 | 5.35E+06 | 25.53% |
| 27.25 | 1996 | 5.36E+06 | 22.70% |
| 28.25 | 1971 | 5.37E+06 | 19.86% |
| 29.25 | 1973 | 5.37E+06 | 17.02% |
| 30.25 | 1978 | 5.37E+06 | 14.18% |
| 31.25 | 1993 | 5.37E+06 | 11.35% |
| 32.25 | 1976 | 5.47E+06 | 8.51% |
| 33.25 | 1997 | 5.52E+06 | 5.67% |
| 34.25 | 1977 | 5.53E+06 | 2.84% |



Chapter 6

CONCLUSIONS

From the pumped storage reservoir operation study for 35 years of Tehri Project presented in Chapter 4 and discussed in Chapter 5, it is seen that both the irrigation and power benefits can be improved upon. The results of the project operation schedule and the proposed optimized operation schedule have been compared below:

1. Proposed operation schedule has better result, average percentage of meeting irrigation demands is more succeed and more energy generated.

| Description | Average Annual % of Meeting Irrigation Demand | Average Annual Energy Generated in 35 years ($\times 10^9$ KWh) |
|--|---|--|
| 1. Project Operation Schedule (Table 4.1 and Table 4.2) | 97.11 | 4.32 |
| 2. Proposed Operation Schedule (Table 4.8 and Table 4.9) | 98.50 | 5.22 |
| Difference | 1.39 | 0.90 (20.83%) |

2. The comparison of the period of deficient irrigation the two sets of operation schedule is given below:

| Description | Water Deficient Months | Minimum Average % Meeting Irrigation Demand |
|--|--|--|
| 1. Project Operation Schedule (Table 4.1 and Table 4.2) | April, May, June, November, and December | 3 rd ten daily period of November (78.66 %) |
| 2. Proposed Operation Schedule (Table 4.8 And Table 4.9) | May and June | 3 rd ten daily period of May (83.70 %) |

The above comparison shows that the proposed operation schedule gives better irrigation facility. Deficiency irrigation in November and December during Rabi corps is not very desirable.

Crash
The percentage of irrigation demands deficiency during April to June has been reduced substantially with the proposed operation schedule.

3. The proposed optimized operation schedule, because of improvement both in irrigation and power generation is recommended for adoption.

The results show that the proposed operation schedule slightly improves irrigation facility from the project but the increase in power generation is substantial.

The increase in power generation is associated with increase in total generating and pumping hours in a year. The average annual increase is as below:

$$\text{Increase in generating hours} = \frac{2777 \text{ hr} - 2580.62 \text{ hr}}{2580.62 \text{ hr}} \times 100 \% = 7.61 \%$$

$$\text{Increase in pumping hours} = \frac{2832 \text{ hr} - 2324.70 \text{ hr}}{2324.70 \text{ hr}} \times 100 \% = 21.82 \%$$

4. The models runs have helped in developing a trade off curve between percentage of meeting irrigation demand and power generation. It is helpful in selecting the

operation schedule based on the weightage to be given to the two benefits of the project i.e. irrigation and power generation.

Suggestion for further study

The computer program developed in this study for reservoir operation of a pumped storage scheme can be used as a tool to optimize the installed capacity as well as the capacity of the lower reservoir.

References

1. Chow, VT., Maidment, DR., Mays, LW.(1988), *Applied Hydrology*, McGraw Hill Book Co.,
2. *Design Criteria and Construction Procedures, Hydrologic Analysis for Reservoir Simulation*, Le Groupe AFH International Inc., (1993) In cooperation with Research Institute of Water Resources Development – Bandung Indonesia.
3. Ellis T. Cox, (1975), *Pumped Storage Generation Factors to be Considered*, An Engineering Foundation Conference, Published by American Society of Civil Engineers (ASCE).
4. Indian Standard, IS 12800 (Part 2/Sec 1): 1989, *Guidelines for Selection of Turbines, Preliminary Dimensioning and Layout of Surface Hydroelectric Power Houses*, Part 2 Pumped Storage Power House.
5. *International Symposium on Real Time Operation of Hydro System* (1981) University of Waterloo, Waterloo Ontario.
6. Mosonyi E. (1965), *Water Power Development*, Volume II, *High-Head Power Plants, Midget Stations and Pumped-Storage Schemes*, Second English Edition, Akademiai Kiado, Publishing House of the Hungarian Academy of Sciences, Budapest.
7. Mutreja KN. (1995), *Applied Hydrology*, Fourth Reprint, Tata McGraw Hill Publishing Co. Ltd. New Delhi.
8. Nigam, PS. (1995), *Handbook of Hydroelectric Engineering*, Nem Chand & Bros., Roorkee.
9. Punmia, BC., Lal, BB. (1992), *Irrigation and Water Power Engineering*, 12th Edition, Laxmi Publications, New Delhi.
10. Rajasekaran, S. (1999), *Numerical Methods in Science and Engineering, A Practical Approach*, Second Edition, Wheeler Publishing, New Delhi.
11. Soesianto, F. and Nugroho, E. (1986), *Belajar Sendiri Bahasa FORTRAN*, Andi Offset, Yogyakarta.
12. Subramanya, K. (1994), *Engineering Hydrology*, Second Edition, Tata McGraw Hill Publishing Co. Ltd. New Delhi.

13. Taha, Hamdy A. (1999), *Operation Research an Introduction*, Sixth Edition, Prentice Hall of India Private Ltd. New Delhi.
14. Varshney, RS. (1986), *Hydropower Structures*, Third Edition, Nem Chand & Bros., Roorkee.
15. Varma, CVJ., Rao, ARG. (1997), *Pumped Storage Schemes in India*, Central Board of Irrigation & Power, New Delhi.

The catchment area of of river Bhagirathi upto Tehri Dam Site is 7511 Sq Km, out of which about 2300 Sq Km area is snow bound. The catchment area upto Koteswar dam site is 7691 Sq Km which also includes the snow bound area of 2300 Sq Km. The river runoff data at Tehri dam site is enclosed. Some contribution of the intervening catchment area of 180 Sq Km may be suitably assumed. There is no major tributary joining the main river in the reach of 20 Km between Tehri and Koteswar.

For Tehri Reservoir:

**F.R.L. = 830.00 m.
M.D.D.L = 740.00 m.**

For Koteswar Reservoir:

**F.R.L. = 612.00 m.
M.D.D.L = 598.50 m.**

The power house complex at Tehri comprises of 8 machines of 250 MW each. Four of these machines are turbines and have an installed capacity of 1000 MW (4X250MW). The other four machines are reversible machines and these can operate in turbine as well as pump mode. The capacity of the reversible machines is also 250 MW each and these reversible machines are installed in the PSP. Apart from this there is another power house at Koteswar with an installed capacity of 400 MW. This lower power house is equipped with four turbines of 100 MW each,

TAKE CARE OF UNITS OF ALL THE DATA.

MONTHLY RUNOFF DATA OF RIVER BHAGIRATHI AT TEHRI SITE
(Runoff in Million Cubic Metre)

| | JAN | FEB | MAR | APR | MAY | JUNE |
|------|------|------|------|------|------|-------|
| 1963 | 173. | 206. | 201. | 293. | 293. | 581. |
| 1964 | 174. | 175. | 178. | 185. | 254. | 877. |
| 1965 | 168. | 163. | 402. | 191. | 229. | 658. |
| 1966 | 215. | 205. | 234. | 260. | 321. | 944. |
| 1967 | 175. | 175. | 181. | 194. | 358. | 762. |
| 1968 | 192. | 187. | 182. | 229. | 309. | 561. |
| 1969 | 143. | 124. | 133. | 191. | 247. | 1051. |
| 1970 | 138. | 175. | 157. | 198. | 363. | 596. |
| 1971 | 154. | 152. | 213. | 359. | 605. | 1158. |
| 1972 | 143. | 137. | 132. | 187. | 240. | 501. |
| 1973 | 150. | 180. | 209. | 372. | 455. | 832. |
| 1974 | 127. | 125. | 158. | 276. | 487. | 753. |
| 1975 | 126. | 105. | 86. | 114. | 175. | 369. |
| 1976 | 141. | 118. | 278. | 318. | 703. | 1440. |
| 1977 | 138. | 150. | 159. | 272. | 373. | 1481. |
| 1978 | 135. | 95. | 83. | 145. | 321. | 998. |
| 1979 | 98. | 90. | 111. | 216. | 388. | 700. |
| 1980 | 105. | 102. | 226. | 327. | 456. | 888. |
| 1981 | 115. | 110. | 149. | 279. | 565. | 824. |
| 1982 | 118. | 139. | 125. | 138. | 395. | 853. |
| 1983 | 84. | 73. | 74. | 113. | 247. | 654. |
| 1984 | 109. | 99. | 109. | 200. | 493. | 1283. |
| 1985 | 132. | 145. | 171. | 234. | 346. | 682. |
| 1986 | 104. | 100. | 206. | 389. | 628. | 828. |
| 1987 | 166. | 131. | 128. | 164. | 368. | 828. |
| 1988 | 104. | 96. | 198. | 289. | 610. | 925. |
| 1989 | 153. | 140. | 174. | 256. | 436. | 1005. |
| 1990 | 153. | 154. | 159. | 153. | 333. | 603. |
| 1991 | 172. | 154. | 178. | 280. | 449. | 709. |
| 1992 | 137. | 130. | 142. | 160. | 251. | 648. |
| 1993 | 170. | 159. | 158. | 241. | 578. | 964. |
| 1994 | 160. | 147. | 160. | 224. | 318. | 645. |
| 1995 | 173. | 154. | 153. | 149. | 239. | 438. |
| 1996 | 230. | 195. | 333. | 383. | 577. | 950. |
| 1997 | 286. | 239. | 188. | 211. | 403. | 643. |

MONTHLY RUNOFF DATA OF RIVER BHAGIRATHI AT TEHRI SITE
(Runoff in Million Cubic Metre)

| | JULY | AUG | SEP | OCT | NOV | DEC |
|------|-------|-------|-------|-------|------|------|
| 1963 | 1724. | 2172. | 1459. | 431. | 263. | 207. |
| 1964 | 1329. | 1241. | 567. | 267. | 207. | 189. |
| 1965 | 1606. | 2265. | 769. | 238. | 196. | 181. |
| 1966 | 1439. | 2991. | 865. | 342. | 248. | 217. |
| 1967 | 1538. | 1954. | 730. | 306. | 205. | 182. |
| 1968 | 1311. | 2098. | 1014. | 332. | 237. | 207. |
| 1969 | 1162. | 2126. | 1049. | 356. | 270. | 238. |
| 1970 | 1864. | 2193. | 1032. | 373. | 231. | 181. |
| 1971 | 1355. | 1354. | 1024. | 360. | 199. | 167. |
| 1972 | 1794. | 2176. | 1256. | 404. | 206. | 170. |
| 1973 | 1397. | 2035. | 758. | 369. | 207. | 164. |
| 1974 | 1267. | 1809. | 1433. | 598. | 283. | 165. |
| 1975 | 1814. | 1782. | 1142. | 380. | 200. | 146. |
| 1976 | 2091. | 2228. | 1457. | 489. | 262. | 203. |
| 1977 | 2437. | 3167. | 2281. | 794. | 484. | 187. |
| 1978 | 3430. | 3445. | 1445. | 578. | 180. | 136. |
| 1979 | 2540. | 2271. | 1242. | 572. | 213. | 106. |
| 1980 | 1739. | 2355. | 1051. | 375. | 235. | 118. |
| 1981 | 1261. | 1247. | 757. | 353. | 332. | 138. |
| 1982 | 1350. | 2062. | 1269. | 450. | 240. | 163. |
| 1983 | 1406. | 1437. | 1026. | 264. | 147. | 106. |
| 1984 | 1615. | 2323. | 1398. | 761. | 264. | 131. |
| 1985 | 2592. | 2851. | 936. | 375. | 186. | 148. |
| 1986 | 1061. | 1132. | 923. | 282. | 169. | 123. |
| 1987 | 2012. | 2660. | 1176. | 460. | 224. | 174. |
| 1988 | 1336. | 1650. | 1195. | 398. | 213. | 125. |
| 1989 | 1654. | 1917. | 815. | 270. | 221. | 164. |
| 1990 | 1545. | 1618. | 1008. | 343. | 234. | 181. |
| 1991 | 1225. | 2493. | 1651. | 469. | 266. | 185. |
| 1992 | 1438. | 1446. | 1418. | 506. | 258. | 171. |
| 1993 | 2096. | 2275. | 1526. | 514. | 280. | 211. |
| 1994 | 1362. | 1795. | 1436. | 369. | 234. | 181. |
| 1995 | 1461. | 1983. | 1538. | 447. | 283. | 246. |
| 1996 | 1344. | 1986. | 1225. | 458. | 281. | 260. |
| 1997 | 2037. | 2303. | 1654. | 1018. | 555. | 341. |

AREA CAPACITY DATA OF KOTESHWAR RESERVOIR

| Elevation in Metre | Surface Area in Sq Km | Capacity in Million Cubic Metre |
|--------------------|-----------------------|---------------------------------|
| 530.0 | 0.0 | 0.00 |
| 540.0 | 0.045 | 1.00 |
| 550.0 | 0.18 | 2.40 |
| 560.0 | 0.45 | 5.00 |
| 570.0 | 0.90 | 11.40 |
| 580.0 | 1.29 | 20.80 |
| 590.0 | 1.65 | 38.90 |
| 600.0 | 2.04 | 58.00 |
| 610.0 | 2.40 | 80.20 |
| 620.0 | 3.15 | 106.80 |

AREA CAPACITY DATA OF TEHRI RESERVOIR

| Elevation in Metre | Surface Area in Sq Km | Capacity in Million Cubic Metre |
|--------------------|-----------------------|---------------------------------|
| 620.0 | 0.4 | 8.0 |
| 630.0 | | 15.0 |
| 640.0 | 1.8 | 25.0 |
| 650.0 | | 50.0 |
| 660.0 | 4.1 | 85.0 |
| 670.0 | | 140.0 |
| 680.0 | 6.4 | 200.0 |
| 690.0 | | 270.0 |
| 700.0 | 10.2 | 350.0 |
| 710.0 | | 450.0 |
| 720.0 | 13.8 | 590.0 |
| 730.0 | | 735.0 |
| 740.0 | 17.3 | 925.0 |
| 750.0 | | 1100.0 |
| 760.0 | 22.4 | 1315.0 |
| 770.0 | | 1550.0 |
| 780.0 | 27.6 | 1820.0 |
| 790.0 | | 2110.0 |
| 800.0 | 33.0 | 2420.0 |
| 810.0 | | 2780.0 |
| 820.0 | 40.0 | 3150.0 |
| 830.0 | 43.8 | 3540.0 |
| 835.0 | | 3770.0 |

EVAPORATION LOSSES IN mm/month

| Month | Evaporation | Month | Evaporation |
|----------|-------------|-----------|-------------|
| January | 39.0 | July | 124.0 |
| February | 57.0 | August | 108.0 |
| March | 102.0 | September | 108.0 |
| April | 172.0 | October | 101.0 |
| May | 210.0 | November | 68.0 |
| June | 193.0 | December | 42.0 |

IRRIGATION REQUIREMENTS

(Irrigation Requirement in Million Cubic Metre per Month)

| Month | Irrigation Requirement | Month | Irrigation Requirement |
|----------|------------------------|-----------|------------------------|
| January | 653.2 | July | 0.0 |
| February | 639.4 | August | 0.0 |
| March | 607.4 | September | 0.0 |
| April | 559.0 | October | 176.2 |
| May | 684.2 | November | 341.2 |
| June | 479.5 | December | 465.8 |

**DAILY SCHEDULE OF GENERATION & PUMPING AT
TEHRI RESERVOIR**

| PERIOD | PARAMETERS | 06-08 hrs | 8-12hrs | 12-18hrs | 18-22 hrs | 22-06 hrs |
|-------------|--|-----------|--------------------------|----------|--------------------------|--------------------------|
| JAN (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 3.00 (+) 13.30 | / | 8 T 4.00 (+) 17.79 | 4 P 8.00 (-) 10.13 |
| JAN (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 3.50 (+) 15.15 | / | 8 T 4.00 (+) 17.51 | 4 P 8.00 (-) 10.71 |
| JAN (21-31) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 3.80 (+) 16.35 | / | 8 T 4.00 (+) 17.28 | 4 P 8.00 (-) 11.17 |
| FEB (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 17.05 | / | 8 T 4.00 (+) 17.05 | 4 P 7.00 (-) 10.25 |
| FEB (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 3.50 (+) 14.63 | / | 8 T 4.00 (+) 16.82 | 4 P 8.00 (-) 12.10 |
| FEB (21-28) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 16.47 | / | 8 T 4.00 (+) 16.47 | 4 P 7.80 (-) 12.29 |
| MAR (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 16.24 | / | 8 T 4.00 (+) 16.24 | 4 P 7.10 (-) 11.66 |
| MAR (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 15.90 | / | 8 T 4.00 (+) 15.90 | 4 P 8.00 (-) 10.89 |
| MAR (21-31) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 15.65 | / | 8 T 4.00 (+) 15.65 | 4 P 6.80 (-) 12.09 |
| APR (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 15.32 | / | 8 T 4.00 (+) 15.32 | 4 P 7.40 (-) 13.36 |
| APR (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 15.09 | / | 8 T 4.00 (+) 15.09 | 4 P 6.70 (-) 12.30 |
| APR (21-30) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 14.86 | / | 8 T 4.00 (+) 14.86 | 4 P 4.80 (-) 9.07 |

8 T → EIGHT MACHINES IN TURBINE MODE
4 P → FOUR MACHINES IN PUMP MODE

| PERIOD | PARAMETERS | 06-08 hrs | 8-12hrs | 12-18hrs | 18-22 hrs | 22-06 hrs |
|--------------|--|-----------|--------------------------|-------------------------|--------------------------|--------------------------|
| MAY (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 14.51 | / | 8 T 4.00 (+) 14.51 | 4 P 2.70 (-) 5.26 |
| MAY (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 14.17 | / | 8 T 4.00 (+) 14.17 | 4 P 3.40 (-) 6.74 |
| MAY (21-31) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 14.05 | / | 8 T 4.00 (+) 14.05 | 4 P 2.50 (-) 5.03 |
| JUNE (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 13.71 | / | 8 T 4.00 (+) 13.71 | 4 P 1.80 (-) 3.83 |
| JUNE (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 13.36 | / | 8 T 4.00 (+) 13.36 | 4 P 1.10 (-) 2.36 |
| JUNE (21-30) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 13.36 | / | 8 T 4.00 (+) 13.36 | 4 P 5.50 (-) 11.79 |
| JULY (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 13.59 | / | 8 T 4.00 (+) 13.59 | 4 P 5.90 (-) 12.32 |
| JULY (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 14.17 | / | 8 T 4.00 (+) 14.17 | 4 P 7.40 (-) 14.52 |
| JULY (21-31) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 2.60 (+) 10.38 | / | 8 T 4.00 (+) 15.67 | 4 P 8.00 (-) 13.82 |
| AUG (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 1.20 (+) 5.16 | / | 8 T 4.00 (+) 17.28 | 4 P 8.00 (-) 11.29 |
| AUG (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 0.50 (+) 1.96 | / | 8 T 4.00 (+) 17.39 | 4 P 8.00 (-) 9.33 |
| AUG (21-31) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 16.93 | 8 T 1.10 (+) 4.76 | 8 T 4.00 (+) 16.93 | |

| PERIOD | PARAMETERS | 06-08 hrs | 8-12hrs | 12-18hrs | 18-22 hrs | 22-06 hrs |
|----------------|---|-----------|--------------------------|----------|--------------------------|-------------------------|
| SEP (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 4.00 (+) 16.62 | / | 8 T 4.00 (+) 16.82 | |
| SEP (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 3.80 (+) 15.92 | / | 8 T 4.00 (+) 16.82 | 4 P 8.00 (-) 8.64 |
| SEP (21-30) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 2.40 (+) 10.05 | / | 8 T 4.00 (+) 16.82 | 4 P 8.00 (-) 8.64 |
| OCT (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 2.10 (+) 9.01 | / | 8 T 4.00 (+) 16.82 | 4 P 8.00 (-) 8.64 |
| OCT (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 2.20 (+) 9.16 | / | 8 T 4.00 (+) 16.93 | 4 P 8.00 (-) 8.64 |
| OCT (21-31) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 1.00 (+) 4.29 | / | 8 T 4.00 (+) 17.05 | 4 P 8.00 (-) 8.64 |
| NOV (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 0.60 (+) 2.65 | / | 8 T 4.00 (+) 17.05 | 4 P 8.00 (-) 8.64 |
| NOV (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 0.70 (+) 3.02 | / | 8 T 4.00 (+) 17.05 | 4 P 8.00 (-) 8.75 |
| NOV (21-30) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 0.80 (+) 3.30 | / | 8 T 4.00 (+) 17.16 | 4 P 8.00 (-) 8.75 |
| DEC (1-10) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 2.30 (+) 10.92 | / | 8 T 4.00 (+) 17.16 | 4 P 8.00 (-) 8.99 |
| DEC (11-20) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 2.70 (+) 11.73 | / | 8 T 4.00 (+) 17.39 | 4 P 8.00 (-) 9.33 |
| DEC (21-31) | Units Running Hrs of running Net inflow in.D/S reservoir (MCM) | / | 8 T 2.02 (+) 9.00 | / | 8 T 4.00 (+) 17.72 | 4 P 4.60 (-) 5.61 |

APPENDIX II

**DROPS (D_Reservoir Operation
of Pumped Storage Scheme) Program**

Appendix IIA

Definition of Variables

The major arrays and symbols used in the program are defined below, some temporary storage variables are not defined here, but their definitions are evident from the context.

| | |
|--------|--|
| ARA | = Surface Area of Reservoir A from data (M^2) |
| ARB | = Surface Area of Reservoir B from data (M^2) |
| AREA | = Surface Area of Reservoir A from calculation (M^2) |
| ASTORE | = Storage at Reservoir A (M^3) |
| AVEN | = Average Energy Generated (MWh) |
| AVEP | = Average Power Generated at end period (MW) |
| AVGTE | = Average Annual Energy Generated of U/S powerhouse (MWh) |
| AVGSY | = Average Annual Energy Generated of System (MWh) |
| AVIRR | = Average Percentage of Irrigation Supply |
| AVSP | = Average Power Generated at start period (MW) |
| BMDDLA | = Lower Limit of Minimum Draw Down Level (MDDL) at Reservoir A (M) |
| BREA | = Surface Area of Reservoir B from calculation (M^2) |
| BSTORE | = Storage at Reservoir B (M^3) |
| CAPA | = Capacity storage at Reservoir A (M^3) |
| CAPB | = Capacity storage at Reservoir B (M^3) |
| DATE | = Date of the day |
| DAY | = Number of days in a month |
| DIA | = Diameter of power tunnel (M) |
| DMAX | = Discharge Release Max through water conductor (cumec) |
| DPMAX | = Pumping Discharge Max through water conductor (cumec) |
| DT | = Duration time of period (hour) |
| EFF | = Efficiency of Powerhouse |
| ELA | = Elevation at Reservoir A from data (M) |
| ELB | = Elevation at Reservoir B from data (M) |
| END | = Energy Generated at D/S Powerhouse (MWh) |

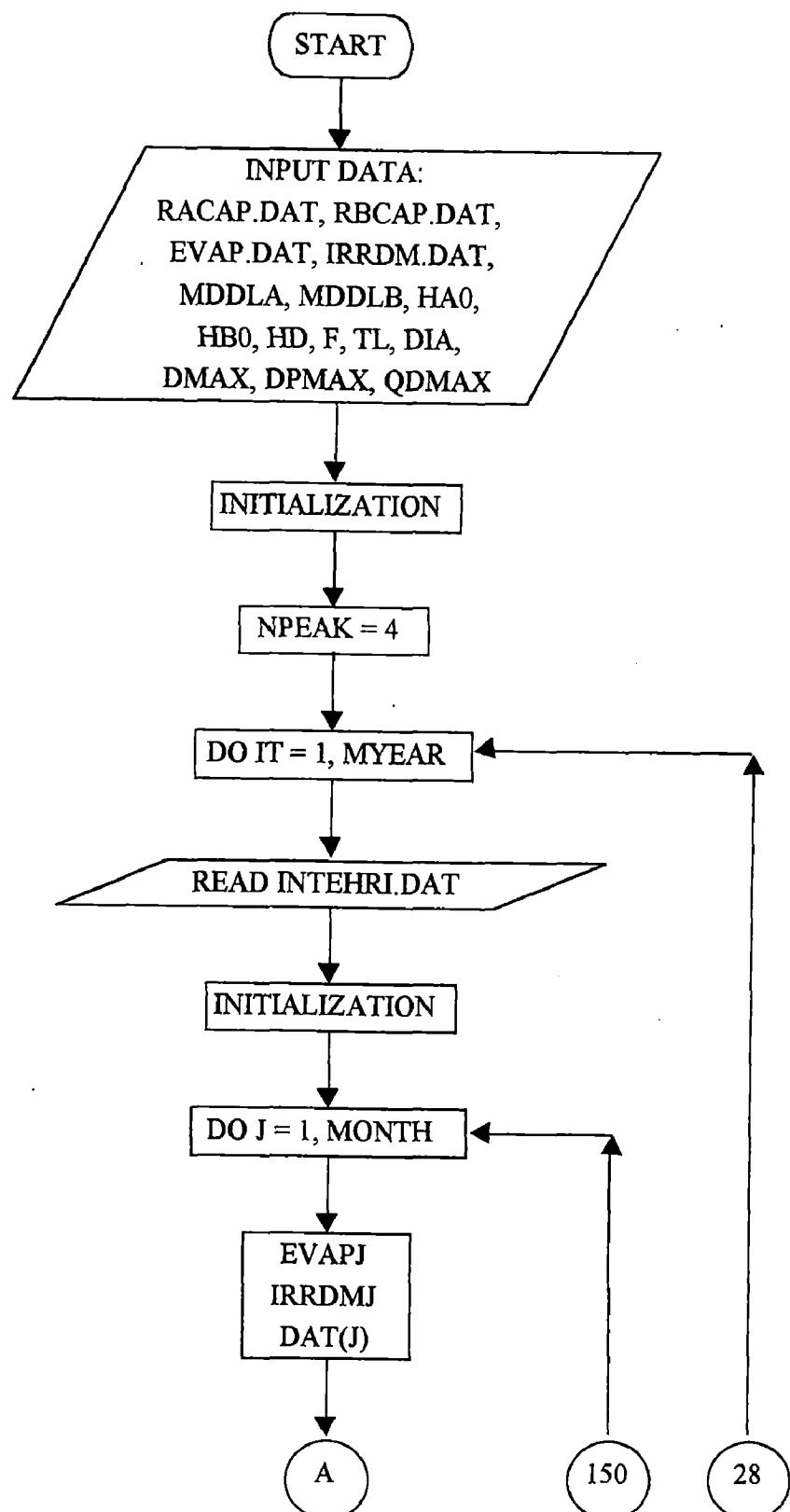
| | |
|--------|---|
| ENSYS | = Energy Generated from System (MWh) |
| EP | = Power Generated at end period (MW) |
| EVAP | = Data of Evaporation Losses (mm/day) |
| EVAPLA | = Evaporation Losses at Reservoir A (M^3) |
| EVAPLB | = Evaporation Losses at Reservoir B (M^3) |
| F | = Coefficient of friction |
| GH | = Gross Head (M) |
| GSYS | = Grand Total Energy Generated from System (MWh) |
| GTEN | = Grand Total Energy Generated (MWh) |
| HA | = Elevation at Reservoir A from calculation (M) |
| HA0 | = Initial Elevation at Reservoir A (M) |
| HAMIN | = Minimum Elevation at Reservoir A (M) |
| HB | = Elevation at Reservoir B from calculation (M) |
| HB0 | = Initial Elevation at Reservoir B (M) |
| HBMIN | = Minimum Elevation at Reservoir B (M) |
| HD | = Net Head of D/S Powerhouse (M) |
| HF | = Losses of Head due to friction (M) |
| HHAMIN | = Minimum Elevation at Reservoir A for all year of data (M) |
| HHBMIN | = Minimum Elevation at Reservoir B for all year of data (M) |
| HN | = Net Head of U/S Powerhouse (M) |
| INFLA | = Inflow to Reservoir A (M^3) |
| INFLAM | = Inflow to Reservoir A in a month (M^3) |
| INFLB | = Inflow to Reservoir B (M^3) |
| INFLBM | = Inflow to Reservoir B in a month (M^3) |
| IR | = Status of Irrigation |
| IRRD | = Irrigation Demand (M^3) |
| IRRDM | = Irrigation Demand in a month (M^3) |
| IRRS | = Irrigation Supply (M^3) |
| KMDDLA | = Upper limit of MDDL of Reservoir A (M) |
| L | = Step of Duration Time (1 to 4) |
| M | = Number of data of Area-Capacity Data of Reservoir A |
| MDDLA | = Minimum Draw Down Level at Reservoir A (M) |
| MDDLB | = Minimum Draw Down Level at Reservoir B (M) |

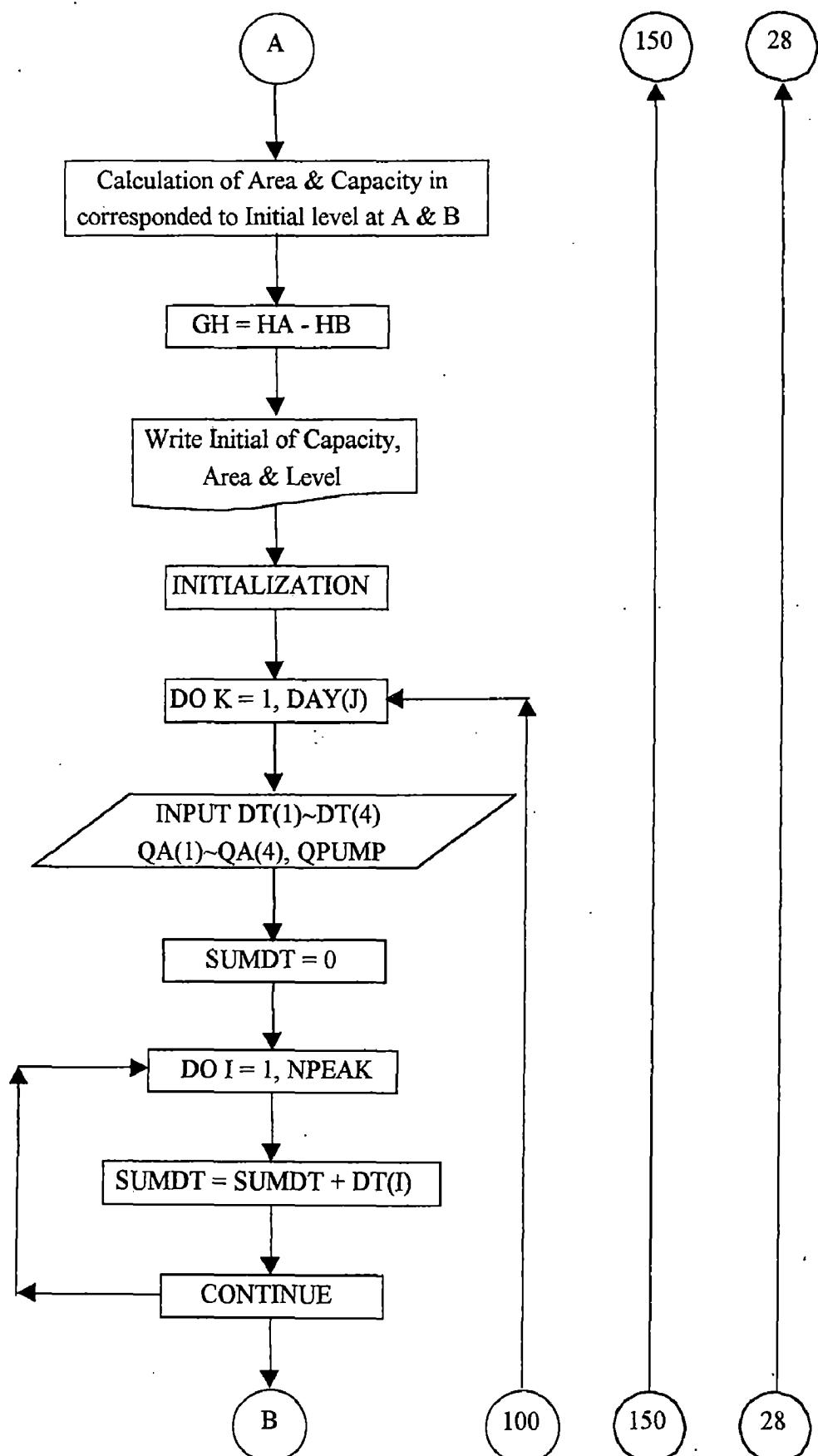
| | |
|--------|---|
| MONTH | = Number of month in a year |
| MYEAR | = Number of year of data |
| N | = Number of data of Area-Capacity Data of Reservoir B |
| ND | = Number of power tunnel |
| NMONTH | = Name of the month |
| NPEAK | = Number of period in a day |
| NYEAR | = Name of year |
| PD | = Power Generated from D/S Powerhouse (MW) |
| PMDDL | = Percentage reach of MDDL at Reservoir A |
| PPMDDL | = Percentage reach of MDDL at Reservoir A for all year |
| PSIRR | = Percentage of Irrigation supply |
| PIGG | = Percentage of Irrigation supply for each time step |
| Q | = Discharge for Power Generation (cumec) |
| QA | = Volume of water Release for Power Generation (M^3) |
| QD | = Discharge for Power Generation (cumec) for D/S Powerhouse |
| QDMAX | = Discharge Maximum for Power Generation (cumec) for D/S Powerhouse |
| QIRR | = Volume of water release for Irrigation and Evaporation at B (M^3) |
| QPUMP | = Volume of water pumped up from Reservoir B (M^3) |
| QR | = Volume of water release beside for Irrigation and Evaporation (M^3) |
| SIRRD | = Summation of Irrigation demand (M^3) |
| SIRRDM | = Summation of Irrigation demand in a month (M^3) |
| SMAXA | = Maximum Storage Capacity at Reservoir A (M^3) |
| SMAXB | = Maximum Storage Capacity at Reservoir B (M^3) |
| SMDDLA | = Storage Capacity at MDDL of Reservoir A (M^3) |
| SMDDLB | = Storage Capacity at MDDL of Reservoir B (M^3) |
| SP | = Power Generated at start (MW) |
| SPILLA | = Volume of water spill from Reservoir A (M^3) |
| SPILLB | = Volume of water spill from Reservoir B (M^3) |
| SPIRR | = Summation of Irrigation Percentage |
| SSIRRD | = Total summation of Irrigation demand (M^3) |
| SUMDT | = Summation of duration time (hour) |

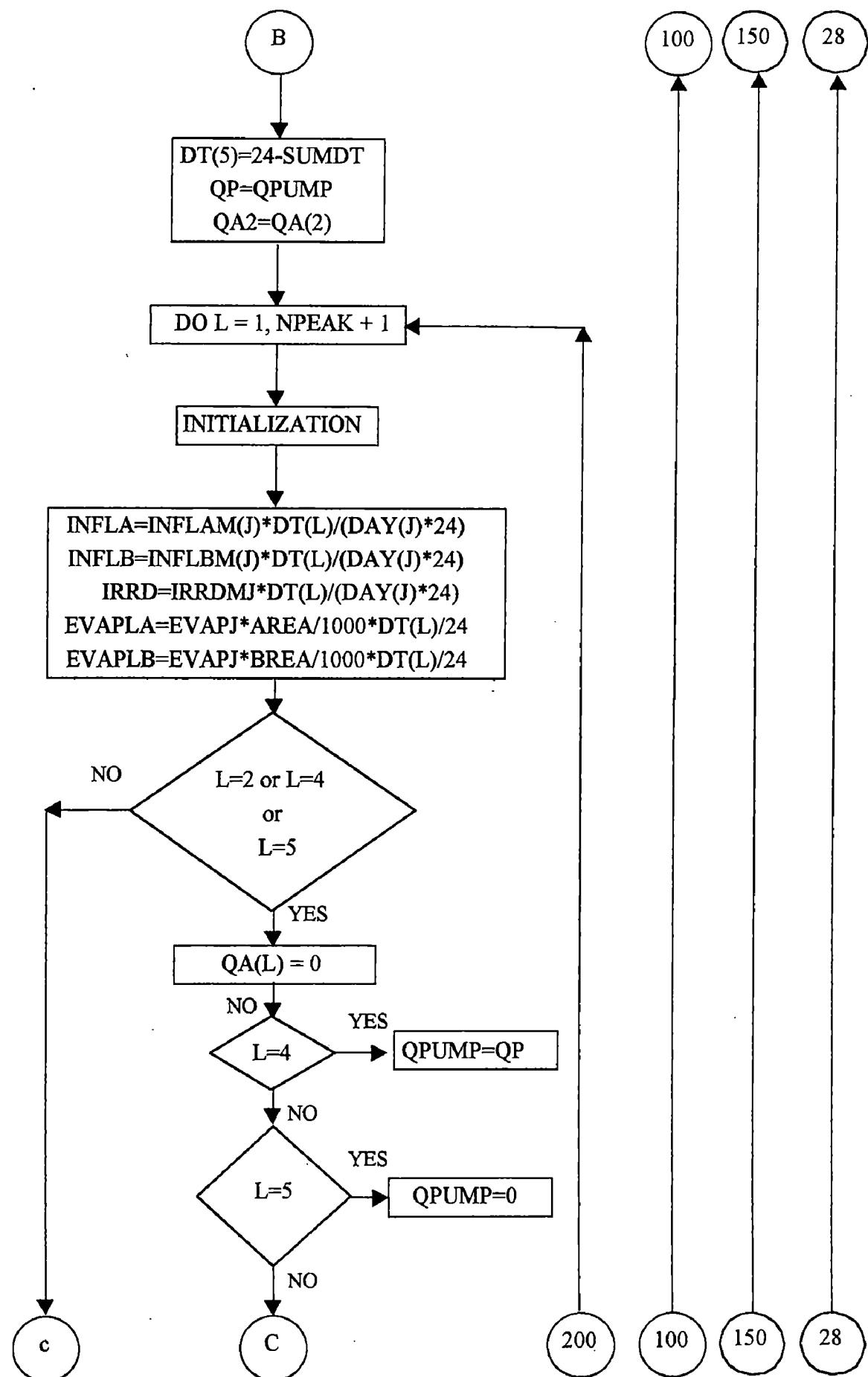
| | |
|--------|--|
| SUMEN | = Summation of Energy Generated (MWh) |
| SUMIR | = Summation of hourly Irrigation Supply (M^3) |
| SUMSPB | = Summation of water spill from Reservoir B (M^3) |
| SUMSYS | = Summation of Energy Generated from system (MWh) |
| TEN | = Total Energy Generated (MWh) |
| TINFLA | = Total Inflow to Reservoir A (M^3) |
| TINFLB | = Total Inflow to Reservoir B (exclude from Reservoir A) (M^3) |
| TINFLM | = Total Inflow to Reservoir A and B (M^3) |
| TL | = Length of Power tunnel (M) |
| TOL | = Tolerance for Irrigation Supply Success |
| TOTSPB | = Total Volume of water spill from Reservoir B (M^3) |
| TP | = PEAK or NON-PEAK period |
| TSYS | = Total Energy Generated from system (MWh) |
| TTINFL | = Total Inflow to Reservoir A and B in a year (M^3) |
| V | = Velocity of water through power tunnel (M/sec) |

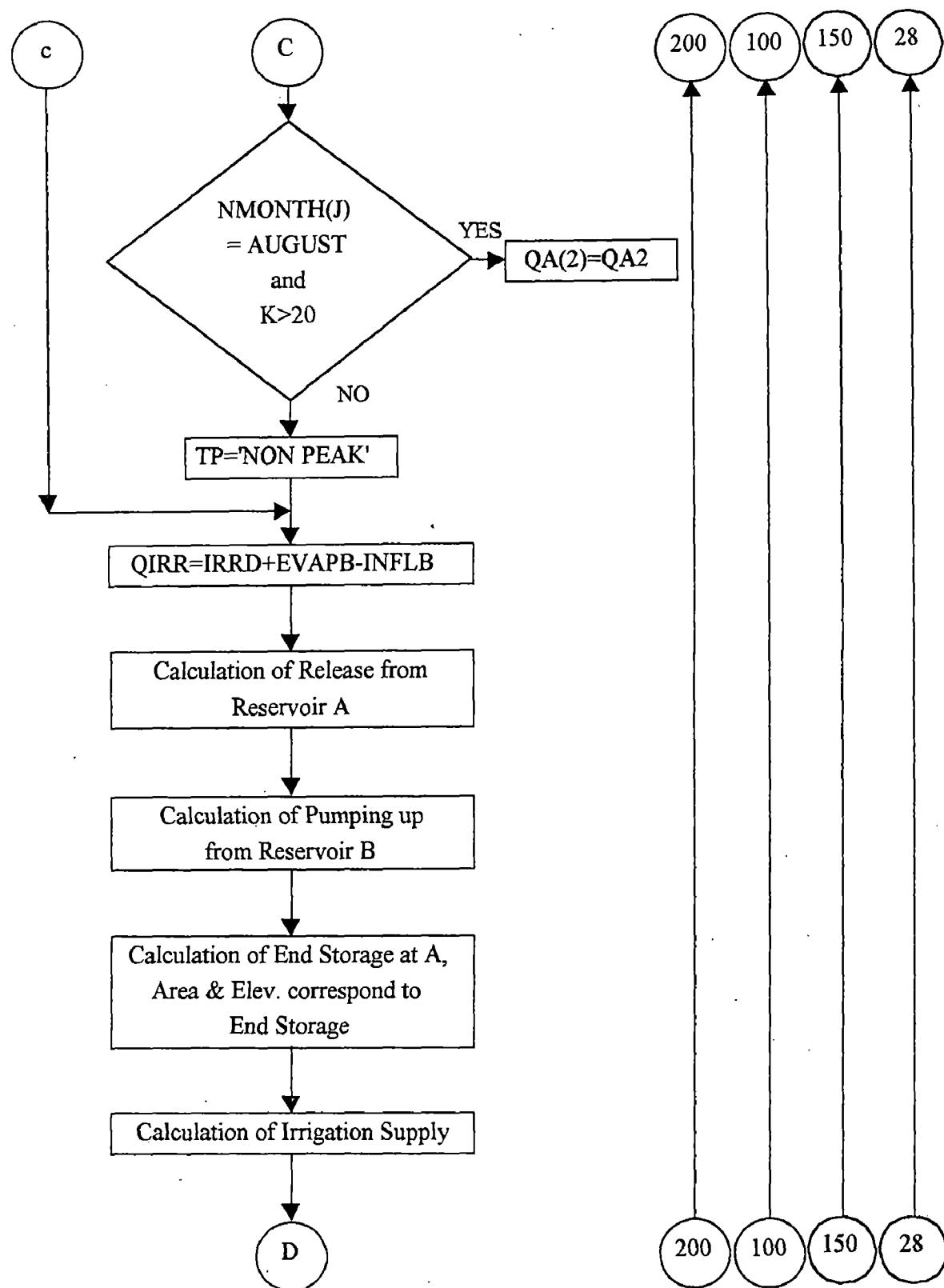
APPENDIX IIB

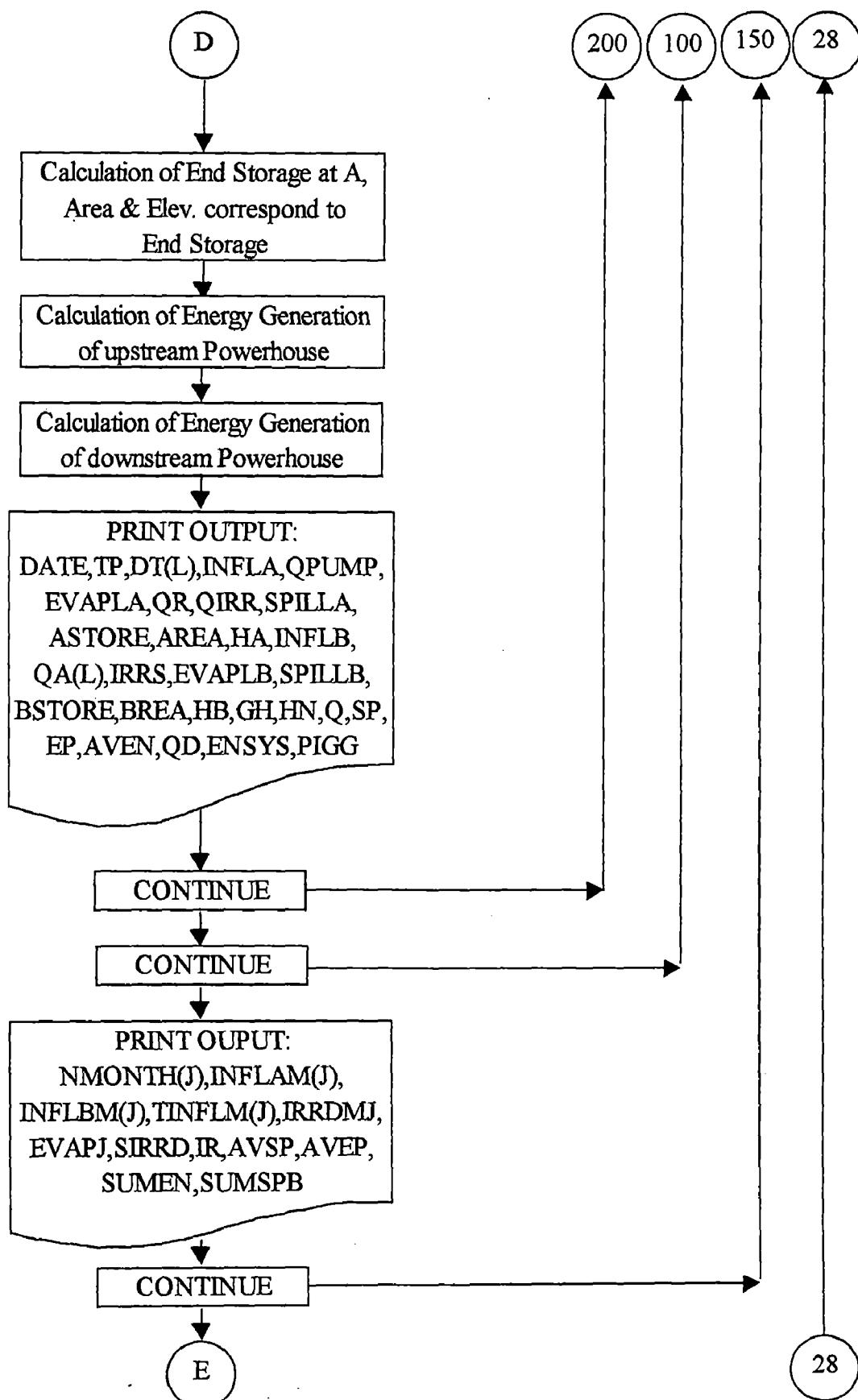
Flowchart

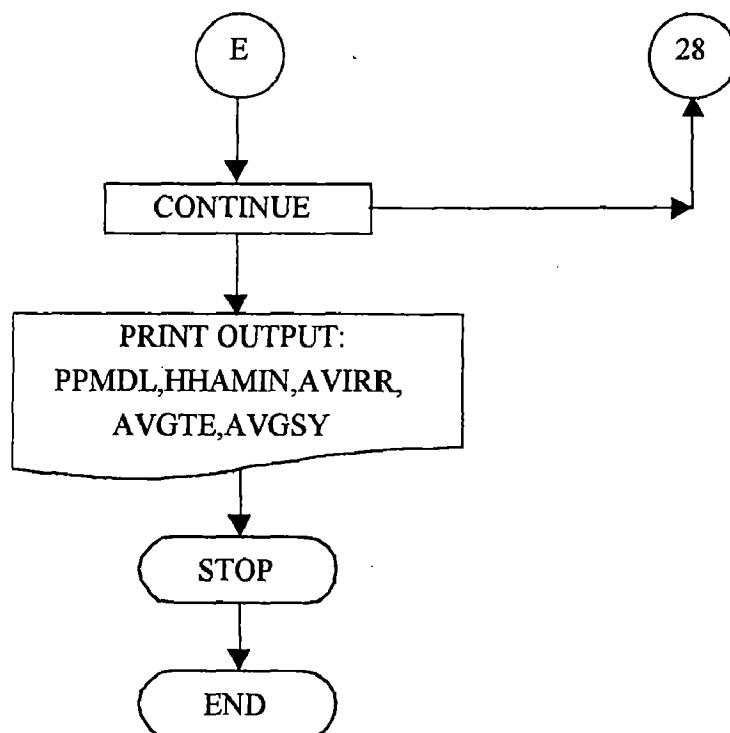












Appendix IIC

Listing of DROPS Program

```

* Program of Reservoir Operation of Pumped Storage Scheme
* With Control the MDDL by Control of Qrelease and
* Qpump (Output file:ROAXXX, ROBXXX, SROXXX)
$TITLE:'DROPS Program by Dinny'

PROGRAM DROPS
REAL INFLA,INFLB,MDDLA,MDDLB,IRRD,IRRDM,IRRDMJ,INFLAM,INFLBM,IRRS,
1IRR1
DOUBLE PRECISION ASTORE,HA,BSTORE,HB,PI
INTEGER DAY,DATE
CHARACTER TP*10,NMONTH*10,NNMONT*10,IR*11,FILE*13
CHARACTER*13 FILE1,FILE2,FILE3,FILE4,FILE5,FILE7,FILE6,FILE8,
1FILE9,FILE20,FILE26
DIMENSION ELA(10),ARA(10),CAPA(10),ELB(10),ARB(10),CAPB(10),DT(5),
1EVAP(12),DAY(12),IRRDM(12),INFLAM(12),INFLBM(12),NMONTH(12),
2TINFLM(12),FILE(30),QA(5),QP(5),AV(12,3),QDAT(5)
WRITE(*,*)'*****' PROGRAM DROPS *****'
WRITE(*,*)'*      Program of Reservoir Operation      *'
WRITE(*,*)'* for Pumped Storage Scheme with 2 Reservoir *'
WRITE(*,*)'*          (C) Dinny Suryakencana-2000      *'
WRITE(*,*)'*****'*****'*****'*****'*****'*****'*****'

C      WRITE(*,*) 'How many peak hour per day'
C      WRITE(*,*) ' 1) Once a day'
C      WRITE(*,*) ' 2) Twice a day'
C      WRITE(*,*) '      Choose 1 or 2'
C      READ (*,*) LC
C ----- Default is Once a day
IF ((LC .LT. 1) .OR. (LC .GT. 2)) LC = 1
*****Read Data*****
LC=2
NPEAK=2
IF(LC.NE.1)NPEAK=4
WRITE(*,*)'File Name for Input Data of Area-Capacity of Res. A'
READ (*,*)FILE1
OPEN (UNIT=1,FILE=FILE1,STATUS='OLD')
WRITE(*,*)'File Name for Input Data of Area-Capacity of Res. B'
READ (*,*)FILE2
OPEN (UNIT=2,FILE=FILE2,STATUS='OLD')
WRITE(*,*)'File Name for Input Data of Evaporation Losses'
READ (*,*)FILE5
OPEN (UNIT=5,FILE=FILE5,STATUS='OLD')
WRITE(*,*)'File Name for Input Data of Irrigation Demands'
READ (*,*)FILE6
OPEN (UNIT=6,FILE=FILE6,STATUS='OLD')
WRITE(*,*)'File Name for Input Data of Inflow to A & B Res.'
READ (*,47)FILE7
OPEN (UNIT=7,FILE=FILE7,STATUS='OLD')

47 FORMAT(A13)
OPEN (1,FILE='RACAP.DAT',STATUS='OLD')
OPEN (2,FILE='RBCAP.DAT',STATUS='OLD')
OPEN (5,FILE='EVAP.DAT',STATUS='OLD')
OPEN (6,FILE='IRRDM.DAT',STATUS='OLD')
OPEN (70,FILE='TEMP.DAT',STATUS='NEW')
WRITE(70,109)FILE7
CLOSE(70)
OPEN (70,FILE='TEMP.DAT',STATUS='OLD')

```

```

READ(70,109)FILE7
CLOSE(70,STATUS='DELETE')
109 FORMAT(A3)
  WRITE(*,*)'Your Output file name will be :'
  WRITE(*,113)'ROA',FILE7,'x','OUT','ROB',FILE7,'x','OUT','ENG',
  1FILE7,'x','OUT','SRO',FILE7,'x','OUT'
113 FORMAT(1X,2A3,A1,A5,1X,2A3,A1,A5,1X,2A3,A1,A5,1X,2A3,A1,A4)
  PI=3.141592654
  WRITE(*,*) 'Do you want use File Data SCHEDULE.DAT?'
  WRITE(*,*) ' 1) Yes !'
  WRITE(*,*) ' 2) No !'
  WRITE(*,*) '      Choose 1 or 2'
  READ (*,*) LC2
C ----- Default is use SCHEDULE.DAT
  IF ((LC2.LT. 2) .OR. (LC2.GT. 2)) LC2= 1
  FILE26='SCHEDULE.DAT'
  IF(LC2.EQ.2)THEN
    WRITE(*,*)'File Name of Working Table? '
    READ (*,47)FILE26
  ENDIF
  WRITE(*,*) 'Do you want use File Data SCHEME.DAT?'
  WRITE(*,*) ' 1) Yes !'
  WRITE(*,*) ' 2) No !'
  WRITE(*,*) '      Choose 1 or 2'
  READ (*,*) LC1
C ----- Default is use SCHEME.DAT
  IF ((LC1.LT. 1) .OR. (LC1.GT. 2)) LC1= 1
  OPEN (UNIT=25,FILE='SCHEME.DAT',STATUS='OLD')
  READ(25,*)EFF,F,TL,DIA,ND,MDDLA,MDDLB,DMAX,DPMAX,QDMAX,HA0,HBO,HD
  CLOSE(25)
  IF(LC1.EQ.2)THEN
    WRITE(*,*)' INPUT EFFICIENCY FACTOR OF M/C & TURBINE = '
    READ(*,*)EFF
    WRITE(*,*)' INPUT FRICTION LOSSES FACTOR = '
    READ(*,*)F
    WRITE(*,*)' INPUT LENGTH OF POWER TUNNEL (M) = '
    READ(*,*)TL
    WRITE(*,*)' INPUT DIAMETER OF POWER TUNNEL (M) = '
    READ(*,*)DIA
    WRITE(*,*)' INPUT NUMBER OF POWER TUNNEL = '
    READ(*,*)ND
    WRITE(*,*)' INPUT MDDL AT RESERVOIR A (M) = '
    READ(*,*)MDDLA
    WRITE(*,*)' INPUT MDDL AT RESERVOIR B (M) = '
    READ(*,*)MDDLB
    WRITE(*,*)' INPUT DISCHARGE MAX. FOR RELEASE (CUMEC) = '
    READ(*,*)DMAX
    WRITE(*,*)' INPUT DISCHARGE MAX. FOR PUMPING (CUMEC) = '
    READ(*,*)DPMAX
    WRITE(*,*)' INPUT DISCHARGE MAX. FOR D/S POWERHOUSE = '
    READ(*,*)QDMAX
    WRITE(*,*)' INPUT INITIAL EL. AT RESERVOIR A (M) = '
    READ(*,*)HA0
    WRITE(*,*)' INPUT INITIAL EL. AT RESERVOIR B (M) = '
    READ(*,*)HBO
    WRITE(*,*)' INPUT NETT HEAD OF D/S POWERHOUSE (M) = '
    READ(*,*)HD
  ENDIF

```

```

KMDDLA=MDDLA-.005
BMDDLA=MDDLA+.005

      READ(1,*)N
      DO 10 I=1,N
10      READ(1,*) ELA(I),ARA(I),CAPA(I)
      SMAXA=CAPA(1)
      CLOSE(1)
      READ(2,*)M
      DO 20 I=1,M
20      READ(2,*)ELB(I),ARB(I),CAPB(I)
      SMAXB=CAPB(1)
      CLOSE(2)
      DO 21 I=1,N
         IF(MDDLA.LE.ELA(I).AND.MDDLA.GT.ELA(I+1))THEN
            C1=(MDDLA-ELA(I+1))/(ELA(I)-ELA(I+1))
            SMDDLA=CAPA(I+1)+C1*(CAPA(I)-CAPA(I+1))
         ENDIF
21 CONTINUE
      DO 23 I=1,M
         IF(MDDLB.LE.ELB(I).AND.MDDLB.GT.ELB(I+1))THEN
            C1=(MDDLB-ELB(I+1))/(ELB(I)-ELB(I+1))
            SMDDLB=CAPB(I+1)+C1*(CAPB(I)-CAPB(I+1))
         ENDIF
23 CONTINUE
      READ(5,*)MONTH
      DO 25 I=1,MONTH
25      READ(5,*)EVAP(I)
      CLOSE(5)
      READ(6,*)MONTH
      SIRRDM=0
      DO 27 I=1,MONTH
27      READ(6,*)IRRDM(I)
      CLOSE(6)
      HA=HA0
      HB=HB0
      HHAMIN=ELA(1)
      HHBMIN=ELB(1)
      NNMDDL=0
      NNIT=0
      GTEN=0
      GSYS=0
      SPIRR=0
      ASTEMP=0
      READ(7,*)MYEAR
      IF(MYEAR.GT.8)THEN
      NMYEAR=MYEAR/8
      DMYEAR=FLOAT(MYEAR)/8-NMYEAR
      IF(DMYEAR.EQ.0)NMYEAR=NMYEAR-1
      OPEN (70,FILE='TEMP.DAT',STATUS='NEW')
      WRITE(70,111)'ROA',FILE7,0,'.OUT','ROB',FILE7,0,'.OUT','ENG',
1FILE7,0,'.OUT'
      WRITE(70,111)'SRO',FILE7,0,'.OUT','SRO',FILE7,1,'.OUT'
      DO 49 I=1,NMYEAR
49      WRITE(70,111)'ROA',FILE7,I,'.OUT','ROB',FILE7,I,'.OUT','ENG',
1FILE7,I,'.OUT'
      CLOSE(70)
      OPEN(70,FILE='TEMP.DAT',STATUS='OLD')
      READ(70,112)FILE3,FILE4,FILE20

```

```

READ(70,112)FILE8,FILE9
DO 50 I=1,NMYEAR
  NF1=9+I
  NF2=15+I
  NF3=20+I
  READ(70,112)FILE(NF1),FILE(NF2),FILE(NF3)
50 CONTINUE
ENDIF
OPEN (UNIT=3,FILE=FILE3,STATUS='NEW')
OPEN (UNIT=4,FILE=FILE4,STATUS='NEW')
OPEN (UNIT=8,FILE=FILE8,STATUS='NEW')
OPEN (UNIT=9,FILE=FILE9,STATUS='NEW')
OPEN (UNIT=20,FILE=FILE20,STATUS='NEW')
111 FORMAT(A3,A3,I1,A4,1X,A3,A3,I1,A4,1X,A3,A3,I1,A4)
112 FORMAT(3A12)
CLOSE(70,STATUS='DELETE')

WRITE(*,*)"Please Wait for Data Processing!"
WRITE(9,7551)
  NJAN=0
  NFEB=0
  NMAR=0
  NAPR=0
  NMAY=0
  NJUN=0
  NJUL=0
  NAUG=0
  NSEP=0
  NOCT=0
  NNOV=0
  NDEC=0
  SV11=0
  SV21=0
  SV31=0
  SV12=0
  SV22=0
  SV32=0
  SV13=0
  SV23=0
  SV33=0
  SV14=0
  SV24=0
  SV34=0
  SV15=0
  SV25=0
  SV35=0
  SV16=0
  SV26=0
  SV36=0
  SV17=0
  SV27=0
  SV37=0
  SV18=0
  SV28=0
  SV38=0
  SV19=0
  SV29=0
  SV39=0
  SV110=0

```

```

SV210=0
SV310=0
SV111=0
SV211=0
SV311=0
SV112=0
SV212=0
SV312=0
DO 28 IT=1,MYEAR
READ(7,*)NYEAR,MONTH
DO 29 I=1,MONTH
29     READ(7,8000)INFLAM(I),INFLBM(I),NMONT(H,I)
DYEAR=FLOAT(NYEAR)/4-NYEAR/4

*****Initialization*****
HAMIN=ELA(1)
HBMIN=ELB(1)
DATE=0
TEN=0
TSYS=0
NMDDL=0
NIT=0
TOTSPB=0
TINFLA=0
TINFLB=0
TTINFL=0
SSIRRD=0
SIRRDM=0
IF(IT.EQ.8)THEN
    CLOSE(3)
    CLOSE(4)
    CLOSE(20)
    OPEN (UNIT=10,FILE=FILE(10),STATUS='NEW')
    OPEN (UNIT=16,FILE=FILE(16),STATUS='NEW')
    OPEN (UNIT=21,FILE=FILE(21),STATUS='NEW')
ELSEIF(IT.EQ.15)THEN
    CLOSE(10)
    CLOSE(16)
    CLOSE(21)
    OPEN (UNIT=11,FILE=FILE(11),STATUS='NEW')
    OPEN (UNIT=17,FILE=FILE(17),STATUS='NEW')
    OPEN (UNIT=22,FILE=FILE(22),STATUS='NEW')
ELSEIF(IT.EQ.22)THEN
    CLOSE(11)
    CLOSE(17)
    CLOSE(22)
    OPEN (UNIT=12,FILE=FILE(12),STATUS='NEW')
    OPEN (UNIT=18,FILE=FILE(18),STATUS='NEW')
    OPEN (UNIT=23,FILE=FILE(23),STATUS='NEW')
ELSEIF(IT.EQ.29)THEN
    CLOSE(12)
    CLOSE(18)
    CLOSE(23)
    OPEN (UNIT=13,FILE=FILE(13),STATUS='NEW')
    OPEN (UNIT=19,FILE=FILE(19),STATUS='NEW')
    OPEN (UNIT=24,FILE=FILE(24),STATUS='NEW')
ENDIF
*****Calculation Reservoir Operation*****
WRITE(8,7550)NYEAR

```

```

OPEN(26,FILE=FILE26,STATUS='OLD')
DO 150 J=1,MONTH
IF(IT.LE.7)THEN
  WRITE(3,9000)NMONTH(J),NYEAR,'A'
  WRITE(4,9000)NMONTH(J),NYEAR,'B'
  WRITE(20,9001)NMONTH(J),NYEAR
ELSEIF(IT.GT.7.AND.IT.LE.14)THEN
  WRITE(10,9000)NMONTH(J),NYEAR,'A'
  WRITE(16,9000)NMONTH(J),NYEAR,'B'
  WRITE(21,9001)NMONTH(J),NYEAR
ELSEIF(IT.GT.14.AND.IT.LE.21)THEN
  WRITE(11,9000)NMONTH(J),NYEAR,'A'
  WRITE(17,9000)NMONTH(J),NYEAR,'B'
  WRITE(22,9001)NMONTH(J),NYEAR
ELSEIF(IT.GT.21.AND.IT.LE.28)THEN
  WRITE(12,9000)NMONTH(J),NYEAR,'A'
  WRITE(18,9000)NMONTH(J),NYEAR,'B'
  WRITE(23,9001)NMONTH(J),NYEAR
ELSEIF(IT.GT.28)THEN
  WRITE(13,9000)NMONTH(J),NYEAR,'A'
  WRITE(19,9000)NMONTH(J),NYEAR,'B'
  WRITE(24,9001)NMONTH(J),NYEAR
ENDIF

IF(NMONTH(J).EQ.'JANUARY')THEN
  EVAPJ=EVAP(1)
  IRRDMJ=IRRDM(1)
  DAY(J)=31
ELSEIF(NMONTH(J).EQ.'FEBRUARY')THEN
  EVAPJ=EVAP(2)
  IRRDMJ=IRRDM(2)
  DAY(J)=28
IF(DYEAR.EQ.0)DAY(J)=29
ELSEIF(NMONTH(J).EQ.'MARCH')THEN
  EVAPJ=EVAP(3)
  IRRDMJ=IRRDM(3)
  DAY(J)=31
ELSEIF(NMONTH(J).EQ.'APRIL')THEN
  EVAPJ=EVAP(4)
  IRRDMJ=IRRDM(4)
  DAY(J)=30
ELSEIF(NMONTH(J).EQ.'MAY')THEN
  EVAPJ=EVAP(5)
  IRRDMJ=IRRDM(5)
  DAY(J)=31
ELSEIF(NMONTH(J).EQ.'JUNE')THEN
  EVAPJ=EVAP(6)
  IRRDMJ=IRRDM(6)
  DAY(J)=30
ELSEIF(NMONTH(J).EQ.'JULY')THEN
  EVAPJ=EVAP(7)
  IRRDMJ=IRRDM(7)
  DAY(J)=31
ELSEIF(NMONTH(J).EQ.'AUGUST')THEN
  EVAPJ=EVAP(8)
  IRRDMJ=IRRDM(8)
  DAY(J)=31
ELSEIF(NMONTH(J).EQ.'SEPTEMBER')THEN
  EVAPJ=EVAP(9)

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```

IRRDMJ=IRRDM(9)
DAY(J)=30
ELSEIF(NMONTH(J).EQ.'OCTOBER')THEN
EVAPJ=EVAP(10)
IRRDMJ=IRRDM(10)
DAY(J)=31
ELSEIF(NMONTH(J).EQ.'NOVEMBER')THEN
EVAPJ=EVAP(11)
IRRDMJ=IRRDM(11)
DAY(J)=30
ELSEIF(NMONTH(J).EQ.'DECEMBER')THEN
EVAPJ=EVAP(12)
IRRDMJ=IRRDM(12)
DAY(J)=31
ENDIF
*****Calculation of Area & Capacity at Initial Level*****
DO 30 I=1,N
  IF(HA.LE.ELA(I).AND.HA.GT.ELA(I+1))THEN
    C1=(HA-ELA(I+1))/(ELA(I)-ELA(I+1))
    AREA=ARA(I+1)+C1*(ARA(I)-ARA(I+1))
    ASTORE=CAPA(I+1)+C1*(CAPA(I)-CAPA(I+1))
  ENDIF
30 CONTINUE
DO 40 I=1,M
  IF(HB.LE.ELB(I).AND.HB.GT.ELB(I+1))THEN
    C1=(HB-ELB(I+1))/(ELB(I)-ELB(I+1))
    BREA=ARB(I+1)+C1*(ARB(I)-ARB(I+1))
    BSTORE=CAPB(I+1)+C1*(CAPB(I)-CAPB(I+1))
  ENDIF
40 CONTINUE
GH=HA-HB
IF(IT.LE.7)THEN
  WRITE(3,5000)
  WRITE(3,6000)
  WRITE(3,5000)
  WRITE(3,5175)ASTORE,AREA,HA
  WRITE(4,5050)
  WRITE(4,6100)
  WRITE(4,5050)
  WRITE(4,5250)BSTORE,BREA,HB
  WRITE(20,5001)
  WRITE(20,6001)
  WRITE(20,5001)
  WRITE(20,*)'
ELSEIF(IT.GT.7.AND.IT.LE.14)THEN
  WRITE(10,5000)
  WRITE(10,6000)
  WRITE(10,5000)
  WRITE(10,5175)ASTORE,AREA,HA
  WRITE(16,5050)
  WRITE(16,6100)
  WRITE(16,5050)
  WRITE(16,5250)BSTORE,BREA,HB
  WRITE(21,5001)
  WRITE(21,6001)
  WRITE(21,5001)
  WRITE(21,*)'
ELSEIF(IT.GT.14.AND.IT.LE.21)THEN
  WRITE(11,5000)

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```

      WRITE(11,6000)
      WRITE(11,5000)
      WRITE(11,5175) ASTORE, AREA, HA
      WRITE(17,5050)
      WRITE(17,6100)
      WRITE(17,5050)
      WRITE(17,5250) BSTORE, BREA, HB
      WRITE(22,5001)
      WRITE(22,6001)
      WRITE(22,5001)
      WRITE(22,'')
      ELSEIF(IT.GT.21.AND.IT.LE.28)THEN
      WRITE(12,5000)
      WRITE(12,6000)
      WRITE(12,5000)
      WRITE(12,5175) ASTORE, AREA, HA
      WRITE(18,5050)
      WRITE(18,6100)
      WRITE(18,5050)
      WRITE(18,5250) BSTORE, BREA, HB
      WRITE(23,5001)
      WRITE(23,6001)
      WRITE(23,5001)
      WRITE(23,'')
      ELSEIF(IT.GT.28)THEN
      WRITE(13,5000)
      WRITE(13,6000)
      WRITE(13,5000)
      WRITE(13,5175) ASTORE, AREA, HA
      WRITE(19,5050)
      WRITE(19,6100)
      WRITE(19,5050)
      WRITE(19,5250) BSTORE, BREA, HB
      WRITE(24,5001)
      WRITE(24,6001)
      WRITE(24,5001)
      WRITE(24,'')
      ENDIF
*****Calculation of Area & Capacity at each period*****
      DATE=1
      SUMSP=0.
      SUMEP=0.
      SUMEN=0.
      SUMSYS=0.
      SUMSPB=0.
      SIRRD=0
      SPILLA=0
      NSP=0
      SDPIGG=0
      DO 100 K=1, DAY(J)
777 IF(K.EQ.1)THEN
      READ(26,8001) NNMONT
      READ(26,'') DT(1), QDAT(1), DT(2), QDAT(2), DT(3), QDAT(3), DT(4), QDAT(4)
      ELSEIF(K.EQ.11)THEN
      READ(26,'') DT(1), QDAT(1), DT(2), QDAT(2), DT(3), QDAT(3), DT(4), QDAT(4)
      ELSEIF(K.EQ.21)THEN
      READ(26,'') DT(1), QDAT(1), DT(2), QDAT(2), DT(3), QDAT(3), DT(4), QDAT(4)
      ENDIF
      IF(NNMONT.NE.NMONTH(J))THEN

```

```

READ(26,*) DT(1),QDAT(1),DT(2),QDAT(2),DT(3),QDAT(3),DT(4),QDAT(4)
READ(26,*) DT(1),QDAT(1),DT(2),QDAT(2),DT(3),QDAT(3),DT(4),QDAT(4)
GOTO 777
ENDIF
DO 2 I=1,NPEAK
2   QA(I)=QDAT(I)
SUMDT=0
DO 3 I=1,NPEAK
3   SUMDT=SUMDT+DT(I)
DT(5)=24.-SUMDT
DO 4 I=1,2
4   QP(I)=QA(I*2)
QA2=QA(2)
ASTEMP=0
SPIGG=0
SUMIR=0
DO 200 L=1,NPEAK+1
    INFLA=INFLAM(J)*DT(L)/(DAY(J)*24.)
    INFLB=INFLBM(J)*DT(L)/(DAY(J)*24.)
    IRRD=IRRDMJ*DT(L)/(DAY(J)*24.)
    IRR=IRRDMJ/DAY(J)
    EVAPLA=EVAPJ*AREA/1000*DT(L)/24.
    EVAPLB=EVAPJ*BREA/1000*DT(L)/24.
*****Calculation release from DAM A*****
IF(L.EQ.2.OR.L.EQ.4.OR.L.EQ.5)THEN
    QA(L)=0.0
    IF(L.EQ.4)QPUMP=QP(2)
    IF(L.EQ.5)QPUMP=0.0
    IF(NMONTH(J).EQ.'AUGUST'.AND.K.GT.20)QA(2)=QA2
    TP='NON-PEAK'
ENDIF
QRC=QA(L)
N5=0
*****Calculation adding release for irr.demand & evap.losses at B****
QIRR=IRRD+EVAPLB-INFLB-SPILLA
888  IF(QIRR.LT.0.OR.L.EQ.2.OR.L.EQ.4.OR.ASTORE.LT.SMDDLA)QIRR=0.
*****Calculation release for power generation*****
QR1=SMAXB-BSTORE
ASTORA=ASTORE+INFLA+QPUMP-EVAPLA-(QIRR+QR1)
IF(ASTORA.GE.SMDDLA)QR=QR1-EVAPLA-QIRR
QR=ASTORE-SMDDLA-EVAPLA-QIRR-ASTEMP
IF(ASTORA.EQ.SMAXA.AND.BSTORE.EQ.SMAXB)
1   QR=SMAXB-SMDDLB-EVAPLA-QIRR
IF(QR.LT.0.)QR=QR1-EVAPLA-QIRR
IF(QR.GT.QRC-QIRR)QR=QRC-QIRR
CALL CHECK(QR,QIRR,DT,DMAX,QR)
IF(QR.LT.0.)QR=0.0
IF(L.EQ.2.AND.NMONTH(J).EQ.'AUGUST'.AND.K.GT.20)QTEMP=QA2
IF(L.EQ.2.OR.L.EQ.4.OR.L.EQ.5)THEN
QR=0.0
IF(NMONTH(J).EQ.'AUGUST'.AND.K.GT.20)THEN
    IF(L.EQ.2)THEN
        QR=QTEMP-QIRR
        QPUMP=0.0
    ENDIF
ENDIF
IF(L.EQ.5)QPUMP=0.0
TP='NON-PEAK'
ENDIF

```

```

*****Calculation total release for power generation*****
    IF(QR.EQ.0) QIRR=0
*****Calculation for pumping up*****
    QPMAX=DPMAX*DT(L)*3600
    QP1=BSTORE-SMDDLB-EVAPLB-IRRD
    QA(L)=QR+QIRR
    ASTOR1=ASTORE+INFLA+QPUMP-EVAPLA-QA(L)
    IF(ASTOR1.LT.SMAXA) QPUMP=QP1-(IRR-SUMIR)
    IF(ASTOR1.GE.SMAXA) QPUMP=SMAXA-ASTORE-EVAPLB-IRRD-
1        (IRR-SUMIR)
    BSTOR1=BSTORE+INFLB+QA(L)-IRRD-EVAPLB-QPUMP
    IF(BSTOR1.LT.SMDDLB) QPUMP=BSTORE-SMDDLB-EVAPLB-IRRD-
1        (IRR-SUMIR)
    IF(QPUMP.GT.QP(L/2)) QPUMP=QP(L/2)
    IF(QPUMP.GT.QPMAX) QPUMP=QPMAX
    ASTOR1=ASTORE+INFLA+QPUMP-EVAPLA-QA(L)
    IF(ASTOR1.GE.SMAXA) QPUMP=0.0
    IF(QPUMP.LT.0.OR.L.EQ.5) QPUMP=0.0
    IF(L.EQ.2.AND.NMONTH(J).EQ.'AUGUST'.AND.K.GT.20) QPUMP=0.0
    IF(L.EQ.1.OR.L.EQ.3) THEN
        QPUMP=0.0
        TP='PEAK'
    ENDIF
*****Calculation of end storage at A*****
    ASTOR1=ASTORE+INFLA+QPUMP-EVAPLA-QA(L)
    SPILLA=ASTOR1-SMAXA
    IF(SPILLA.LT.0.) SPILLA=0.
    IF(SPILLA.GT.0.AND.(L.EQ.1.OR.L.EQ.3)) THEN
        QR=SMAXB-SMDDLB-EVAPLA-QIRR+SPILLA
        IF(QR.LT.0.) QR=SMAXB-BSTORE-EVAPLA-QIRR+SPILLA
        IF(QR.GT.QRC-QIRR) QR=QRC-QIRR
        CALL CHECK(QR,QIRR,DT,DMAX,QR)
        IF(QR.LT.0.) QR=0.0
        QA(L)=QR+QIRR
        ASTOR1=ASTORE+INFLA+QPUMP-EVAPLA-QA(L)
        IF(ASTOR1.GE.SMAXA) QPUMP=0.0
        ASTOR1=ASTORE+INFLA+QPUMP-EVAPLA-QA(L)
        SPILLA=ASTOR1-SMAXA
        IF(SPILLA.LT.0.) SPILLA=0.
    ENDIF
    ASTOR2=ASTOR1-SPILLA
    SA=.8*SMAXA
    SB=.8*SMAXB
    IF(ASTOR2.GT.SA.AND.BSTORE.GT.SB.AND.(L.EQ.1.OR.L.EQ.3))
1        QR=SMAXB-SMDDLB-EVAPLA-QIRR+SPILLA
        IF(QR.GT.QRC-QIRR) QR=QRC-QIRR
        CALL CHECK(QR,QIRR,DT,DMAX,QR)
        QA(L)=QR+QIRR
        ASTOR2=ASTORE+INFLA+QPUMP-EVAPLA-QA(L)-SPILLA
        IF(N5.EQ.250) THEN
            WRITE(*,*) 'Res.A may be Below MDDL, wait for Iteration process!'
            QR=ASTORE-SMDDLA-EVAPLA-QIRR-ASTEMP
            IF(L.EQ.2.OR.L.EQ.4.OR.QR.LT.0) QR=0.0
            IF(QR.GT.QRC-QIRR) QR=QRC-QIRR
            CALL CHECK(QR,QIRR,DT,DMAX,QR)
            QA(L)=QR+QIRR
            ASTORE=ASTORE+INFLA+QPUMP-EVAPLA-QA(L)
            GOTO 666
        ENDIF

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        IF(ASTOR2.LT.SMDDLA) THEN
          QIRR=0.0
C           IRRD=0.0
           N5=N5+1
           GOTO 888
        ENDIF
        ASTORE=ASTOR2
666      IF(ASTORE.LT.0)ASTORE=0
        IF(L.EQ.1.OR.L.EQ.3)ASTEMP=ASTORE-SMDDLA
        DO 70 I=1,N
          IF(ASTORE.LE.CAPA(I).AND.ASTORE.GT.CAPA(I+1)) THEN
            C2=CAPA(I)-CAPA(I+1)
            IF(C2.LE.0)GOTO 70
            C1=(ASTORE-CAPA(I+1))/(CAPA(I)-CAPA(I+1))
            AREA=ARA(I+1)+C1*(ARA(I)-ARA(I+1))
            HA=ELA(I+1)+C1*(ELA(I)-ELA(I+1))
            IF(HA.LT.HAMIN)HAMIN=HA
          ENDIF
          IF(HA.GE.KMDDLA.AND.HA.LE.BMDDLA)NMDDL=NMDDL+1
          NIT=NIT+1
70       CONTINUE
        IRRS=IRRD
        BSTOR1=BSTORE+INFLB+QA(L)-IRRS-EVAPLB-QPUMP+SPILLA
        IF(BSTOR1.LT.SMDDLB)THEN
          IRR1=0.0
          BSTOR2=BSTORE+INFLB+QA(L)-IRR1-EVAPLB-QPUMP+SPILLA
          IRRS=BSTOR2-SMDDLB-EVAPLB
          IF(IRRS.LT.0.)IRRS=0.0
        ENDIF
        BSTORE=BSTORE+INFLB+QA(L)-IRRS-EVAPLB-QPUMP+SPILLA
        IF(SMAXB.GT.BSTORE)THEN
          SPILLB=0.0
        ELSE
          SPILLB=BSTORE-SMAXB
          SUMSPB=SUMSPB+SPILLB
          BSTORE=SMAXB
        ENDIF
        IF(BSTORE.LT.0)BSTORE=0
        SUMIR=SUMIR+IRRS
        DO 90 I=1,M
          IF(BSTORE.LE.CAPB(I).AND.BSTORE.GT.CAPB(I+1)) THEN
            C2=CAPB(I)-CAPB(I+1)
            IF(C2.LE.0)GOTO 90
            C1=(BSTORE-CAPB(I+1))/(CAPB(I)-CAPB(I+1))
            BREB=ARB(I+1)+C1*(ARB(I)-ARB(I+1))
            HB=ELB(I+1)+C1*(ELB(I)-ELB(I+1))
            IF(HB.LE.HBMIN)HBMIN=HB
          ENDIF
90       CONTINUE.
        IF(IRRD.LE.0)THEN
          PIGG=0
          GOTO 5
        ENDIF
        PIGG=IRRS*100/IRRD
*****Energy Computation of U/S PH*****
5         IF(DT(L).EQ.0)THEN
          Q=0
          GOTO 6
        ENDIF

```

```

Q=QA(L)/(DT(L)*3600)
*****Calculation of nett Head*****
6   V=(Q/ND)/(PI*DIA*DIA/4)
      HF=(F*TL*V*V)/(2*9.81*DIA)
      HN=GH-HF
      SP=9.81*Q*HN*EFF/1000
      IF(SP.GT.0)NSP=NSP+1
      SUMSP=SUMSP+SP
      GH=HA-HB
      HN=GH-HF
      EP=9.81*Q*HN*EFF/1000
      SUMEP=SUMEP+EP
      AVEN=(SP+EP)/2*DT(L)
      SUMEN=SUMEN+AVEN
*****Energy Computation of D/S PH*****
      IF(DT(L).EQ.0)THEN
        QD=0
        GOTO 8
      ENDIF
      QD=IRRS/(DT(L)*3600)
8     IF(QD.GT.QDMAX)QD=QDMAX
      PD=9.81*QD*HD*EFF/1000
      END=PD*DT(L)
      ENSYS=AVEN+END
      SUMSYS=SUMSYS+ENSYS
      IF(SPILLA.GT.0)INFLB=SPILLA+INFLB
      IF(L.EQ.1)THEN
        IF(IT.LE.7)THEN
          WRITE(3,5100)DATE,TP,DT(L),INFLA,QPUMP,-EVAPLA,-QA(L),-SPILLA,
          1ASTORE,AREA,HA
          WRITE(4,5125)DATE,TP,DT(L),INFLB,QA(L),-IRRS,-EVAPLB,-QPUMP,
          1-SPILLB,BSTORE,BREA,HB
          WRITE(20,5126)DATE,TP,DT(L),GH,HN,Q,SP,EP,AVEN,QD,END,ENSYS,PIGG
          ELSEIF(IT.GT.7.AND.IT.LE.14)THEN
            WRITE(10,5100)DATE,TP,DT(L),INFLA,QPUMP,-EVAPLA,-QA(L),-SPILLA,
            1ASTORE,AREA,HA
            WRITE(16,5125)DATE,TP,DT(L),INFLB,QA(L),-IRRS,-EVAPLB,-QPUMP,
            1-SPILLB,BSTORE,BREA,HB
            WRITE(21,5126)DATE,TP,DT(L),GH,HN,Q,SP,EP,AVEN,QD,END,ENSYS,PIGG
            ELSEIF(IT.GT.14.AND.IT.LE.21)THEN
              WRITE(11,5100)DATE,TP,DT(L),INFLA,QPUMP,-EVAPLA,-QA(L),-SPILLA,
              1ASTORE,AREA,HA
              WRITE(17,5125)DATE,TP,DT(L),INFLB,QA(L),-IRRS,-EVAPLB,-QPUMP,
              1-SPILLB,BSTORE,BREA,HB
              WRITE(22,5126)DATE,TP,DT(L),GH,HN,Q,SP,EP,AVEN,QD,END,ENSYS,PIGG
              ELSEIF(IT.GT.21.AND.IT.LE.28)THEN
                WRITE(12,5100)DATE,TP,DT(L),INFLA,QPUMP,-EVAPLA,-QA(L),-SPILLA,
                1ASTORE,AREA,HA
                WRITE(18,5125)DATE,TP,DT(L),INFLB,QA(L),-IRRS,-EVAPLB,-QPUMP,
                1-SPILLB,BSTORE,BREA,HB
                WRITE(23,5126)DATE,TP,DT(L),GH,HN,Q,SP,EP,AVEN,QD,END,ENSYS,PIGG
                ELSEIF(IT.GT.28)THEN
                  WRITE(13,5100)DATE,TP,DT(L),INFLA,QPUMP,-EVAPLA,-QA(L),-SPILLA,
                  1ASTORE,AREA,HA
                  WRITE(19,5125)DATE,TP,DT(L),INFLB,QA(L),-IRRS,-EVAPLB,-QPUMP,
                  1-SPILLB,BSTORE,BREA,HB
                  WRITE(24,5126)DATE,TP,DT(L),GH,HN,Q,SP,EP,AVEN,QD,END,ENSYS,PIGG
                ENDIF
              ELSE
            
```

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        IF(DT(5).EQ.0.AND.L.EQ.5)GOTO 11
        IF(IT.LE.7)THEN
        WRITE(3,5150)TP,DT(L),INFLA,QPUMP,-EVAPLA,-QA(L),-SPILLA,
1ASTORE,AREA,HA
        WRITE(4,5200)TP,DT(L),INFLB,QA(L),-IRRS,-EVAPLB,-QPUMP,-SPILLB,
1BSTORE,BREA,HB
        WRITE(20,5201)TP,DT(L),GH,HN,Q,SP,EP,AVEN,QD,END,ENSYS,PIGG
ELSEIF(IT.GT.7.AND.IT.LE.14)THEN
        WRITE(10,5150)TP,DT(L),INFLA,QPUMP,-EVAPLA,-QA(L),-SPILLA,
1ASTORE,AREA,HA
        WRITE(16,5200)TP,DT(L),INFLB,QA(L),-IRRS,-EVAPLB,-QPUMP,-SPILLB,
1BSTORE,BREA,HB
        WRITE(21,5201)TP,DT(L),GH,HN,Q,SP,EP,AVEN,QD,END,ENSYS,PIGG
ELSEIF(IT.GT.14.AND.IT.LE.21)THEN
        WRITE(11,5150)TP,DT(L),INFLA,QPUMP,-EVAPLA,-QA(L),-SPILLA,
1ASTORE,AREA,HA
        WRITE(17,5200)TP,DT(L),INFLB,QA(L),-IRRS,-EVAPLB,-QPUMP,-SPILLB,
1BSTORE,BREA,HB
        WRITE(22,5201)TP,DT(L),GH,HN,Q,SP,EP,AVEN,QD,END,ENSYS,PIGG
ELSEIF(IT.GT.21.AND.IT.LE.28)THEN
        WRITE(12,5150)TP,DT(L),INFLA,QPUMP,-EVAPLA,-QA(L),-SPILLA,
1ASTORE,AREA,HA
        WRITE(18,5200)TP,DT(L),INFLB,QA(L),-IRRS,-EVAPLB,-QPUMP,-SPILLB,
1BSTORE,BREA,HB
        WRITE(23,5201)TP,DT(L),GH,HN,Q,SP,EP,AVEN,QD,END,ENSYS,PIGG
ELSEIF(IT.GT.28)THEN
        WRITE(13,5150)TP,DT(L),INFLA,QPUMP,-EVAPLA,-QA(L),-SPILLA,
1ASTORE,AREA,HA
        WRITE(19,5200)TP,DT(L),INFLB,QA(L),-IRRS,-EVAPLB,-QPUMP,-SPILLB,
1BSTORE,BREA,HB
        WRITE(24,5201)TP,DT(L),GH,HN,Q,SP,EP,AVEN,QD,END,ENSYS,PIGG
ENDIF
11      ENDIF
        SPIGG=SPIGG+PIGG
        SIRRD=SIRRD+IRRS
200     CONTINUE
        DATE=DATE+1
        DPIGG=SPIGG/(NPEAK+1)
        IF(DT(5).EQ.0)DPIGG=SPIGG/NPEAK
        SDPIGG=SDPIGG+DPIGG
        IF(K.EQ.10)AV1=SDPIGG/10
        IF(K.EQ.20)AV2=(SDPIGG-AV1*10)/10
        IF(K.EQ.DAY(J))AV3=(SDPIGG-AV1*10-AV2*10)/(DAY(J)-20)
100    CONTINUE
        IF(NMONTH(J).EQ.'JANUARY')THEN
        SV11=SV11+AV1
        SV21=SV21+AV2
        SV31=SV31+AV3
        NJAN=NJAN+1
ELSEIF(NMONTH(J).EQ.'FEBRUARY')THEN
        SV12=SV12+AV1
        SV22=SV22+AV2
        SV32=SV32+AV3
        NFEB=NFEB+1
ELSEIF(NMONTH(J).EQ.'MARCH')THEN
        SV13=SV13+AV1
        SV23=SV23+AV2
        SV33=SV33+AV3
        NMAR=NMAR+1

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ELSEIF (NMMONTH(J) .EQ. 'APRIL') THEN
    SV14=SV14+AV1
    SV24=SV24+AV2
    SV34=SV34+AV3
    NAPR=NAPR+1
ELSEIF (NMMONTH(J) .EQ. 'MAY') THEN
    SV15=SV15+AV1
    SV25=SV25+AV2
    SV35=SV35+AV3
    NMAY=NMAY+1
ELSEIF (NMMONTH(J) .EQ. 'JUNE') THEN
    SV16=SV16+AV1
    SV26=SV26+AV2
    SV36=SV36+AV3
    NJUN=NJUN+1
ELSEIF (NMMONTH(J) .EQ. 'JULY') THEN
    SV17=SV17+AV1
    SV27=SV27+AV2
    SV37=SV37+AV3
    NJUL=NJUL+1
ELSEIF (NMMONTH(J) .EQ. 'AUGUST') THEN
    SV18=SV18+AV1
    SV28=SV28+AV2
    SV38=SV38+AV3
    NAUG=NAUG+1
ELSEIF (NMMONTH(J) .EQ. 'SEPTEMBER') THEN
    SV19=SV19+AV1
    SV29=SV29+AV2
    SV39=SV39+AV3
    NSEP=NSEP+1
ELSEIF (NMMONTH(J) .EQ. 'OCTOBER') THEN
    SV110=SV110+AV1
    SV210=SV210+AV2
    SV310=SV310+AV3
    NOCT=NOCT+1
ELSEIF (NMMONTH(J) .EQ. 'NOVEMBER') THEN
    SV111=SV111+AV1
    SV211=SV211+AV2
    SV311=SV311+AV3
    NNOV=NNOV+1
ELSEIF (NMMONTH(J) .EQ. 'DECEMBER') THEN
    SV112=SV112+AV1
    SV212=SV212+AV2
    SV312=SV312+AV3
    NDEC=NDEC+1
ENDIF
C
    IR='NON-SUCCEED'
    DEL=ABS(SIRRD-IRRDMJ)
    IF(IRRDMJ.EQ.0) GOTO 7
    AR=SIRRD*100/IRRDMJ
    TOL=DEL/IRRDMJ
    IF(SIRRD.GE.IRRDMJ.OR.TOL.LT.0.01) IR='SUCCEED'
7   IF(IRRDMJ.EQ.0) IR=' '
    AVSP=SUMSP/NSP
    AVEP=SUMEP/NSP
    TEN=TEN+SUMEN
    TSYS=TSYS+SUMSYS
    TOTSPB=TOTSPB+SUMSPB
    TINFLM(J)=INFLAM(J)+INFLBM(J)

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    IF(SIRR.D.GE.IRRDMJ.OR.TOL.LT.0.01.OR.IRRDMJ.EQ.0)THEN
      WRITE(8,7525)NMONT(J),INFLAM(J),INFLBM(J),TINFLM(J),IRRDMJ,
      1EVAPJ,SIRR.D,IR,AVSP,AVEP,SUMEN,SUMSPB
      GOTO 88
    ENDIF
    WRITE(8,7526)NMONT(J),INFLAM(J),INFLBM(J),TINFLM(J),IRRDMJ,
    1EVAPJ,SIRR.D,AR,AVSP,AVEP,SUMEN,SUMSPB
  88 TINFLA=TINFLA+INFLAM(J)
    TINFLB=TINFLB+INFLBM(J)
    TTINFL=TTINFL+TINFLM(J)
    SSIRR.D=SSIRR.D+SIRR.D
    SIRRDM=SIRRDM+IRRDMJ
    IF(IT.LE.7)THEN
      WRITE(3,5000)
      WRITE(4,5050)
      WRITE(4,7000)-SUMSPB
      WRITE(20,5001)
      WRITE(20,7002)SUMEN,SUMSYS
      WRITE(20,7001)AV1,AV2,AV3
    ELSEIF(IT.GT.7.AND.IT.LE.14)THEN
      WRITE(10,5000)
      WRITE(16,5050)
      WRITE(16,7000)-SUMSPB
      WRITE(21,5001)
      WRITE(21,7002)SUMEN,SUMSYS
      WRITE(21,7001)AV1,AV2,AV3
    ELSEIF(IT.GT.14.AND.IT.LE.21)THEN
      WRITE(11,5000)
      WRITE(17,5050)
      WRITE(17,7000)-SUMSPB
      WRITE(22,5001)
      WRITE(22,7002)SUMEN,SUMSYS
      WRITE(22,7001)AV1,AV2,AV3
    ELSEIF(IT.GT.21.AND.IT.LE.28)THEN
      WRITE(12,5000)
      WRITE(18,5050)
      WRITE(18,7000)-SUMSPB
      WRITE(23,5001)
      WRITE(23,7002)SUMEN,SUMSYS
      WRITE(23,7001)AV1,AV2,AV3
    ELSEIF(IT.GT.28)THEN
      WRITE(13,5000)
      WRITE(19,5050)
      WRITE(19,7000)-SUMSPB
      WRITE(24,5001)
      WRITE(24,7002)SUMEN,SUMSYS
      WRITE(24,7001)AV1,AV2,AV3
    ENDIF
  150 CONTINUE
  CLOSE(26)
  NNMDDL=NNMDDL+NMDDL
  NNIT=NNIT+NIT
  GTEN=GTEN+TEN
  GSYS=GSYS+TSYS
  PMDDL=FLOAT(NMDDL)/(NIT)*100
  PSIRR=SSIRR.D/SIRRDM*100
  SPIRR=SPIRR+PSIRR
  *****Write the Output*****
  WRITE(8,7575)

```

```

      WRITE(8,7600)TINFLA,TINFLB,TTINFL,SIRRDM,SSIRR,D,PSIRR,TEN,TOTSPB
      WRITE(9,7602)NYEAR,TTINFL,SIRRDM,SSIRR,D,PSIRR,TEN,TOTSPB,HAMIN,
      1HBMIN,TSYS
      IF(IT.LE.7)THEN
        WRITE(4,7000)TOTSPB
        WRITE(20,7003)TEN,TSYS
      ELSEIF(IT.GT.7.AND.IT.LE.14)THEN
        WRITE(16,7000)TOTSPB
        WRITE(21,7003)TEN,TSYS
      ELSEIF(IT.GT.14.AND.IT.LE.21)THEN
        WRITE(17,7000)TOTSPB
        WRITE(22,7003)TEN,TSYS
      ELSEIF(IT.GT.21.AND.IT.LE.28)THEN
        WRITE(18,7000)TOTSPB
        WRITE(23,7003)TEN,TSYS
      ELSEIF(IT.GT.28)THEN
        WRITE(19,7000)TOTSPB
        WRITE(24,7003)TEN,TSYS
      ENDIF
C      WRITE(8,7500)PMDDL
      WRITE(8,7601)ELA(1),MDDLA,HAMIN,ELB(1),MDDLB,HBMIN
      WRITE(*,4000)IT,MYEAR
      IF(HAMIN.LT.HHAMIN)HHAMIN=HAMIN
      IF(HBMIN.LT.HHBMIN)HHBMIN=HBMIN
28  CONTINUE
      AV(1,1)=SV11/NJAN
      AV(1,2)=SV21/NJAN
      AV(1,3)=SV31/NJAN
      AV(2,1)=SV12/NFEB
      AV(2,2)=SV22/NFEB
      AV(2,3)=SV32/NFEB
      AV(3,1)=SV13/NMAR
      AV(3,2)=SV23/NMAR
      AV(3,3)=SV33/NMAR
      AV(4,1)=SV14/NAPR
      AV(4,2)=SV24/NAPR
      AV(4,3)=SV34/NAPR
      AV(5,1)=SV15/NMAY
      AV(5,2)=SV25/NMAY
      AV(5,3)=SV35/NMAY
      AV(6,1)=SV16/NJUN
      AV(6,2)=SV26/NJUN
      AV(6,3)=SV36/NJUN
      AV(7,1)=SV17/NJUL
      AV(7,2)=SV27/NJUL
      AV(7,3)=SV37/NJUL
      AV(8,1)=SV18/NAUG
      AV(8,2)=SV28/NAUG
      AV(8,3)=SV38/NAUG
      AV(9,1)=SV19/NSEP
      AV(9,2)=SV29/NSEP
      AV(9,3)=SV39/NSEP
      AV(10,1)=SV110/NOCT
      AV(10,2)=SV210/NOCT
      AV(10,3)=SV310/NOCT
      AV(11,1)=SV111/NNOV
      AV(11,2)=SV211/NNOV
      AV(11,3)=SV311/NNOV
      AV(12,1)=SV112/NDEC

```

```

AV(12,2)=SV212/NDEC
AV(12,3)=SV312/NDEC

PPMDDL=FLOAT(NNMDDL) / (NNIT)*100
AVIRR=SPIRR/MYEAR
AVGTE=GTEN/MYEAR
AVGSY=GSYS/MYEAR
WRITE(8,7603)HHAMIN,HHBMIN
WRITE(9,7542)
WRITE(9,7553)AVIRR,AVGTE,AVGSY
WRITE(9,7552)
WRITE(9,7603)HHAMIN,HHBMIN
WRITE(9,8019)
DO 99 I=1,12
99   WRITE(9,8020)NMONT(I),(AV(I,J),J=1,3)
*****Format the Output*****
4000 FORMAT(' PROCESSING THE NO.',I3,' OF ',I3,' YEAR DATA')
5000 FORMAT('=====
1'=====
      ')
5001 FORMAT('=====
1'=====
      ')
5050 FORMAT('=====
1'=====
      ')
5100 FORMAT(I3,1X,A9,F10.2,5F10.0,2E10.3,F10.2)
5125 FORMAT(I3,1X,A9,F10.2,6F10.0,2E10.3,F10.2)
5126 FORMAT(I3,1X,A9,F10.2,10F9.0)
5150 FORMAT(4X,A9,F10.2,5F10.0,2E10.3,F10.2)
5175 FORMAT(73X,2E10.3,F10.2)
5200 FORMAT(4X,A9,F10.2,6F10.0,2E10.3,F10.2)
5201 FORMAT(4X,A9,F10.2,10F9.0)
5250 FORMAT(83X,2E10.3,F10.2)
6000 FORMAT(
1' DATE PERIOD DURATION INFLA QPUMP EVAPLA QA ',
2' SPILLA STOREA AREA EL.A'/
3'           (HR) (M3) (M3) (M3) (M3) (M3) ,
4'       (M3)     (M3)     (M2)     (M) ')
6001 FORMAT(
1'DATE PERIOD DURATION GROSSH NETTH Q STARTP ,
2'ENDP AV.ENERGY QD ENERGY TOT.ENERGY IRR.'/
3'           (HR) (M) (M) (M3/S) (MW) ,
4'       (MW)     (MWh) (M3/S)     (MWh)     (%) ')
6100 FORMAT(
1'DATE PERIOD DURATION INFLB QA IRRS EVAPLB',
2' QPUMP SPILLB STOREB BREA EL.B '/
3'           (HR) (M3) (M3) (M3) (M3) (M3) ,
4'       (M3)     (M3)     (M3)     (M2)     (M) ')
7000 FORMAT(74X,E9.3)
7001 FORMAT(2X,'AVERAGE % 10 DAILY IRR.SUPPLY =',53X,3F9.2)
7002 FORMAT(2X,'T O T A L          =',35X,F9.0,18X,F9.0)
7003 FORMAT(2X,'T O T A L A N N U A L          =',35X,F9.0,18X,F9.0)
C 7500 FORMAT(2X,'REACH OF MDDL AT A = ',F9.2,' %')
7525 FORMAT(A10,4E10.4,F6.2,E10.4,1X,A11,2F8.2,F9.0,E9.3)
7526 FORMAT(A10,4E10.4,F6.2,E10.4,1X,F7.2,'%',3X,2F8.2,F9.0,E9.3)
7550 FORMAT(/'SUMMARY OF RESERVOIR OPERATION ',I5/
1'=====
2'=====
      ')
3'MONTH           RUNOFF        TOTAL    IRRIG.  EVAP.  IRRIG',
4'  IRRIG.        AV. POWER    AV. ENERGY SPILL'/
5'  OF            A             B           DEMAND LOSS SUPPL',

```

```

6'Y      DEMAND      START      END  GENERATED  AT B'/
1'          (M3)      (M3)      (M3)      (M3)      (MM/D)  (M3)',,
2'      STATUS      (MW)      (MW)      (MWh)      (M3)'/
7'=====',
8'=====')
7551 FORMAT ('SUMMARY OF TOTAL RESERVOIR OPERATION ')
1'=====',
1'=====')/
2'YEAR    TOTAL    IRRIG.   IRRIG.   IRRIG. AV.ENERGY SPILL  ,
2' HA      HB TOT. SYSTEM'/
3' OF     INFLOW    DEMAND   SUPPLY   DEMAND GENERATED AT B  ,
3' MIN     MIN EN.GENERATE'/
4'          (M3)      (M3)      (M3)      STATUS   (MWh)      (M3)  ,
4'      (M)      (M)      (MWh)'/
5'=====',
5'=====')
7542 FORMAT(
1'--',
2'-----')
7552 FORMAT(
1'=====',
2'=====')
7553 FORMAT ('AVERAGE =',27X,F6.2,'%',E9.3,27X,E9.3)
7575 FORMAT(
1'=====',
2'=====')
7600 FORMAT(10X,4E10.4,6X,E10.4,2X,F6.2,'%',19X,F9.0,E9.3/)
7601 FORMAT(2X,'FRL. AT A      = ',F9.2,' M'/
1      2X,'MDDL. AT A      = ',F9.2,' M'/
2      2X,'MIN.ELEVATION AT A = ',F9.2,' M'//,
3      2X,'FRL. AT B      = ',F9.2,' M'/
4      2X,'MDDL. AT B      = ',F9.2,' M'/
5      2X,'MIN.ELEVATION AT B = ',F9.2,' M')
7602 FORMAT(I4,3E10.4,2X,F6.2,'%',2E9.3,2F9.2,E9.3)
7603 FORMAT(2X,'MIN.ELEVATION AT A = ',F9.2,' M'/
2      2X,'MIN.ELEVATION AT B = ',F9.2,' M'/)
C   3      2X,'TOT.ENERGY GENERATE= ',E9.4,' MWh')
8000 FORMAT(2F13.2,A10)
8001 FORMAT(A10)
8019 FORMAT(
1'=====',
2' 10 DAYS & AVERAGE MEETING IRR. DEMAND',//,
3'  MONTH      1st      2nd      3rd  ',/
5'=====')
8020 FORMAT(2X,A10,3F9.2)
9000 FORMAT(/2X,'MONTH OF : ',A10,' YEAR : 'I5,2X,'OPERATION AT RESERVO
1IIR',A2)
9001 FORMAT(/2X,'MONTH OF : ',A10,' YEAR : 'I5,2X,'ENERGY GENERATION IN
1 U/S, D/S POWER HOUSE AND % MEETING IRR.DEMAND')
STOP
END

SUBROUTINE CHECK(QR,QIRR,DT,DMAX,QR1)
QA=QR+QIRR
DQR=QA/(DT*3600)
IF(DQR.GT.DMAX)QR1=DMAX*DT*3600-QIRR
RETURN
END

```

APPENDIX IID

Instruction for User

DROPS INSTALLATION AND EXECUTION

The DROPS software is written in FORTRAN 77 language for the IBM/PC/XT/AT and true compatible. It requires 512K RAM and MS-DOS 3.2 or higher.

The software uses the notation and procedures developed in:
SURYAKENCANA, D., RESERVOIR OPERATIONS FOR PUMPED STORAGE SCHEME - A CASE STUDY, Water Resources Development Training Centre, University of Roorkee, India - 2000.

DROPS should be executed from the hard disk (c:).

DISKETTE CONTENTS:

README.DOC
DROPS.EXE
DROPS.FOR
RACAP.DAT
RBCAP.DAT
EVAP.DAT
IRRDM.DAT
INTEHRI.DAT
SCHEME.DAT
SCHEDULE.DAT

7 example-data files needed (*.dat) taken from ., RESERVOIR OPERATIONS FOR PUMPED STORAGE SCHEME - A CASE STUDY

INSTALLATION ON HARD DISK:

Make a separate directory named DROPS (or any other name of your choice) and copy all the contents of this diskette into the created directory.

STEP-BY-STEP HARD DISK INSTALLATION:

1. Turn on the computer.
2. Make new directory named DROPS:
At the DOS prompt C:>, type md DROPS and press ENTER (or RETURN) key.
3. At the DOS prompt C:>, type cd DROPS and press ENTER.
4. Place the DROPS diskette in the 3.5" (or 5.25") drive (A or B).
5. At the DOS prompt C:\DROPS>, type copy a:\DROPS*.* (if diskette is in drive A)
copy b:\DROPS*.* (if diskette is in drive B) and press ENTER.
6. The installation is now complete.

EXECUTION:

To execute DROPS from the directory in which it is installed, type DROPS and then press ENTER. The software is NOT totally menu driven and hence requires instruction manual.

These Menu and Comment will be appear on your monitor:

```
C:\>DROPS
***** PROGRAM DROPS *****
* Program of Reservoir Operation *
* for Pumped Storage Scheme with 2 Reservoir *
* (C) Dinny Suryakencana-2000 *
*****
File Name for Input Data of Inflow to A & B Res.
INTEHRI.DAT
Your Output file name will be :
ROAINTx.OUT, ROBINTx.OUT, ENGINTx.OUT, SROINTx.OUT
Do you want use File Data SCHEDULE.DAT?
1) Yes !
2) No !
    Choose 1 or 2
1
Do you want use File Data SCHEME.DAT?
1) Yes !
2) No !
    Choose 1 or 2
1
Please Wait for Data Processing!
PROCESSING THE NO. 1 OF 35 YEAR DATA
PROCESSING THE NO. 2 OF 35 YEAR DATA
PROCESSING THE NO. 3 OF 35 YEAR DATA
PROCESSING THE NO. 4 OF 35 YEAR DATA
PROCESSING THE NO. 5 OF 35 YEAR DATA
PROCESSING THE NO. 6 OF 35 YEAR DATA
PROCESSING THE NO. 7 OF 35 YEAR DATA
PROCESSING THE NO. 8 OF 35 YEAR DATA
PROCESSING THE NO. 9 OF 35 YEAR DATA
PROCESSING THE NO. 10 OF 35 YEAR DATA
PROCESSING THE NO. 11 OF 35 YEAR DATA
PROCESSING THE NO. 12 OF 35 YEAR DATA
PROCESSING THE NO. 13 OF 35 YEAR DATA
PROCESSING THE NO. 14 OF 35 YEAR DATA
PROCESSING THE NO. 15 OF 35 YEAR DATA
PROCESSING THE NO. 16 OF 35 YEAR DATA
PROCESSING THE NO. 17 OF 35 YEAR DATA
PROCESSING THE NO. 18 OF 35 YEAR DATA
PROCESSING THE NO. 19 OF 35 YEAR DATA
PROCESSING THE NO. 20 OF 35 YEAR DATA
PROCESSING THE NO. 21 OF 35 YEAR DATA
PROCESSING THE NO. 22 OF 35 YEAR DATA
PROCESSING THE NO. 23 OF 35 YEAR DATA
PROCESSING THE NO. 24 OF 35 YEAR DATA
PROCESSING THE NO. 25 OF 35 YEAR DATA
PROCESSING THE NO. 26 OF 35 YEAR DATA
PROCESSING THE NO. 27 OF 35 YEAR DATA
PROCESSING THE NO. 28 OF 35 YEAR DATA
PROCESSING THE NO. 29 OF 35 YEAR DATA
PROCESSING THE NO. 30 OF 35 YEAR DATA
PROCESSING THE NO. 31 OF 35 YEAR DATA
PROCESSING THE NO. 32 OF 35 YEAR DATA
PROCESSING THE NO. 33 OF 35 YEAR DATA
PROCESSING THE NO. 34 OF 35 YEAR DATA
PROCESSING THE NO. 35 OF 35 YEAR DATA
Stop - Program terminated
```

OR

```
C:\>DROPS
***** PROGRAM DROPS *****
* Program of Reservoir Operation *
* for Pumped Storage Scheme with 2 Reservoir *
* (C) Dinny Suryakencana-2000 *
*****
File Name for Input Data of Inflow to A & B Res.
Your Output file name will be :
ROAINTx.OUT, ROBINTx.OUT, ENGINTx.OUT, SROINTx.OUT
Do you want use File Data SCHEDULE.DAT?
1) Yes !
2) No !
Choose 1 or 2
1
Do you want use File Data SCHEME.DAT?
1) Yes !
2) No !
Choose 1 or 2
2
INPUT EFFICIENCY FACTOR OF M/C & TURBINE =
.85
INPUT FRICTION LOSSES FACTOR =
.02
INPUT LENGTH OF POWER TUNNEL (M) =
1100
INPUT DIAMETER OF POWER TUNNEL (M) =
8.5
INPUT NUMBER OF POWER TUNNEL =
2
INPUT MDDL AT RESERVOIR A (M) =
740.0
INPUT MDDL AT RESERVOIR B (M) =
598.5
INPUT DISCHARGE MAX. FOR RELEASE (CUMEC) =
1235.42
INPUT DISCHARGE MAX. FOR PUMPING (CUMEC) =
595.96
INPUT DISCHARGE MAX. FOR D/S POWERHOUSE =
639.60
INPUT INITIAL EL. AT RESERVOIR A (M) =
830
INPUT INITIAL EL. AT RESERVOIR B (M) =
598.5
INPUT NETT HEAD OF D/S POWERHOUSE (M) =
75
Please Wait for Data Processing!
PROCESSING THE NO. 1 OF 35 YEAR DATA
PROCESSING THE NO. 2 OF 35 YEAR DATA
PROCESSING THE NO. 3 OF 35 YEAR DATA
PROCESSING THE NO. 4 OF 35 YEAR DATA
PROCESSING THE NO. 5 OF 35 YEAR DATA
PROCESSING THE NO. 6 OF 35 YEAR DATA
PROCESSING THE NO. 7 OF 35 YEAR DATA
PROCESSING THE NO. 8 OF 35 YEAR DATA
```

PROCESSING THE NO. 9 OF 35 YEAR DATA
 PROCESSING THE NO. 10 OF 35 YEAR DATA
 PROCESSING THE NO. 11 OF 35 YEAR DATA
 PROCESSING THE NO. 12 OF 35 YEAR DATA
 PROCESSING THE NO. 13 OF 35 YEAR DATA
 PROCESSING THE NO. 14 OF 35 YEAR DATA
 PROCESSING THE NO. 15 OF 35 YEAR DATA
 PROCESSING THE NO. 16 OF 35 YEAR DATA
 PROCESSING THE NO. 17 OF 35 YEAR DATA
 PROCESSING THE NO. 18 OF 35 YEAR DATA
 PROCESSING THE NO. 19 OF 35 YEAR DATA
 PROCESSING THE NO. 20 OF 35 YEAR DATA
 PROCESSING THE NO. 21 OF 35 YEAR DATA
 PROCESSING THE NO. 22 OF 35 YEAR DATA
 PROCESSING THE NO. 23 OF 35 YEAR DATA
 PROCESSING THE NO. 24 OF 35 YEAR DATA
 PROCESSING THE NO. 25 OF 35 YEAR DATA
 PROCESSING THE NO. 26 OF 35 YEAR DATA
 PROCESSING THE NO. 27 OF 35 YEAR DATA
 PROCESSING THE NO. 28 OF 35 YEAR DATA
 PROCESSING THE NO. 29 OF 35 YEAR DATA
 PROCESSING THE NO. 30 OF 35 YEAR DATA
 PROCESSING THE NO. 31 OF 35 YEAR DATA
 PROCESSING THE NO. 32 OF 35 YEAR DATA
 PROCESSING THE NO. 33 OF 35 YEAR DATA
 PROCESSING THE NO. 34 OF 35 YEAR DATA
 PROCESSING THE NO. 35 OF 35 YEAR DATA

Stop - Program terminated.

Output files:

The program will be automatically divide the output file in every 8 years data,

ROAXXXx : ROA = Reservoir Operation at A,
 XXX = Three initial first letter from input of Inflow data file
 x = Number of file automatically given by program,
 start from 0

ROBXXXx : ROB = Reservoir Operation at B,
 XXX = Three initial first letter from input of Inflow data file
 x = Number of file automatically given by program,
 start from 0

ENGXXXx : ENG = Total Energy Generated,
 XXX = Three initial first letter from input of Inflow data file
 x = Number of file automatically given by program,
 start from 0

SROXXXx : SRO = Summary of Reservoir Operation,
 XXX = Three initial first letter from input of Inflow data file
 x = Number of file automatically given by program, 0 and 1

COMMENTS AND INQUIRIES:

If you have any comments or questions about this software,
please direct them to the author at the address below:

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□

APPENDIX IIIA

Input of Program

Input to computer program (DROPS program) of reservoir operation model consist of the storage-elevation curve and the area-elevation curve for each reservoir (File name "RACAP.DAT" and "RBCAP.DAT"), value of FRL, MDDL of each reservoir, and data of physical construction (File name "SCHEME.DAT") are read in. This program also facilitated with interactive input of physical construction data if needed. The following input data has been computerized:

1. Inflow into. (File name is "INTEHRI.DAT")
2. Evaporation losses. (File name "EVAP.DAT")
3. Irrigation demand. (File name "IRRDM.DAT")

FILE NAME : **RACAP.DAT** (=Reservoir A CAPacity DATA)

| | | |
|-------------|----------------|-----------------|
| 12 | | |
| 830.0000000 | 43800000.00000 | 3540000000.0000 |
| 820.0000000 | 40000000.00000 | 3150000000.0000 |
| 810.0000000 | 36500000.00000 | 2780000000.0000 |
| 800.0000000 | 33000000.00000 | 2420000000.0000 |
| 790.0000000 | 30300000.00000 | 2110000000.0000 |
| 780.0000000 | 27600000.00000 | 1820000000.0000 |
| 770.0000000 | 25000000.00000 | 1550000000.0000 |
| 760.0000000 | 22400000.00000 | 1315000000.0000 |
| 750.0000000 | 19850000.00000 | 1100000000.0000 |
| 740.0000000 | 17300000.00000 | 925000000.0000 |
| 730.0000000 | 15550000.00000 | 735000000.0000 |
| 720.0000000 | 13800000.00000 | 590000000.0000 |

- Here we wrote first line the number of data we have for Reservoir
- First column are Elevation in Meter
- Second column are Surface Area in M² and
- Third column are Capacity in M³

FILE NAME : RBCAP.DAT (=Reservoir B CAPacity DATA)

```

6
612.000 2550000.00 85520000.0
610.000 2400000.00 80200000.0
600.000 2040000.00 58000000.0
590.000 1650000.00 38900000.0
580.000 1290000.00 20800000.0
570.000 900000.00 11400000.0

```

Here wrote same as in RACAP.DAT

FILE NAME : SCHEME.DAT (data of physical construction)

```
.85 .02 1100 8.5 2 740.00 598.50 1235.42 595.96 639.60 830 598.50 75
```

Here we wrote respectively:

Efficiency factor of M/C and turbine, Friction losses factor, Length of power tunnel in M, Diameter of power tunnel in M, Number of power tunnel, MDDL at reservoir A in M, MDDL at reservoir B in M, Maximum discharge for release from A in M³/Sec., Maximum discharge for pumping from B in M³/Sec., Maximum discharge for D/S powerhouse in M³/Sec., Initial elevation at reservoir A in M, Initial elevation at reservoir B in M, and Net head of D/S powerhouse.

FILE NAME : EVAP.DAT (=EVAPoration losses DATA)

```

12 Monthly Evaporation mm/day
1.258 JAN
2.036 FEB
3.290 MAR
5.733 APR
6.774 MAY
6.433 JUN
4.000 JUL
3.484 AUG
3.600 SEP
3.258 OCT
2.267 NOV
1.355 DEC

```

FILE NAME : IRRDM.DAT (=IRRigation DeMand DATA)

12 Monthly Irrigation Demand (M3)
 653200000 JAN
 639400000 FEB
 607400000 MAR
 559000000 APR
 684200000 MAY
 479500000 JUN
 0.0 JUL
 0.0 AUG
 0.0 SEP
 176200000 OCT
 341200000 NOV
 465800000 DEC

FILE NAME : SCHEDULE.DAT (=reservoir operation SCHEDULE DATA)

JANUARY
 3 13300000 6 0 4 17790000 8 10130000
 3.5 15150000 6 0 4 17510000 8 10710000
 3.8 16350000 6 0 4 17280000 8 11170000
 FEBRUARY
 4 17050000 6 0 4 17050000 8 10250000
 3.5 14630000 6 0 4 16820000 8 12100000
 4 16470000 6 0 4 16470000 8 12290000
 MARCH
 4 16240000 6 0 4 16240000 7.1 11660000
 4 15900000 6 0 4 15900000 8 10890000
 4 15650000 6 0 4 15650000 6.8 12090000
 APRIL
 4 15320000 6 0 4 15320000 7.4 13360000
 4 15090000 6 0 4 15090000 6.7 12300000
 4 14860000 6 0 4 14860000 4.8 9070000
 MAY
 4 14510000 6 0 4 14510000 2.7 5260000
 4 14170000 6 0 4 14170000 3.4 6740000
 4 14050000 6 0 4 14050000 2.5 5030000
 JUNE
 4 13710000 6 0 4 13710000 1.8 3830000
 4 13360000 6 0 4 13360000 1.1 2360000
 4 13360000 6 0 4 13360000 5.5 11790000
 JULY
 4 13590000 6 0 4 13590000 5.9 12320000
 4 14170000 6 0 4 14170000 7.4 14520000
 2.6 10380000 6 0 4 15670000 8 13820000
 AUGUST
 1.2 5160000 6 0 4 17280000 8 11290000
 0.5 1960000 6 0 4 17390000 8 9330000
 4 16930000 1.1 4760000 4 16930000 0 0
 SEPTEMBER
 4 16620000 6 0 4 16820000 0 0
 3.8 15920000 6 0 4 16820000 8 8640000
 2.4 10050000 6 0 4 16820000 8 8640000
 (to be continued)

OCTOBER

| | | | | | | | |
|-----|---------|---|---|---|----------|---|---------|
| 2.1 | 9010000 | 6 | 0 | 4 | 16820000 | 8 | 8640000 |
| 2.2 | 9160000 | 6 | 0 | 4 | 16930000 | 8 | 8640000 |
| 1 | 4290000 | 6 | 0 | 4 | 17050000 | 8 | 8640000 |

NOVEMBER

| | | | | | | | |
|-----|---------|---|---|---|----------|---|---------|
| 0.6 | 2650000 | 6 | 0 | 4 | 17050000 | 8 | 8640000 |
| 0.7 | 3020000 | 6 | 0 | 4 | 17050000 | 8 | 8750000 |
| 0.8 | 3300000 | 6 | 0 | 4 | 17160000 | 8 | 8750000 |

DECEMBER

| | | | | | | | |
|------|----------|---|---|---|----------|-----|---------|
| 2.3 | 10920000 | 6 | 0 | 4 | 17160000 | 8 | 8990000 |
| 2.7 | 11730000 | 6 | 0 | 4 | 17390000 | 8 | 9330000 |
| 2.02 | 9000000 | 6 | 0 | 4 | 17720000 | 4.6 | 5610000 |

- Here we wrote first line the name of month
- First column are first peak hour duration
- Second column are volume of water release in M^3
- Third column are first non-peak hour duration
- Fourth column are volume of water pumping in M^3
- Fifth column are second peak hour duration
- Sixth column are volume of water release in M^3
- Seventh column are second non-peak hour duration
- Eighth column are volume of water pumping in M^3

FILE NAME : INTEHRI.DAT (=Inflow to reservoir DATA)

```

35
1963 3 Monthly inflow of A, B (M3)
431000000      0.0 OCTOBER
263000000      0.0 NOVEMBER
207000000      0.0 DECEMBER
1964 12
174000000      0.0 JANUARY
175000000      0.0 FEBRUARY
178000000      0.0 MARCH
185000000      0.0 APRIL
254000000      0.0 MAY
877000000      0.0 JUNE
1329000000     0.0 JULY
1241000000     0.0 AUGUST
567000000      0.0 SEPTEMBER
267000000      0.0 OCTOBER
207000000      0.0 NOVEMBER
189000000      0.0 DECEMBER

```

(to be continued)

- Here we wrote first line the number of year we have for inflow to Reservoir
- Second line name of year and number of month in that year
- First column are monthly inflow to reservoir A in M^3
- Second column are monthly inflow to reservoir B in M^3
- Third column are name of month

APPENDIX IIIB

Output of Program

Outputs of the program are in form of tables and the program will be automatically divide the output file in every 8 years data,

ROAXXXx : ROA = Reservoir Operation at A (upper reservoir),

XXX = Three initial first letter from input of Inflow data file

x = Number of file automatically given by program, start from 0

In ROA file, there are the name of month, year of operation and 11 columns, the value of flow is +ve if into the reservoir and -ve if out from reservoir

Column 1, DATE: Date of operation

Column 2, PERIOD: Condition of period (Peak or non-peak hours)

Column 3, DURATION: Duration of period in hours

Column 4, INFLA: Natural inflow to the reservoir A in M^3

Column 5, QPUMP: Volume of water pumping from lower reservoir in M^3

Column 6, EVAPLA: Evaporation Losses of reservoir A in M^3

Column 7, QA: Volume of water releases from reservoir A, through power tunnel in M^3

Column 8, SPILLA: Volume of water spills from reservoir A in M^3

Column 9, STOREA: Volume of water stores in reservoir A in M^3

Column 10, AREA: Area of water surfaces in reservoir A in M^3

Column 11, EL.A: Elevation of water surface in reservoir A in M

ROBXXXx : ROB = Reservoir Operation at B (lower reservoir),

XXX = Three initial first letter from input of Inflow data file

x = Number of file automatically given by program, start from 0

In ROB file, there are the name of month, year of operation and 12 columns, the value of flow is +ve if into the reservoir and -ve if out from reservoir

Column 1, DATE: Date of operation

Column 2, PERIOD: Condition of period (Peak or non-peak hours)

Column 3, DURATION: Duration of period in hours

Column 4, INFLB: Natural inflow + Spill from reservoir A to the reservoir B in M^3

Column 5, QA: Volume of water release from reservoir A to reservoir B, through power tunnel in M^3

Column 6, IRRS: Volume of water release from B to meet irrigation demand in M^3

Column 7, EVAPLB: Evaporation Losses of reservoir B in M^3

Column 8, QPUMP: Volume of water pumping to upper reservoir in M^3

Column 9, SPILLB: Volume of water spills from reservoir B in M^3

Column 10, STOREB: Volume of water stores in reservoir B in M^3

Column 11, BREA: Area of water surfaces in reservoir B in M^3

Column 12, EL.B: Elevation of water surface in reservoir B in M

After end of month, there is summation of spilling water from reservoir B in M^3

ENGXXXx : ENG = Total Energy Generated,

XXX = Three initial first letter from input of Inflow data file

x = Number of file automatically given by program, start from 0

In ENG file, there are the name of month, year of operation and 13 columns.

Column 1, DATE: Date of operation

Column 2, PERIOD: Condition of period (Peak or non-peak hours)

Column 3, DURATION: Duration of period in hours

Column 4, GROSSH: Gross Head in M

Column 5, NETTH: Net Head = Gross Head – Friction head loss in M

Column 6, Q: Discharge through power tunnel of U/S powerhouse in M^3/sec

Column 7, STARTP: Power Generated at start period in MW

Column 8, ENDP: Power Generated at end period in MW

Column 9, AV.ENERGY: Average Energy Generated at U/S powerhouse in MWh

Column 10, QD: Discharge through D/S powerhouse in M^3/sec

Column 11, ENERGY: Energy Generated at D/S powerhouse in MWh

Column 12, TOT.ENERGY: Total Energy Generated at U/S and D/S powerhouse in MWh

Column 13, IRR.: Percentage Irrigation Supply in each period

SROXXXx : SRO = Summary of Reservoir Operation,

XXX = Three initial first letter from input of Inflow data file

x = Number of file automatically given by program, 0 and 1

SROXXX0 = File Summary of Reservoir Operation in Every Year (monthly basis)

In SROXXX0 file, there are the year of operation and 12 columns

Column 1, MONTH: Month of operation

Column 2, RUNOFF A: Summary of Inflow to Reservoir A in M^3

Column 3, RUNOFF B: Summary of Inflow to Reservoir B in M^3

Column 4, TOTAL: RUNOFF A + RUNOFF B in M^3
 Column 5, IRRIG.DEMAND: Total Irrigation Demand in M^3
 Column 6, EVAP.LOSS: Evaporation Losses of reservoir in mm/day
 Column 7, IRRIG.SUPPLY: Total Irrigation Supply in M^3
 Column 8, IRRIG.DEMAND STATUS: Status of Percentage Meeting
 Irrigation Demand. Succeed = 100%
 Column 9, AV.POWER START: Average Power Generated at start period
 in MW
 Column 10, AV.POWER END: Average Power Generated at end period in
 MW
 Column 11, AV.ENERGY GENERATED: Total Average Energy
 Generated in MWh at U/S powerhouse
 Column 12, SPILL AT B: Total Volume of water spills from reservoir B in
 M^3

After end of year, there is summation of all parameters, and the minimum elevation occur in reservoir A and reservoir B

SROXXX1 = File Summary of Reservoir Operation in 35 Years (yearly basis)

In SROXXX1 file, there are 2 tables with 10 and 4 columns respectively

In first table, it is Summary of Reservoir Operation in 35 Years (yearly basis)

Column 1, YEAR: Year of operation
 Column 2, TOTAL INFLOW: TOTAL RUNOFF on this year in M^3
 Column 3, IRRIG.DEMAND: Total Irrigation Demand on this year in M^3
 Column 4, IRRIG.SUPPLY: Total Irrigation Supply on this year in M^3
 Column 5, IRRIG.DEMAND STATUS: Status of Percentage Meeting
 Irrigation Demand.
 Column 6, AV.ENERGY GENERATED: Total Average Energy Generated
 in MWh at U/S powerhouse on this year
 Column 7 SPILL AT B: Total Volume of water spills from reservoir B on
 this year in M^3
 Column 8, HA MIN: Minimum Elevation Occurs in reservoir A in M
 Column 9, HB MIN: Minimum Elevation Occurs in reservoir B in M
 Column 10, TOT. SYSTEM EN. GENERATE: Total System Energy
 Generated in MWh on this year

After end of 35 years operation, there are Average Percentage Meeting Irrigation Demand, Average Annual of Energy Generated, and the minimum elevation occur in reservoir A and reservoir B

Second table is Summary of ten daily Average Percentage Meeting Irrigation Demand;

- Column 1, MONTH: Name of month
- Column 2: Average Percentage Meeting Irrigation Demand in first 10 daily
for all 35 years operation on this month.
- Column 3: Average Percentage Meeting Irrigation Demand in second 10
daily for all 35 years operation on this month
- Column 4: Average Percentage Meeting Irrigation Demand in third 10 daily
for all 35 years operation on this month

OUTPUT INDEX

| | Page |
|---|---------------------------|
| Result of DROPS Program with Project Operation | |
| Schedule | IIIB-7 to IIIB-41 |
| • Summary of Reservoir Operation of Year 1963 (Monthly basis) | IIIB-7 |
| • Reservoir Operation at A for 1963 | IIIB-8 to IIIB-17 |
| • Month of October | IIIB-8 to IIIB-9 |
| • Month of November | IIIB-10 to IIIB-13 |
| • Month of December | IIIB-14 to IIIB-17 |
| • Reservoir Operation at B for 1963 | IIIB-18 to IIIB-29 |
| • Month of October | IIIB-18 to IIIB-21 |
| • Month of November | IIIB-22 to IIIB-25 |
| • Month of December | IIIB-26 to IIIB-29 |
| • Energy Generation in U/S, D/S Powerhouse and % Meeting Irrigation Demand | IIIB-30 to IIIB-41 |
| • Month of October | IIIB-30 to IIIB-33 |
| • Month of November | IIIB-34 to IIIB-37 |
| • Month of December | IIIB-38 to IIIB-41 |
| Result of DROPS Program with Proposed Operation | |
| Schedule | IIIB-42 to IIIB-78 |
| • Summary of Reservoir Operation of Year 1963 (Monthly basis) | IIIB-42 |
| • Reservoir Operation at A for 1963 | IIIB-43 to IIIB-54 |
| • Month of October | IIIB-43 to IIIB-46 |
| • Month of November | IIIB-47 to IIIB-50 |
| • Month of December | IIIB-50 to IIIB-54 |
| • Reservoir Operation at B for 1963 | IIIB-55 to IIIB-66 |
| • Month of October | IIIB-55 to IIIB-58 |

- Month of November IIIB-59 to IIIB-62
- Month of December IIIB-63 to IIIB-66
- Energy Generation in U/S, D/S Powerhouse and % Meeting Irrigation Demand IIIB-67 to IIIB-78
 - Month of October IIIB-67 to IIIB-70
 - Month of November IIIB-71 to IIIB-74
 - Month of December IIIB-75 to IIIB-78

File name: SROINT0.OUT for year 1963 with project operation schedule

SUMMARY OF RESERVOIR OPERATION 1963

| MONTH OF | RUNOFF | | TOTAL (M3) | IRRIG. DEMAND (M3) | EVAP. LOSS (MM/D) | IRRIG. SUPPLY (M3) | IRRIG. DEMAND (M3) | AV. POWER START END (MW) | AV. ENERGY GENERATED (MWh) | SPILL AT B (M3) |
|---------------------|-----------|-----------|---------------|--------------------------|-------------------------|--------------------------|--------------------------|-----------------------------------|----------------------------------|-----------------------|
| | A (M3) | B (M3) | | | | | | | | |
| OCTOBER | .4310E+09 | .0000E+00 | .4310E+09 | .1762E+09 | 3.26 | .1762E+09 | SUCCEED | 1486.82 | 1473.58 | 225566. |
| NOVEMBER | .2630E+09 | .0000E+00 | .2630E+09 | .3412E+09 | 2.27 | .2879E+09 | 84.38% | 1213.14 | 1206.29 | 80266. |
| DECEMBER | .2070E+09 | .0000E+00 | .2070E+09 | .4658E+09 | 1.36 | .4658E+09 | SUCCEED | 1731.21 | 1698.09 | 314673. |
| | .9010E+09 | .0000E+00 | .9010E+09 | .9832E+09 | | .9299E+09 | | | | .000E+00 |
| FRL. AT A | = | | 830.00 M | | | | | | | 620505. |
| MDDL. AT A | = | | 740.00 M | | | | | | | .2222E+09 |
| MIN. ELEVATION AT A | = | | 823.08 M | | | | | | | |
| FRL. AT B | = | | 612.00 M | | | | | | | |
| MDDL. AT B | = | | 598.50 M | | | | | | | |
| MIN. ELEVATION AT B | = | | 598.50 M | | | | | | | |

File name: ROAINT0.OUT for year 1963 with project operation schedule

MONTH OF : OCTOBER YEAR : 1963 OPERATION AT RESERVOIR A

| | DATE | PERIOD | DURATION (HR) | INFLA (M3) | QPUMP (M3) | EVAPLA (M3) | QA (M3) | SPIILLA (M3) | STOREA (M3) | AREA (M2) | EL.A (M) |
|---|----------|--------|------------------|---------------|---------------|----------------|------------|-----------------|----------------|--------------|-------------|
| 1 | PEAK | 2.10 | 1216532. | 0. | -12486. | -9010000. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35613. | 0. | 0. | .353E+10 | .437E+08 | 829.80 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -3416304. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | NON-PEAK | 8.00 | 4634409. | 773431. | -47509. | 0. | 0. | .353E+10 | .437E+08 | 829.86 | |
| | NON-PEAK | 3.90 | 2259274. | 0. | -23188. | 0. | -2107904. | .354E+10 | .438E+08 | 830.00 | |
| 2 | PEAK | 2.10 | 1216532. | 0. | -12486. | -9010000. | 0. | .353E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35613. | 0. | 0. | .354E+10 | .437E+08 | 829.80 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9339775. | 0. | .353E+10 | .438E+08 | 829.89 | |
| | NON-PEAK | 8.00 | 4634409. | 6696769. | -47446. | 0. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 3.90 | 2259274. | 0. | -23188. | 0. | -2107648. | .354E+10 | .438E+08 | 830.00 | |
| 3 | PEAK | 2.10 | 1216532. | 0. | -12486. | -9010000. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35613. | 0. | 0. | .353E+10 | .437E+08 | 829.71 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9339775. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 8.00 | 4634409. | 6696580. | -47446. | 0. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 3.90 | 2259274. | 0. | -23188. | 0. | -2107392. | .354E+10 | .437E+08 | 829.80 | |
| 4 | PEAK | 2.10 | 1216532. | 0. | -12486. | -9010000. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35613. | 0. | 0. | .353E+10 | .437E+08 | 829.71 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9339775. | 0. | .353E+10 | .437E+08 | 830.00 | |
| | NON-PEAK | 8.00 | 4634409. | 6696580. | -47446. | 0. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 3.90 | 2259274. | 0. | -23188. | 0. | -2107392. | .354E+10 | .437E+08 | 829.80 | |
| 5 | PEAK | 2.10 | 1216532. | 0. | -12486. | -9010000. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35613. | 0. | 0. | .353E+10 | .437E+08 | 829.71 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9339775. | 0. | .353E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 8.00 | 4634409. | 6696580. | -47446. | 0. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 3.90 | 2259274. | 0. | -23188. | 0. | -2107392. | .354E+10 | .437E+08 | 829.80 | |
| 6 | PEAK | 2.10 | 1216532. | 0. | -12486. | -9010000. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35613. | 0. | 0. | .353E+10 | .437E+08 | 829.71 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9339775. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 8.00 | 4634409. | 6696580. | -47446. | 0. | 0. | .354E+10 | .437E+08 | 829.80 | |
| | NON-PEAK | 3.90 | 2259274. | 0. | -23188. | 0. | -2107392. | .354E+10 | .437E+08 | 830.00 | |
| 7 | PEAK | 2.10 | 1216532. | 0. | -12486. | -9010000. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35613. | 0. | 0. | .353E+10 | .437E+08 | 829.80 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9339775. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | NON-PEAK | 8.00 | 4634409. | 6696580. | -47446. | 0. | 0. | .353E+10 | .437E+08 | 829.71 | |
| | NON-PEAK | 3.90 | 2259274. | 0. | -23188. | 0. | -2107392. | .354E+10 | .438E+08 | 830.00 | |

| | | | | | | | | | | |
|----|----------|------|----------|----------|-------------------|-----------|----------|----------|----------|--------|
| 8 | PEAK | 2.10 | 1216532. | 0. | -12486. -9010000. | 0. | .353E+10 | .437E+08 | 829.80 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35613. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9339775. | 0. | .353E+10 | .437E+08 | 829.71 |
| | NON-PEAK | 8.00 | 4634409. | 6696580. | -47446. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 3.90 | 2259274. | 0. | -23188. | 0. | .354E+10 | .438E+08 | 830.00 | |
| 9 | PEAK | 2.10 | 1216532. | 0. | -12486. | -9010000. | 0. | .353E+10 | .437E+08 | 829.80 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35613. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9339775. | 0. | .353E+10 | .437E+08 | 829.71 |
| | NON-PEAK | 8.00 | 4634409. | 6696580. | -47446. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 3.90 | 2259274. | 0. | -23188. | 0. | .353E+10 | .437E+08 | 830.00 | |
| 10 | PEAK | 2.10 | 1216532. | 0. | -12486. | -9010000. | 0. | .353E+10 | .438E+08 | 829.80 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35613. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9339775. | 0. | .353E+10 | .437E+08 | 829.71 |
| | NON-PEAK | 8.00 | 4634409. | 6696580. | -47446. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 3.90 | 2259274. | 0. | -23188. | 0. | .353E+10 | .437E+08 | 830.00 | |
| 11 | PEAK | 2.20 | 1274462. | 0. | -13081. | -9160000. | 0. | .353E+10 | .438E+08 | 829.89 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35612. | 0. | .353E+10 | .437E+08 | 829.71 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9784527. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 4634409. | 7257606. | -47440. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 3.80 | 2201344. | 0. | -22594. | 0. | .353E+10 | .437E+08 | 830.00 | |
| 12 | PEAK | 2.20 | 1274462. | 0. | -13081. | -9160000. | 0. | .353E+10 | .438E+08 | 829.89 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35612. | 0. | .353E+10 | .437E+08 | 829.69 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9784527. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 4634409. | 7257606. | -47440. | 0. | .354E+10 | .438E+08 | 829.80 | |
| | NON-PEAK | 3.80 | 2201344. | 0. | -22594. | 0. | .353E+10 | .437E+08 | 829.80 | |
| 13 | PEAK | 2.20 | 1274462. | 0. | -13081. | -9160000. | 0. | .353E+10 | .438E+08 | 829.80 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35612. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9784527. | 0. | .353E+10 | .437E+08 | 829.69 |
| | NON-PEAK | 8.00 | 4634409. | 7257606. | -47440. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 3.80 | 2201344. | 0. | -22594. | 0. | .353E+10 | .437E+08 | 830.00 | |
| 14 | PEAK | 2.20 | 1274462. | 0. | -13081. | -9160000. | 0. | .353E+10 | .438E+08 | 829.89 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35612. | 0. | .354E+10 | .438E+08 | 829.80 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9784527. | 0. | .353E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 4634409. | 7257606. | -47440. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | 3.80 | 2201344. | 0. | -22594. | 0. | .353E+10 | .437E+08 | 829.80 | |
| 15 | PEAK | 2.20 | 1274462. | 0. | -13081. | -9160000. | 0. | .353E+10 | .438E+08 | 829.89 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35612. | 0. | .354E+10 | .437E+08 | 829.69 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9784527. | 0. | .353E+10 | .438E+08 | 829.89 |
| | NON-PEAK | 8.00 | 4634409. | 7257606. | -47440. | 0. | .354E+10 | .437E+08 | 829.69 | |
| | NON-PEAK | 3.80 | 2201344. | 0. | -22594. | 0. | .354E+10 | .438E+08 | 830.00 | |

| | | | | | | | | | | |
|----|----------|------|----------|----------|---------|-----------|-----------|----------|----------|--------|
| 16 | PEAK | 2.20 | 1274462. | 0. | -13081. | -9160000. | 0. | .353E+10 | .437E+08 | 829.80 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35612. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9784527. | 0. | .353E+10 | .437E+08 | 829.69 |
| | NON-PEAK | 8.00 | 4634409. | 7257606. | -47440. | 0. | .354E+10 | .438E+08 | 830.00 | |
| 17 | PEAK | 3.80 | 2201344. | 0. | -22594. | 0. | -2073856. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 2.20 | 1274462. | 0. | -13081. | -9160000. | 0. | .353E+10 | .437E+08 | 829.80 |
| | PEAK | 6.00 | 3475807. | 0. | -35612. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | NON-PEAK | 4.00 | 2317204. | 0. | -23760. | -9784527. | 0. | .353E+10 | .437E+08 | 829.69 |
| 18 | PEAK | 3.80 | 2201344. | 0. | -47440. | 0. | -2073856. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35612. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9784527. | 0. | .353E+10 | .437E+08 | 829.80 |
| | NON-PEAK | 8.00 | 4634409. | 7257606. | -47440. | 0. | -2073856. | .354E+10 | .438E+08 | 829.89 |
| 19 | PEAK | 2.20 | 1274462. | 0. | -13081. | -9160000. | 0. | .354E+10 | .438E+08 | 829.80 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35612. | 0. | .353E+10 | .437E+08 | 829.69 | |
| | PEAK | 4.00 | 2317204. | 0. | -23760. | -9784527. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 3.80 | 2201344. | 0. | -47440. | 0. | -2073856. | .354E+10 | .438E+08 | 830.00 |
| 20 | PEAK | 2.20 | 1274462. | 0. | -22594. | 0. | -2073856. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -13081. | -9160000. | 0. | .353E+10 | .437E+08 | 829.80 |
| | PEAK | 4.00 | 2317204. | 0. | -35612. | 0. | .354E+10 | .438E+08 | 829.89 | |
| | NON-PEAK | 8.00 | 4634409. | 7257606. | -47440. | 0. | -2073856. | .354E+10 | .438E+08 | 830.00 |
| | PEAK | 3.80 | 2201344. | 0. | -22594. | 0. | .353E+10 | .437E+08 | 829.80 | |
| | NON-PEAK | 2.20 | 1274462. | 0. | -13081. | -9160000. | 0. | .354E+10 | .438E+08 | 829.89 |
| 21 | PEAK | 1.00 | 579301. | 0. | -5946. | -4290000. | 0. | .353E+10 | .437E+08 | 829.90 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. | 0. | .354E+10 | .438E+08 | 829.99 | |
| | PEAK | 4.00 | 2317204. | 0. | -23782. | -4447512. | 0. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. | 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. | 0. | -2866688. | .354E+10 | .438E+08 | 830.00 |
| 22 | PEAK | 1.00 | 579301. | 0. | -5946. | -4290000. | 0. | .354E+10 | .438E+08 | 829.90 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. | 0. | .354E+10 | .438E+08 | 829.99 | |
| | PEAK | 4.00 | 2317204. | 0. | -23782. | -4447512. | 0. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. | 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. | 0. | -2866688. | .354E+10 | .438E+08 | 830.00 |
| 23 | PEAK | 1.00 | 579301. | 0. | -5946. | -4290000. | 0. | .354E+10 | .438E+08 | 829.90 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. | 0. | .354E+10 | .438E+08 | 829.99 | |
| | PEAK | 4.00 | 2317204. | 0. | -23782. | -4447512. | 0. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. | 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 4.00 | 2317204. | 0. | -23782. | -4447512. | 0. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. | 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. | 0. | -2866688. | .354E+10 | .438E+08 | 830.00 |

| | | | | | | | | | |
|----|----------|------|----------|----|-------------------|-----------|----------|----------|--------|
| 24 | PEAK | 1.00 | 579301. | 0. | -5946. -4290000. | 0. | .354E+10 | .438E+08 | 829.90 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. 0. | 0. | .354E+10 | .438E+08 | 829.99 |
| | PEAK | 4.00 | 2317204. | 0. | -23782. -4447512. | 0. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. 0. | -2866688. | .354E+10 | .438E+08 | 830.00 |
| 25 | PEAK | 1.00 | 579301. | 0. | -5946. -4290000. | 0. | .354E+10 | .438E+08 | 829.90 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. 0. | 0. | .354E+10 | .438E+08 | 829.99 |
| | PEAK | 4.00 | 2317204. | 0. | -23782. -4447512. | 0. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. 0. | -2866688. | .354E+10 | .438E+08 | 830.00 |
| 26 | PEAK | 1.00 | 579301. | 0. | -5946. -4290000. | 0. | .354E+10 | .438E+08 | 829.90 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. 0. | 0. | .354E+10 | .438E+08 | 829.99 |
| | PEAK | 4.00 | 2317204. | 0. | -23782. -4447512. | 0. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. 0. | -2866688. | .354E+10 | .438E+08 | 830.00 |
| 27 | PEAK | 1.00 | 579301. | 0. | -5946. -4290000. | 0. | .354E+10 | .438E+08 | 829.90 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. 0. | 0. | .354E+10 | .438E+08 | 829.94 |
| | PEAK | 4.00 | 2317204. | 0. | -23782. -4447512. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. 0. | -2866688. | .354E+10 | .438E+08 | 829.90 |
| 28 | PEAK | 1.00 | 579301. | 0. | -5946. -4290000. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. 0. | 0. | .354E+10 | .438E+08 | 829.94 |
| | PEAK | 4.00 | 2317204. | 0. | -23782. -4447512. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. 0. | -2866688. | .354E+10 | .438E+08 | 830.00 |
| 29 | PEAK | 1.00 | 579301. | 0. | -5946. -4290000. | 0. | .354E+10 | .438E+08 | 829.90 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. 0. | 0. | .354E+10 | .438E+08 | 829.99 |
| | PEAK | 4.00 | 2317204. | 0. | -23782. -4447512. | 0. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. 0. | -2866688. | .354E+10 | .438E+08 | 830.00 |
| 30 | PEAK | 1.00 | 579301. | 0. | -5946. -4290000. | 0. | .354E+10 | .438E+08 | 829.90 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. 0. | 0. | .354E+10 | .438E+08 | 829.94 |
| | PEAK | 4.00 | 2317204. | 0. | -23782. -4447512. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. 0. | -2156288. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. 0. | -2866688. | .354E+10 | .438E+08 | 829.90 |
| 31 | PEAK | 1.00 | 579301. | 0. | -5946. -4290000. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35646. 0. | 0. | .354E+10 | .438E+08 | 829.94 |
| | PEAK | 4.00 | 2317204. | 0. | -23782. -4447512. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47541. 0. | -2156288. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. 0. | -2866688. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.00 | 2896506. | 0. | -29729. 0. | -2866688. | .354E+10 | .438E+08 | 830.00 |

MONTH OF : NOVEMBER YEAR : 1963 OPERATION AT RESERVOIR A

| DATE | PERIOD | DURATION | INFLA | QPUMP (M3) | EVAPLA (M3) | QA (M3) | SPILLA (M3) | STOREA (M3) | AREA (M2) | EL.A (M) |
|------|----------|----------|----------|---------------|----------------|------------|----------------|----------------|--------------|-------------|
| 1 | PEAK | .60 | 219167. | 0. | -2482. | -2650000. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24810. | 0. | 0. | .354E+10 | .438E+08 | 829.94 |
| | PEAK | 4.00 | 1461111. | 0. | -16548. | -2668508. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33087. | 0. | -1398784. | .354E+10 | .438E+08 | 829.96 |
| | NON-PEAK | 5.40 | 1972500. | 0. | -22341. | 0. | -1950208. | .354E+10 | .438E+08 | 830.00 |
| 2 | PEAK | .60 | 219167. | 0. | -2482. | -2650000. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24810. | 0. | 0. | .354E+10 | .438E+08 | 829.94 |
| | PEAK | 4.00 | 1461111. | 0. | -16548. | -2668508. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33087. | 0. | -1398784. | .354E+10 | .438E+08 | 829.96 |
| | NON-PEAK | 5.40 | 1972500. | 0. | -22341. | 0. | -1950208. | .354E+10 | .438E+08 | 830.00 |
| 3 | PEAK | .60 | 219167. | 0. | -2482. | -2650000. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24810. | 0. | 0. | .354E+10 | .438E+08 | 829.96 |
| | PEAK | 4.00 | 1461111. | 0. | -16548. | -2668508. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33087. | 0. | -1398784. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.40 | 1972500. | 0. | -22341. | 0. | -1950208. | .354E+10 | .438E+08 | 829.94 |
| 4 | PEAK | .60 | 219167. | 0. | -2482. | -2650000. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24810. | 0. | 0. | .354E+10 | .438E+08 | 829.96 |
| | PEAK | 4.00 | 1461111. | 0. | -16548. | -2668508. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33087. | 0. | -1398784. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.40 | 1972500. | 0. | -22341. | 0. | -1950208. | .354E+10 | .438E+08 | 829.94 |
| 5 | PEAK | .60 | 219167. | 0. | -2482. | -2650000. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24810. | 0. | 0. | .354E+10 | .438E+08 | 829.96 |
| | PEAK | 4.00 | 1461111. | 0. | -16548. | -2668508. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33087. | 0. | -1398784. | .354E+10 | .438E+08 | 829.96 |
| | NON-PEAK | 5.40 | 1972500. | 0. | -22341. | 0. | -1950208. | .354E+10 | .438E+08 | 830.00 |
| 6 | PEAK | .60 | 219167. | 0. | -2482. | -2650000. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24810. | 0. | 0. | .354E+10 | .438E+08 | 829.94 |
| | PEAK | 4.00 | 1461111. | 0. | -16548. | -2668508. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33087. | 0. | -1398784. | .354E+10 | .438E+08 | 829.96 |
| | NON-PEAK | 5.40 | 1972500. | 0. | -22341. | 0. | -1950208. | .354E+10 | .438E+08 | 830.00 |
| 7 | PEAK | .60 | 219167. | 0. | -2482. | -2650000. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24810. | 0. | 0. | .354E+10 | .438E+08 | 829.96 |
| | PEAK | 4.00 | 1461111. | 0. | -16548. | -2150172. | 0. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33091. | 0. | -1917184. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.40 | 1972500. | 0. | -22341. | 0. | -1950208. | .354E+10 | .438E+08 | 830.00 |

| | | | | | | | | | | |
|----|----------|------|----------|----|---------|-----------|-----------|----------|----------|--------|
| 8 | PEAK | .60 | 219167. | 0. | -2482. | -2650000. | 0. | -354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24810. | 0. | 0. | .354E+10 | .438E+08 | 829.99 |
| | PEAK | 4.00 | 1461111. | 0. | -16548. | -2150172. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33091. | 0. | -1917184. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 5.40 | 1972500. | 0. | -22341. | 0. | -1950208. | .354E+10 | .438E+08 | 830.00 |
| 9 | PEAK | .60 | 219167. | 0. | -2482. | -2650000. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24810. | 0. | 0. | .354E+10 | .438E+08 | 829.94 |
| | PEAK | 4.00 | 1461111. | 0. | -16548. | -2150172. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33091. | 0. | -1917184. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 5.40 | 1972500. | 0. | -22341. | 0. | -1950208. | .354E+10 | .438E+08 | 830.00 |
| 10 | PEAK | .60 | 219167. | 0. | -2482. | -2650000. | 0. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24810. | 0. | 0. | .354E+10 | .438E+08 | 829.99 |
| | PEAK | 4.00 | 1461111. | 0. | -16548. | -2150172. | 0. | .354E+10 | .438E+08 | 829.99 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33091. | 0. | -1917184. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.40 | 1972500. | 0. | -22341. | 0. | -1950208. | .354E+10 | .438E+08 | 830.00 |
| 11 | PEAK | .70 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.94 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 829.99 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1950208. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.30 | 1935972. | 0. | -21928. | 0. | -1950208. | .354E+10 | .438E+08 | 830.00 |
| 12 | PEAK | .70 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 829.97 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1583360. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.30 | 1935972. | 0. | -21928. | 0. | -1914112. | .354E+10 | .438E+08 | 830.00 |
| 13 | PEAK | .70 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 829.97 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1583360. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.30 | 1935972. | 0. | -21928. | 0. | -1914112. | .354E+10 | .438E+08 | 830.00 |
| 14 | PEAK | .70 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 829.93 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 829.97 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1583360. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.30 | 1935972. | 0. | -21928. | 0. | -1914112. | .354E+10 | .438E+08 | 830.00 |
| 15 | PEAK | .70 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 830.00 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 829.93 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1583360. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 5.30 | 1935972. | 0. | -21928. | 0. | -1914112. | .354E+10 | .438E+08 | 830.00 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 829.97 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1583360. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.30 | 1935972. | 0. | -21928. | 0. | -1914112. | .354E+10 | .438E+08 | 830.00 |

| | | | | | | | | | | |
|----|----------|------|----------|----|---------|-----------|-----------|----------|----------|--------|
| 16 | PEAK | .70 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.93 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 829.98 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 829.97 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1583360. | .354E+10 | .438E+08 | 830.00 |
| | PEAK | 5.30 | 1935972. | 0. | -21928. | 0. | -1914112. | .354E+10 | .438E+08 | 830.00 |
| 17 | PEAK | .70 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.93 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 829.98 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 829.97 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1583360. | .354E+10 | .438E+08 | 830.00 |
| 18 | PEAK | .70 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.93 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 829.98 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1914112. | .354E+10 | .438E+08 | 830.00 |
| 19 | PEAK | .70 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 829.97 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1583360. | .354E+10 | .438E+08 | 829.97 |
| | PEAK | 5.30 | 1935972. | 0. | -21928. | 0. | -1914112. | .354E+10 | .438E+08 | 830.00 |
| 20 | PEAK | .70 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.93 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 829.98 |
| | PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 829.97 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1914112. | .354E+10 | .438E+08 | 830.00 |
| | PEAK | 5.30 | 1935972. | 0. | -21928. | 0. | -1583360. | .354E+10 | .438E+08 | 829.97 |
| | NON-PEAK | 7.00 | 255694. | 0. | -2896. | -3020000. | 0. | .354E+10 | .438E+08 | 829.93 |
| 21 | PEAK | 6.00 | 2191667. | 0. | -24808. | 0. | 0. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 4.00 | 1461111. | 0. | -16547. | -2150173. | 0. | .354E+10 | .438E+08 | 829.97 |
| | PEAK | 8.00 | 2922222. | 0. | -33089. | 0. | -1914112. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.30 | 1935972. | 0. | -21928. | 0. | -1583360. | .354E+10 | .438E+08 | 829.93 |
| | PEAK | .80 | 2922222. | 0. | -3310. | -3300000. | 0. | .354E+10 | .438E+08 | 829.92 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -16546. | -2150174. | 0. | .354E+10 | .438E+08 | 829.96 |
| | PEAK | 4.00 | 1461111. | 0. | -33087. | 0. | -1339392. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 8.00 | 2922222. | 0. | -21514. | 0. | -1878016. | .354E+10 | .438E+08 | 829.96 |
| | PEAK | 5.20 | 1899445. | 0. | -3310. | -3300000. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 5.20 | 1899445. | 0. | -24807. | 0. | 0. | .354E+10 | .438E+08 | 829.92 |
| | PEAK | .80 | 2922222. | 0. | -3310. | -3300000. | 0. | .354E+10 | .438E+08 | 829.98 |
| 22 | PEAK | 6.00 | 2191667. | 0. | -16546. | -2150174. | 0. | .354E+10 | .438E+08 | 829.98 |
| | NON-PEAK | 4.00 | 1461111. | 0. | -33087. | 0. | -1339392. | .354E+10 | .438E+08 | 830.00 |
| | PEAK | 8.00 | 2922222. | 0. | -21514. | 0. | -1878016. | .354E+10 | .438E+08 | 829.92 |
| | NON-PEAK | 5.20 | 1899445. | 0. | -24807. | 0. | 0. | .354E+10 | .438E+08 | 829.96 |
| | PEAK | .80 | 2922222. | 0. | -3310. | -3300000. | 0. | .354E+10 | .438E+08 | 829.98 |
| 23 | PEAK | 6.00 | 2191667. | 0. | -24807. | 0. | 0. | .354E+10 | .438E+08 | 830.00 |
| | NON-PEAK | 4.00 | 1461111. | 0. | -16546. | -2150174. | 0. | .354E+10 | .438E+08 | 829.98 |
| | PEAK | 8.00 | 2922222. | 0. | -3310. | -3300000. | 0. | .354E+10 | .438E+08 | 829.96 |
| | NON-PEAK | 5.20 | 1899445. | 0. | -21514. | 0. | -1339392. | .354E+10 | .438E+08 | 830.00 |
| | PEAK | .80 | 2922222. | 0. | -3310. | -3300000. | 0. | .354E+10 | .438E+08 | 830.00 |

MONTH OF : DECEMBER YEAR : 1963 OPERATION AT RESERVOIR A

| | DATE | PERIOD | DURATION | INFRA (HR) | INFLA (M3) | QPUMP (M3) | EVAPLA (M3) | QA (M3) | SPILLA (M3) | STOREA (M3) | AREA (M2) | EL.A (M) |
|---|----------|--------|----------|---------------|---------------|---------------|----------------|------------|----------------|----------------|--------------|-------------|
| 1 | PEAK | | 2.30 | 639919. | 0. | -5688. | -10229280. | 0. | .354E+10 | .438E+08 | 830.00 | |
| | NON-PEAK | | 6.00 | 1669355. | 0. | -14806. | 0. | 0. | .353E+10 | .437E+08 | 829.75 | |
| | PEAK | | 4.00 | 1112903. | 0. | -9874. | -10229280. | 0. | .352E+10 | .436E+08 | 829.80 | |
| | NON-PEAK | | 8.00 | 2225807. | 422679. | -19708. | 0. | 0. | .353E+10 | .437E+08 | 829.56 | |
| | NON-PEAK | | 3.70 | 1029436. | 0. | -9120. | 0. | 0. | .353E+10 | .437E+08 | 829.63 | |
| 2 | PEAK | | 2.30 | 639919. | 0. | -5671. | -10229280. | 0. | .352E+10 | .436E+08 | 829.41 | |
| | NON-PEAK | | 6.00 | 1669355. | 0. | -14761. | 0. | 0. | .352E+10 | .436E+08 | 829.45 | |
| | PEAK | | 4.00 | 1112903. | 0. | -9845. | -10229280. | 0. | .351E+10 | .435E+08 | 829.22 | |
| | NON-PEAK | | 8.00 | 2225807. | 5429771. | -19649. | 0. | 0. | .352E+10 | .436E+08 | 829.41 | |
| | NON-PEAK | | 3.70 | 1029436. | 0. | -9103. | 0. | 0. | .352E+10 | .436E+08 | 829.44 | |
| 3 | PEAK | | 2.30 | 639919. | 0. | -5660. | -10229280. | 0. | .351E+10 | .435E+08 | 829.19 | |
| | NON-PEAK | | 6.00 | 1669355. | 0. | -14734. | 0. | 0. | .351E+10 | .435E+08 | 829.24 | |
| | PEAK | | 4.00 | 1112903. | 0. | -9826. | -10229280. | 0. | .350E+10 | .434E+08 | 829.00 | |
| | NON-PEAK | | 8.00 | 2225807. | 5429770. | -19612. | 0. | 0. | .351E+10 | .435E+08 | 829.20 | |
| | NON-PEAK | | 3.70 | 1029436. | 0. | -9086. | 0. | 0. | .351E+10 | .435E+08 | 829.22 | |
| 4 | PEAK | | 2.30 | 639919. | 0. | -5649. | -10229280. | 0. | .350E+10 | .434E+08 | 828.98 | |
| | NON-PEAK | | 6.00 | 1669355. | 0. | -14706. | 0. | 0. | .350E+10 | .434E+08 | 829.02 | |
| | PEAK | | 4.00 | 1112903. | 0. | -9807. | -10229280. | 0. | .349E+10 | .433E+08 | 828.79 | |
| | NON-PEAK | | 8.00 | 2225807. | 5429771. | -19575. | 0. | 0. | .350E+10 | .434E+08 | 828.98 | |
| | NON-PEAK | | 3.70 | 1029436. | 0. | -9069. | 0. | 0. | .350E+10 | .434E+08 | 829.01 | |
| 5 | PEAK | | 2.30 | 639919. | 0. | -5639. | -10229280. | 0. | .349E+10 | .433E+08 | 828.76 | |
| | NON-PEAK | | 6.00 | 1669355. | 0. | -14678. | 0. | 0. | .349E+10 | .433E+08 | 828.81 | |
| | PEAK | | 4.00 | 1112903. | 0. | -9789. | -10229280. | 0. | .348E+10 | .433E+08 | 828.57 | |
| | NON-PEAK | | 8.00 | 2225807. | 5429770. | -19538. | 0. | 0. | .349E+10 | .433E+08 | 828.77 | |
| | NON-PEAK | | 3.70 | 1029436. | 0. | -9052. | 0. | 0. | .349E+10 | .433E+08 | 828.79 | |
| 6 | PEAK | | 2.30 | 639919. | 0. | -5628. | -10229280. | 0. | .348E+10 | .432E+08 | 828.55 | |
| | NON-PEAK | | 6.00 | 1669355. | 0. | -14650. | 0. | 0. | .349E+10 | .433E+08 | 828.59 | |
| | PEAK | | 4.00 | 1112903. | 0. | -9770. | -10229280. | 0. | .348E+10 | .432E+08 | 828.36 | |
| | NON-PEAK | | 8.00 | 2225807. | 5429771. | -19501. | 0. | 0. | .348E+10 | .432E+08 | 828.55 | |
| | NON-PEAK | | 3.70 | 1029436. | 0. | -9035. | 0. | 0. | .348E+10 | .433E+08 | 828.58 | |
| 7 | PEAK | | 2.30 | 639919. | 0. | -5617. | -10229280. | 0. | .347E+10 | .432E+08 | 828.33 | |
| | NON-PEAK | | 6.00 | 1669355. | 0. | -14623. | 0. | 0. | .348E+10 | .432E+08 | 828.37 | |
| | PEAK | | 4.00 | 1112903. | 0. | -9752. | -10229280. | 0. | .347E+10 | .431E+08 | 828.14 | |
| | NON-PEAK | | 8.00 | 2225807. | 5429771. | -19464. | 0. | 0. | .348E+10 | .432E+08 | 828.34 | |
| | NON-PEAK | | 3.70 | 1029436. | 0. | -9018. | 0. | 0. | .348E+10 | .432E+08 | 828.36 | |

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|----------|------|----------|----------|------------------|----------|
| 8 PEAK | 2.30 | 639919. | 0. | -5607.-10229280. | 828.12 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14595. | .431E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9733.-10229280. | 828.16 |
| NON-PEAK | 8.00 | 2225807. | 5429770. | -19427. | .430E+08 |
| NON-PEAK | 3.70 | 1029436. | 0. | -9000. | .431E+08 |
| 9 PEAK | 2.30 | 639919. | 0. | -5596.-10229280. | 827.90 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14567. | .430E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9715.-10229280. | 827.94 |
| NON-PEAK | 8.00 | 2225807. | 5429771. | -19390. | .429E+08 |
| NON-PEAK | 3.70 | 1029436. | 0. | -9696.-10229280. | 827.71 |
| 10 PEAK | 2.30 | 639919. | 0. | -8983. | .430E+08 |
| NON-PEAK | 6.00 | 1669355. | 0. | -5586.-10229280. | 827.71 |
| NON-PEAK | 4.00 | 1112903. | 0. | -14539. | .430E+08 |
| PEAK | 2.70 | 751210. | 0. | -6544.-11730000. | 827.73 |
| NON-PEAK | 8.00 | 2225807. | 5429770. | -19353. | .428E+08 |
| NON-PEAK | 3.70 | 1029436. | 0. | -8966. | .429E+08 |
| 11 PEAK | 2.70 | 751210. | 0. | -6544.-11730000. | 827.72 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14507. | .428E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9675.-12008280. | 827.49 |
| NON-PEAK | 8.00 | 2225807. | 8709418. | -19302. | .429E+08 |
| NON-PEAK | 3.30 | 918145. | 0. | -7982. | .429E+08 |
| 12 PEAK | 2.70 | 751210. | 0. | -6532.-11730000. | 827.48 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14479. | .427E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9656.-12008280. | 827.20 |
| NON-PEAK | 8.00 | 2225807. | 8709467. | -19265. | .428E+08 |
| NON-PEAK | 3.30 | 918145. | 0. | -7967. | .428E+08 |
| 13 PEAK | 2.70 | 751210. | 0. | -6519.-11730000. | 827.22 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14451. | .428E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9638.-12008280. | 827.26 |
| NON-PEAK | 8.00 | 2225807. | 8709467. | -19228. | .427E+08 |
| NON-PEAK | 3.30 | 918145. | 0. | -7951. | .427E+08 |
| 14 PEAK | 2.70 | 751210. | 0. | -6507.-11730000. | 827.04 |
| NON-PEAK | 6.00 | 1669355. | 0.. | -14424. | .427E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9619.-12008280. | 826.77 |
| NON-PEAK | 8.00 | 2225807. | 8709467. | -19191. | .426E+08 |
| NON-PEAK | 3.30 | 918145. | 0. | -7936. | .426E+08 |
| 15 PEAK | 2.70 | 751210. | 0. | -6494.-11730000. | 826.83 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14396. | .425E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9601.-12008280. | 826.55 |
| NON-PEAK | 8.00 | 2225807. | 8709468. | -19154. | .424E+08 |
| NON-PEAK | 3.30 | 918145. | 0. | -7921. | .425E+08 |
| | | | | 0. | .425E+08 |

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|----|----------|------|----------|----------|-------------------|----------|
| 16 | PEAK | 2.70 | 751210. | 0. | -6482. -11730000. | .424E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14368. | 826.36 |
| | PEAK | 4.00 | 1112903. | 0. | -9582. -12008280. | 826.40 |
| | NON-PEAK | 8.00 | 2225807. | 8709467. | -19117. | 826.40 |
| | NON-PEAK | 3.30 | 918145. | 0. | -7905. | 826.40 |
| 17 | PEAK | 2.70 | 751210. | 0. | -6469. -11730000. | 826.12 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14340. | 826.40 |
| | PEAK | 4.00 | 1112903. | 0. | -9564. -12008280. | 826.40 |
| | NON-PEAK | 8.00 | 2225807. | 8709467. | -19080. | 826.40 |
| | PEAK | 3.30 | 918145. | 0. | -7890. | 826.40 |
| 18 | PEAK | 2.70 | 751210. | 0. | -6457. -11730000. | 826.18 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14313. | 826.18 |
| | PEAK | 4.00 | 1112903. | 0. | -9545. -12008280. | 826.18 |
| | NON-PEAK | 8.00 | 2225807. | 8709467. | -19043. | 826.18 |
| | PEAK | 3.30 | 918145. | 0. | -7875. | 826.18 |
| 19 | PEAK | 2.70 | 751210. | 0. | -6444. -11730000. | 825.97 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14285. | 825.97 |
| | PEAK | 4.00 | 1112903. | 0. | -9527. -12008280. | 825.97 |
| | NON-PEAK | 8.00 | 2225807. | 8709467. | -19006. | 825.97 |
| | PEAK | 3.30 | 918145. | 0. | -7860. | 825.97 |
| 20 | PEAK | 2.70 | 751210. | 0. | -6432. -11730000. | 825.75 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14257. | 825.75 |
| | PEAK | 4.00 | 1112903. | 0. | -9508. -12008280. | 825.75 |
| | NON-PEAK | 8.00 | 2225807. | 8709467. | -18969. | 825.75 |
| | PEAK | 3.30 | 918145. | 0. | -7844. | 825.75 |
| 21 | PEAK | 2.02 | 562016. | 0. | -4803. -8983975. | 825.54 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14238. | 825.54 |
| | PEAK | 4.00 | 1112903. | 0. | -9495. -8983974. | 825.54 |
| | NON-PEAK | 4.60 | 1279839. | 5068359. | -10900. | 825.54 |
| | NON-PEAK | 7.38 | 2053306. | 0. | -17513. | 825.54 |
| 22 | PEAK | 2.02 | 562016. | 0. | -4796. -8983975. | 825.34 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14217. | 825.34 |
| | PEAK | 4.00 | 1112903. | 0. | -9482. -8983974. | 825.34 |
| | NON-PEAK | 4.60 | 1279839. | 2939247. | -10884. | 825.40 |
| | PEAK | 7.38 | 2053306. | 0. | -17479. | 825.40 |
| 23 | PEAK | 2.02 | 562016. | 0. | -4786. -8983975. | 825.18 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14189. | 825.18 |
| | PEAK | 4.00 | 1112903. | 0. | -9463. -8983974. | 825.02 |
| | NON-PEAK | 4.60 | 1279839. | 2939247. | -10863. | 825.02 |
| | NON-PEAK | 7.38 | 2053306. | 0. | -17445. | 824.91 |

| | | | | | | | | | | |
|----|----------|------|----------|----------|---------|-----------|----|----------|----------|--------|
| 24 | PEAK | 2.02 | 562016. | 0. | -4777. | -8983975. | 0. | .334E+10 | .418E+08 | 824.75 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14162. | 0. | 0. | .334E+10 | .418E+08 | 824.79 |
| | PEAK | 4.00 | 1112903. | 0. | -9445. | -8983974. | 0. | .333E+10 | .417E+08 | 824.59 |
| | NON-PEAK | 4.60 | 1279839. | 2939247. | -10841. | 0. | 0. | .333E+10 | .418E+08 | 824.70 |
| | NON-PEAK | 7.38 | 2053306. | 0. | -17411. | 0. | 0. | .334E+10 | .418E+08 | 824.75 |
| 25 | PEAK | 2.02 | 562016. | 0. | -4768. | -8983975. | 0. | .334E+10 | .418E+08 | 824.54 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14134. | 0. | 0. | .333E+10 | .417E+08 | 824.54 |
| | PEAK | 4.00 | 1112903. | 0. | -9426. | -8983974. | 0. | .333E+10 | .417E+08 | 824.58 |
| | NON-PEAK | 4.60 | 1279839. | 2939247. | -10820. | 0. | 0. | .332E+10 | .417E+08 | 824.38 |
| | NON-PEAK | 7.38 | 2053306. | 0. | -17376. | 0. | 0. | .332E+10 | .417E+08 | 824.48 |
| 26 | PEAK | 2.02 | 562016. | 0. | -4758. | -8983975. | 0. | .333E+10 | .417E+08 | 824.54 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14106. | 0. | 0. | .332E+10 | .416E+08 | 824.32 |
| | PEAK | 4.00 | 1112903. | 0. | -9408. | -8983974. | 0. | .332E+10 | .417E+08 | 824.36 |
| | NON-PEAK | 4.60 | 1279839. | 2939247. | -10799. | 0. | 0. | .331E+10 | .416E+08 | 824.16 |
| | NON-PEAK | 7.38 | 2053306. | 0. | -17342. | 0. | 0. | .332E+10 | .416E+08 | 824.27 |
| 27 | PEAK | 2.02 | 562016. | 0. | -4749. | -8983975. | 0. | .332E+10 | .416E+08 | 824.32 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14078. | 0. | 0. | .331E+10 | .416E+08 | 824.10 |
| | PEAK | 4.00 | 1112903. | 0. | -9389. | -8983974. | 0. | .331E+10 | .416E+08 | 824.15 |
| | NON-PEAK | 4.60 | 1279839. | 2939248. | -10778. | 0. | 0. | .330E+10 | .415E+08 | 823.94 |
| | NON-PEAK | 7.38 | 2053306. | 0. | -17308. | 0. | 0. | .331E+10 | .415E+08 | 824.05 |
| 28 | PEAK | 2.02 | 562016. | 0. | -4740. | -8983975. | 0. | .331E+10 | .416E+08 | 824.10 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14051. | 0. | 0. | .330E+10 | .415E+08 | 823.89 |
| | PEAK | 4.00 | 1112903. | 0. | -9371. | -8983974. | 0. | .330E+10 | .415E+08 | 823.93 |
| | NON-PEAK | 4.60 | 1279839. | 2939247. | -10756. | 0. | 0. | .330E+10 | .414E+08 | 823.73 |
| | NON-PEAK | 7.38 | 2053306. | 0. | -17274. | 0. | 0. | .330E+10 | .415E+08 | 823.84 |
| 29 | PEAK | 2.02 | 562016. | 0. | -4730. | -8983975. | 0. | .330E+10 | .415E+08 | 823.62 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14023. | 0. | 0. | .329E+10 | .414E+08 | 823.67 |
| | PEAK | 4.00 | 1112903. | 0. | -9352. | -8983974. | 0. | .329E+10 | .414E+08 | 823.72 |
| | NON-PEAK | 4.60 | 1279839. | 2939247. | -10735. | 0. | 0. | .329E+10 | .413E+08 | 823.51 |
| | NON-PEAK | 7.38 | 2053306. | 0. | -17240. | 0. | 0. | .329E+10 | .414E+08 | 823.30 |
| 30 | PEAK | 2.02 | 562016. | 0. | -4721. | -8983975. | 0. | .329E+10 | .413E+08 | 823.67 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13995. | 0. | 0. | .328E+10 | .413E+08 | 823.46 |
| | PEAK | 4.00 | 1112903. | 0. | -9334. | -8983974. | 0. | .328E+10 | .412E+08 | 823.50 |
| | NON-PEAK | 4.60 | 1279839. | 2939247. | -10714. | 0. | 0. | .328E+10 | .413E+08 | 823.30 |
| | NON-PEAK | 7.38 | 2053306. | 0. | -17206. | 0. | 0. | .328E+10 | .413E+08 | 823.41 |
| 31 | PEAK | 2.02 | 562016. | 0. | -4712. | -8983975. | 0. | .327E+10 | .412E+08 | 823.46 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13967. | 0. | 0. | .327E+10 | .412E+08 | 823.24 |
| | PEAK | 4.00 | 1112903. | 0. | -9315. | -8983974. | 0. | .327E+10 | .412E+08 | 823.08 |
| | NON-PEAK | 4.60 | 1279839. | 2939247. | -10693. | 0. | 0. | .328E+10 | .412E+08 | 823.19 |
| | NON-PEAK | 7.38 | 2053306. | 0. | -17172. | 0. | 0. | .328E+10 | .412E+08 | 823.24 |

File name: ROBINT0.OUT for year 1963 with project operation schedule

| MONTH OF : OCTOBER | | YEAR : 1963 | | OPERATION AT RESERVOIR B | | | | | | | |
|--------------------|--------|-------------|----------|--------------------------|--------------|----------------|---------------|----------------|----------------|--------------|-------------|
| DATE | PERIOD | DURATION | INFIL | QA (M3) | IRRS (M3) | EVAPLB (M3) | QPUMP (M3) | SPILLB (M3) | STOREB (M3) | BREA (M2) | EL.B (M) |
| 1 PEAK | 2.10 | 0. | 9010000. | -497339. | -565. | 0. | 0. | .551E+08 | .198E+07 | 598.50 | |
| NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1736. | 0. | 0. | .636E+08 | .213E+07 | 602.54 | |
| PEAK | 4.00 | 0. | 3416304. | -947312. | -1145. | 0. | 0. | .622E+08 | .211E+07 | 601.90 | |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2333. | -773431. | 0. | .647E+08 | .215E+07 | 603.01 | |
| NON-PEAK | 3.90 | 2107904. | 0. | -923629. | *1115. | 0. | 0. | .620E+08 | .211E+07 | 601.81 | |
| 2 PEAK | 2.10 | 0. | 9010000. | -497339. | -606. | 0. | 0. | .632E+08 | .212E+07 | 602.34 | |
| NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1843. | 0. | 0. | .717E+08 | .226E+07 | 606.18 | |
| PEAK | 4.00 | 0. | 9339775. | -947312. | -1216. | 0. | 0. | .703E+08 | .224E+07 | 605.54 | |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2580. | -6696769. | 0. | .787E+08 | .238E+07 | 609.32 | |
| NON-PEAK | 3.90 | 2107648. | 0. | -923629. | -1184. | 0. | 0. | .701E+08 | .224E+07 | 605.45 | |
| 3 PEAK | 2.10 | 0. | 9010000. | -497339. | -643. | 0. | 0. | .713E+08 | .226E+07 | 605.98 | |
| NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1949. | 0. | 0. | .798E+08 | .239E+07 | 609.81 | |
| PEAK | 4.00 | 0. | 9339775. | -947312. | -1287. | 0. | -1234645. | .855E+08 | .237E+07 | 609.17 | |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | -6696580. | 0. | .769E+08 | .235E+07 | 612.00 | |
| NON-PEAK | 3.90 | 2107392. | 0. | -923629. | -1243. | 0. | 0. | .781E+08 | .237E+07 | 609.06 | |
| 4 PEAK | 2.10 | 0. | 9010000. | -497339. | -675. | 0. | -1100535. | .855E+08 | .255E+07 | 612.00 | |
| NON-PEAK | 6.00 | 0. | 0. | -1420968. | -2077. | 0. | 0. | .841E+08 | .251E+07 | 611.47 | |
| PEAK | 4.00 | 0. | 9339775. | -947312. | -1363. | 0. | -6968056. | .855E+08 | .255E+07 | 608.53 | |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | -6696580. | 0. | .769E+08 | .235E+07 | 608.53 | |
| NON-PEAK | 3.90 | 2107392. | 0. | -923629. | -1243. | 0. | 0. | .781E+08 | .237E+07 | 609.06 | |
| 5 PEAK | 2.10 | 0. | 9010000. | -497339. | -675. | 0. | -1100535. | .855E+08 | .255E+07 | 612.00 | |
| NON-PEAK | 6.00 | 0. | 0. | -1420968. | -2077. | 0. | 0. | .841E+08 | .251E+07 | 611.47 | |
| PEAK | 4.00 | 0. | 9339775. | -947312. | -1363. | 0. | -6968056. | .855E+08 | .235E+07 | 608.53 | |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | -6696580. | 0. | .769E+08 | .235E+07 | 608.53 | |
| NON-PEAK | 3.90 | 2107392. | 0. | -923629. | -1243. | 0. | 0. | .781E+08 | .237E+07 | 609.06 | |
| 6 PEAK | 2.10 | 0. | 9010000. | -497339. | -675. | 0. | -1100535. | .855E+08 | .255E+07 | 612.00 | |
| NON-PEAK | 6.00 | 0. | 0. | -1420968. | -2077. | 0. | 0. | .841E+08 | .251E+07 | 611.47 | |
| PEAK | 4.00 | 0. | 9339775. | -947312. | -1363. | 0. | -6968056. | .855E+08 | .235E+07 | 608.53 | |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | -6696580. | 0. | .769E+08 | .235E+07 | 608.53 | |
| NON-PEAK | 3.90 | 2107392. | 0. | -923629. | -1243. | 0. | 0. | .781E+08 | .237E+07 | 609.06 | |
| 7 PEAK | 2.10 | 0. | 9010000. | -497339. | -675. | 0. | -1100535. | .855E+08 | .255E+07 | 612.00 | |
| NON-PEAK | 6.00 | 0. | 0. | -1420968. | -2077. | 0. | 0. | .841E+08 | .251E+07 | 611.47 | |
| PEAK | 4.00 | 0. | 9339775. | -947312. | -1363. | 0. | -6968056. | .855E+08 | .255E+07 | 612.00 | |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | -6696580. | 0. | .769E+08 | .235E+07 | 608.53 | |
| NON-PEAK | 3.90 | 2107392. | 0. | -923629. | -1243. | 0. | 0. | .781E+08 | .237E+07 | 609.06 | |

| | | | | | | | | | | | |
|----|----------|------|----------|-----------|-----------|--------|-----------|-----------|----------|----------|--------|
| 16 | PEAK | 2.20 | 0. | 9160000. | -521022. | -704. | 0. | -655980. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | .841E+08 | .251E+07 | 611.47 | |
| | PEAK | 4.00 | 0. | 9784527. | -947312. | -1363. | 0. | -7412808. | .855E+08 | .255E+07 | |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | -7257606. | 0. | .764E+08 | .234E+07 | 612.00 |
| | NON-PEAK | 3.80 | 2073856. | 0. | -899946. | -1206. | 0. | 0. | .775E+08 | .236E+07 | 608.27 |
| 17 | PEAK | 2.20 | 0. | 9160000. | -521022. | -704. | 0. | -655980. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | -1363. | 0. | 0. | .841E+08 | .251E+07 | |
| | PEAK | 4.00 | 0. | 9784527. | -947312. | -2769. | -7257606. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -1206. | 0. | 0. | .764E+08 | .234E+07 | 608.80 |
| | NON-PEAK | 3.80 | 2073856. | 0. | -899946. | -2769. | -7257606. | 0. | .775E+08 | .236E+07 | 608.80 |
| 18 | PEAK | 2.20 | 0. | 9160000. | -521022. | -704. | 0. | -655980. | .855E+08 | .255E+07 | 611.47 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | 0. | .841E+08 | .251E+07 | |
| | PEAK | 4.00 | 0. | 9784527. | -947312. | -1363. | 0. | -7412808. | .855E+08 | .234E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -1206. | 0. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 3.80 | 2073856. | 0. | -899946. | -2769. | -7257606. | 0. | .764E+08 | .234E+07 | 608.27 |
| 19 | PEAK | 2.20 | 0. | 9160000. | -521022. | -704. | 0. | -655980. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | PEAK | 4.00 | 0. | 9784527. | -947312. | -1363. | 0. | -7412808. | .855E+08 | .234E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -1206. | 0. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 3.80 | 2073856. | 0. | -899946. | -2769. | -7257606. | 0. | .764E+08 | .234E+07 | 608.80 |
| 20 | PEAK | 2.20 | 0. | 9160000. | -521022. | -704. | 0. | -655980. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | -1363. | 0. | -7412808. | .855E+08 | .234E+07 | |
| | PEAK | 4.00 | 0. | 9784527. | -947312. | -2769. | -7257606. | 0. | .764E+08 | .234E+07 | 608.27 |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -1206. | 0. | 0. | .855E+08 | .234E+07 | 608.80 |
| | NON-PEAK | 3.80 | 2073856. | 0. | -899946. | -2769. | -7257606. | 0. | .775E+08 | .236E+07 | 612.00 |
| 21 | PEAK | 1.00 | 0. | 4290000. | -236828. | -320. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -1987. | 0. | 0. | 0. | .855E+08 | .255E+07 | 612.00 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -1303. | 0. | 0. | .764E+08 | .234E+07 | 608.27 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -2713. | 0. | 0. | .837E+08 | .250E+07 | |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -1700. | 0. | 0. | .839E+08 | .236E+07 | 608.80 |
| | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -86300. | .855E+08 | .244E+07 | 610.52 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | -1363. | 0. | 0. | .802E+08 | .240E+07 | 609.99 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -2769. | -7257606. | 0. | .837E+08 | .250E+07 | 611.30 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -1206. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -2769. | 0. | 0. | .855E+08 | .255E+07 | 612.00 |
| 22 | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -4052826. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | -1363. | 0. | 0. | .841E+08 | .255E+07 | 612.00 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -2769. | -7257606. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -1206. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -2769. | 0. | 0. | .855E+08 | .255E+07 | 612.00 |
| 23 | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -4052826. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | -1363. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -1363. | 0. | -2075793. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -2769. | 0. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -1731. | 0. | 0. | .855E+08 | .255E+07 | 612.00 |

| | | | | | | | | | | | |
|----|----------|------|----------|-----------|-----------|--------|----|-----------|----------|----------|--------|
| 24 | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -4052826. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -1363. | 0. | -2075793. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -2769. | 0. | -258895. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -1731. | 0. | -1680818. | .855E+08 | .255E+07 | 612.00 |
| 25 | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -4052826. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -1363. | 0. | -2075793. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -2769. | 0. | -258895. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -1731. | 0. | -1680818. | .855E+08 | .255E+07 | 612.00 |
| 26 | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -4052826. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -1363. | 0. | -2075793. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -2769. | 0. | -258895. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -1731. | 0. | -1680818. | .855E+08 | .255E+07 | 612.00 |
| 27 | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -4052826. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -1363. | 0. | -2075793. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -2769. | 0. | -258895. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -1731. | 0. | -1680818. | .855E+08 | .255E+07 | 612.00 |
| 28 | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -4052826. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -1363. | 0. | -2075793. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -2769. | 0. | -258895. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -1731. | 0. | -1680818. | .855E+08 | .255E+07 | 612.00 |
| 29 | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -4052826. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -1363. | 0. | -2075793. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -2769. | 0. | -258895. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -1731. | 0. | -1680818. | .855E+08 | .255E+07 | 612.00 |
| 30 | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -4052826. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -1363. | 0. | -2075793. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -2769. | 0. | -258895. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -1731. | 0. | -1680818. | .855E+08 | .255E+07 | 612.00 |
| 31 | PEAK | 1.00 | 0. | 4290000. | -236828. | -346. | 0. | -4052826. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | 0. | .841E+08 | .251E+07 | 611.47 |
| | PEAK | 4.00 | 0. | 4447512. | -947312. | -1363. | 0. | -2075793. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 2156288. | 0. | -1894624. | -2769. | 0. | -258895. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 5.00 | 2866688. | 0. | -1184140. | -1731. | 0. | -1680818. | .855E+08 | .255E+07 | 612.00 |

-.220E+09

MONTH OF : NOVEMBER YEAR : 1963 OPERATION AT RESERVOIR B

| | DATE | PERIOD | DURATION (HR) | INFLB (M3) | QA (M3) | IRRS (M3) | EVAPLB (M3) | QPUMP (M3) | SPILLB (M3) | STOREB (M3) | BREA (M2) | EL.B (M) | |
|---|----------|--------|------------------|---------------|------------|--------------|----------------|---------------|----------------|----------------|--------------|-------------|--|
| 1 | PEAK | .60 | 0. | 2650000. | -284333. | -145. | 0. | -2365522. | .855E+08 | .255E+07 | 612.00 | | |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -145. | 0. | 0. | .827E+08 | .255E+07 | 612.00 | | |
| | PEAK | 4.00 | 0. | 2668508. | -1895556. | -933. | 0. | 0. | .834E+08 | .249E+07 | 610.93 | | |
| | NON-PEAK | 8.00 | 0. | 1398784. | 0. | -3791111. | -1883. | 0. | 0. | .811E+08 | .242E+07 | 611.22 | |
| | NON-PEAK | 5.40 | 1950208. | 0. | -2559000. | -1236. | 0. | 0. | .804E+08 | .241E+07 | 610.32 | | |
| 2 | PEAK | .60 | 0. | 2650000. | -284333. | -136. | 0. | 0. | .828E+08 | .247E+07 | 610.98 | | |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -1402. | 0. | 0. | .800E+08 | .240E+07 | 609.89 | | |
| | PEAK | 4.00 | 0. | 2668508. | -1895556. | -905. | 0. | 0. | .807E+08 | .242E+07 | 610.20 | | |
| | NON-PEAK | 8.00 | 0. | 1398784. | 0. | -3791111. | -1825. | 0. | 0. | .783E+08 | .237E+07 | 609.16 | |
| | NON-PEAK | 5.40 | 1950208. | 0. | -2559000. | -1209. | 0. | 0. | .777E+08 | .236E+07 | 608.89 | | |
| 3 | PEAK | .60 | 0. | 2650000. | -284333. | -134. | 0. | 0. | .801E+08 | .240E+07 | 609.95 | | |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -1359. | 0. | 0. | .773E+08 | .235E+07 | 608.67 | | |
| | PEAK | 4.00 | 0. | 2668508. | -1895556. | -889. | 0. | 0. | .780E+08 | .236E+07 | 609.02 | | |
| | NON-PEAK | 8.00 | 0. | 1398784. | 0. | -3791111. | -1787. | 0. | 0. | .756E+08 | .233E+07 | 607.94 | |
| | NON-PEAK | 5.40 | 1950208. | 0. | -2559000. | -1186. | 0. | 0. | .750E+08 | .232E+07 | 607.67 | | |
| 4 | PEAK | .60 | 0. | 2650000. | -284333. | -131. | 0. | 0. | .774E+08 | .235E+07 | 608.73 | | |
| | NON-PEAK | 6.00 | 0. | 0. | -284333. | -1334. | 0. | 0. | .745E+08 | .231E+07 | 607.45 | | |
| | PEAK | 4.00 | 0. | 2668508. | -1895556. | -872. | 0. | 0. | .753E+08 | .232E+07 | 607.80 | | |
| | NON-PEAK | 8.00 | 0. | 1398784. | 0. | -3791111. | -1754. | 0. | 0. | .729E+08 | .228E+07 | 606.72 | |
| | NON-PEAK | 5.40 | 1950208. | 0. | -2559000. | -1164. | 0. | 0. | .723E+08 | .227E+07 | 606.45 | | |
| 5 | PEAK | .60 | 0. | 2650000. | -284333. | -129. | 0. | 0. | .747E+08 | .231E+07 | 607.51 | | |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -1309. | 0. | 0. | .718E+08 | .226E+07 | 606.23 | | |
| | PEAK | 4.00 | 0. | 2668508. | -1895556. | -856. | 0. | 0. | .726E+08 | .228E+07 | 606.58 | | |
| | NON-PEAK | 8.00 | 0. | 1398784. | 0. | -3791111. | -1720. | 0. | 0. | .702E+08 | .224E+07 | 605.50 | |
| | NON-PEAK | 5.40 | 1950208. | 0. | -2559000. | -1142. | 0. | 0. | .696E+08 | .223E+07 | 605.22 | | |
| 6 | PEAK | .60 | 0. | 2650000. | -284333. | -126. | 0. | 0. | .720E+08 | .227E+07 | 606.29 | | |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -1285. | 0. | 0. | .691E+08 | .222E+07 | 605.01 | | |
| | PEAK | 4.00 | 0. | 2668508. | -1895556. | -839. | 0. | 0. | .699E+08 | .223E+07 | 605.36 | | |
| | NON-PEAK | 8.00 | 0. | 1398784. | 0. | -3791111. | -1687. | 0. | 0. | .675E+08 | .219E+07 | 604.28 | |
| | NON-PEAK | 5.40 | 1950208. | 0. | -2559000. | -1119. | 0. | 0. | .669E+08 | .218E+07 | 604.00 | | |
| 7 | PEAK | .60 | 0. | 2650000. | -284333. | -124. | 0. | 0. | .693E+08 | .222E+07 | 605.07 | | |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -1260. | 0. | 0. | .664E+08 | .218E+07 | 603.79 | | |
| | PEAK | 4.00 | 0. | 2150172. | -1895556. | -822. | 0. | 0. | .667E+08 | .218E+07 | 603.90 | | |
| | NON-PEAK | 8.00 | 0. | 1917184. | 0. | -3791111. | -1648. | 0. | 0. | .648E+08 | .215E+07 | 603.06 | |
| | NON-PEAK | 5.40 | 1950208. | 0. | -2559000. | -1097. | 0. | 0. | .642E+08 | .214E+07 | 602.78 | | |

| | | | | | | | | | | | |
|----|----------|------|----------|-----------|-----------|--------|----|----|----------|----------|--------|
| 16 | PEAK | .70 | 0. | 30200000. | -331722. | -131. | 0. | 0. | .578E+08 | .204E+07 | 599.91 |
| | NON-PEAK | 6.00 | 0. | 0. | -2686830. | -1154. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | PEAK | 4.00 | 0. | 2150173. | -1895556. | -749. | 0. | 0. | .554E+08 | .199E+07 | 598.63 |
| | NON-PEAK | 8.00 | 0. | 0. | -1835383. | -1501. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.30 | 1914112. | 0. | -1913628. | -992. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| 17 | PEAK | .70 | 0. | 30200000. | -331722. | -131. | 0. | 0. | .578E+08 | .204E+07 | 599.91 |
| | NON-PEAK | 6.00 | 0. | 0. | -2686830. | -1154. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | PEAK | 4.00 | 0. | 2150173. | -1895556. | -749. | 0. | 0. | .554E+08 | .199E+07 | 598.63 |
| | NON-PEAK | 8.00 | 1583360. | 0. | -1835383. | -1501. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.30 | 1914112. | 0. | -1913628. | -992. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| 18 | PEAK | .70 | 0. | 30200000. | -331722. | -131. | 0. | 0. | .578E+08 | .204E+07 | 599.91 |
| | NON-PEAK | 6.00 | 0. | 0. | -2686830. | -1154. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | PEAK | 4.00 | 0. | 2150173. | -1895556. | -749. | 0. | 0. | .554E+08 | .199E+07 | 598.63 |
| | NON-PEAK | 8.00 | 1583360. | 0. | -1835379. | -1501. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.30 | 1914112. | 0. | -1913632. | -992. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| 19 | PEAK | .70 | 0. | 30200000. | -331722. | -131. | 0. | 0. | .578E+08 | .204E+07 | 599.91 |
| | NON-PEAK | 6.00 | 0. | 0. | -2686830. | -1154. | 0. | 0. | .551E+08 | .198E+07 | 598.63 |
| | PEAK | 4.00 | 0. | 2150173. | -1895556. | -749. | 0. | 0. | .554E+08 | .199E+07 | 598.63 |
| | NON-PEAK | 8.00 | 1583360. | 0. | -1835379. | -1501. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.30 | 1914112. | 0. | -1913632. | -992. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| 20 | PEAK | .70 | 0. | 30200000. | -331722. | -131. | 0. | 0. | .578E+08 | .204E+07 | 599.91 |
| | NON-PEAK | 6.00 | 0. | 0. | -2686830. | -1154. | 0. | 0. | .551E+08 | .198E+07 | 598.63 |
| | PEAK | 4.00 | 0. | 2150173. | -1895556. | -749. | 0. | 0. | .554E+08 | .199E+07 | 598.63 |
| | NON-PEAK | 8.00 | 1583360. | 0. | -1835379. | -1501. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.30 | 1914112. | 0. | -1913632. | -992. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| 21 | PEAK | .80 | 0. | 3300000. | -379111. | -150. | 0. | 0. | .581E+08 | .204E+07 | 600.03 |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -1157. | 0. | 0. | .552E+08 | .198E+07 | 598.54 |
| | PEAK | 4.00 | 0. | 2150174. | -1895556. | -749. | 0. | 0. | .555E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1667498. | -1502. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1877574. | -973. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| 22 | PEAK | .80 | 0. | 3300000. | -379111. | -150. | 0. | 0. | .581E+08 | .204E+07 | 600.03 |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -1157. | 0. | 0. | .552E+08 | .198E+07 | 598.54 |
| | PEAK | 4.00 | 0. | 2150174. | -1895556. | -749. | 0. | 0. | .555E+08 | .198E+07 | 598.67 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1667498. | -1502. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1877574. | -973. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| 23 | PEAK | .80 | 0. | 3300000. | -379111. | -150. | 0. | 0. | .581E+08 | .204E+07 | 600.03 |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -1157. | 0. | 0. | .552E+08 | .198E+07 | 598.67 |
| | PEAK | 4.00 | 0. | 2150174. | -1895556. | -749. | 0. | 0. | .555E+08 | .198E+07 | 598.54 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1667498. | -1502. | 0. | 0. | .551E+08 | .198E+07 | 598.67 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1667482. | -1502. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | | | | -1877571. | -973. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |

| | | | | | | | | | | |
|----|----------|------|----------|-----------|------------|--------|----|----------|----------|--------|
| 24 | PEAK | .80 | 0. | 33000000. | -379111. | -150. | 0. | .581E+08 | .204E+07 | 600.03 |
| | NON-PEAK | 6.00 | 0. | 0. | -28433333. | -1157. | 0. | .552E+08 | .198E+07 | 598.54 |
| | PEAK | 4.00 | 0. | 2150174. | -1895556. | -749. | 0. | .555E+08 | .199E+07 | 598.67 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1667478. | -1502. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1877575. | -973. | 0. | .551E+08 | .198E+07 | 598.50 |
| 25 | PEAK | .80 | 0. | 33000000. | -379111. | -150. | 0. | .581E+08 | .204E+07 | 600.03 |
| | NON-PEAK | 6.00 | 0. | 0. | -28433333. | -1157. | 0. | .552E+08 | .198E+07 | 598.54 |
| | PEAK | 4.00 | 0. | 2150174. | -1895556. | -749. | 0. | .555E+08 | .199E+07 | 598.67 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1667478. | -1502. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1877571. | -973. | 0. | .551E+08 | .198E+07 | 598.50 |
| 26 | PEAK | .80 | 0. | 33000000. | -379111. | -150. | 0. | .581E+08 | .204E+07 | 600.03 |
| | NON-PEAK | 6.00 | 0. | 0. | -28433333. | -1157. | 0. | .552E+08 | .198E+07 | 598.54 |
| | PEAK | 4.00 | 0. | 2150174. | -1895556. | -749. | 0. | .555E+08 | .199E+07 | 598.67 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1667478. | -1502. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1877571. | -973. | 0. | .552E+08 | .198E+07 | 598.50 |
| 27 | PEAK | .80 | 0. | 33000000. | -379111. | -150. | 0. | .581E+08 | .204E+07 | 600.03 |
| | NON-PEAK | 6.00 | 0. | 0. | -28433333. | -749. | 0. | .555E+08 | .199E+07 | 598.67 |
| | PEAK | 4.00 | 0. | 2150174. | -1895556. | -749. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1667478. | -1502. | 0. | .552E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1877571. | -973. | 0. | .551E+08 | .198E+07 | 598.50 |
| | PEAK | .80 | 0. | 33000000. | -379111. | -150. | 0. | .552E+08 | .198E+07 | 598.50 |
| 28 | PEAK | 6.00 | 0. | 0. | -28433333. | -1157. | 0. | .555E+08 | .199E+07 | 598.67 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1667478. | -1502. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1877571. | -973. | 0. | .552E+08 | .198E+07 | 598.50 |
| | PEAK | .80 | 0. | 33000000. | -379111. | -150. | 0. | .551E+08 | .198E+07 | 598.50 |
| 29 | PEAK | 4.00 | 0. | 2150174. | -1895556. | -749. | 0. | .551E+08 | .204E+07 | 600.03 |
| | NON-PEAK | 6.00 | 0. | 0. | -1667482. | -1502. | 0. | .555E+08 | .199E+07 | 598.67 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1877571. | -973. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1877571. | -150. | 0. | .552E+08 | .198E+07 | 598.50 |
| | PEAK | .80 | 0. | 33000000. | -379111. | -150. | 0. | .551E+08 | .198E+07 | 598.50 |
| 30 | PEAK | 6.00 | 0. | 0. | -28433333. | -1157. | 0. | .555E+08 | .199E+07 | 598.67 |
| | NON-PEAK | 4.00 | 0. | 2150174. | -1895556. | -749. | 0. | .552E+08 | .204E+07 | 600.03 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1667478. | -1502. | 0. | .551E+08 | .198E+07 | 598.54 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1877571. | -973. | 0. | .551E+08 | .198E+07 | 598.50 |
| | PEAK | .80 | 0. | 33000000. | -379111. | -973. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 6.00 | 0. | 0. | -28433333. | -150. | 0. | .551E+08 | .198E+07 | 598.50 |
| | PEAK | 4.00 | 0. | 2150174. | -1895556. | -749. | 0. | .555E+08 | .199E+07 | 598.67 |
| | NON-PEAK | 8.00 | 1339392. | 0. | -1667478. | -1502. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 5.20 | 1878016. | 0. | -1877571. | -973. | 0. | .551E+08 | .198E+07 | 598.50 |

-237E+07

MONTH OF : DECEMBER YEAR : 1963 OPERATION AT RESERVOIR B

| DATE | PERIOD | DURATION | INFLB (M3) | QA (M3) | IRRS (M3) | EVAPLB (M3) | QPUMP (M3) | SPILLB (M3) | STOREB (M3) | BREA (M2) | EL.B (M) |
|------|----------|----------|---------------|------------|--------------|----------------|---------------|----------------|----------------|--------------|-------------|
| 1 | PEAK | 2.30 | 0. | 10229280. | -1439973. | -257. | 0. | 0. | .551E+08 | .198E+07 | 598.50 |
| | NON-PEAK | 6.00 | 0. | -3756452. | -724. | 0. | 0. | 0. | .639E+08 | .214E+07 | 602.67 |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -469. | 0. | 0. | .602E+08 | .208E+07 | 600.98 |
| | NON-PEAK | 8.00 | 0. | -5008602. | -994. | -422679. | 0. | 0. | .679E+08 | .220E+07 | 604.46 |
| | NON-PEAK | 3.70 | 0. | -2316479. | -441. | 0. | 0. | 0. | .625E+08 | .211E+07 | 602.01 |
| 2 | PEAK | 2.30 | 0. | 10229280. | -1439973. | -269. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| | NON-PEAK | 6.00 | 0. | -3756452. | -751. | 0. | 0. | 0. | .689E+08 | .222E+07 | 604.92 |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -487. | 0. | 0. | .652E+08 | .216E+07 | 603.23 |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1031. | -5429771. | 0. | 0. | .625E+08 | .228E+07 | 606.71 |
| | NON-PEAK | 3.70 | 0. | -2316479. | -441. | 0. | 0. | 0. | .601E+08 | .211E+07 | 602.01 |
| 3 | PEAK | 2.30 | 0. | 10229280. | -1439973. | -269. | 0. | 0. | .689E+08 | .222E+07 | 604.92 |
| | NON-PEAK | 6.00 | 0. | -3756452. | -751. | 0. | 0. | 0. | .652E+08 | .216E+07 | 603.23 |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -487. | 0. | 0. | .729E+08 | .228E+07 | 606.71 |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1031. | -5429770. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| | NON-PEAK | 3.70 | 0. | -2316479. | -441. | 0. | 0. | 0. | .689E+08 | .222E+07 | 604.92 |
| 4 | PEAK | 2.30 | 0. | 10229280. | -1439973. | -269. | 0. | 0. | .652E+08 | .216E+07 | 603.23 |
| | NON-PEAK | 6.00 | 0. | -3756452. | -751. | 0. | 0. | 0. | .729E+08 | .228E+07 | 606.71 |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -487. | 0. | 0. | .625E+08 | .211E+07 | 602.01 |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1031. | -5429771. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| | NON-PEAK | 3.70 | 0. | -2316479. | -441. | 0. | 0. | 0. | .689E+08 | .222E+07 | 604.92 |
| 5 | PEAK | 2.30 | 0. | 10229280. | -1439973. | -269. | 0. | 0. | .652E+08 | .216E+07 | 603.23 |
| | NON-PEAK | 6.00 | 0. | -3756452. | -751. | 0. | 0. | 0. | .625E+08 | .211E+07 | 602.01 |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -487. | 0. | 0. | .689E+08 | .222E+07 | 600.97 |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1031. | -5429770. | 0. | 0. | .601E+08 | .207E+07 | 603.23 |
| | NON-PEAK | 3.70 | 0. | -2316479. | -441. | 0. | 0. | 0. | .689E+08 | .222E+07 | 604.92 |
| 6 | PEAK | 2.30 | 0. | 10229280. | -1439973. | -269. | 0. | 0. | .652E+08 | .216E+07 | 603.23 |
| | NON-PEAK | 6.00 | 0. | -3756452. | -751. | 0. | 0. | 0. | .729E+08 | .228E+07 | 606.71 |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -487. | 0. | 0. | .625E+08 | .211E+07 | 602.01 |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1031. | -5429771. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| | NON-PEAK | 3.70 | 0. | -2316479. | -441. | 0. | 0. | 0. | .689E+08 | .222E+07 | 604.92 |
| 7 | PEAK | 2.30 | 0. | 10229280. | -1439973. | -269. | 0. | 0. | .652E+08 | .222E+07 | 603.23 |
| | NON-PEAK | 6.00 | 0. | -3756452. | -751. | 0. | 0. | 0. | .625E+08 | .211E+07 | 602.01 |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -487. | 0. | 0. | .729E+08 | .228E+07 | 606.71 |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1031. | -5429771. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| | NON-PEAK | 3.70 | 0. | -2316479. | -441. | 0. | 0. | 0. | .689E+08 | .222E+07 | 604.92 |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -487. | 0. | 0. | .652E+08 | .216E+07 | 603.23 |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1031. | -5429771. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| | NON-PEAK | 3.70 | 0. | -2316479. | -441. | 0. | 0. | 0. | .689E+08 | .222E+07 | 604.92 |
| | PEAK | 4.00 | 0. | 10229280. | -1439973. | -269. | 0. | 0. | .652E+08 | .211E+07 | 602.01 |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1031. | -5429771. | 0. | 0. | .625E+08 | .211E+07 | 602.01 |
| | NON-PEAK | 3.70 | 0. | -2316479. | -441. | 0. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |

| | | | | | | | | | | | | | |
|----|----------|------|----|-----------|------------|-----------|-----------|----|----|----------|----------|----------|--------|
| 8 | PEAK | 2.30 | 0. | 10229280. | -1439973. | -269. | 0. | 0. | 0. | .689E+08 | .222E+07 | 604.92 | |
| | NON-PEAK | 6.00 | 0. | -3756452. | -751. | -751. | 0. | 0. | 0. | .652E+08 | .216E+07 | 603.23 | |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -487. | 0. | 0. | 0. | .729E+08 | .228E+07 | 606.71 | |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1031. | -5429770. | 0. | 0. | 0. | .625E+08 | .211E+07 | 602.01 | |
| | PEAK | 3.70 | 0. | 0. | -2316479. | -441. | 0. | 0. | 0. | .601E+08 | .207E+07 | 600.97 | |
| 9 | PEAK | 2.30 | 0. | 10229280. | -1439973. | -269. | 0. | 0. | 0. | .689E+08 | .222E+07 | 604.92 | |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -751. | 0. | 0. | 0. | .652E+08 | .216E+07 | 603.23 | |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -487. | 0. | 0. | 0. | .729E+08 | .228E+07 | 606.71 | |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1031. | -5429771. | 0. | 0. | 0. | .625E+08 | .211E+07 | 602.01 |
| | PEAK | 3.70 | 0. | 0. | -2316479. | -441. | 0. | 0. | 0. | .601E+08 | .207E+07 | 600.97 | |
| 10 | PEAK | 2.30 | 0. | 10229280. | -1439973. | -269. | 0. | 0. | 0. | .689E+08 | .222E+07 | 604.92 | |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -751. | 0. | 0. | 0. | .652E+08 | .216E+07 | 603.23 | |
| | PEAK | 4.00 | 0. | 10229280. | -2504301. | -487. | 0. | 0. | 0. | .729E+08 | .228E+07 | 606.71 | |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1031. | -5429770. | 0. | 0. | 0. | .625E+08 | .211E+07 | 602.01 |
| | PEAK | 3.70 | 0. | 0. | -2316479. | -441. | 0. | 0. | 0. | .601E+08 | .207E+07 | 600.97 | |
| 11 | PEAK | 2.70 | 0. | 11730000. | -1690403. | -316. | 0. | 0. | 0. | .702E+08 | .224E+07 | 605.49 | |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -758. | 0. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| | PEAK | 4.00 | 0. | 12008280. | -2504301. | -492. | 0. | 0. | 0. | .759E+08 | .233E+07 | 608.08 | |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1053. | -8709418. | 0. | 0. | 0. | .622E+08 | .211E+07 | 601.90 |
| | PEAK | 3.30 | 0. | 0. | -2066048. | -393. | 0. | 0. | 0. | .601E+08 | .207E+07 | 600.97 | |
| | NON-PEAK | 2.70 | 0. | 0. | -11730000. | -1690403. | -316. | 0. | 0. | .702E+08 | .224E+07 | 605.49 | |
| 12 | PEAK | 6.00 | 0. | 0. | -3756452. | -758. | 0. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| | NON-PEAK | 4.00 | 0. | 0. | -2504301. | -492. | 0. | 0. | 0. | .759E+08 | .233E+07 | 608.08 | |
| | PEAK | 8.00 | 0. | 0. | -5008602. | -1053. | -8709467. | 0. | 0. | 0. | .622E+08 | .211E+07 | 601.90 |
| | NON-PEAK | 3.30 | 0. | 0. | -2066048. | -393. | 0. | 0. | 0. | .601E+08 | .207E+07 | 600.97 | |
| 13 | PEAK | 2.70 | 0. | 0. | -11730000. | -1690403. | -316. | 0. | 0. | .702E+08 | .224E+07 | 605.49 | |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -758. | 0. | 0. | 0. | .664E+08 | .218E+07 | 608.08 | |
| | PEAK | 4.00 | 0. | 0. | -2504301. | -492. | 0. | 0. | 0. | .759E+08 | .233E+07 | 601.90 | |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1053. | -8709467. | 0. | 0. | 0. | .622E+08 | .211E+07 | 600.97 |
| | PEAK | 3.30 | 0. | 0. | -2066048. | -393. | 0. | 0. | 0. | .601E+08 | .207E+07 | 600.97 | |
| 14 | PEAK | 2.70 | 0. | 0. | -11730000. | -1690403. | -316. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -758. | 0. | 0. | 0. | .622E+08 | .211E+07 | 601.90 | |
| | PEAK | 4.00 | 0. | 0. | -2504301. | -492. | 0. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1053. | -8709467. | 0. | 0. | 0. | .622E+08 | .211E+07 | 601.90 |
| | PEAK | 3.30 | 0. | 0. | -2066048. | -393. | 0. | 0. | 0. | .601E+08 | .207E+07 | 600.97 | |
| 15 | PEAK | 2.70 | 0. | 0. | -11730000. | -1690403. | -316. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -758. | 0. | 0. | 0. | .622E+08 | .211E+07 | 608.08 | |
| | PEAK | 4.00 | 0. | 0. | -2504301. | -492. | 0. | 0. | 0. | .664E+08 | .218E+07 | 601.90 | |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1053. | -8709468. | 0. | 0. | 0. | .622E+08 | .211E+07 | 601.90 |
| | NON-PEAK | 3.30 | 0. | 0. | -2066048. | -393. | 0. | 0. | 0. | .601E+08 | .207E+07 | 600.97 | |

| | | | | | | | | | | | |
|----|----------|------|----|-----------|------------|-----------|-----------|----------|----------|----------|--------|
| 16 | PEAK | 2.70 | 0. | 11730000. | -1690403. | -316. | 0. | .702E+08 | .224E+07 | 605.49 | |
| | NON-PEAK | 6.00 | 0. | -3756452. | -758. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| | PEAK | 4.00 | 0. | 12008280. | -2504301. | -492. | 0. | .759E+08 | .233E+07 | 608.08 | |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1053. | -8709467. | 0. | .622E+08 | .211E+07 | 601.90 |
| | PEAK | 3.30 | 0. | 0. | -2066048. | -393. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| 17 | PEAK | 2.70 | 0. | 11730000. | -1690403. | -316. | 0. | .702E+08 | .224E+07 | 605.49 | |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -758. | 0. | 0. | .664E+08 | .218E+07 | 603.80 |
| | PEAK | 4.00 | 0. | 12008280. | -2504301. | -492. | 0. | .759E+08 | .233E+07 | 608.08 | |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1053. | -8709467. | 0. | .622E+08 | .211E+07 | 600.97 |
| 18 | PEAK | 3.30 | 0. | 0. | -2066048. | -393. | 0. | 0. | .702E+08 | .224E+07 | 603.80 |
| | NON-PEAK | 2.70 | 0. | 0. | -3756452. | -758. | 0. | 0. | .664E+08 | .218E+07 | 601.90 |
| | PEAK | 6.00 | 0. | 0. | -2504301. | -492. | 0. | 0. | .759E+08 | .233E+07 | 608.08 |
| | NON-PEAK | 4.00 | 0. | 0. | -1690403. | -1053. | -8709467. | 0. | .622E+08 | .211E+07 | 601.90 |
| | PEAK | 8.00 | 0. | 0. | -2066048. | -393. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| 19 | PEAK | 3.30 | 0. | 0. | -1690403. | -316. | 0. | 0. | .702E+08 | .224E+07 | 605.49 |
| | NON-PEAK | 2.70 | 0. | 0. | -3756452. | -758. | 0. | 0. | .664E+08 | .218E+07 | 603.80 |
| | PEAK | 6.00 | 0. | 0. | -2504301. | -492. | 0. | 0. | .759E+08 | .233E+07 | 608.08 |
| | NON-PEAK | 4.00 | 0. | 0. | -1690403. | -1053. | -8709467. | 0. | .622E+08 | .211E+07 | 601.90 |
| | PEAK | 8.00 | 0. | 0. | -2066048. | -393. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| | NON-PEAK | 3.30 | 0. | 0. | -2066048. | -316. | 0. | 0. | .702E+08 | .224E+07 | 605.49 |
| 20 | PEAK | 2.70 | 0. | 0. | -11730000. | -1690403. | -492. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 6.00 | 0. | 0. | -2504301. | -758. | 0. | 0. | .622E+08 | .211E+07 | 601.90 |
| | PEAK | 4.00 | 0. | 0. | -12008280. | -1053. | -8709467. | 0. | .759E+08 | .233E+07 | 608.08 |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -393. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| | PEAK | 3.30 | 0. | 0. | -2066048. | -316. | 0. | 0. | .702E+08 | .224E+07 | 605.49 |
| 21 | PEAK | 2.70 | 0. | 0. | -11730000. | -1690403. | -492. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -758. | 0. | 0. | .622E+08 | .211E+07 | 601.90 |
| | PEAK | 4.00 | 0. | 0. | -12008280. | -1053. | -8709467. | 0. | .759E+08 | .233E+07 | 608.08 |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -393. | 0. | 0. | .601E+08 | .207E+07 | 600.97 |
| | PEAK | 3.30 | 0. | 0. | -2066048. | -316. | 0. | 0. | .702E+08 | .224E+07 | 603.80 |
| 22 | PEAK | 2.02 | 0. | 0. | 8983975. | -1264672. | -237. | 0. | .679E+08 | .220E+07 | 604.44 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -745. | 0. | 0. | .641E+08 | .214E+07 | 602.75 |
| | PEAK | 4.00 | 0. | 0. | 8983974. | -2504301. | -483. | 0. | .706E+08 | .224E+07 | 605.67 |
| | NON-PEAK | 8.00 | 0. | 0. | -2066048. | -393. | -5068359. | 0. | .626E+08 | .212E+07 | 602.09 |
| | PEAK | 3.30 | 0. | 0. | -2879946. | -583. | 0. | 0. | .580E+08 | .204E+07 | 600.01 |
| | NON-PEAK | 4.60 | 0. | 0. | -4620435. | -881. | 0. | 0. | .657E+08 | .217E+07 | 603.48 |
| | PEAK | 7.38 | 0. | 0. | -4620435. | -745. | 0. | 0. | .620E+08 | .210E+07 | 601.79 |
| | NON-PEAK | 2.02 | 0. | 0. | 8983975. | -1264672. | -233. | 0. | .657E+08 | .217E+07 | 603.48 |
| 23 | PEAK | 6.00 | 0. | 0. | -3756452. | -734. | 0. | 0. | .620E+08 | .210E+07 | 601.79 |
| | NON-PEAK | 4.00 | 0. | 0. | -2504301. | -475. | 0. | 0. | .685E+08 | .221E+07 | 604.71 |
| | PEAK | 4.60 | 0. | 0. | -2879946. | -574. | -2939247. | 0. | .626E+08 | .212E+07 | 602.09 |
| | NON-PEAK | 7.38 | 0. | 0. | -4620435. | -881. | 0. | 0. | .580E+08 | .204E+07 | 600.01 |
| | PEAK | 2.02 | 0. | 0. | 8983975. | -1264672. | -233. | 0. | .657E+08 | .217E+07 | 603.48 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -734. | 0. | 0. | .620E+08 | .210E+07 | 601.79 |
| | PEAK | 4.00 | 0. | 0. | -2504301. | -475. | 0. | 0. | .685E+08 | .221E+07 | 604.71 |
| | NON-PEAK | 4.60 | 0. | 0. | 8983974. | -2504301. | -574. | 0. | .626E+08 | .212E+07 | 602.09 |
| | NON-PEAK | 7.38 | 0. | 0. | -2879946. | -574. | -2939247. | 0. | .580E+08 | .204E+07 | 600.01 |
| | NON-PEAK | 7.38 | 0. | 0. | -4620435. | -881. | 0. | 0. | .657E+08 | .217E+07 | 603.48 |

File name: ENGINTO.OUT for year 1963 with project operation schedule

| MONTH OF : OCTOBER | | YEAR : 1963 | | ENERGY GENERATION IN U/S, D/S POWER HOUSE AND % MEETING DEMAND | | | |
|--------------------|----------|-------------|---------------|--|-------------|---------------------|--------------|
| DATE | PERIOD | DURATION | GROSSH (M) | NETTH (M) | Q (M3/S) | STARTP (MW) | ENDP (MW) |
| | | (HR) | | | | AV. ENERGY (MWh) | QD (M3/S) |
| 1 | PEAK | 2.10 | 227. | 213. | 1192. | 2114. | 4483. |
| | NON-PEAK | 6.00 | 228. | 228. | 0. | 0. | 66. |
| | PEAK | 4.00 | 227. | 226. | 237. | 450. | 448. |
| | NON-PEAK | 8.00 | 228. | 228. | 0. | 0. | 1795. |
| | NON-PEAK | 3.90 | 228. | 228. | 0. | 0. | 66. |
| 2 | PEAK | 2.10 | 224. | 209. | 1192. | 2118. | 2078. |
| | NON-PEAK | 6.00 | 224. | 224. | 0. | 0. | 4405. |
| | PEAK | 4.00 | 220. | 216. | 649. | 1190. | 1169. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 4717. |
| | NON-PEAK | 3.90 | 224. | 224. | 0. | 0. | 66. |
| 3 | PEAK | 2.10 | 220. | 205. | 1192. | 2082. | 2042. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 4329. |
| | PEAK | 4.00 | 218. | 213. | 649. | 1170. | 1154. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 4649. |
| | NON-PEAK | 3.90 | 221. | 221. | 0. | 0. | 66. |
| 4 | PEAK | 2.10 | 218. | 203. | 1192. | 2051. | 2020. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 4275. |
| | NON-PEAK | 4.00 | 218. | 213. | 649. | 1158. | 1154. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 4624. |
| | NON-PEAK | 3.90 | 221. | 221. | 0. | 0. | 66. |
| 5 | PEAK | 2.10 | 218. | 203. | 1192. | 2051. | 2020. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 4275. |
| | NON-PEAK | 4.00 | 218. | 213. | 649. | 1158. | 1154. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 4624. |
| | NON-PEAK | 3.90 | 221. | 221. | 0. | 0. | 66. |
| 6 | PEAK | 2.10 | 218. | 203. | 1192. | 2051. | 2020. |
| | NON-PEAK | 6.00 | 218. | 213. | 649. | 1158. | 1154. |
| | NON-PEAK | 4.00 | 218. | 213. | 0. | 0. | 4624. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 66. |
| | NON-PEAK | 3.90 | 221. | 221. | 0. | 0. | 66. |
| 7 | PEAK | 2.10 | 218. | 203. | 1192. | 2051. | 2020. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 4275. |
| | PEAK | 4.00 | 218. | 213. | 649. | 1158. | 1154. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 4624. |
| | NON-PEAK | 3.90 | 221. | 221. | 0. | 0. | 66. |

| | | | | | | | | | |
|----------|------|------|------|-------|-------|-------|-------|-----|-------|
| 8 PEAK | 2.10 | 218. | 203. | 1192. | 2051. | 2020. | 4275. | 86. | 4361. |
| NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. |
| PEAK | 4.00 | 218. | 213. | 649. | 1158. | 1154. | 4624. | 66. | 247. |
| NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 165. |
| PEAK | 3.90 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 4789. |
| NON-PEAK | 2.10 | 218. | 203. | 1192. | 2051. | 2020. | 4275. | 66. | 100. |
| 9 PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. |
| NON-PEAK | 4.00 | 218. | 218. | 649. | 1158. | 1154. | 4624. | 66. | 100. |
| PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 329. |
| NON-PEAK | 3.90 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 160. |
| 10 PEAK | 2.10 | 218. | 203. | 1192. | 2051. | 2020. | 4275. | 66. | 160. |
| NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 86. |
| PEAK | 4.00 | 218. | 213. | 649. | 1158. | 1154. | 4624. | 66. | 4361. |
| NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. |
| PEAK | 3.90 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 100. |
| NON-PEAK | 2.10 | 218. | 203. | 1192. | 2051. | 2020. | 4275. | 66. | 100. |
| 11 PEAK | 2.20 | 218. | 204. | 1157. | 1999. | 1968. | 4364. | 66. | 247. |
| NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 165. |
| PEAK | 4.00 | 218. | 218. | 679. | 1211. | 1207. | 4835. | 66. | 4789. |
| NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 100. |
| 12 PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 329. |
| NON-PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 100. |
| 13 PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. |
| NON-PEAK | 4.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 100. |
| PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 156. |
| NON-PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 4454. |
| 14 PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 100. |
| NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. |
| PEAK | 4.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 100. |
| NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 4999. |
| 15 PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 100. |
| NON-PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 100. |
| PEAK | 6.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 100. |
| NON-PEAK | 4.00 | 218. | 213. | 0. | 0. | 0. | 0. | 66. | 156. |
| PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 4457. |
| NON-PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 100. |
| PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 247. |
| NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 100. |
| PEAK | 4.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 100. |
| NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 4999. |
| 15 PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 100. |
| NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. |
| PEAK | 4.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 100. |
| NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 156. |
| 15 PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 4457. |
| NON-PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 100. |
| PEAK | 6.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 247. |
| NON-PEAK | 4.00 | 218. | 213. | 0. | 0. | 0. | 0. | 66. | 100. |
| PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 4999. |
| NON-PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 100. |
| PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 329. |
| NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 156. |
| PEAK | 4.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 4457. |
| NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 100. |
| 15 PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. |
| NON-PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 100. |
| PEAK | 6.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 4999. |
| NON-PEAK | 4.00 | 218. | 213. | 0. | 0. | 0. | 0. | 66. | 100. |
| PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 329. |
| NON-PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 156. |

| | | | | | | | | | | |
|----|----------|------|------|------|-------|-------|-------|-------|-----|-------|
| 16 | PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 91. | 4457. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. |
| | PEAK | 4.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 165. |
| | NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 4999. |
| | NON-PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 329. |
| 17 | PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 156. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 91. |
| | PEAK | 4.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 165. |
| | NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 4999. |
| | NON-PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 329. |
| 18 | PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 156. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. |
| | PEAK | 4.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 165. |
| | NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 4999. |
| | NON-PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 329. |
| 19 | PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 156. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. |
| | PEAK | 4.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 165. |
| | NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 4999. |
| | NON-PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 329. |
| 20 | PEAK | 2.20 | 218. | 204. | 1157. | 2001. | 1968. | 4366. | 66. | 156. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. |
| | PEAK | 4.00 | 218. | 213. | 679. | 1211. | 1207. | 4835. | 66. | 165. |
| | NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 66. | 4999. |
| | NON-PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 329. |
| 21 | PEAK | 1.00 | 218. | 205. | 1192. | 2053. | 2035. | 2044. | 66. | 156. |
| | NON-PEAK | 6.00 | 220. | 220. | 0. | 0. | 0. | 0. | 66. | 247. |
| | PEAK | 4.00 | 219. | 218. | 309. | 564. | 561. | 2249. | 66. | 165. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 329. |
| | NON-PEAK | 3.80 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 156. |
| 22 | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 66. | 2414. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. |
| | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 66. | 206. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 206. |
| | PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 206. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. |
| 23 | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 66. | 206. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 206. |
| | PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 206. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. |
| | PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 206. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. |

| TOTAL | | WATERFALL & 10 DAILY TPP SUPPLY = | | | | | | | | | |
|-------|----------|-----------------------------------|------|------|-------|-------|-------|-------|-------|-------|-------|
| 24 | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 2021. | 2062. | 41. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 165. | 2403. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. | 206. |
| 25 | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 2021. | 2062. | 41. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 165. | 2403. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 5.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 2021. | 2062. | 41. |
| 26 | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 2021. | 2062. | 41. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 165. | 2403. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. | 206. |
| 27 | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 2021. | 2062. | 41. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 165. | 2403. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. | 206. |
| 28 | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 2021. | 2062. | 41. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | NON-PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 165. | 2403. |
| | PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. | 206. |
| 29 | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 2021. | 2062. | 41. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 165. | 2403. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 5.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 2021. | 2062. | 41. |
| 30 | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 2021. | 2062. | 41. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 165. | 2403. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. | 206. |
| 31 | PEAK | 1.00 | 218. | 203. | 1192. | 2022. | 2021. | 2021. | 2021. | 2062. | 41. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 218. | 217. | 309. | 560. | 559. | 2238. | 66. | 165. | 2403. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. | 206. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. | 206. |
| | NON-PEAK | 5.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 206. | 206. |

MONTH OF : NOVEMBER YEAR : 1963 ENERGY GENERATION IN U/S, D/S POWER HOUSE AND % MEETING IRR.DEMAND

| DATE | PERIOD | DURATION (HR) | GROSSH (M) | NETTH (M) | Q (M3/S) | STARTP (MW) | ENDP (MW) | AV. ENERGY (MWh) | QD (M3/S) | ENERGY (MWh) | TOT. ENERGY (MWh) | IRR. (%) |
|----------|--------|---------------|------------|-----------|----------|-------------|-----------|------------------|-----------|--------------|-------------------|----------|
| 1 PEAK | .60 | 218. | 203. | 1227. | 2072. | 2072. | 1243. | 132. | 49. | 1293. | 100. | |
| NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. | |
| PEAK | 4.00 | 219. | 218. | 185. | 338. | 337. | 1351. | 132. | 329. | 329. | 100. | |
| NON-PEAK | 8.00 | 220. | 220. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. | |
| NON-PEAK | 5.40 | 220. | 220. | 0. | 0. | 0. | 0. | 132. | 445. | 445. | 100. | |
| 2 PEAK | .60 | 219. | 204. | 1227. | 2092. | 2082. | 1252. | 132. | 49. | 1302. | 100. | |
| NON-PEAK | 6.00 | 220. | 220. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. | |
| PEAK | 4.00 | 220. | 219. | 185. | 340. | 339. | 1357. | 132. | 329. | 329. | 100. | |
| NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. | |
| NON-PEAK | 5.40 | 221. | 221. | 0. | 0. | 0. | 0. | 132. | 445. | 445. | 100. | |
| 3 PEAK | .60 | 220. | 205. | 1227. | 2104. | 2093. | 1259. | 132. | 49. | 1309. | 100. | |
| NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. | |
| PEAK | 4.00 | 221. | 221. | 185. | 341. | 341. | 1365. | 132. | 329. | 329. | 100. | |
| NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. | |
| NON-PEAK | 5.40 | 222. | 222. | 0. | 0. | 0. | 0. | 132. | 445. | 445. | 100. | |
| 4 PEAK | .60 | 221. | 206. | 1227. | 2117. | 2105. | 1267. | 132. | 49. | 1316. | 100. | |
| NON-PEAK | 6.00 | 223. | 223. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. | |
| PEAK | 4.00 | 222. | 222. | 185. | 343. | 343. | 1372. | 132. | 329. | 329. | 100. | |
| NON-PEAK | 5.40 | 222. | 223. | 0. | 0. | 0. | 0. | 132. | 445. | 445. | 100. | |
| NON-PEAK | 6.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 49. | 1316. | 100. | |
| NON-PEAK | 8.00 | 223. | 224. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. | |
| NON-PEAK | 5.40 | 224. | 224. | 185. | 345. | 345. | 1380. | 132. | 329. | 329. | 100. | |
| 5 PEAK | .60 | 222. | 207. | 1227. | 2129. | 2118. | 1274. | 132. | 49. | 1323. | 100. | |
| NON-PEAK | 6.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. | |
| NON-PEAK | 8.00 | 223. | 223. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. | |
| NON-PEAK | 5.40 | 224. | 224. | 185. | 345. | 345. | 1380. | 132. | 329. | 329. | 100. | |
| 6 PEAK | .60 | 224. | 208. | 1227. | 2142. | 2130. | 1282. | 132. | 49. | 1331. | 100. | |
| NON-PEAK | 6.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. | |
| PEAK | 4.00 | 225. | 224. | 185. | 347. | 347. | 1387. | 132. | 329. | 329. | 100. | |
| NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. | |
| NON-PEAK | 5.40 | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 445. | 445. | 100. | |
| 7 PEAK | .60 | 225. | 209. | 1227. | 2154. | 2143. | 1289. | 132. | 49. | 1338. | 100. | |
| NON-PEAK | 6.00 | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. | |
| PEAK | 4.00 | 226. | 149. | 281. | 281. | 1125. | 132. | 329. | 329. | 1454. | 100. | |
| NON-PEAK | 8.00 | 227. | 227. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. | |
| NON-PEAK | 5.40 | 227. | 227. | 0. | 0. | 0. | 0. | 132. | 445. | 445. | 100. | |

| | | | | | | | | | | | |
|----|----------|------|------|------|-------|-------|-------|-------|------|------|-------|
| 8 | PEAK | 6.00 | 226. | 211. | 1227. | 2167. | 2155. | 1297. | 132. | 49. | 1346. |
| | NON-PEAK | 6.00 | 227. | 227. | 0. | 0. | 0. | 0. | 132. | 494. | 494. |
| | PEAK | 4.00 | 227. | 227. | 149. | 283. | 283. | 1131. | 132. | 329. | 1460. |
| | NON-PEAK | 8.00 | 228. | 228. | 0. | 0. | 0. | 0. | 132. | 659. | 659. |
| | NON-PEAK | 5.40 | 228. | 228. | 0. | 0. | 0. | 0. | 132. | 445. | 445. |
| 9 | PEAK | .60 | 227. | 212. | 1227. | 2179. | 2168. | 1304. | 132. | 49. | 1353. |
| | NON-PEAK | 6.00 | 229. | 229. | 0. | 0. | 0. | 0. | 132. | 494. | 494. |
| | PEAK | 4.00 | 229. | 228. | 149. | 284. | 284. | 1137. | 132. | 329. | 1467. |
| | NON-PEAK | 8.00 | 229. | 229. | 0. | 0. | 0. | 0. | 132. | 659. | 659. |
| | NON-PEAK | 5.40 | 230. | 230. | 0. | 0. | 0. | 0. | 132. | 445. | 445. |
| 10 | PEAK | .60 | 229. | 213. | 1227. | 2192. | 2180. | 1312. | 132. | 49. | 1361. |
| | NON-PEAK | 6.00 | 230. | 230. | 0. | 0. | 0. | 0. | 132. | 494. | 494. |
| | PEAK | 4.00 | 230. | 230. | 149. | 286. | 286. | 1143. | 132. | 329. | 1473. |
| | NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 659. | 659. |
| | NON-PEAK | 5.40 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 445. | 445. |
| 11 | PEAK | .70 | 230. | 215. | 1198. | 2162. | 2147. | 1508. | 132. | 58. | 1566. |
| | NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 494. | 494. |
| | PEAK | 4.00 | 231. | 231. | 149. | 287. | 287. | 1149. | 132. | 329. | 1479. |
| | NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 450. | 450. |
| | NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 332. | 332. |
| 12 | PEAK | .70 | 230. | 215. | 1198. | 2166. | 2152. | 1511. | 132. | 58. | 1569. |
| | NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 124. | 467. | 467. |
| | PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 329. | 1481. |
| | NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 64. | 319. | 319. |
| | NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 332. | 332. |
| 13 | PEAK | .70 | 230. | 215. | 1198. | 2166. | 2152. | 1511. | 132. | 58. | 1569. |
| | NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 124. | 467. | 467. |
| | PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 329. | 1481. |
| | NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 64. | 319. | 319. |
| | NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 332. | 332. |
| 14 | PEAK | .70 | 230. | 215. | 1198. | 2166. | 2152. | 1511. | 132. | 58. | 1569. |
| | NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 124. | 467. | 467. |
| | PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 329. | 1481. |
| | NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 64. | 319. | 319. |
| | NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 332. | 332. |
| 15 | PEAK | .70 | 230. | 215. | 1198. | 2166. | 2152. | 1511. | 132. | 58. | 1569. |
| | NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 124. | 467. | 467. |
| | PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 329. | 1481. |
| | NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 64. | 319. | 319. |
| | NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 332. | 332. |

| | | | | | | | | | |
|----------|------|------|-------|-------|-------|-------|-------|-------|-------|
| 16 PEAK | 230. | 215. | 1198. | 2166. | 2152. | 1511. | 132. | 1569. | 100. |
| NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 467. | 94. |
| PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 100. |
| NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 329. | 1481. |
| NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 64. | 319. |
| NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 332. | 76. |
| 17 PEAK | 70 | 230. | 215. | 1198. | 2166. | 2152. | 1511. | 132. | 100. |
| NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 58. | 1569. |
| PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 467. |
| NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 124. | 94. |
| NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 100. |
| 18 PEAK | 70 | 230. | 215. | 1198. | 2166. | 2152. | 1511. | 132. | 329. |
| NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 124. | 1481. |
| PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 319. |
| NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 64. | 48. |
| NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 332. |
| 19 PEAK | 70 | 230. | 215. | 1198. | 2166. | 2152. | 1511. | 132. | 58. |
| NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 124. | 1569. |
| PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 467. |
| NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 64. | 1481. |
| NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 319. |
| NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 124. | 48. |
| 20 PEAK | 70 | 230. | 215. | 1198. | 2166. | 2152. | 1511. | 132. | 329. |
| NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 64. | 332. |
| PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 58. |
| NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 1569. |
| NON-PEAK | 5.30 | 231. | 231. | 0. | 0. | 0. | 0. | 124. | 467. |
| 21 PEAK | 80 | 230. | 216. | 1146. | 2083. | 2068. | 1661. | 132. | 467. |
| NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 64. | 1481. |
| PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 319. |
| NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 64. | 48. |
| NON-PEAK | 5.20 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 332. |
| 22 PEAK | 80 | 230. | 216. | 1146. | 2083. | 2068. | 1661. | 132. | 58. |
| NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 1726. |
| PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 290. |
| NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 326. |
| NON-PEAK | 5.20 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 76. |
| 23 PEAK | 80 | 230. | 216. | 1146. | 2083. | 2068. | 1661. | 132. | 66. |
| NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 1726. |
| PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 290. |
| NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 326. |
| NON-PEAK | 5.20 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 76. |
| 23 PEAK | 80 | 230. | 216. | 1146. | 2083. | 2068. | 1661. | 132. | 66. |
| NON-PEAK | 6.00 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 1726. |
| PEAK | 4.00 | 231. | 231. | 149. | 288. | 288. | 1151. | 132. | 290. |
| NON-PEAK | 8.00 | 231. | 231. | 0. | 0. | 0. | 0. | 100. | 326. |
| NON-PEAK | 5.20 | 231. | 231. | 0. | 0. | 0. | 0. | 132. | 76. |

MONTH OF : DECEMBER YEAR : 1963 ENERGY GENERATION IN U/S, D/S POWER HOUSE AND & MEETING IRR. DEMAND

| | DATE | PERIOD | DURATION (HR) | GROSSH (M) | NETTH (M) | Q (M3/S) | STARTP (MW) | ENDP (MW) | AV. ENERGY (MWh) | QD (M3/S) | ENERGY TOT. ENERGY (MWh) | IRR. (8) |
|---|----------|--------|------------------|---------------|--------------|-------------|----------------|--------------|---------------------|--------------|-----------------------------|-------------|
| 1 | PEAK | 2.30 | 227. | 211. | 1235. | 2224. | 2178. | 5062. | 174. | 250. | 5313. | 100. |
| | NON-PEAK | 6.00 | 229. | 229. | 0. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| | PEAK | 4.00 | 225. | 220. | 710. | 1325. | 1303. | 5255. | 174. | 435. | 5690. | 100. |
| | NON-PEAK | 8.00 | 228. | 228. | 0. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.70 | 229. | 229. | 0. | 0. | 0. | 0. | 0. | 174. | 402. | 100. |
| 2 | PEAK | 2.30 | 224. | 209. | 1235. | 2195. | 2152. | 4998. | 174. | 250. | 5248. | 100. |
| | NON-PEAK | 6.00 | 226. | 226. | 0. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| | PEAK | 4.00 | 223. | 217. | 710. | 1309. | 1287. | 5194. | 174. | 435. | 5629. | 100. |
| | NON-PEAK | 8.00 | 227. | 227. | 0. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.70 | 228. | 228. | 0. | 0. | 0. | 0. | 0. | 174. | 402. | 100. |
| 3 | PEAK | 2.30 | 224. | 209. | 1235. | 2193. | 2149. | 4993. | 174. | 250. | 5243. | 100. |
| | NON-PEAK | 6.00 | 226. | 226. | 0. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| | PEAK | 4.00 | 222. | 217. | 710. | 1308. | 1286. | 5188. | 174. | 435. | 5623. | 100. |
| | NON-PEAK | 8.00 | 227. | 227. | 0. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.70 | 228. | 228. | 0. | 0. | 0. | 0. | 0. | 174. | 402. | 100. |
| 4 | PEAK | 2.30 | 224. | 208. | 1235. | 2190. | 2147. | 4988. | 174. | 250. | 5243. | 100. |
| | NON-PEAK | 6.00 | 226. | 226. | 0. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| | PEAK | 4.00 | 222. | 217. | 710. | 1307. | 1285. | 5183. | 174. | 435. | 5623. | 100. |
| | NON-PEAK | 8.00 | 228. | 228. | 0. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.70 | 227. | 227. | 0. | 0. | 0. | 0. | 0. | 174. | 402. | 100. |
| 5 | PEAK | 2.30 | 224. | 208. | 1235. | 2188. | 2145. | 4983. | 174. | 250. | 5238. | 100. |
| | NON-PEAK | 6.00 | 226. | 226. | 0. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| | PEAK | 4.00 | 222. | 217. | 710. | 1307. | 1285. | 5183. | 174. | 435. | 5618. | 100. |
| | NON-PEAK | 8.00 | 227. | 227. | 0. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.70 | 228. | 228. | 0. | 0. | 0. | 0. | 0. | 174. | 402. | 100. |
| 6 | PEAK | 2.30 | 224. | 208. | 1235. | 2186. | 2143. | 4978. | 174. | 250. | 5233. | 100. |
| | NON-PEAK | 6.00 | 226. | 226. | 0. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| | PEAK | 4.00 | 222. | 217. | 710. | 1306. | 1284. | 5178. | 174. | 435. | 5613. | 100. |
| | NON-PEAK | 8.00 | 227. | 227. | 0. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.70 | 228. | 228. | 0. | 0. | 0. | 0. | 0. | 174. | 402. | 100. |
| 7 | PEAK | 2.30 | 224. | 208. | 1235. | 2186. | 2143. | 4978. | 174. | 250. | 5228. | 100. |
| | NON-PEAK | 6.00 | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| | PEAK | 4.00 | 222. | 216. | 710. | 1304. | 1282. | 5173. | 174. | 435. | 5608. | 100. |
| | NON-PEAK | 8.00 | 227. | 227. | 0. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.70 | 228. | 228. | 0. | 0. | 0. | 0. | 0. | 174. | 402. | 100. |
| | NON-PEAK | 2.30 | 223. | 208. | 1235. | 2184. | 2140. | 4973. | 174. | 250. | 5223. | 100. |
| | NON-PEAK | 6.00 | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| | PEAK | 4.00 | 221. | 216. | 710. | 1303. | 1281. | 5168. | 174. | 435. | 5603. | 100. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.70 | 227. | 227. | 0. | 0. | 0. | 0. | 0. | 174. | 402. | 100. |

| | | | | | | | | | | |
|----|----------|------|------|------|-------|-------|-------|-------|------|-------|
| 8 | PEAK | 2.30 | 223. | 208. | 1235. | 2182. | 2138. | 4968. | 174. | 5218. |
| | NON-PEAK | 6.00 | 225. | 225. | 0. | 0. | 0. | 0. | 174. | 653. |
| | PEAK | 4.00 | 221. | 216. | 710. | 1302. | 1280. | 5163. | 174. | 435. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 174. | 5598. |
| | NON-PEAK | 3.70 | 227. | 227. | 0. | 0. | 0. | 0. | 174. | 870. |
| 9 | PEAK | 2.30 | 223. | 207. | 1235. | 2179. | 2136. | 4963. | 174. | 402. |
| | NON-PEAK | 6.00 | 225. | 225. | 0. | 0. | 0. | 0. | 174. | 250. |
| | PEAK | 4.00 | 221. | 216. | 710. | 1300. | 1278. | 5158. | 174. | 5213. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 174. | 653. |
| | NON-PEAK | 3.70 | 227. | 227. | 0. | 0. | 0. | 0. | 174. | 435. |
| 10 | PEAK | 2.30 | 223. | 207. | 1235. | 2177. | 2134. | 4957. | 174. | 5593. |
| | NON-PEAK | 6.00 | 224. | 224. | 0. | 0. | 0. | 0. | 174. | 870. |
| | PEAK | 4.00 | 221. | 216. | 710. | 1299. | 1277. | 5153. | 174. | 402. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 174. | 402. |
| | NON-PEAK | 3.70 | 227. | 227. | 0. | 0. | 0. | 0. | 174. | 5208. |
| 11 | PEAK | 2.70 | 222. | 207. | 1207. | 2132. | 2083. | 5690. | 174. | 653. |
| | NON-PEAK | 6.00 | 224. | 224. | 0. | 0. | 0. | 0. | 174. | 435. |
| | PEAK | 4.00 | 219. | 212. | 834. | 1506. | 1474. | 5960. | 174. | 5588. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 174. | 870. |
| | NON-PEAK | 3.30 | 227. | 227. | 0. | 0. | 0. | 0. | 174. | 402. |
| 12 | PEAK | 2.70 | 222. | 207. | 1207. | 2129. | 2081. | 5684. | 174. | 5984. |
| | NON-PEAK | 6.00 | 223. | 223. | 0. | 0. | 0. | 0. | 174. | 653. |
| | PEAK | 4.00 | 219. | 212. | 834. | 1504. | 1473. | 5954. | 174. | 6395. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 0. | 174. | 870. |
| | NON-PEAK | 3.30 | 226. | 226. | 0. | 0. | 0. | 0. | 174. | 359. |
| 13 | PEAK | 2.70 | 222. | 207. | 1207. | 2127. | 2079. | 5678. | 174. | 5978. |
| | NON-PEAK | 6.00 | 223. | 223. | 0. | 0. | 0. | 0. | 174. | 653. |
| | PEAK | 4.00 | 219. | 212. | 834. | 1503. | 1471. | 5948. | 174. | 6383. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 0. | 174. | 359. |
| | NON-PEAK | 3.30 | 226. | 226. | 0. | 0. | 0. | 0. | 174. | 870. |
| 14 | PEAK | 2.70 | 221. | 206. | 1207. | 2125. | 2077. | 5673. | 174. | 359. |
| | NON-PEAK | 6.00 | 223. | 223. | 0. | 0. | 0. | 0. | 174. | 5966. |
| | PEAK | 4.00 | 218. | 211. | 834. | 1501. | 1470. | 5942. | 174. | 359. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 0. | 174. | 870. |
| | NON-PEAK | 3.30 | 226. | 226. | 0. | 0. | 0. | 0. | 174. | 359. |
| 15 | PEAK | 2.70 | 221. | 206. | 1207. | 2123. | 2075. | 5667. | 174. | 5960. |
| | NON-PEAK | 6.00 | 223. | 223. | 0. | 0. | 0. | 0. | 174. | 653. |
| | PEAK | 4.00 | 218. | 211. | 834. | 1500. | 1468. | 5936. | 174. | 6371. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 0. | 174. | 870. |
| | NON-PEAK | 3.30 | 226. | 226. | 0. | 0. | 0. | 0. | 174. | 359. |

| | | | | | | | |
|----|----------|------|------|-------|-------|-------|-------|
| 16 | PEAK | 2.70 | 221. | 2121. | 2072. | 5661. | 294. |
| | NON-PEAK | 6.00 | 223. | 0. | 0. | 0. | 174. |
| | PEAK | 4.00 | 218. | 211. | 1498. | 1467. | 5930. |
| | NON-PEAK | 8.00 | 225. | 0. | 0. | 0. | 174. |
| | NON-PEAK | 3.30 | 225. | 0. | 0. | 0. | 174. |
| 17 | PEAK | 2.70 | 221. | 206. | 2119. | 2070. | 5655. |
| | NON-PEAK | 6.00 | 222. | 0. | 0. | 0. | 174. |
| | PEAK | 4.00 | 218. | 211. | 834. | 1497. | 1465. |
| | NON-PEAK | 8.00 | 224. | 0. | 0. | 0. | 174. |
| | NON-PEAK | 3.30 | 225. | 0. | 0. | 0. | 174. |
| 18 | PEAK | 2.70 | 220. | 206. | 2107. | 2116. | 2068. |
| | NON-PEAK | 6.00 | 222. | 0. | 0. | 0. | 174. |
| | PEAK | 4.00 | 218. | 210. | 834. | 1495. | 1464. |
| | NON-PEAK | 8.00 | 224. | 0. | 0. | 0. | 174. |
| | NON-PEAK | 3.30 | 225. | 0. | 0. | 0. | 174. |
| 19 | PEAK | 2.70 | 220. | 205. | 1207. | 2114. | 2066. |
| | NON-PEAK | 6.00 | 222. | 0. | 0. | 0. | 174. |
| | PEAK | 4.00 | 217. | 210. | 834. | 1494. | 1462. |
| | NON-PEAK | 8.00 | 224. | 0. | 0. | 0. | 174. |
| | NON-PEAK | 3.30 | 225. | 0. | 0. | 0. | 174. |
| 20 | PEAK | 2.70 | 220. | 205. | 1207. | 2112. | 2064. |
| | NON-PEAK | 6.00 | 222. | 0. | 0. | 0. | 174. |
| | PEAK | 4.00 | 217. | 210. | 834. | 1492. | 1461. |
| | NON-PEAK | 8.00 | 224. | 0. | 0. | 0. | 174. |
| | NON-PEAK | 3.30 | 225. | 0. | 0. | 0. | 174. |
| 21 | PEAK | 2.02 | 221. | 205. | 1235. | 2153. | 2115. |
| | NON-PEAK | 6.00 | 223. | 0. | 0. | 0. | 174. |
| | PEAK | 4.00 | 220. | 216. | 624. | 1137. | 1121. |
| | NON-PEAK | 4.60 | 223. | 0. | 0. | 0. | 174. |
| | NON-PEAK | 7.38 | 225. | 0. | 0. | 0. | 174. |
| 22 | PEAK | 2.02 | 222. | 206. | 1235. | 2161. | 2123. |
| | NON-PEAK | 6.00 | 223. | 0. | 0. | 0. | 174. |
| | PEAK | 4.00 | 220. | 216. | 624. | 1142. | 1125. |
| | NON-PEAK | 4.60 | 223. | 0. | 0. | 0. | 174. |
| | NON-PEAK | 7.38 | 225. | 0. | 0. | 0. | 174. |
| 23 | PEAK | 2.02 | 221. | 206. | 1235. | 2159. | 2121. |
| | NON-PEAK | 6.00 | 223. | 0. | 0. | 0. | 174. |
| | PEAK | 4.00 | 220. | 216. | 624. | 1141. | 1124. |
| | NON-PEAK | 4.60 | 223. | 0. | 0. | 0. | 174. |
| | NON-PEAK | 7.38 | 225. | 0. | 0. | 0. | 174. |

File name: SROPRF0.OUT for year 1963 with proposed operation schedule

SUMMARY OF RESERVOIR OPERATION 1963

| MONTH OF | RUNOFF A (M3) | RUNOFF B (M3) | TOTAL (M3) | DEMAND (M3) | LOSS (MM/D) | SUPPLY (M3) | DEMAND (MW) | IRRIG. STATUS | IRRIG. (MW) | AV. POWER START (MW) | END (MW) | AV. ENERGY GENERATED (MWh) | SPILL AT B (M3) |
|-------------|---------------------|---------------------|---------------|----------------|----------------|----------------|----------------|------------------|----------------|----------------------------|-------------|----------------------------------|-----------------------|
| OCTOBER | .4310E+09 | .0000E+00 | .4310E+09 | .1762E+09 | 3.26 | .1762E+09 | SUCCEED | | 1875.11 | 1838.34 | 394476. | .237E+09 | |
| NOVEMBER | .2630E+09 | .0000E+00 | .2630E+09 | .3412E+09 | 2.27 | .3412E+09 | SUCCEED | | 1898.94 | 1851.35 | 386132. | .179E+08 | |
| DECEMBER | .2070E+09 | .0000E+00 | .2070E+09 | .4658E+09 | 1.36 | .4658E+09 | SUCCEED | | 1864.15 | 1816.81 | 391693. | .000E+00 | |
| | .9010E+09 | .0000E+00 | .9010E+09 | .9832E+09 | .9832E+09 | .9832E+09 | 100.00% | | | 1172301. | .255E+09 | | |

FRL. AT A = 830.00 M
 MDDL. AT A = 740.00 M
 MIN. ELEVATION AT A = 820.49 M

FRL. AT B = 612.00 M
 MDDL. AT B = 598.50 M
 MIN. ELEVATION AT B = 603.16 M

File name: ROAPRF0.OUT for year 1963 with proposed operation schedule

| MONTH OF : OCTOBER YEAR : 1963 OPERATION AT RESERVOIR A | | | | | | | |
|---|----------|----------|----------|---------------|-------------------|--------------|-------------------|
| DATE | PERIOD | DURATION | INFELA | QPUMP (M3) | EVAPLA (M3) | QA (M3) | SPILLA (M3) |
| | | | | | | AREA (M2) | EL.A (M) |
| 1 | PEAK | 3.00 | 1737903. | 0. | -17838.-13340000. | 0. | .354E+10 .438E+08 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35583.0. | 0. | .353E+10 .437E+08 |
| | PEAK | 4.00 | 2317204. | 0. | -23740.-3416324. | 0. | .353E+10 .437E+08 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47468.0. | 0. | .354E+10 .438E+08 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17819.0. | 0. | .354E+10 .438E+08 |
| 2 | PEAK | 3.00 | 1737903. | 0. | -17826.-13340000. | 0. | .353E+10 .437E+08 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35559.0. | 0. | .353E+10 .437E+08 |
| | PEAK | 4.00 | 2317204. | 0. | -23724.-13340000. | 0. | .352E+10 .436E+08 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47332.0. | 0. | .354E+10 .438E+08 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17836.0. | -1245696. | .354E+10 .438E+08 |
| 3 | PEAK | 3.00 | 1737903. | 0. | -17838.-13340000. | 0. | .353E+10 .437E+08 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35583.0. | 0. | .353E+10 .437E+08 |
| | PEAK | 4.00 | 2317204. | 0. | -23740.-13340000. | 0. | .352E+10 .436E+08 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47363.0. | 0. | .353E+10 .437E+08 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17779.0. | 0. | .353E+10 .437E+08 |
| 4 | PEAK | 3.00 | 1737903. | 0. | -17786.-13340000. | 0. | .352E+10 .436E+08 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35480.0. | 0. | .352E+10 .436E+08 |
| | PEAK | 4.00 | 2317204. | 0. | -23672.-13340000. | 0. | .351E+10 .435E+08 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47227.0. | 0. | .353E+10 .437E+08 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17796.0. | 0. | .353E+10 .437E+08 |
| 5 | PEAK | 3.00 | 1737903. | 0. | -17803.-13340000. | 0. | .352E+10 .436E+08 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35514.0. | 0. | .352E+10 .436E+08 |
| | PEAK | 4.00 | 2317204. | 0. | -23694.-13340000. | 0. | .351E+10 .435E+08 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47272.0. | 0. | .353E+10 .437E+08 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17813.0. | 0. | .354E+10 .438E+08 |
| 6 | PEAK | 3.00 | 1737903. | 0. | -17820.-13340000. | 0. | .352E+10 .436E+08 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35548.0. | 0. | .353E+10 .437E+08 |
| | PEAK | 4.00 | 2317204. | 0. | -23717.-13340000. | 0. | .352E+10 .436E+08 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47316.0. | 0. | .354E+10 .438E+08 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17830.0. | 0. | .354E+10 .438E+08 |
| 7 | PEAK | 3.00 | 1737903. | 0. | -17837.-13340000. | 0. | .353E+10 .437E+08 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35581.0. | 0. | .353E+10 .437E+08 |
| | PEAK | 4.00 | 2317204. | 0. | -23739.-13340000. | 0. | .352E+10 .436E+08 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47361.0. | 0. | .353E+10 .437E+08 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17779.0. | 0. | .353E+10 .437E+08 |

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|------|----------|----------|----------|-------------------|-------------------|----------|--------|
| 8 | PEAK | 3.00 | 1737903. | 0. | -17786.-13340000. | .436E+08 | 829.37 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35479. | .436E+08 | 829.45 |
| PEAK | 4.00 | 2317204. | 0. | -23671.-13340000. | .435E+08 | 829.17 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47225. | .437E+08 | 829.73 |
| PEAK | 3.00 | 1737903. | 0. | -17796. | .437E+08 | 829.77 | |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17802.-13340000. | .436E+08 | 829.47 |
| 9 | PEAK | 3.00 | 1737903. | 0. | -17802.-13340000. | .436E+08 | 829.47 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35512. | .436E+08 | 829.56 |
| PEAK | 4.00 | 2317204. | 0. | -23693.-13340000. | .435E+08 | 829.28 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47269. | .437E+08 | 829.84 |
| PEAK | 3.00 | 1737903. | 0. | -17812. | .438E+08 | 829.88 | |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17819.-13340000. | .436E+08 | 829.58 |
| 10 | PEAK | 3.00 | 1737903. | 0. | -17829. | .438E+08 | 829.99 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -17836.-13340000. | .437E+08 | 829.67 |
| PEAK | 4.00 | 2317204. | 0. | -17836.-13340000. | .436E+08 | 829.39 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47314. | .438E+08 | 829.95 |
| PEAK | 3.00 | 1737903. | 0. | -17846. | .437E+08 | 829.28 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -178546. | .437E+08 | 829.84 |
| PEAK | 4.00 | 2317204. | 0. | -23716.-13340000. | .437E+08 | 829.88 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47314. | .437E+08 | 829.58 |
| PEAK | 3.00 | 1737903. | 0. | -17829. | .437E+08 | 829.67 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -17836.-13340000. | .437E+08 | 829.39 |
| PEAK | 4.00 | 2317204. | 0. | -17836.-13340000. | .436E+08 | 829.95 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47359. | .438E+08 | 829.99 |
| PEAK | 3.00 | 1737903. | 0. | -17778. | .437E+08 | 829.66 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -17785.-13340000. | .437E+08 | 829.78 |
| PEAK | 4.00 | 2317204. | 0. | -17738.-13340000. | .436E+08 | 829.50 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47359. | .437E+08 | 829.61 |
| PEAK | 3.00 | 1737903. | 0. | -17778. | .437E+08 | 829.36 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -17785.-13340000. | .436E+08 | 829.45 |
| PEAK | 4.00 | 2317204. | 0. | -17738.-13340000. | .436E+08 | 829.45 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47359. | .437E+08 | 829.17 |
| PEAK | 3.00 | 1737903. | 0. | -17778. | .437E+08 | 829.72 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -17795. | .437E+08 | 829.77 |
| PEAK | 4.00 | 2317204. | 0. | -17802.-13340000. | .436E+08 | 829.47 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47223. | .435E+08 | 829.56 |
| PEAK | 3.00 | 1737903. | 0. | -17795. | .437E+08 | 829.83 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -17802.-13340000. | .436E+08 | 829.88 |
| PEAK | 4.00 | 2317204. | 0. | -35511. | .436E+08 | 829.56 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -23670.-13340000. | .435E+08 | 829.27 |
| PEAK | 3.00 | 1737903. | 0. | -47223. | .437E+08 | 829.72 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -17795. | .437E+08 | 829.77 |
| PEAK | 4.00 | 2317204. | 0. | -17812. | .436E+08 | 829.47 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -35511. | .436E+08 | 829.56 |
| PEAK | 3.00 | 1737903. | 0. | -17818.-13340000. | .435E+08 | 829.27 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -23692.-13340000. | .435E+08 | 829.67 |
| PEAK | 4.00 | 2317204. | 0. | -47267. | .437E+08 | 829.83 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -17812. | .437E+08 | 829.94 |
| PEAK | 3.00 | 1737903. | 0. | -17818.-13340000. | .436E+08 | 829.58 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35545. | .437E+08 | 829.67 |
| PEAK | 4.00 | 2317204. | 0. | -23715.-13340000. | .436E+08 | 829.38 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47312. | .437E+08 | 829.49 |
| PEAK | 3.00 | 1737903. | 0. | -17828. | .437E+08 | 829.61 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -17835.-13340000. | .437E+08 | 829.65 |
| PEAK | 4.00 | 2317204. | 0. | -35578. | .437E+08 | 829.78 | |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -23737.-13340000. | .436E+08 | 829.49 |
| PEAK | 3.00 | 1737903. | 0. | -47357. | .437E+08 | 829.61 | |
| | NON-PEAK | 6.00 | 3475807. | 0. | -17777. | .437E+08 | 829.65 |

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|----|----------|------|----------|-----------|-------------------|----------|--------|
| 16 | PEAK | 3.00 | 1737903. | 0. | -17784.-13340000. | .436E+08 | 829.36 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35476. | .351E+10 | 829.44 |
| | PEAK | 4.00 | 2317204. | 0. | -23669.-13340000. | .351E+10 | 829.16 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47220. | .353E+10 | 829.72 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17794. | .353E+10 | 829.76 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17801.-13340000. | .352E+10 | 829.46 |
| 17 | PEAK | 3.00 | 1737903. | 0. | -35509. | .352E+10 | 829.55 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -23691.-13340000. | .351E+10 | 829.27 |
| | PEAK | 4.00 | 2317204. | 0. | -47265. | .353E+10 | 829.83 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -17811. | .353E+10 | 829.87 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17818.-13340000. | .352E+10 | 829.57 |
| 18 | PEAK | 3.00 | 1737903. | 0. | -35543. | .353E+10 | 829.66 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -23714.-13340000. | .352E+10 | 829.38 |
| | PEAK | 4.00 | 2317204. | 0. | -47310. | .354E+10 | 829.94 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -17828. | .354E+10 | 829.98 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17834.-13340000. | .353E+10 | 829.68 |
| 19 | PEAK | 3.00 | 1737903. | 0. | -35577. | .353E+10 | 829.77 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -23736.-13340000. | .352E+10 | 829.49 |
| | PEAK | 4.00 | 2317204. | 0. | -47355. | .352E+10 | 829.60 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -17776. | .353E+10 | 829.65 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17783.-13340000. | .351E+10 | 829.35 |
| 20 | PEAK | 3.00 | 1737903. | 0. | -35474. | .352E+10 | 829.44 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -23668.-13340000. | .351E+10 | 829.16 |
| | PEAK | 4.00 | 2317204. | 0. | -23690.-13340000. | .351E+10 | 829.71 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47218. | .353E+10 | 829.82 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17793. | .353E+10 | 829.46 |
| 21 | PEAK | 3.00 | 1737903. | 0. | -17800.-13340000. | .352E+10 | 829.55 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35508. | .352E+10 | 829.57 |
| | PEAK | 4.00 | 2317204. | 0. | -23690.-13340000. | .351E+10 | 829.26 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47263. | .353E+10 | 829.37 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17810. | .354E+10 | 829.93 |
| 22 | PEAK | 3.00 | 1737903. | 0. | -17817.-13340000. | .353E+10 | 829.97 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35541. | .353E+10 | 829.66 |
| | PEAK | 4.00 | 2317204. | 0. | -23713.-13340000. | .352E+10 | 829.68 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47308. | .354E+10 | 829.77 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17827. | .354E+10 | 829.57 |
| 23 | PEAK | 3.00 | 1737903. | 0. | -17834.-13340000. | .353E+10 | 829.64 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35575. | .353E+10 | 829.77 |
| | PEAK | 4.00 | 2317204. | 0. | -23735.-13340000. | .352E+10 | 829.48 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47353. | .352E+10 | 829.60 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17776. | .353E+10 | 829.64 |

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|----|----------|------|----------|-----------|-------------------|----|----------|----------|--------|
| 24 | PEAK | 3.00 | 1737903. | 0. | -17782.-13340000. | 0. | .351E+10 | .436E+08 | 829.35 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35473. | 0. | .352E+10 | .436E+08 | 829.43 |
| | PEAK | 4.00 | 2317204. | 10. | -23667.-13340000. | 0. | .351E+10 | .435E+08 | 829.15 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47216. | 0. | .353E+10 | .437E+08 | 829.71 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17792. | 0. | .353E+10 | .437E+08 | 829.75 |
| 25 | PEAK | 3.00 | 1737903. | 0. | -17799.-13340000. | 0. | .352E+10 | .436E+08 | 829.45 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35506. | 0. | .352E+10 | .436E+08 | 829.54 |
| | PEAK | 4.00 | 2317204. | 0. | -23689.-13340000. | 0. | .351E+10 | .435E+08 | 829.26 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47261. | 0. | .353E+10 | .437E+08 | 829.82 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17809. | 0. | .353E+10 | .437E+08 | 829.86 |
| 26 | PEAK | 3.00 | 1737903. | 0. | -17816.-13340000. | 0. | .352E+10 | .436E+08 | 829.56 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35540. | 0. | .353E+10 | .437E+08 | 829.65 |
| | PEAK | 4.00 | 2317204. | 10. | -23711.-13340000. | 0. | .352E+10 | .436E+08 | 829.37 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47306. | 0. | .354E+10 | .438E+08 | 829.93 |
| | NON-PEAK | 3.00 | 1737903. | 10. | -17826. | 0. | .354E+10 | .438E+08 | 829.97 |
| 27 | PEAK | 3.00 | 1737903. | 10. | -17833.-13340000. | 0. | .353E+10 | .437E+08 | 829.67 |
| | NON-PEAK | 6.00 | 3475807. | 10. | -35574. | 0. | .353E+10 | .437E+08 | 829.76 |
| | PEAK | 4.00 | 2317204. | 10. | -23734.-13340000. | 0. | .352E+10 | .436E+08 | 829.48 |
| | NON-PEAK | 8.00 | 4634409. | 0. | -47351. | 0. | .352E+10 | .436E+08 | 829.59 |
| | NON-PEAK | 3.00 | 1737903. | 0. | -17775. | 0. | .353E+10 | .437E+08 | 829.70 |
| 28 | PEAK | 3.00 | 1737903. | 0. | -17782.-13340000. | 0. | .351E+10 | .435E+08 | 829.34 |
| | NON-PEAK | 6.00 | 3475807. | 0. | -35471. | 0. | .352E+10 | .436E+08 | 829.43 |
| | PEAK | 4.00 | 2317204. | 0. | -23666.-13340000. | 0. | .351E+10 | .435E+08 | 829.45 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47214. | 0. | .353E+10 | .437E+08 | 829.64 |
| | NON-PEAK | 3.00 | 1737903. | 10. | -17792. | 0. | .353E+10 | .437E+08 | 829.75 |
| 29 | PEAK | 3.00 | 1737903. | 10. | -17798.-13340000. | 0. | .352E+10 | .436E+08 | 829.45 |
| | NON-PEAK | 6.00 | 3475807. | 10. | -35505. | 0. | .352E+10 | .435E+08 | 829.54 |
| | PEAK | 4.00 | 2317204. | 10. | -23688.-13340000. | 0. | .351E+10 | .435E+08 | 829.25 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47259. | 0. | .353E+10 | .437E+08 | 829.81 |
| | NON-PEAK | 3.00 | 1737903. | 10. | -17808. | 0. | .353E+10 | .437E+08 | 829.86 |
| 30 | PEAK | 3.00 | 1737903. | 10. | -17815.-13340000. | 0. | .352E+10 | .436E+08 | 829.56 |
| | NON-PEAK | 6.00 | 3475807. | 10. | -35538. | 0. | .353E+10 | .437E+08 | 829.65 |
| | PEAK | 4.00 | 2317204. | 10. | -23710.-13340000. | 0. | .352E+10 | .436E+08 | 829.36 |
| | NON-PEAK | 8.00 | 4634409. | 17160000. | -47304. | 0. | .354E+10 | .438E+08 | 829.92 |
| | NON-PEAK | 3.00 | 1737903. | 10. | -17825. | 0. | .354E+10 | .438E+08 | 829.96 |
| 31 | PEAK | 3.00 | 1737903. | 10. | -17832.-13340000. | 0. | .353E+10 | .437E+08 | 829.67 |
| | NON-PEAK | 6.00 | 3475807. | 10. | -35572. | 0. | .353E+10 | .437E+08 | 829.76 |
| | PEAK | 4.00 | 2317204. | 10. | -23733.-13340000. | 0. | .352E+10 | .436E+08 | 829.47 |
| | NON-PEAK | 8.00 | 4634409. | 10. | -47349. | 0. | .352E+10 | .436E+08 | 829.59 |
| | NON-PEAK | 3.00 | 1737903. | 10. | -17774. | 0. | .353E+10 | .437E+08 | 829.63 |

MONTH OF : NOVEMBER YEAR : 1963 OPERATION AT RESERVOIR A

| | DATE | PERIOD | DURATION (HR) | INFLA (M3) | OPUMP (M3) | EVAPLA (M3) | QA (M3) | SPILLA (M3) | STOREA (M3) | AREA (M2) | EL.A (M) |
|---|----------|--------|---------------|------------|-------------------|-------------|----------|-------------|-------------|-----------|----------|
| 1 | PEAK | 3.00 | 1095833. | 0. | -12372.-13340000. | 0. | .353E+10 | .437E+08 | 829.63 | | |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24677. | 0. | .351E+10 | .435E+08 | 829.32 | | |
| | PEAK | 4..00 | 1461111. | 0.. | -16459.-13340000. | 0. | .352E+10 | .436E+08 | 829.38 | | |
| | NON-PEAK | 8..00 | 2922222. | 15300000. | -32831. | 0. | .350E+10 | .434E+08 | 829.07 | | |
| | NON-PEAK | 3..00 | 1095833. | 0.. | -12362. | 0. | .352E+10 | .436E+08 | 829.54 | | |
| 2 | PEAK | 3..00 | 1095833. | 0.. | -12365.-13340000. | 0. | .351E+10 | .436E+08 | 829.56 | | |
| | NON-PEAK | 6..00 | 2191667. | 0.. | -24662. | 0. | .351E+10 | .435E+08 | 829.25 | | |
| | PEAK | 4..00 | 1461111. | 0.. | -16449.-13340000. | 0. | .350E+10 | .434E+08 | 829.31 | | |
| | NON-PEAK | 8..00 | 2922222. | 15300000. | -32811. | 0. | .352E+10 | .436E+08 | 829.00 | | |
| | NON-PEAK | 3..00 | 1095833. | 0.. | -12354. | 0. | .352E+10 | .436E+08 | 829.47 | | |
| 3 | PEAK | 3..00 | 1095833. | 0.. | -12357.-13340000. | 0. | .351E+10 | .435E+08 | 829.49 | | |
| | NON-PEAK | 6..00 | 2191667. | 0.. | -24647. | 0. | .351E+10 | .434E+08 | 829.18 | | |
| | PEAK | 4..00 | 1461111. | 0.. | -16439.-13340000. | 0. | .350E+10 | .436E+08 | 829.24 | | |
| | NON-PEAK | 8..00 | 2922222. | 15300000. | -32791. | 0. | .352E+10 | .436E+08 | 828.93 | | |
| | NON-PEAK | 3..00 | 1095833. | 0.. | -12347. | 0. | .351E+10 | .435E+08 | 829.40 | | |
| 4 | PEAK | 3..00 | 1095833. | 0.. | -12350.-13340000. | 0. | .351E+10 | .435E+08 | 829.11 | | |
| | NON-PEAK | 6..00 | 2191667. | 0.. | -24632. | 0. | .351E+10 | .435E+08 | 829.17 | | |
| | PEAK | 4..00 | 1461111. | 0.. | -16429.-13340000. | 0. | .350E+10 | .434E+08 | 828.86 | | |
| | NON-PEAK | 8..00 | 2922222. | 15300000. | -32771. | 0. | .352E+10 | .436E+08 | 829.43 | | |
| | NON-PEAK | 3..00 | 1095833. | 0.. | -12339. | 0. | .351E+10 | .435E+08 | 829.36 | | |
| 5 | PEAK | 3..00 | 1095833. | 0.. | -12342.-13340000. | 0. | .350E+10 | .434E+08 | 829.04 | | |
| | NON-PEAK | 6..00 | 2191667. | 0.. | -24617. | 0.. | .350E+10 | .435E+08 | 829.10 | | |
| | PEAK | 4..00 | 1461111. | 0.. | -16419.-13340000. | 0. | .351E+10 | .433E+08 | 828.79 | | |
| | NON-PEAK | 8..00 | 2922222. | 15300000. | -32751. | 0.. | .351E+10 | .435E+08 | 829.26 | | |
| | NON-PEAK | 3..00 | 1095833. | 0.. | -12332. | 0.. | .351E+10 | .435E+08 | 829.29 | | |
| 6 | PEAK | 3..00 | 1095833. | 0.. | -12335.-13340000. | 0.. | .350E+10 | .434E+08 | 828.97 | | |
| | NON-PEAK | 6..00 | 2191667. | 0.. | -24602. | 0.. | .350E+10 | .434E+08 | 829.03 | | |
| | PEAK | 4..00 | 1461111. | 0.. | -16409.-13340000. | 0.. | .349E+10 | .433E+08 | 828.72 | | |
| | NON-PEAK | 8..00 | 2922222. | 15300000. | -32731. | 0.. | .351E+10 | .435E+08 | 829.19 | | |
| | NON-PEAK | 3..00 | 1095833. | 0.. | -12324. | 0.. | .351E+10 | .435E+08 | 829.22 | | |
| 7 | PEAK | 3..00 | 1095833. | 0.. | -12327.-13340000. | 0.. | .350E+10 | .434E+08 | 828.90 | | |
| | NON-PEAK | 6..00 | 2191667. | 0.. | -24587. | 0.. | .350E+10 | .434E+08 | 828.96 | | |
| | PEAK | 4..00 | 1461111. | 0.. | -16399.-13340000. | 0.. | .349E+10 | .433E+08 | 828.65 | | |
| | NON-PEAK | 8..00 | 2922222. | 15300000. | -32711. | 0.. | .351E+10 | .435E+08 | 829.12 | | |
| | NON-PEAK | 3..00 | 1095833. | 0.. | -12317. | 0.. | .351E+10 | .435E+08 | 829.15 | | |

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| 8 | PEAK | 3.00 | 1095833. | 0. | -12320.-13340000. | .349E+10 | .434E+08 | 828.83 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24572. | 0. | .350E+10 | .434E+08 |
| | PEAK | 4.00 | 1461111. | 0. | -16389.-13340000. | .348E+10 | .433E+08 | 828.69 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32691. | 0. | .350E+10 | .434E+08 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12309. | 0. | .350E+10 | .434E+08 |
| 9 | PEAK | 3.00 | 1095833. | 0. | -12312.-13340000. | .349E+10 | .433E+08 | 828.58 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24557. | 0. | .349E+10 | .434E+08 |
| | PEAK | 4.00 | 1461111. | 0. | -16379.-13340000. | .348E+10 | .432E+08 | 829.05 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32671. | 0. | .350E+10 | .434E+08 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12302. | 0. | .350E+10 | .434E+08 |
| 10 | PEAK | 3.00 | 1095833. | 0. | -12305.-13340000. | .349E+10 | .433E+08 | 828.82 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24542. | 0. | .349E+10 | .432E+08 |
| | PEAK | 4.00 | 1461111. | 0. | -16370.-13340000. | .348E+10 | .434E+08 | 828.51 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32651. | 0. | .350E+10 | .434E+08 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12295. | 0. | .350E+10 | .433E+08 |
| 11 | PEAK | 3.00 | 1095833. | 0. | -12298.-13340000. | .349E+10 | .433E+08 | 828.75 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24527. | 0. | .349E+10 | .432E+08 |
| | PEAK | 4.00 | 1461111. | 0. | -16360.-13340000. | .348E+10 | .434E+08 | 828.91 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32631. | 0. | .350E+10 | .434E+08 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12287. | 0. | .349E+10 | .433E+08 |
| 12 | PEAK | 3.00 | 1095833. | 0. | -12290.-13340000. | .348E+10 | .433E+08 | 828.62 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24512. | 0. | .348E+10 | .432E+08 |
| | PEAK | 4.00 | 1461111. | 0. | -16350.-13340000. | .349E+10 | .434E+08 | 828.94 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32612. | 0. | .350E+10 | .433E+08 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12280. | 0. | .349E+10 | .433E+08 |
| 13 | PEAK | 3.00 | 1095833. | 0. | -12283.-13340000. | .348E+10 | .433E+08 | 828.61 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24497. | 0. | .347E+10 | .432E+08 |
| | PEAK | 4.00 | 1461111. | 0. | -16340.-13340000. | .348E+10 | .433E+08 | 828.31 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32592. | 0. | .347E+10 | .433E+08 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12272. | 0. | .349E+10 | .433E+08 |
| 14 | PEAK | 3.00 | 1095833. | 0. | -12275.-13340000. | .348E+10 | .432E+08 | 828.42 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24482. | 0. | .348E+10 | .432E+08 |
| | PEAK | 4.00 | 1461111. | 0. | -16330.-13340000. | .347E+10 | .431E+08 | 828.47 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32572. | 0. | .349E+10 | .433E+08 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12265. | 0. | .349E+10 | .433E+08 |
| 15 | PEAK | 3.00 | 1095833. | 0. | -12268.-13340000. | .348E+10 | .432E+08 | 828.35 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24467. | 0. | .348E+10 | .432E+08 |
| | PEAK | 4.00 | 1461111. | 0. | -16320.-13340000. | .347E+10 | .431E+08 | 828.10 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32552. | 0. | .348E+10 | .433E+08 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12257. | 0. | .349E+10 | .433E+08 |

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|----|----------|------|----------|-----------|-------------------|----|----------|----------|--------|
| 16 | PEAK | 3.00 | 1095833. | 0. | -12260.-13340000. | 0. | -347E+10 | .431E+08 | 828.28 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24452. | 0. | .347E+10 | .432E+08 | 828.33 |
| | PEAK | 4.00 | 1461111. | 0. | -16310.-13340000. | 0. | .346E+10 | .431E+08 | 828.03 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32532. | 0. | .348E+10 | .432E+08 | 828.49 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12250. | 0. | .348E+10 | .432E+08 | 828.52 |
| 17 | PEAK | 3.00 | 1095833. | 0. | -12253.-13340000. | 0. | .347E+10 | .431E+08 | 828.21 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24437. | 0. | .347E+10 | .431E+08 | 828.26 |
| | PEAK | 4.00 | 1461111. | 0. | -16300.-13340000. | 0. | .346E+10 | .430E+08 | 827.96 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32512. | 0. | .348E+10 | .432E+08 | 828.42 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12242. | 0. | .348E+10 | .432E+08 | 828.45 |
| 18 | PEAK | 3.00 | 1095833. | 0. | -12245.-13340000. | 0. | .347E+10 | .431E+08 | 828.14 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24423. | 0. | .347E+10 | .431E+08 | 828.19 |
| | PEAK | 4.00 | 1461111. | 0. | -16290.-13340000. | 0. | .346E+10 | .430E+08 | 827.89 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32492. | 0. | .348E+10 | .432E+08 | 828.35 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12235. | 0. | .348E+10 | .432E+08 | 828.38 |
| 19 | PEAK | 3.00 | 1095833. | 0. | -12238.-13340000. | 0. | .346E+10 | .431E+08 | 828.07 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24408. | 0. | .347E+10 | .431E+08 | 828.12 |
| | PEAK | 4.00 | 1461111. | 0. | -16280.-13340000. | 0. | .345E+10 | .430E+08 | 827.82 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32472. | 0. | .347E+10 | .431E+08 | 828.28 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12227. | 0. | .347E+10 | .432E+08 | 828.31 |
| 20 | PEAK | 3.00 | 1095833. | 0. | -12230.-13340000. | 0. | .346E+10 | .430E+08 | 828.00 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24393. | 0. | .346E+10 | .431E+08 | 828.05 |
| | PEAK | 4.00 | 1461111. | 0. | -16270.-13340000. | 0. | .345E+10 | .429E+08 | 827.75 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32452. | 0. | .347E+10 | .431E+08 | 828.22 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12220. | 0. | .347E+10 | .431E+08 | 828.24 |
| 21 | PEAK | 3.00 | 1095833. | 0. | -12223.-13340000. | 0. | .346E+10 | .430E+08 | 827.93 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24378. | 0. | .346E+10 | .430E+08 | 827.98 |
| | PEAK | 4.00 | 1461111. | 0. | -16260.-13340000. | 0. | .345E+10 | .429E+08 | 827.68 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32432. | 0. | .347E+10 | .431E+08 | 828.15 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12212. | 0. | .347E+10 | .431E+08 | 828.17 |
| 22 | PEAK | 3.00 | 1095833. | 0. | -12215.-13340000. | 0. | .346E+10 | .430E+08 | 827.86 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24363. | 0. | .346E+10 | .430E+08 | 827.92 |
| | PEAK | 4.00 | 1461111. | 0. | -16250.-13340000. | 0. | .345E+10 | .429E+08 | 827.61 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32412. | 0. | .346E+10 | .431E+08 | 828.08 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12205. | 0. | .347E+10 | .431E+08 | 828.10 |
| 23 | PEAK | 3.00 | 1095833. | 0. | -12208.-13340000. | 0. | .345E+10 | .430E+08 | 827.79 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24348. | 0. | .346E+10 | .430E+08 | 827.85 |
| | PEAK | 4.00 | 1461111. | 0. | -16240.-13340000. | 0. | .344E+10 | .429E+08 | 827.54 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32392. | 0. | .346E+10 | .430E+08 | 828.01 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12197. | 0. | .346E+10 | .431E+08 | 828.03 |

| | | | | | | | | | |
|----|----------|------|----------|-----------|-------------------|----|----------|----------|--------|
| 24 | PEAK | 3.00 | 1095833. | 0. | -12200.-13340000. | 0. | .345E+10 | .429E+08 | 827.72 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24333. | 0. | .345E+10 | .430E+08 | 827.78 |
| | PEAK | 4.00 | 1461111. | 0. | -16230.-13340000. | 0. | .344E+10 | .428E+08 | 827.47 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32372. | 0. | .346E+10 | .430E+08 | 827.94 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12190. | 0. | .346E+10 | .430E+08 | 827.97 |
| 25 | PEAK | 3.00 | 1095833. | 0. | -12193.-13340000. | 0. | .345E+10 | .429E+08 | 827.65 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24318. | 0. | .345E+10 | .429E+08 | 827.71 |
| | PEAK | 4.00 | 1461111. | 0. | -16220.-13340000. | 0. | .344E+10 | .428E+08 | 827.40 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32352. | 0. | .346E+10 | .430E+08 | 827.87 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12182. | 0. | .346E+10 | .430E+08 | 827.90 |
| 26 | PEAK | 3.00 | 1095833. | 0. | -12185.-13340000. | 0. | .345E+10 | .429E+08 | 827.58 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24303. | 0. | .345E+10 | .429E+08 | 827.64 |
| | PEAK | 4.00 | 1461111. | 0. | -16210.-13340000. | 0. | .344E+10 | .428E+08 | 827.33 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32332. | 0. | .345E+10 | .430E+08 | 827.80 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12175. | 0. | .346E+10 | .430E+08 | 827.83 |
| 27 | PEAK | 3.00 | 1095833. | 0. | -12178.-13340000. | 0. | .344E+10 | .429E+08 | 827.51 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24288. | 0. | .345E+10 | .429E+08 | 827.57 |
| | PEAK | 4.00 | 1461111. | 0. | -16200.-13340000. | 0. | .343E+10 | .428E+08 | 827.44 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32312. | 0. | .344E+10 | .428E+08 | 827.26 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12167. | 0. | .345E+10 | .429E+08 | 827.73 |
| | PEAK | 3.00 | 1095833. | 0. | -12170.-13340000. | 0. | .344E+10 | .429E+08 | 827.76 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24273. | 0. | .344E+10 | .428E+08 | 827.44 |
| | PEAK | 4.00 | 1461111. | 0. | -16190.-13340000. | 0. | .345E+10 | .429E+08 | 827.50 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32292. | 0. | .343E+10 | .427E+08 | 827.19 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12160. | 0. | .345E+10 | .429E+08 | 827.66 |
| 28 | PEAK | 3.00 | 1095833. | 0. | -12163.-13340000. | 0. | .345E+10 | .429E+08 | 827.69 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24258. | 0. | .344E+10 | .428E+08 | 827.37 |
| | PEAK | 4.00 | 1461111. | 0. | -16180.-13340000. | 0. | .344E+10 | .428E+08 | 827.43 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32272. | 0. | .343E+10 | .427E+08 | 827.12 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12152. | 0. | .345E+10 | .429E+08 | 827.59 |
| 29 | PEAK | 3.00 | 1095833. | 0. | -12155.-13340000. | 0. | .345E+10 | .429E+08 | 827.62 |
| | NON-PEAK | 6.00 | 2191667. | 0. | -24243. | 0. | .343E+10 | .428E+08 | 827.30 |
| | PEAK | 4.00 | 1461111. | 0. | -16170.-13340000. | 0. | .344E+10 | .428E+08 | 827.36 |
| | NON-PEAK | 8.00 | 2922222. | 15300000. | -32252. | 0. | .343E+10 | .427E+08 | 827.05 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12145. | 0. | .344E+10 | .429E+08 | 827.52 |
| | NON-PEAK | 3.00 | 1095833. | 0. | -12145. | 0. | .344E+10 | .429E+08 | 827.55 |

MONTH OF : DECEMBER YEAR : 1963 OPERATION AT RESERVOIR A

| | DATE | PERIOD | DURATION (HR) | INFLA (M3) | QPUMP (M3) | EVAPLA (M3) | QA (M3) | SPIILA (M3) | STOREA (M3) | AREA (M2) | EIL.A (M) |
|----------|------|--------|---------------|------------|------------|------------------|---------|-------------|-------------|-----------|-----------|
| 1 PEAK | 3.00 | | | 834677. | 0. | -7261.-13340000. | 0. | .344E+10 | .429E+08 | 827.55 | |
| NON-PEAK | 6.00 | | | 1669355. | 0. | -14480. | 0. | .343E+10 | .427E+08 | 827.23 | |
| PEAK | 4.00 | | | 1112903. | 0. | -9657.-13340000. | 0. | .342E+10 | .428E+08 | 827.27 | |
| NON-PEAK | 8.00 | | | 2225807. | 11650000. | -19261. | 0. | .344E+10 | .426E+08 | 826.96 | |
| NON-PEAK | 3.00 | | | 834677. | 0. | -7246. | 0. | .344E+10 | .428E+08 | 827.31 | |
| NON-PEAK | 3.00 | | | 834677. | 0. | -7247.-13340000. | 0. | .342E+10 | .427E+08 | 827.33 | |
| 2 PEAK | 3.00 | | | 834677. | 0. | -7247.-13340000. | 0. | .342E+10 | .427E+08 | 827.01 | |
| NON-PEAK | 6.00 | | | 1669355. | 0. | -14453. | 0. | .343E+10 | .427E+08 | 827.05 | |
| PEAK | 4.00 | | | 1112903. | 0. | -9639.-13340000. | 0. | .341E+10 | .426E+08 | 826.74 | |
| NON-PEAK | 8.00 | | | 2225807. | 11650000. | -19224. | 0. | .343E+10 | .427E+08 | 827.10 | |
| NON-PEAK | 3.00 | | | 834677. | 0. | -7232. | 0. | .343E+10 | .427E+08 | 827.12 | |
| 3 PEAK | 3.00 | | | 834677. | 0. | -7233.-13340000. | 0. | .342E+10 | .426E+08 | 826.80 | |
| NON-PEAK | 6.00 | | | 1669355. | 0. | -14425. | 0. | .342E+10 | .426E+08 | 826.84 | |
| PEAK | 4.00 | | | 1112903. | 0. | -9620.-13340000. | 0. | .340E+10 | .425E+08 | 826.52 | |
| NON-PEAK | 8.00 | | | 2225807. | 11650000. | -19187. | 0. | .342E+10 | .426E+08 | 826.88 | |
| NON-PEAK | 3.00 | | | 834677. | 0. | -7218. | 0. | .342E+10 | .426E+08 | 826.90 | |
| 4 PEAK | 3.00 | | | 834677. | 0. | -7219.-13340000. | 0. | .341E+10 | .425E+08 | 826.58 | |
| NON-PEAK | 6.00 | | | 1669355. | 0. | -14397. | 0. | .340E+10 | .425E+08 | 826.62 | |
| PEAK | 4.00 | | | 1112903. | 0. | -9602.-13340000. | 0. | .340E+10 | .424E+08 | 826.31 | |
| NON-PEAK | 8.00 | | | 2225807. | 11650000. | -19150. | 0. | .341E+10 | .425E+08 | 826.66 | |
| NON-PEAK | 3.00 | | | 834677. | 0. | -7204. | 0. | .341E+10 | .425E+08 | 826.69 | |
| 5 PEAK | 3.00 | | | 834677. | 0. | -7205.-13340000. | 0. | .340E+10 | .424E+08 | 826.36 | |
| NON-PEAK | 6.00 | | | 1669355. | 0. | -14369. | 0. | .340E+10 | .424E+08 | 826.41 | |
| NON-PEAK | 4.00 | | | 1112903. | 0. | -9583.-13340000. | 0. | .339E+10 | .423E+08 | 826.09 | |
| NON-PEAK | 8.00 | | | 2225807. | 11650000. | -19113. | 0. | .340E+10 | .425E+08 | 826.45 | |
| NON-PEAK | 3.00 | | | 834677. | 0. | -7190. | 0. | .340E+10 | .425E+08 | 826.23 | |
| NON-PEAK | 6.00 | | | 1669355. | 0. | -14369. | 0. | .339E+10 | .423E+08 | 826.15 | |
| PEAK | 4.00 | | | 1112903. | 0. | -9583.-13340000. | 0. | .339E+10 | .424E+08 | 826.19 | |
| NON-PEAK | 8.00 | | | 2225807. | 11650000. | -19075. | 0. | .338E+10 | .422E+08 | 825.88 | |
| NON-PEAK | 3.00 | | | 834677. | 0. | -7191.-13340000. | 0. | .339E+10 | .424E+08 | 826.23 | |
| NON-PEAK | 6.00 | | | 1669355. | 0. | -14342. | 0. | .339E+10 | .424E+08 | 826.45 | |
| PEAK | 4.00 | | | 1112903. | 0. | -9565.-13340000. | 0. | .338E+10 | .422E+08 | 825.98 | |
| NON-PEAK | 8.00 | | | 2225807. | 11650000. | -19075. | 0. | .337E+10 | .422E+08 | 825.66 | |
| NON-PEAK | 3.00 | | | 834677. | 0. | -7176. | 0. | .338E+10 | .423E+08 | 826.02 | |
| 7 PEAK | 3.00 | | | 834677. | 0. | -7178.-13340000. | 0. | .338E+10 | .423E+08 | 825.93 | |
| NON-PEAK | 6.00 | | | 1669355. | 0. | -14314. | 0. | .338E+10 | .423E+08 | 825.98 | |
| PEAK | 4.00 | | | 1112903. | 0. | -9546.-13340000. | 0. | .337E+10 | .422E+08 | 825.66 | |
| NON-PEAK | 8.00 | | | 2225807. | 11650000. | -19038. | 0. | .338E+10 | .423E+08 | 826.04 | |
| NON-PEAK | 3.00 | | | 834677. | 0. | -7162. | 0. | .339E+10 | .423E+08 | 826.04 | |

| | | | | | |
|----------|------|----------|-----------|------------------|--------|
| 8 PEAK | 3.00 | 834677. | 0. | -7164.-13340000. | 825.72 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14286. | 825.76 |
| PEAK | 4.00 | 1112903. | 0. | -9528.-13340000. | 825.45 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -19001. | 825.80 |
| NON-PEAK | 3.00 | 834677. | 0. | -7148. | 825.82 |
| 9 PEAK | 3.00 | 834677. | 0. | -7150.-13340000. | 825.50 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14258. | 825.54 |
| PEAK | 4.00 | 1112903. | 0. | -9509.-13340000. | 825.23 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18964. | 825.59 |
| NON-PEAK | 3.00 | 834677. | 0. | -7135. | 825.61 |
| 10 PEAK | 3.00 | 834677. | 0. | -7136.-13340000. | 825.29 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14231. | 825.33 |
| PEAK | 4.00 | 1112903. | 0. | -9491.-13340000. | 825.02 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18927. | 825.37 |
| NON-PEAK | 3.00 | 834677. | 0. | -7121. | 825.39 |
| 11 PEAK | 3.00 | 834677. | 0. | -7122.-13340000. | 825.07 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14203. | 825.11 |
| NON-PEAK | 4.00 | 1112903. | 0. | -9472.-13340000. | 824.80 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18890. | 825.15 |
| NON-PEAK | 3.00 | 834677. | 0. | -7107. | 825.18 |
| 12 PEAK | 3.00 | 834677. | 0. | -7108.-13340000. | 824.86 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14175. | 824.90 |
| PEAK | 4.00 | 1112903. | 0. | -9454.-13340000. | 824.58 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18853. | 824.94 |
| NON-PEAK | 3.00 | 834677. | 0. | -7093. | 824.96 |
| 13 PEAK | 3.00 | 834677. | 0. | -7094.-13340000. | 824.64 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14147. | 824.68 |
| PEAK | 4.00 | 1112903. | 0. | -9435.-13340000. | 824.37 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18816. | 824.72 |
| NON-PEAK | 3.00 | 834677. | 0. | -7079. | 824.74 |
| 14 PEAK | 3.00 | 834677. | 0. | -7080.-13340000. | 824.42 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14119. | 824.47 |
| PEAK | 4.00 | 1112903. | 0. | -9417.-13340000. | 824.15 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18779. | 824.51 |
| NON-PEAK | 3.00 | 834677. | 0. | -7065. | 824.53 |
| 15 PEAK | 3.00 | 834677. | 0. | -7067.-13340000. | 824.21 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14092. | 824.25 |
| PEAK | 4.00 | 1112903. | 0. | -9398.-13340000. | 823.94 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18742. | 824.29 |
| NON-PEAK | 3.00 | 834677. | 0. | -7051. | 824.31 |

MONTH OF : DECEMBER YEAR : 1963 OPERATION AT RESERVOIR A

| | DATE | PERIOD | DURATION (HR) | INFLA (M3) | QPUMP (M3) | EVAPLA (M3) | QA (M3) | SPILLA (M3) | STOREA (M3) | AREA (M2) | EL.A (M) |
|----------|------|----------|------------------|------------------|---------------|----------------|------------|----------------|----------------|--------------|-------------|
| 1 PEAK | 3.00 | 834677. | 0. | -7261.-13340000. | 0. | .344E+10 | .429E+08 | 827.55 | | | |
| NON-PEAK | 6.00 | 1669355. | 0. | -14480. | 0. | .343E+10 | .427E+08 | 827.23 | | | |
| PEAK | 4.00 | 1112903. | 0. | -9657.-13340000. | 0. | .342E+10 | .428E+08 | 827.27 | | | |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -19261. | 0. | .344E+10 | .426E+08 | 826.96 | | | |
| NON-PEAK | 3.00 | 834677. | 0. | -7246. | 0. | .344E+10 | .428E+08 | 827.31 | | | |
| 2 PEAK | 3.00 | 834677. | 0. | -7247.-13340000. | 0. | .342E+10 | .427E+08 | 827.33 | | | |
| NON-PEAK | 6.00 | 1669355. | 0. | -14453. | 0. | .343E+10 | .427E+08 | 827.01 | | | |
| PEAK | 4.00 | 1112903. | 0. | -9639.-13340000. | 0. | .341E+10 | .426E+08 | 827.05 | | | |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -19224. | 0. | .343E+10 | .427E+08 | 826.74 | | | |
| NON-PEAK | 3.00 | 834677. | 0. | -7232. | 0. | .343E+10 | .427E+08 | 827.10 | | | |
| 3 PEAK | 3.00 | 834677. | 0. | -7233.-13340000. | 0. | .342E+10 | .426E+08 | 827.12 | | | |
| NON-PEAK | 6.00 | 1669355. | 0. | -14425. | 0. | .342E+10 | .426E+08 | 826.74 | | | |
| PEAK | 4.00 | 1112903. | 0. | -9620.-13340000. | 0. | .340E+10 | .425E+08 | 827.08 | | | |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -19187. | 0. | .342E+10 | .426E+08 | 826.80 | | | |
| NON-PEAK | 3.00 | 834677. | 0. | -7218. | 0. | .342E+10 | .426E+08 | 826.84 | | | |
| 4 PEAK | 3.00 | 834677. | 0. | -7219.-13340000. | 0. | .341E+10 | .425E+08 | 826.84 | | | |
| NON-PEAK | 6.00 | 1669355. | 0. | -14397. | 0. | .341E+10 | .425E+08 | 826.52 | | | |
| PEAK | 4.00 | 1112903. | 0. | -9602.-13340000. | 0. | .340E+10 | .424E+08 | 826.88 | | | |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -19150. | 0. | .342E+10 | .425E+08 | 826.90 | | | |
| NON-PEAK | 3.00 | 834677. | 0. | -7204. | 0. | .341E+10 | .425E+08 | 826.58 | | | |
| 5 PEAK | 3.00 | 834677. | 0. | -7205.-13340000. | 0. | .340E+10 | .425E+08 | 826.62 | | | |
| NON-PEAK | 6.00 | 1669355. | 0. | -14369. | 0. | .340E+10 | .424E+08 | 826.31 | | | |
| PEAK | 4.00 | 1112903. | 0. | -9583.-13340000. | 0. | .341E+10 | .425E+08 | 826.66 | | | |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -19113. | 0. | .341E+10 | .425E+08 | 826.69 | | | |
| NON-PEAK | 3.00 | 834677. | 0. | -7205.-13340000. | 0. | .340E+10 | .424E+08 | 826.36 | | | |
| NON-PEAK | 6.00 | 1669355. | 0. | -14369. | 0. | .340E+10 | .424E+08 | 826.41 | | | |
| PEAK | 4.00 | 1112903. | 0. | -9583.-13340000. | 0. | .339E+10 | .423E+08 | 826.09 | | | |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -19075. | 0. | .340E+10 | .425E+08 | 826.45 | | | |
| NON-PEAK | 3.00 | 834677. | 0. | -7190. | 0. | .340E+10 | .425E+08 | 826.47 | | | |
| 6 PEAK | 3.00 | 834677. | 0. | -7191.-13340000. | 0. | .339E+10 | .423E+08 | 826.15 | | | |
| NON-PEAK | 6.00 | 1669355. | 0. | -14342. | 0. | .339E+10 | .424E+08 | 826.19 | | | |
| PEAK | 4.00 | 1112903. | 0. | -9565.-13340000. | 0. | .338E+10 | .422E+08 | 825.88 | | | |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -19075. | 0. | .339E+10 | .424E+08 | 826.23 | | | |
| NON-PEAK | 3.00 | 834677. | 0. | -7176. | 0. | .339E+10 | .424E+08 | 826.25 | | | |
| 7 PEAK | 3.00 | 834677. | 0. | -7178.-13340000. | 0. | .338E+10 | .423E+08 | 825.93 | | | |
| NON-PEAK | 6.00 | 1669355. | 0. | -14314. | 0. | .338E+10 | .423E+08 | 825.98 | | | |
| PEAK | 4.00 | 1112903. | 0. | -9546.-13340000. | 0. | .337E+10 | .422E+08 | 825.66 | | | |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -19038. | 0. | .338E+10 | .423E+08 | 826.02 | | | |
| NON-PEAK | 3.00 | 834677. | 0. | -7162. | 0. | .339E+10 | .423E+08 | 826.04 | | | |

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| 8 PEAK | 3.00 | 834677. | 0. | -7164.-13340000. | 825.72 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14286. | 825.76 |
| PEAK | 4.00 | 1112903. | 0. | -9528.-13340000. | 825.45 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -19001. | 825.80 |
| NON-PEAK | 3.00 | 834677. | 0. | -7148. | 825.82 |
| 9 PEAK | 3.00 | 834677. | 0. | -7150.-13340000. | 422E+08 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14258. | 422E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9509.-13340000. | 421E+08 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18964. | 422E+08 |
| NON-PEAK | 3.00 | 834677. | 0. | -7135. | 421E+08 |
| 10 PEAK | 3.00 | 834677. | 0. | -7136.-13340000. | 421E+08 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14231. | 420E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9491.-13340000. | 420E+08 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18927. | 419E+08 |
| NON-PEAK | 3.00 | 834677. | 0. | -7121. | 419E+08 |
| 11 PEAK | 3.00 | 834677. | 0. | -7122.-13340000. | 419E+08 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14203. | 419E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9472.-13340000. | 420E+08 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18890. | 420E+08 |
| NON-PEAK | 3.00 | 834677. | 0. | -7107. | 419E+08 |
| 12 PEAK | 3.00 | 834677. | 0. | -7108.-13340000. | 419E+08 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14175. | 419E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9454.-13340000. | 420E+08 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18853. | 420E+08 |
| NON-PEAK | 3.00 | 834677. | 0. | -7093. | 418E+08 |
| 13 PEAK | 3.00 | 834677. | 0. | -7094.-13340000. | 419E+08 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14147. | 417E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9435.-13340000. | 419E+08 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18816. | 419E+08 |
| NON-PEAK | 3.00 | 834677. | 0. | -7079. | 418E+08 |
| 14 PEAK | 3.00 | 834677. | 0. | -7080.-13340000. | 417E+08 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14119. | 417E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9417.-13340000. | 417E+08 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18779. | 416E+08 |
| NON-PEAK | 3.00 | 834677. | 0. | -7065. | 416E+08 |
| 15 PEAK | 3.00 | 834677. | 0. | -7067.-13340000. | 416E+08 |
| NON-PEAK | 6.00 | 1669355. | 0. | -14092. | 416E+08 |
| PEAK | 4.00 | 1112903. | 0. | -9398.-13340000. | 415E+08 |
| NON-PEAK | 8.00 | 2225807. | 11650000. | -18742. | 416E+08 |
| NON-PEAK | 3.00 | 834677. | 0. | -7051. | 416E+08 |

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| 16 | PEAK | 3.00 | 834677. | 0. | -7053.-13340000. | 0. | .331E+10 | .415E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14064. | 0. | .331E+10 | .415E+08 |
| | PEAK | 4.00 | 1112903. | 0. | -9380.-13340000. | 0. | .330E+10 | .414E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18705. | 0. | .331E+10 | .415E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -7037. | 0. | .331E+10 | .415E+08 |
| 17 | PEAK | 3.00 | 834677. | 0. | -7039.-13340000. | 0. | .330E+10 | .416E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14036. | 0. | .330E+10 | .414E+08 |
| | PEAK | 4.00 | 1112903. | 0. | -9361.-13340000. | 0. | .329E+10 | .413E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18668. | 0. | .330E+10 | .415E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -7024. | 0. | .330E+10 | .415E+08 |
| 18 | PEAK | 3.00 | 834677. | 0. | -7025.-13340000. | 0. | .329E+10 | .414E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -14008. | 0. | .329E+10 | .414E+08 |
| | PEAK | 4.00 | 1112903. | 0. | -9343.-13340000. | 0. | .328E+10 | .413E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18631. | 0. | .329E+10 | .414E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -7010. | 0. | .329E+10 | .414E+08 |
| 19 | PEAK | 3.00 | 834677. | 0. | -7011.-13340000. | 0. | .328E+10 | .413E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13981. | 0. | .328E+10 | .413E+08 |
| | PEAK | 4.00 | 1112903. | 0. | -9324.-13340000. | 0. | .327E+10 | .412E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18594. | 0. | .328E+10 | .413E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6996. | 0. | .328E+10 | .413E+08 |
| 20 | PEAK | 3.00 | 834677. | 0. | -6997.-13340000. | 0. | .327E+10 | .412E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13953. | 0. | .327E+10 | .412E+08 |
| | PEAK | 4.00 | 1112903. | 0. | -9306.-13340000. | 0. | .326E+10 | .411E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18557. | 0. | .328E+10 | .412E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6982. | 0. | .328E+10 | .412E+08 |
| 21 | PEAK | 3.00 | 834677. | 0. | -6983.-13340000. | 0. | .326E+10 | .411E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13925. | 0. | .327E+10 | .411E+08 |
| | PEAK | 4.00 | 1112903. | 0. | -9287.-13340000. | 0. | .325E+10 | .410E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18520. | 0. | .327E+10 | .411E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6968. | 0. | .326E+10 | .411E+08 |
| 22 | PEAK | 3.00 | 834677. | 0. | -6969.-13340000. | 0. | .326E+10 | .410E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13897. | 0. | .326E+10 | .410E+08 |
| | PEAK | 4.00 | 1112903. | 0. | -9269.-13340000. | 0. | .324E+10 | .409E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18483. | 0. | .326E+10 | .411E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6954. | 0. | .326E+10 | .411E+08 |
| 23 | PEAK | 3.00 | 834677. | 0. | -6956.-13340000. | 0. | .325E+10 | .409E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13870. | 0. | .325E+10 | .410E+08 |
| | PEAK | 4.00 | 1112903. | 0. | -9250.-13340000. | 0. | .324E+10 | .408E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18446. | 0. | .325E+10 | .410E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6940. | 0. | .325E+10 | .410E+08 |

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|----|----------|------|----------|-----------|------------------|----|----------|----------|
| 24 | PEAK | 3.00 | 834677. | 0. | -6942.-13340000. | 0. | -324E+10 | -409E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13842. | 0. | -324E+10 | -409E+08 |
| 25 | PEAK | 4.00 | 1112903. | 0. | -9232.-13340000. | 0. | -323E+10 | -408E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18409. | 0. | -324E+10 | -409E+08 |
| 26 | PEAK | 3.00 | 834677. | 0. | -6926. | 0. | -324E+10 | -409E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6928.-13340000. | 0. | -323E+10 | -408E+08 |
| 27 | PEAK | 6.00 | 1669355. | 0. | -13814. | 0. | -323E+10 | -408E+08 |
| | NON-PEAK | 4.00 | 1112903. | 0. | -9213.-13340000. | 0. | -322E+10 | -407E+08 |
| 28 | PEAK | 8.00 | 2225807. | 11650000. | -18372. | 0. | -323E+10 | -408E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6913. | 0. | -323E+10 | -408E+08 |
| 29 | PEAK | 3.00 | 834677. | 0. | -6914.-13340000. | 0. | -322E+10 | -407E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13786. | 0. | -322E+10 | -407E+08 |
| 30 | PEAK | 4.00 | 1112903. | 0. | -9195.-13340000. | 0. | -321E+10 | -406E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18335. | 0. | -322E+10 | -407E+08 |
| 31 | PEAK | 3.00 | 834677. | 0. | -6899. | 0. | -323E+10 | -407E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6900.-13340000. | 0. | -321E+10 | -406E+08 |
| 32 | PEAK | 6.00 | 1669355. | 0. | -13759. | 0. | -321E+10 | -406E+08 |
| | NON-PEAK | 4.00 | 1112903. | 0. | -9176.-13340000. | 0. | -320E+10 | -405E+08 |
| 33 | PEAK | 8.00 | 2225807. | 11650000. | -18298. | 0. | -322E+10 | -406E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6885. | 0. | -322E+10 | -407E+08 |
| 34 | PEAK | 3.00 | 834677. | 0. | -6886.-13340000. | 0. | -320E+10 | -405E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13731. | 0. | -321E+10 | -406E+08 |
| 35 | PEAK | 4.00 | 1112903. | 0. | -9158.-13340000. | 0. | -319E+10 | -404E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18261. | 0. | -321E+10 | -406E+08 |
| 36 | PEAK | 3.00 | 834677. | 0. | -6871. | 0. | -321E+10 | -406E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6872.-13340000. | 0. | -320E+10 | -405E+08 |
| 37 | PEAK | 6.00 | 1669355. | 0. | -13703. | 0. | -320E+10 | -405E+08 |
| | NON-PEAK | 4.00 | 1112903. | 0. | -9139.-13340000. | 0. | -319E+10 | -404E+08 |
| 38 | PEAK | 8.00 | 2225807. | 11650000. | -18224. | 0. | -320E+10 | -405E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6857. | 0. | -320E+10 | -405E+08 |
| 39 | PEAK | 3.00 | 834677. | 0. | -6858.-13340000. | 0. | -319E+10 | -404E+08 |
| | NON-PEAK | 6.00 | 1669355. | 0. | -13675. | 0. | -319E+10 | -404E+08 |
| 40 | PEAK | 3.00 | 834677. | 0. | -9121.-13340000. | 0. | -318E+10 | -403E+08 |
| | NON-PEAK | 8.00 | 2225807. | 11650000. | -18187. | 0. | -317E+10 | -402E+08 |
| 41 | PEAK | 3.00 | 834677. | 0. | -6843. | 0. | -319E+10 | -404E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6844.-13340000. | 0. | -318E+10 | -403E+08 |
| 42 | PEAK | 6.00 | 1669355. | 0. | -13648. | 0. | -318E+10 | -403E+08 |
| | NON-PEAK | 4.00 | 1112903. | 0. | -9102.-13340000. | 0. | -317E+10 | -402E+08 |
| 43 | PEAK | 8.00 | 2225807. | 11650000. | -18150. | 0. | -318E+10 | -403E+08 |
| | NON-PEAK | 3.00 | 834677. | 0. | -6829. | 0. | -318E+10 | -403E+08 |

File name: ROBPRF0.OUT for year 1963 with proposed operation schedule

| MONTH OF : OCTOBER | YEAR : 1963 | OPERATION AT RESERVOIR B | | | | | | | | | |
|--------------------|-------------|--------------------------|-----------|-----------|----------------|------------|---------------|----------------|---------------|----------------|--------------|
| | | DATE | PERIOD | DURATION | INFILB (M3) | QA (M3) | IRRIS (M3) | EVAPLB (M3) | QPUMP (M3) | SPILLB (M3) | BREA (M2) |
| 1 PEAK | 3.00 | 0. | 13340000. | -710484. | -807. | 0. | 0. | 0. | .678E+08 | .198E+07 | 598.50 |
| | 6.00 | 0. | 0. | -1420968. | -1791. | 0. | 0. | 0. | .663E+08 | .220E+07 | 604.40 |
| PEAK | 4.00 | 0. | 3416324. | -947312. | -1181. | 0. | 0. | 0. | .688E+08 | .216E+07 | 603.76 |
| | 8.00 | 0. | 0. | -1894624. | -2406. | 0. | 0. | 0. | .669E+08 | .222E+07 | 604.87 |
| NON-PEAK | 3.00 | 0. | 0. | -710484. | -890. | 0. | 0. | 0. | .662E+08 | .218E+07 | 604.01 |
| | 2 PEAK | 3.00 | 0. | 13340000. | -710484. | -885. | 0. | 0. | .788E+08 | .238E+07 | 609.38 |
| NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1937. | 0. | 0. | 0. | .774E+08 | .235E+07 | 608.74 |
| | PEAK | 4.00 | 0. | 13340000. | -947312. | -1279. | 0. | -4277516. | .855E+08 | .255E+07 | 612.00 |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | 0. | .665E+08 | .218E+07 | 603.81 |
| | NON-PEAK | 3.00 | 1245696. | 0. | -710484. | -887. | 0. | 0. | .670E+08 | .219E+07 | 604.05 |
| 3 PEAK | 3.00 | 0. | 13340000. | -710484. | -890. | 0. | 0. | .796E+08 | .239E+07 | 609.74 | |
| | 6.00 | 0. | 0. | -1420968. | -1947. | 0. | 0. | .782E+08 | .237E+07 | 609.10 | |
| NON-PEAK | 4.00 | 0. | 13340000. | -947312. | -1286. | 0. | -5074046. | .855E+08 | .255E+07 | 612.00 | |
| | PEAK | 8.00 | 0. | -1894624. | -2769. | 0. | 0. | .836E+08 | .250E+07 | 611.29 | |
| NON-PEAK | 3.00 | 0. | 0. | -710484. | -1017. | 0. | 0. | .829E+08 | .248E+07 | 611.02 | |
| | 4 PEAK | 3.00 | 0. | 13340000. | -710484. | -1009. | 0. | -10019610. | .855E+08 | .255E+07 | 612.00 |
| NON-PEAK | 6.00 | 0. | 0. | -1420968. | -2077. | 0. | 0. | .841E+08 | .251E+07 | 611.47 | |
| | PEAK | 4.00 | 0. | 13340000. | -947312. | -1363. | 0. | -10968280. | .855E+08 | .255E+07 | 612.00 |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | 0. | .665E+08 | .218E+07 | 603.81 |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.49 |
| 5 PEAK | 3.00 | 0. | 13340000. | -710484. | -882. | 0. | 0. | .784E+08 | .237E+07 | 609.18 | |
| | NON-PEAK | 6.00 | 0. | -1420968. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 608.54 | |
| NON-PEAK | 8.00 | 0. | 0. | -710484. | -1275. | 0. | -3828386. | .855E+08 | .255E+07 | 612.00 | |
| | PEAK | 4.00 | 0. | 13340000. | -947312. | -2769. | -17160000. | 0. | 0. | .665E+08 | .218E+07 |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.49 | |
| | NON-PEAK | 3.00 | 0. | -710484. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.49 | |
| 6 PEAK | 3.00 | 0. | 13340000. | -710484. | -882. | 0. | 0. | .784E+08 | .237E+07 | 609.18 | |
| | NON-PEAK | 6.00 | 0. | -1420968. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 608.54 | |
| NON-PEAK | 8.00 | 0. | 0. | -710484. | -1275. | 0. | -3828386. | .855E+08 | .255E+07 | 612.00 | |
| | PEAK | 4.00 | 0. | 13340000. | -947312. | -2769. | -17160000. | 0. | 0. | .665E+08 | .218E+07 |
| NON-PEAK | 8.00 | 0. | 0. | -1894624. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.49 | |
| | NON-PEAK | 3.00 | 0. | -710484. | -887. | 0. | 0. | .784E+08 | .237E+07 | 609.18 | |
| 7 PEAK | 3.00 | 0. | 13340000. | -710484. | -882. | 0. | 0. | .658E+08 | .218E+07 | 603.81 | |
| | NON-PEAK | 6.00 | 0. | -1420968. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 608.54 | |
| PEAK | 4.00 | 0. | 13340000. | -947312. | -1275. | 0. | -3828386. | .855E+08 | .255E+07 | 612.00 | |
| | NON-PEAK | 8.00 | 0. | -1894624. | -2769. | 0. | 0. | .836E+08 | .250E+07 | 611.29 | |
| NON-PEAK | 3.00 | 0. | 0. | -710484. | -1017. | 0. | 0. | .829E+08 | .248E+07 | 611.02 | |

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|----|----------|------|----|-----------|------------|-----------|------------|------------|------------|----------|----------|--------|
| 16 | PEAK | 3.00 | 0. | 13340000. | -710484. | -1009. | 0. | -10019610. | .855E+08 | .255E+07 | 612.00 | |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | .841E+08 | .251E+07 | 611.47 | | |
| | PEAK | 4.00 | 0. | 13340000. | -947312. | -1363. | 0. | -10968280. | .855E+08 | .255E+07 | 612.00 | |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.49 | |
| 17 | PEAK | 3.00 | 0. | 13340000. | -710484. | -882. | 0. | 0. | .784E+08 | .237E+07 | 609.18 | |
| | NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 608.54 | |
| | PEAK | 4.00 | 0. | 13340000. | -947312. | -1275. | 0. | -3828386. | .855E+08 | .255E+07 | 612.00 | |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 | |
| 18 | PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.49 | |
| | NON-PEAK | 6.00 | 0. | 0. | -710484. | -882. | 0. | 0. | .784E+08 | .237E+07 | 609.18 | |
| | PEAK | 4.00 | 0. | 0. | -1420968. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 608.54 | |
| | NON-PEAK | 3.00 | 0. | 0. | -947312. | -1275. | 0. | -3828386. | .855E+08 | .255E+07 | 612.00 | |
| | PEAK | 3.00 | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 | |
| 19 | PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | 0. | .658E+08 | .217E+07 | 609.18 | |
| | NON-PEAK | 6.00 | 0. | 0. | -710484. | -882. | 0. | 0. | .784E+08 | .237E+07 | 608.54 | |
| | PEAK | 4.00 | 0. | 0. | -1420968. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 612.00 | |
| | NON-PEAK | 8.00 | 0. | 0. | -947312. | -1275. | 0. | -3828386. | .855E+08 | .255E+07 | 603.81 | |
| | PEAK | 3.00 | 0. | 0. | -1894624. | -2769. | 0. | 0. | .658E+08 | .218E+07 | 603.49 | |
| 20 | PEAK | 3.00 | 0. | 0. | -710484. | -1017. | 0. | 0. | .784E+08 | .237E+07 | 609.18 | |
| | NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1009. | 0. | -10019610. | .770E+08 | .235E+07 | 608.54 | |
| | PEAK | 4.00 | 0. | 0. | -947312. | -1275. | 0. | -3828386. | .855E+08 | .255E+07 | 612.00 | |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | 0. | 0. | .836E+08 | .217E+07 | 603.81 | |
| | PEAK | 3.00 | 0. | 0. | -710484. | -1017. | 0. | 0. | .829E+08 | .248E+07 | 609.18 | |
| | NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1009. | 0. | -10019610. | .855E+08 | .255E+07 | 608.54 | |
| | PEAK | 4.00 | 0. | 0. | -947312. | -1275. | 0. | 0. | .836E+08 | .250E+07 | 611.29 | |
| | NON-PEAK | 8.00 | 0. | 0. | -710484. | -1017. | 0. | 0. | .829E+08 | .248E+07 | 611.02 | |
| | PEAK | 3.00 | 0. | 0. | -13340000. | -710484. | -1009. | 0. | .855E+08 | .255E+07 | 612.00 | |
| | NON-PEAK | 6.00 | 0. | 0. | 0. | -1420968. | -2077. | 0. | .841E+08 | .251E+07 | 611.47 | |
| | PEAK | 4.00 | 0. | 0. | 0. | -947312. | -1363. | 0. | -10968280. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 |
| | PEAK | 3.00 | 0. | 0. | 0. | -710484. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.49 |
| | NON-PEAK | 6.00 | 0. | 0. | 0. | -1420968. | -882. | 0. | 0. | .784E+08 | .237E+07 | 609.18 |
| | PEAK | 4.00 | 0. | 0. | 0. | -947312. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 608.54 |
| | NON-PEAK | 8.00 | 0. | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .855E+08 | .255E+07 | 612.00 |
| 21 | PEAK | 3.00 | 0. | 0. | -13340000. | -710484. | -887. | 0. | 0. | .658E+08 | .218E+07 | 603.49 |
| | NON-PEAK | 6.00 | 0. | 0. | 0. | -1420968. | -882. | 0. | 0. | .784E+08 | .237E+07 | 609.18 |
| | PEAK | 4.00 | 0. | 0. | 0. | -947312. | -1275. | 0. | -3828386. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 |
| | PEAK | 3.00 | 0. | 0. | 0. | -710484. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.49 |
| | NON-PEAK | 6.00 | 0. | 0. | 0. | -1420968. | -882. | 0. | 0. | .784E+08 | .237E+07 | 609.18 |
| | PEAK | 4.00 | 0. | 0. | 0. | -947312. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 608.54 |
| | NON-PEAK | 8.00 | 0. | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .855E+08 | .255E+07 | 612.00 |
| 22 | PEAK | 3.00 | 0. | 0. | 0. | -710484. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.49 |
| | NON-PEAK | 6.00 | 0. | 0. | 0. | -1420968. | -882. | 0. | 0. | .784E+08 | .237E+07 | 609.18 |
| | PEAK | 4.00 | 0. | 0. | 0. | -947312. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 608.54 |
| | NON-PEAK | 8.00 | 0. | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .855E+08 | .255E+07 | 612.00 |
| | PEAK | 3.00 | 0. | 0. | 0. | -710484. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.81 |
| | NON-PEAK | 6.00 | 0. | 0. | 0. | -1420968. | -882. | 0. | 0. | .784E+08 | .237E+07 | 609.18 |
| | PEAK | 4.00 | 0. | 0. | 0. | -947312. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 608.54 |
| | NON-PEAK | 8.00 | 0. | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .855E+08 | .255E+07 | 612.00 |
| 23 | PEAK | 3.00 | 0. | 0. | 0. | -710484. | -887. | 0. | 0. | .658E+08 | .217E+07 | 603.49 |
| | NON-PEAK | 6.00 | 0. | 0. | 0. | -947312. | -1275. | 0. | -3828386. | .855E+08 | .237E+07 | 609.18 |
| | PEAK | 4.00 | 0. | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .665E+08 | .218E+07 | 608.54 |
| | NON-PEAK | 8.00 | 0. | 0. | 0. | -710484. | -887. | 0. | 0. | .784E+08 | .235E+07 | 612.00 |
| | PEAK | 3.00 | 0. | 0. | 0. | -1420968. | -1931. | 0. | 0. | .770E+08 | .235E+07 | 603.81 |
| | NON-PEAK | 6.00 | 0. | 0. | 0. | -947312. | -1275. | 0. | -3828386. | .855E+08 | .235E+07 | 609.18 |
| | PEAK | 4.00 | 0. | 0. | 0. | -1894624. | -2769. | -17160000. | 0. | .836E+08 | .250E+07 | 611.29 |
| | NON-PEAK | 8.00 | 0. | 0. | 0. | -710484. | -1017. | 0. | 0. | .829E+08 | .248E+07 | 611.02 |

| | | | | | | | | | | | | |
|----|----------|------|----|-----------|------------|------------|--------------|------------|----------|----------|----------|--------|
| 24 | PEAK | 3.00 | 0. | 13340000. | -710484. | -1009. | 0.-10019610. | .855E+08 | .255E+07 | 612.00 | | |
| | NON-PEAK | 6.00 | 0. | -1420968. | -2077. | 0. | 0. | .841E+08 | .251E+07 | 611.47 | | |
| | PEAK | 4.00 | 0. | 13340000. | -947312. | -1363. | 0.-10968280. | .855E+08 | .255E+07 | 612.00 | | |
| | NON-PEAK | 8.00 | 0. | -1894624. | -2769.- | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 | | |
| | PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | .658E+08 | .217E+07 | 603.49 | | |
| | NON-PEAK | 3.00 | 0. | 13340000. | -710484. | -882. | 0. | .784E+08 | .237E+07 | 609.18 | | |
| 25 | PEAK | 6.00 | 0. | 0. | -1420968. | -1931. | 0. | .770E+08 | .235E+07 | 608.54 | | |
| | NON-PEAK | 4.00 | 0. | 13340000. | -947312. | -1275. | 0.-3828386. | .855E+08 | .255E+07 | 612.00 | | |
| | PEAK | 8.00 | 0. | 0. | -1894624. | -2769.- | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | .658E+08 | .217E+07 | 603.49 | | |
| | PEAK | 3.00 | 0. | 0. | -710484. | -882. | 0. | .784E+08 | .237E+07 | 609.18 | | |
| 26 | PEAK | 6.00 | 0. | 0. | -1420968. | -1931. | 0. | .770E+08 | .235E+07 | 608.54 | | |
| | NON-PEAK | 4.00 | 0. | 0. | -1420968. | -1275. | 0.-3828386. | .855E+08 | .255E+07 | 612.00 | | |
| | PEAK | 8.00 | 0. | 0. | -1894624. | -2769.- | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | .658E+08 | .217E+07 | 603.49 | | |
| | PEAK | 6.00 | 0. | 0. | -1894624. | -1931. | 0. | .784E+08 | .237E+07 | 609.18 | | |
| | NON-PEAK | 4.00 | 0. | 0. | -947312. | -1275. | 0.-3828386. | .855E+08 | .255E+07 | 603.81 | | |
| | PEAK | 8.00 | 0. | 0. | -1894624. | -2769.- | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | .658E+08 | .217E+07 | 603.49 | | |
| | PEAK | 3.00 | 0. | 0. | -710484. | -882. | 0. | .784E+08 | .237E+07 | 609.18 | | |
| 27 | PEAK | 6.00 | 0. | 0. | -1420968. | -1931. | 0. | .770E+08 | .235E+07 | 612.00 | | |
| | NON-PEAK | 4.00 | 0. | 0. | -947312. | -1275. | 0.-3828386. | .855E+08 | .255E+07 | 603.81 | | |
| | PEAK | 8.00 | 0. | 0. | -1894624. | -2769.- | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | .658E+08 | .217E+07 | 603.49 | | |
| | PEAK | 3.00 | 0. | 0. | -710484. | -1017. | 0. | .784E+08 | .237E+07 | 609.18 | | |
| | NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1931. | 0.-10019610. | .855E+08 | .235E+07 | 608.54 | | |
| | PEAK | 4.00 | 0. | 0. | -947312. | -1275. | 0.-3828386. | .855E+08 | .255E+07 | 612.00 | | |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769. | 0. | .836E+08 | .250E+07 | 611.29 | | |
| | PEAK | 3.00 | 0. | 0. | -710484. | -1017. | 0. | .829E+08 | .248E+07 | 611.02 | | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -1009. | 0.-10019610. | .855E+08 | .255E+07 | 612.00 | | |
| 28 | PEAK | 3.00 | 0. | 0. | -1420968. | -2077. | 0. | .841E+08 | .251E+07 | 611.47 | | |
| | NON-PEAK | 6.00 | 0. | 0. | -1420968. | -2077. | 0. | .784E+08 | .237E+07 | 612.00 | | |
| | PEAK | 4.00 | 0. | 0. | -947312. | -1363. | 0.-10968280. | .855E+08 | .255E+07 | 612.00 | | |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769.- | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 | |
| | PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | .658E+08 | .217E+07 | 603.49 | | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -882. | 0. | .784E+08 | .237E+07 | 609.18 | | |
| 29 | PEAK | 3.00 | 0. | 0. | -13340000. | -710484. | -1931. | 0. | .770E+08 | .235E+07 | 608.54 | |
| | NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1275. | 0.-3828386. | .855E+08 | .255E+07 | 612.00 | | |
| | PEAK | 4.00 | 0. | 0. | -13340000. | -947312. | -2769.- | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -887. | 0. | .658E+08 | .217E+07 | 603.49 | | |
| | PEAK | 3.00 | 0. | 0. | -710484. | -882. | 0. | .784E+08 | .237E+07 | 609.18 | | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -1931. | 0.-3828386. | .855E+08 | .255E+07 | 612.00 | | |
| | PEAK | 6.00 | 0. | 0. | -1420968. | -1275. | 0.-3828386. | .855E+08 | .255E+07 | 603.81 | | |
| | NON-PEAK | 4.00 | 0. | 0. | -947312. | -1931. | 0. | .665E+08 | .218E+07 | 603.49 | | |
| | PEAK | 8.00 | 0. | 0. | -1894624. | -2769.- | -17160000. | 0. | .658E+08 | .217E+07 | 603.49 | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | .784E+08 | .237E+07 | 609.18 | | |
| 30 | PEAK | 3.00 | 0. | 0. | -13340000. | -710484. | -887. | 0. | .770E+08 | .235E+07 | 608.54 | |
| | NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1931. | 0. | .658E+08 | .218E+07 | 603.81 | | |
| | PEAK | 4.00 | 0. | 0. | -947312. | -1275. | 0.-3828386. | .855E+08 | .255E+07 | 612.00 | | |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769.- | -17160000. | 0. | .665E+08 | .218E+07 | 603.81 | |
| | PEAK | 3.00 | 0. | 0. | -710484. | -887. | 0. | .658E+08 | .217E+07 | 603.49 | | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -882. | 0. | .784E+08 | .237E+07 | 609.18 | | |
| 31 | PEAK | 3.00 | 0. | 0. | -13340000. | -710484. | -882. | 0. | .770E+08 | .235E+07 | 608.54 | |
| | NON-PEAK | 6.00 | 0. | 0. | -1420968. | -1931. | 0. | .665E+08 | .218E+07 | 612.00 | | |
| | PEAK | 4.00 | 0. | 0. | -947312. | -1275. | 0.-3828386. | .855E+08 | .255E+07 | 612.00 | | |
| | NON-PEAK | 8.00 | 0. | 0. | -1894624. | -2769.- | -17160000. | 0. | .836E+08 | .250E+07 | 611.29 | |
| | NON-PEAK | 3.00 | 0. | 0. | -710484. | -1017. | 0. | .829E+08 | .248E+07 | 611.02 | | |

-.237E+09

MONTH OF : NOVEMBER YEAR : 1963 OPERATION AT RESERVOIR B

| | DATE | PERIOD | DURATION | INFLB (M3) | QA (M3) | IRRS (M3) | EVAPLB (M3) | QPUMP (M3) | SPILLB (M3) | STOREB (M3) | BREA (M2) | EL.B (M) |
|----------|------|--------|----------|---------------|------------|--------------|----------------|---------------|----------------|----------------|--------------|-------------|
| 1 PEAK | 3.00 | | 0. | 13340000. | -1421667. | -702. | 0. | -9308738. | .829E+08 | .248E+07 | 611.02 | |
| NON-PEAK | 6.00 | | 0. | -2843333. | -1445. | 0. | 0. | 0. | .855E+08 | .255E+07 | 612.00 | |
| PEAK | 4.00 | | 0. | 13340000. | -1895556. | -933. | 0. | -8598733. | .827E+08 | .247E+07 | 610.93 | |
| NON-PEAK | 8.00 | | 0. | -3791111. | -1927. | -15300000. | 0. | 0. | .855E+08 | .255E+07 | 612.00 | |
| NON-PEAK | 3.00 | | 0. | -1421667. | -617. | 0. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| NON-PEAK | 3.00 | | 0. | 13340000. | -1421667. | -610. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| 2 PEAK | 3.00 | | 0. | -2843333. | -1330. | 0. | 0. | 0. | .769E+08 | .235E+07 | 608.52 | |
| NON-PEAK | 6.00 | | 0. | -1895556. | -869. | 0. | 0. | 0. | .741E+08 | .230E+07 | 607.24 | |
| PEAK | 4.00 | | 0. | 13340000. | -3791111. | -1927. | -15300000. | 0. | .855E+08 | .255E+07 | 612.00 | |
| NON-PEAK | 8.00 | | 0. | -1421667. | -617. | 0. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| NON-PEAK | 3.00 | | 0. | 13340000. | -1421667. | -610. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| 3 PEAK | 3.00 | | 0. | -2843333. | -1330. | 0. | 0. | 0. | .769E+08 | .235E+07 | 608.52 | |
| NON-PEAK | 6.00 | | 0. | -1895556. | -869. | 0. | 0. | 0. | .741E+08 | .230E+07 | 607.24 | |
| PEAK | 4.00 | | 0. | 13340000. | -3791111. | -1927. | -15300000. | 0. | .855E+08 | .255E+07 | 612.00 | |
| NON-PEAK | 8.00 | | 0. | -1421667. | -617. | 0. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| NON-PEAK | 3.00 | | 0. | 13340000. | -1421667. | -610. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| 4 PEAK | 3.00 | | 0. | -2843333. | -1330. | 0. | 0. | 0. | .769E+08 | .235E+07 | 608.52 | |
| NON-PEAK | 6.00 | | 0. | -1895556. | -869. | 0. | 0. | 0. | .741E+08 | .230E+07 | 607.24 | |
| PEAK | 4.00 | | 0. | 13340000. | -3791111. | -1927. | -15300000. | 0. | .855E+08 | .255E+07 | 612.00 | |
| NON-PEAK | 8.00 | | 0. | -1421667. | -617. | 0. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| NON-PEAK | 3.00 | | 0. | 13340000. | -1421667. | -610. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| 5 PEAK | 3.00 | | 0. | -2843333. | -1330. | 0. | 0. | 0. | .769E+08 | .235E+07 | 608.52 | |
| NON-PEAK | 6.00 | | 0. | -1895556. | -869. | 0. | 0. | 0. | .741E+08 | .230E+07 | 612.00 | |
| PEAK | 4.00 | | 0. | 13340000. | -3791111. | -1927. | -15300000. | 0. | .855E+08 | .255E+07 | 603.80 | |
| NON-PEAK | 8.00 | | 0. | -1421667. | -617. | 0. | 0. | 0. | .664E+08 | .218E+07 | 603.16 | |
| NON-PEAK | 3.00 | | 0. | 13340000. | -1421667. | -610. | 0. | 0. | .650E+08 | .215E+07 | 603.00 | |
| 6 PEAK | 3.00 | | 0. | -2843333. | -1330. | 0. | 0. | 0. | .769E+08 | .235E+07 | 607.24 | |
| NON-PEAK | 6.00 | | 0. | -1895556. | -869. | 0. | 0. | 0. | .741E+08 | .230E+07 | 612.00 | |
| PEAK | 4.00 | | 0. | 13340000. | -3791111. | -1927. | -15300000. | 0. | .855E+08 | .255E+07 | 603.80 | |
| NON-PEAK | 8.00 | | 0. | -1421667. | -617. | 0. | 0. | 0. | .664E+08 | .218E+07 | 603.16 | |
| NON-PEAK | 3.00 | | 0. | 13340000. | -1421667. | -610. | 0. | 0. | .650E+08 | .215E+07 | 603.00 | |
| 7 PEAK | 3.00 | | 0. | -2843333. | -1330. | 0. | 0. | 0. | .769E+08 | .235E+07 | 607.24 | |
| NON-PEAK | 6.00 | | 0. | -1895556. | -869. | 0. | 0. | 0. | .741E+08 | .230E+07 | 612.00 | |
| PEAK | 4.00 | | 0. | 13340000. | -3791111. | -1927. | -15300000. | 0. | .855E+08 | .255E+07 | 603.80 | |
| NON-PEAK | 8.00 | | 0. | -1421667. | -617. | 0. | 0. | 0. | .664E+08 | .218E+07 | 603.16 | |
| NON-PEAK | 3.00 | | 0. | 13340000. | -1421667. | -610. | 0. | 0. | .650E+08 | .215E+07 | 603.00 | |

| | | | | | | | | | | | | |
|----|----------|------|----|-----------|------------|------------|------------|--------|----------|----------|----------|--------|
| 8 | PEAK | 3.00 | 0. | 13340000. | -1421667. | -610. | 0. | 0. | .769E+08 | .235E+07 | 608.52 | |
| | NON-PEAK | 6.00 | 0. | -2843333. | -1330. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 | |
| | PEAK | 4.00 | 0. | 13340000. | -1895556. | -869. | 0. | -1314. | .855E+08 | .255E+07 | 612.00 | |
| | NON-PEAK | 8.00 | 0. | -3791111. | -1927. | -15300000. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| 9 | PEAK | 3.00 | 0. | -1421667. | -617. | 0. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| | NON-PEAK | 3.00 | 0. | -1421667. | -610. | 0. | 0. | 0. | .769E+08 | .235E+07 | 608.52 | |
| 10 | PEAK | 6.00 | 0. | -2843333. | -1330. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 | |
| | NON-PEAK | 4.00 | 0. | 13340000. | -1895556. | -869. | 0. | -1314. | .855E+08 | .255E+07 | 612.00 | |
| | PEAK | 8.00 | 0. | -3791111. | -1927. | -15300000. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| | NON-PEAK | 3.00 | 0. | -1421667. | -617. | 0. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| 11 | PEAK | 3.00 | 0. | 0. | -2843333. | -1330. | 0. | 0. | .769E+08 | .235E+07 | 608.52 | |
| | NON-PEAK | 6.00 | 0. | 13340000. | -1895556. | -869. | 0. | -1314. | .855E+08 | .255E+07 | 612.00 | |
| | PEAK | 4.00 | 0. | 0. | -3791111. | -1927. | -15300000. | 0. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 3.00 | 0. | 0. | -1421667. | -617. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| 12 | PEAK | 3.00 | 0. | 0. | -1421667. | -610. | 0. | 0. | .769E+08 | .235E+07 | 608.52 | |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -1330. | 0. | -1314. | .855E+08 | .255E+07 | 612.00 | |
| | PEAK | 4.00 | 0. | 13340000. | -1895556. | -869. | 0. | 0. | .664E+08 | .218E+07 | 603.80 | |
| | NON-PEAK | 3.00 | 0. | 0. | -3791111. | -1927. | -15300000. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 13 | PEAK | 3.00 | 0. | 0. | -1421667. | -617. | 0. | 0. | .769E+08 | .235E+07 | 608.52 | |
| | NON-PEAK | 6.00 | 0. | 0. | -2843333. | -1330. | 0. | -1314. | .855E+08 | .255E+07 | 612.00 | |
| | PEAK | 4.00 | 0. | 0. | -1895556. | -869. | 0. | 0. | .741E+08 | .230E+07 | 607.24 | |
| | NON-PEAK | 3.00 | 0. | 0. | -3791111. | -1927. | -15300000. | 0. | 0. | .664E+08 | .235E+07 | 608.52 |
| 14 | PEAK | 3.00 | 0. | 0. | -1421667. | -617. | 0. | 0. | .741E+08 | .230E+07 | 607.24 | |
| | NON-PEAK | 6.00 | 0. | 0. | -1421667. | -610. | 0. | 0. | .769E+08 | .235E+07 | 608.52 | |
| | PEAK | 4.00 | 0. | 0. | -2843333. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 | |
| | NON-PEAK | 8.00 | 0. | 0. | -1895556. | -869. | 0. | -1314. | .855E+08 | .255E+07 | 612.00 | |
| | PEAK | 3.00 | 0. | 0. | -3791111. | -1927. | -15300000. | 0. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 3.00 | 0. | 0. | -1421667. | -617. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| 15 | PEAK | 3.00 | 0. | 0. | -13340000. | -1895556. | -869. | 0. | .769E+08 | .235E+07 | 608.52 | |
| | NON-PEAK | 6.00 | 0. | 0. | -3791111. | -1927. | -15300000. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| | PEAK | 4.00 | 0. | 0. | -2843333. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 | |
| | NON-PEAK | 8.00 | 0. | 0. | -1895556. | -869. | 0. | -1314. | .855E+08 | .255E+07 | 612.00 | |
| | PEAK | 3.00 | 0. | 0. | -3791111. | -1927. | -15300000. | 0. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 3.00 | 0. | 0. | -1421667. | -617. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |

| | | | | | | | | | | |
|----|----------|------|----|-----------|-----------|------------|----|----------|----------|--------|
| 24 | PEAK | 3.00 | 0. | 13340000. | -1421667. | -610. | 0. | .769E+08 | .235E+07 | 608.52 |
| | NON-PEAK | 6.00 | 0. | -2843333. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 |
| | PEAK | 4.00 | 0. | 13340000. | -1895556. | -869. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | -3791111. | -1927. | -15300000. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 3.00 | 0. | -1421667. | -617. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 25 | PEAK | 3.00 | 0. | 13340000. | -1421667. | -610. | 0. | .769E+08 | .235E+07 | 608.52 |
| | NON-PEAK | 6.00 | 0. | -2843333. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 |
| | PEAK | 4.00 | 0. | 13340000. | -1895556. | -869. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | -3791111. | -1927. | -15300000. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 3.00 | 0. | -1421667. | -617. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 26 | PEAK | 3.00 | 0. | 13340000. | -1421667. | -610. | 0. | .769E+08 | .235E+07 | 608.52 |
| | NON-PEAK | 6.00 | 0. | -2843333. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 |
| | PEAK | 4.00 | 0. | 13340000. | -1895556. | -869. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | -3791111. | -1927. | -15300000. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 3.00 | 0. | -1421667. | -617. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 27 | PEAK | 3.00 | 0. | 13340000. | -1421667. | -610. | 0. | .769E+08 | .235E+07 | 608.52 |
| | NON-PEAK | 6.00 | 0. | -2843333. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 |
| | PEAK | 4.00 | 0. | 13340000. | -1895556. | -869. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | -3791111. | -1927. | -15300000. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 3.00 | 0. | -1421667. | -617. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 28 | PEAK | 3.00 | 0. | 13340000. | -1421667. | -610. | 0. | .769E+08 | .235E+07 | 608.52 |
| | NON-PEAK | 6.00 | 0. | -2843333. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 |
| | PEAK | 4.00 | 0. | 13340000. | -1895556. | -869. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | -3791111. | -1927. | -15300000. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 3.00 | 0. | -1421667. | -617. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 29 | PEAK | 3.00 | 0. | 13340000. | -1421667. | -610. | 0. | .769E+08 | .235E+07 | 608.52 |
| | NON-PEAK | 6.00 | 0. | -2843333. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 |
| | PEAK | 4.00 | 0. | 13340000. | -1895556. | -869. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | -3791111. | -1927. | -15300000. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 3.00 | 0. | -1421667. | -617. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 30 | PEAK | 3.00 | 0. | 13340000. | -1421667. | -610. | 0. | .769E+08 | .235E+07 | 608.52 |
| | NON-PEAK | 6.00 | 0. | -2843333. | -1330. | 0. | 0. | .741E+08 | .230E+07 | 607.24 |
| | PEAK | 4.00 | 0. | 13340000. | -1895556. | -869. | 0. | .855E+08 | .255E+07 | 612.00 |
| | NON-PEAK | 8.00 | 0. | -3791111. | -1927. | -15300000. | 0. | .664E+08 | .218E+07 | 603.80 |
| | NON-PEAK | 3.00 | 0. | -1421667. | -617. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |

| MONTH OF : DECEMBER | | YEAR : 1963 | | OPERATION AT RESERVOIR B | | | | | | | |
|---------------------|--------|---------------|------------|--------------------------|------------------|-------------|------------|-------------|-------------|-----------|----------|
| DATE | PERIOD | DURATION (HR) | INFIL (M3) | QA (M3) | IRRS (M3) | EVAPLB (M3) | QPUMP (M3) | SPILLB (M3) | STOREB (M3) | BREA (M2) | EL.B (M) |
| 1 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| NON-PEAK | 6.00 | 0. | -3756452. | -792. | 0. | 0. | 0. | .765E+08 | .234E+07 | 608.32 | |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .727E+08 | .228E+07 | 606.63 | |
| NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0. | 0. | 0. | .835E+08 | .249E+07 | 611.26 | |
| NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0. | 0. | 0. | .669E+08 | .218E+07 | 604.00 | |
| NON-PEAK | 2 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .765E+08 | .234E+07 | 608.32 |
| NON-PEAK | 6.00 | 0. | -3756452. | -792. | 0. | 0. | 0. | .727E+08 | .228E+07 | 606.63 | |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .835E+08 | .249E+07 | 611.26 | |
| NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0. | 0. | 0. | .669E+08 | .218E+07 | 604.00 | |
| NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| 3 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .765E+08 | .234E+07 | 608.32 | |
| NON-PEAK | 6.00 | 0. | -3756452. | -792. | 0. | 0. | 0. | .727E+08 | .228E+07 | 606.63 | |
| NON-PEAK | 4 PEAK | 3.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .835E+08 | .249E+07 | 611.26 |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -1127.-11650000. | 0. | 0. | .669E+08 | .218E+07 | 604.00 | |
| NON-PEAK | 8.00 | 0. | -5008602. | -370. | 0. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| NON-PEAK | 3.00 | 0. | -1878226. | -365. | 0. | 0. | 0. | .765E+08 | .234E+07 | 608.32 | |
| NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0. | 0. | 0. | .727E+08 | .228E+07 | 606.63 | |
| NON-PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .835E+08 | .249E+07 | 611.26 | |
| NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0. | 0. | 0. | .669E+08 | .218E+07 | 604.00 | |
| NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0. | 0. | 0. | .835E+08 | .249E+07 | 611.26 | |
| NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0. | 0. | 0. | .669E+08 | .218E+07 | 606.63 | |
| NON-PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .835E+08 | .249E+07 | 611.26 | |
| NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0. | 0. | 0. | .669E+08 | .215E+07 | 603.16 | |
| NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0. | 0. | 0. | .727E+08 | .228E+07 | 606.63 | |
| NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0. | 0. | 0. | .835E+08 | .249E+07 | 611.26 | |
| NON-PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .765E+08 | .234E+07 | 608.32 | |
| NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0. | 0. | 0. | .765E+08 | .234E+07 | 608.32 | |
| NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0. | 0. | 0. | .727E+08 | .228E+07 | 606.63 | |
| NON-PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .835E+08 | .249E+07 | 611.26 | |
| NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0. | 0. | 0. | .669E+08 | .218E+07 | 604.00 | |
| NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| 6 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .765E+08 | .234E+07 | 608.32 | |
| NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0. | 0. | 0. | .727E+08 | .228E+07 | 606.63 | |
| NON-PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .835E+08 | .249E+07 | 611.26 | |
| NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0. | 0. | 0. | .669E+08 | .218E+07 | 604.00 | |
| NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |
| 7 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .765E+08 | .234E+07 | 608.32 | |
| NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0. | 0. | 0. | .727E+08 | .228E+07 | 606.63 | |
| NON-PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .836E+08 | .249E+07 | 611.26 | |
| NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0. | 0. | 0. | .669E+08 | .218E+07 | 604.00 | |
| NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0. | 0. | 0. | .650E+08 | .215E+07 | 603.16 | |

| | | | | | | | | | | |
|----------|------|----|-----------|-----------|------------------|----|----|----------|----------|--------|
| 8 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .765E+08 | .234E+07 | 608.32 |
| NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0. | 0. | 0. | .727E+08 | .228E+07 | 606.63 |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .836E+08 | .249E+07 | 611.26 |
| NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | 0. | .669E+08 | .218E+07 | 604.01 |
| NON-PEAK | 3.00 | 0. | 0. | -1878226. | -370. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 9 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .765E+08 | .234E+07 | 608.32 |
| NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | 0. | .727E+08 | .228E+07 | 606.63 |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .836E+08 | .249E+07 | 611.26 |
| NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | 0. | .669E+08 | .218E+07 | 604.01 |
| NON-PEAK | 3.00 | 0. | 0. | -1878226. | -370. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 10 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .765E+08 | .234E+07 | 608.32 |
| NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | 0. | .727E+08 | .228E+07 | 606.63 |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .836E+08 | .249E+07 | 611.26 |
| NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | 0. | .669E+08 | .218E+07 | 604.01 |
| NON-PEAK | 3.00 | 0. | 0. | -1878226. | -370. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 11 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .765E+08 | .234E+07 | 608.32 |
| NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | 0. | .727E+08 | .228E+07 | 606.63 |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .836E+08 | .249E+07 | 611.26 |
| NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | 0. | .669E+08 | .218E+07 | 604.01 |
| NON-PEAK | 3.00 | 0. | 0. | -1878226. | -370. | 0. | 0. | .650E+08 | .228E+07 | 606.63 |
| 12 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .836E+08 | .249E+07 | 611.26 |
| NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | 0. | .669E+08 | .218E+07 | 604.01 |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .765E+08 | .234E+07 | 603.16 |
| NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | 0. | .669E+08 | .218E+07 | 604.01 |
| NON-PEAK | 3.00 | 0. | 0. | -1878226. | -370. | 0. | 0. | .765E+08 | .234E+07 | 608.32 |
| 13 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .727E+08 | .228E+07 | 606.63 |
| NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | 0. | .836E+08 | .249E+07 | 611.26 |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .669E+08 | .218E+07 | 604.01 |
| NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| NON-PEAK | 3.00 | 0. | 0. | -1878226. | -370. | 0. | 0. | .765E+08 | .234E+07 | 608.32 |
| 14 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .669E+08 | .218E+07 | 604.01 |
| NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | 0. | .727E+08 | .228E+07 | 606.63 |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .836E+08 | .249E+07 | 611.26 |
| NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | 0. | .669E+08 | .218E+07 | 604.01 |
| NON-PEAK | 3.00 | 0. | 0. | -1878226. | -370. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |
| 15 PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | .765E+08 | .234E+07 | 608.32 |
| NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | 0. | .727E+08 | .228E+07 | 606.63 |
| PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | 0. | .836E+08 | .249E+07 | 611.26 |
| NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | 0. | .669E+08 | .218E+07 | 604.01 |
| NON-PEAK | 3.00 | 0. | 0. | -1878226. | -370. | 0. | 0. | .650E+08 | .215E+07 | 603.16 |

| | | | | | | | | | | |
|----|----------|------|----|-----------|-----------|------------------|-------|----------|----------|----------|
| 16 | PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | .765E+08 | .234E+07 | |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | .727E+08 | .228E+07 | |
| | PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0. | .836E+08 | .249E+07 | |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | .669E+08 | .218E+07 | |
| | NON-PEAK | 3.00 | 0. | 0. | -1878226. | -370. | 0. | .650E+08 | .215E+07 | |
| | PEAK | 3.00 | 0. | 0. | 13340000. | -1878226. | -365. | 0. | .765E+08 | .234E+07 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | .727E+08 | .228E+07 | |
| | PEAK | 4.00 | 0. | 0. | 13340000. | -2504301. | -515. | 0. | .836E+08 | .249E+07 |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | .669E+08 | .218E+07 | |
| | NON-PEAK | 3.00 | 0. | 0. | 0. | -1878226. | -370. | 0. | .650E+08 | .215E+07 |
| 17 | PEAK | 3.00 | 0. | 0. | 13340000. | -1878226. | -365. | 0. | .765E+08 | .234E+07 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | .727E+08 | .228E+07 | |
| | PEAK | 4.00 | 0. | 0. | 13340000. | -2504301. | -515. | 0. | .836E+08 | .249E+07 |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | .669E+08 | .218E+07 | |
| | NON-PEAK | 3.00 | 0. | 0. | 0. | -1878226. | -370. | 0. | .650E+08 | .215E+07 |
| 18 | PEAK | 3.00 | 0. | 0. | 13340000. | -1878226. | -365. | 0. | .765E+08 | .234E+07 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | .727E+08 | .228E+07 | |
| | PEAK | 4.00 | 0. | 0. | 13340000. | -2504301. | -515. | 0. | .836E+08 | .249E+07 |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | .669E+08 | .218E+07 | |
| | NON-PEAK | 3.00 | 0. | 0. | 0. | -1878226. | -370. | 0. | .650E+08 | .215E+07 |
| 19 | PEAK | 3.00 | 0. | 0. | 13340000. | -1878226. | -365. | 0. | .727E+08 | .228E+07 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | .836E+08 | .249E+07 | |
| | PEAK | 4.00 | 0. | 0. | 13340000. | -2504301. | -515. | 0. | .669E+08 | .218E+07 |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | .650E+08 | .234E+07 | |
| | NON-PEAK | 3.00 | 0. | 0. | 0. | -1878226. | -370. | 0. | .650E+08 | .215E+07 |
| 20 | PEAK | 3.00 | 0. | 0. | 13340000. | -1878226. | -365. | 0. | .765E+08 | .234E+07 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | .727E+08 | .228E+07 | |
| | PEAK | 4.00 | 0. | 0. | 13340000. | -2504301. | -515. | 0. | .836E+08 | .249E+07 |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | .669E+08 | .218E+07 | |
| | NON-PEAK | 3.00 | 0. | 0. | 0. | -1878226. | -370. | 0. | .650E+08 | .215E+07 |
| 21 | PEAK | 3.00 | 0. | 0. | 13340000. | -1878226. | -365. | 0. | .765E+08 | .234E+07 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | .727E+08 | .228E+07 | |
| | PEAK | 4.00 | 0. | 0. | 13340000. | -2504301. | -515. | 0. | .836E+08 | .249E+07 |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | .669E+08 | .218E+07 | |
| | NON-PEAK | 3.00 | 0. | 0. | 0. | -1878226. | -370. | 0. | .650E+08 | .215E+07 |
| 22 | PEAK | 3.00 | 0. | 0. | 13340000. | -1878226. | -365. | 0. | .727E+08 | .228E+07 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | .836E+08 | .249E+07 | |
| | PEAK | 4.00 | 0. | 0. | 13340000. | -2504301. | -515. | 0. | .669E+08 | .218E+07 |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | .650E+08 | .234E+07 | |
| | NON-PEAK | 3.00 | 0. | 0. | 0. | -1878226. | -370. | 0. | .650E+08 | .215E+07 |
| 23 | PEAK | 3.00 | 0. | 0. | 13340000. | -1878226. | -365. | 0. | .765E+08 | .234E+07 |
| | NON-PEAK | 6.00 | 0. | 0. | -3756452. | -793. | 0. | .727E+08 | .228E+07 | |
| | PEAK | 4.00 | 0. | 0. | 13340000. | -2504301. | -515. | 0. | .836E+08 | .249E+07 |
| | NON-PEAK | 8.00 | 0. | 0. | -5008602. | -1127.-11650000. | 0. | .669E+08 | .218E+07 | |
| | NON-PEAK | 3.00 | 0. | 0. | 0. | -1878226. | -370. | 0. | .650E+08 | .215E+07 |

| | | | | | | | | | | | |
|----|----------|------|----|-----------|------------------|-------|-----|----------|----------|----------|--------|
| 24 | PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0. | 0. | -765E+08 | .234E+07 | 608.33 |
| | NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0.. | 0. | -727E+08 | .228E+07 | 606.64 | |
| | PEAK | 4.00 | 0. | -2504301. | -515. | 0.. | 0. | -836E+08 | .249E+07 | 611.27 | |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0.. | 0. | -669E+08 | .218E+07 | 604.01 | |
| | NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0.. | 0. | -650E+08 | .215E+07 | 603.17 | |
| 25 | PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0.. | -765E+08 | .234E+07 | 608.33 | |
| | NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0.. | 0. | -727E+08 | .228E+07 | 606.64 | |
| | PEAK | 4.00 | 0. | -2504301. | -515. | 0.. | 0. | -836E+08 | .249E+07 | 611.27 | |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0.. | 0. | -669E+08 | .218E+07 | 604.01 | |
| | NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0.. | 0. | -650E+08 | .215E+07 | 603.17 | |
| 26 | PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0.. | -765E+08 | .234E+07 | 608.33 | |
| | NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0.. | 0. | -727E+08 | .228E+07 | 606.64 | |
| | PEAK | 4.00 | 0. | 13340000. | -2504301. | -515. | 0.. | -836E+08 | .250E+07 | 611.27 | |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0.. | 0. | -669E+08 | .218E+07 | 604.01 | |
| | NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0.. | 0. | -650E+08 | .215E+07 | 603.17 | |
| 27 | PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0.. | -765E+08 | .234E+07 | 608.33 | |
| | NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0.. | 0. | -727E+08 | .228E+07 | 606.64 | |
| | PEAK | 4.00 | 0. | -2504301. | -515. | 0.. | 0. | -836E+08 | .250E+07 | 611.27 | |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0.. | 0. | -669E+08 | .218E+07 | 604.01 | |
| | NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0.. | 0. | -650E+08 | .215E+07 | 603.17 | |
| 28 | PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0.. | -765E+08 | .234E+07 | 608.33 | |
| | NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0.. | 0. | -727E+08 | .228E+07 | 606.64 | |
| | PEAK | 4.00 | 0. | -2504301. | -515. | 0.. | 0. | -836E+08 | .250E+07 | 611.27 | |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0.. | 0. | -669E+08 | .218E+07 | 604.01 | |
| | NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0.. | 0. | -650E+08 | .215E+07 | 603.17 | |
| 29 | PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0.. | -765E+08 | .234E+07 | 608.33 | |
| | NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0.. | 0. | -727E+08 | .228E+07 | 606.64 | |
| | PEAK | 4.00 | 0. | -2504301. | -515. | 0.. | 0. | -836E+08 | .250E+07 | 611.27 | |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0.. | 0. | -669E+08 | .218E+07 | 604.01 | |
| | NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0.. | 0. | -650E+08 | .215E+07 | 603.17 | |
| 30 | PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0.. | -765E+08 | .234E+07 | 608.33 | |
| | NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0.. | 0. | -727E+08 | .228E+07 | 606.64 | |
| | PEAK | 4.00 | 0. | -2504301. | -515. | 0.. | 0. | -836E+08 | .250E+07 | 611.27 | |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0.. | 0. | -669E+08 | .218E+07 | 604.01 | |
| | NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0.. | 0. | -650E+08 | .215E+07 | 603.17 | |
| 31 | PEAK | 3.00 | 0. | 13340000. | -1878226. | -365. | 0.. | -765E+08 | .234E+07 | 608.33 | |
| | NON-PEAK | 6.00 | 0. | -3756452. | -793. | 0.. | 0. | -836E+08 | .228E+07 | 606.64 | |
| | PEAK | 4.00 | 0. | -2504301. | -515. | 0.. | 0. | -727E+08 | .250E+07 | 611.27 | |
| | NON-PEAK | 8.00 | 0. | -5008602. | -1127.-11650000. | 0.. | 0. | -669E+08 | .218E+07 | 604.02 | |
| | NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0.. | 0. | -650E+08 | .215E+07 | 603.17 | |
| | NON-PEAK | 3.00 | 0. | -1878226. | -370. | 0.. | 0. | -650E+08 | .215E+07 | 603.17 | |
| | | | | | | | | 000E+00 | | | |
| | | | | | | | | .255E+09 | | | |

File name: ENGPRF0.OUT for year 1963 with proposed operation schedule

| MONTH OF : | OCTOBER | YEAR : | 1963 | ENERGY GENERATION IN U/S, D/S POWER HOUSE AND % MEETING IRR. DEMAND | | | | | | | |
|------------|----------|----------|---------------|---|-------------|----------------|--------------|----------------------|--------------|-----------------------------|-------------|
| DATE | PERIOD | DURATION | GROSSH (M) | NETTH (M) | Q (M3/S) | STARTP (MW) | ENDP (MW) | A.V. ENERGY (MWh) | QD (M3/S) | ENERGY TOT. ENERGY (MWh) | IRR. (%) |
| 1 | PEAK | 3.00 | 225. | 210. | 1235. | 2223. | 2160. | 6575. | 66. | 123. | 6698. |
| | NON-PEAK | 6.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 225. | 224. | 237. | 446. | 444. | 1780. | 66. | 165. | 1944. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 123. |
| 2 | PEAK | 3.00 | 220. | 205. | 1235. | 2169. | 2107. | 6415. | 66. | 123. | 6538. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 217. | 209. | 926. | 1639. | 1612. | 6501. | 66. | 165. | 6666. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 123. |
| 3 | PEAK | 3.00 | 220. | 204. | 1235. | 2166. | 2105. | 6406. | 66. | 123. | 6530. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 218. | 209. | 926. | 1637. | 1612. | 6498. | 66. | 165. | 6663. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 123. | 123. |
| 4 | PEAK | 3.00 | 217. | 202. | 1235. | 2091. | 2078. | 6253. | 66. | 123. | 6377. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | NON-PEAK | 4.00 | 217. | 208. | 926. | 1616. | 1610. | 6452. | 66. | 165. | 6616. |
| | PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 123. |
| 5 | PEAK | 3.00 | 220. | 205. | 1235. | 2170. | 2108. | 6417. | 66. | 123. | 6540. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1639. | 1611. | 6500. | 66. | 165. | 6665. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 123. |
| 6 | PEAK | 3.00 | 220. | 205. | 1235. | 2171. | 2109. | 6420. | 66. | 123. | 6543. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 217. | 209. | 926. | 1640. | 1611. | 6503. | 66. | 165. | 6668. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 227. | 227. | 0. | 0. | 0. | 0. | 66. | 123. | 123. |
| 7 | PEAK | 3.00 | 221. | 205. | 1235. | 2172. | 2110. | 6423. | 66. | 123. | 6547. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 218. | 209. | 926. | 1641. | 1612. | 6507. | 66. | 165. | 6671. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 123. | 123. |

| | | | | | | | |
|----------|------|------|-------|-------|-------|-------|------|
| 8 PEAK | 3.00 | 217. | 1235. | 2091. | 2078. | 6253. | 100. |
| NON-PEAK | 6.00 | 218. | 0. | 0. | 0. | 66. | 123. |
| PEAK | 4.00 | 217. | 208. | 926. | 1616. | 1610. | 247. |
| NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 6451. | 247. |
| NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 66. | 165. |
| 9 PEAK | 3.00 | 220. | 205. | 1235. | 2170. | 2108. | 100. |
| NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 66. | 100. |
| PEAK | 4.00 | 217. | 208. | 926. | 1639. | 1611. | 100. |
| NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 6500. | 100. |
| NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 66. | 329. |
| 10 PEAK | 3.00 | 220. | 205. | 1235. | 2171. | 2109. | 100. |
| NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 6420. | 100. |
| PEAK | 4.00 | 217. | 209. | 926. | 1640. | 1611. | 100. |
| NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 6503. | 100. |
| NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 66. | 123. |
| 11 PEAK | 3.00 | 220. | 226. | 0. | 0. | 6423. | 100. |
| NON-PEAK | 6.00 | 221. | 205. | 1235. | 2172. | 2110. | 100. |
| NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 66. | 165. |
| PEAK | 4.00 | 217. | 209. | 926. | 1641. | 1612. | 100. |
| NON-PEAK | 3.00 | 226. | 218. | 0. | 0. | 6507. | 100. |
| NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 66. | 123. |
| 12 PEAK | 3.00 | 219. | 219. | 0. | 0. | 66. | 123. |
| NON-PEAK | 3.00 | 217. | 202. | 1235. | 2091. | 2078. | 100. |
| NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 6253. | 100. |
| PEAK | 4.00 | 217. | 208. | 926. | 1616. | 1610. | 100. |
| NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 6451. | 100. |
| NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 66. | 165. |
| 13 PEAK | 3.00 | 220. | 205. | 1235. | 2170. | 2108. | 100. |
| NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 6416. | 100. |
| PEAK | 4.00 | 217. | 208. | 926. | 1639. | 1610. | 100. |
| NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 6500. | 100. |
| NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 66. | 123. |
| 14 PEAK | 3.00 | 220. | 205. | 1235. | 2171. | 2109. | 100. |
| NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 6420. | 100. |
| PEAK | 4.00 | 217. | 209. | 926. | 1640. | 1611. | 100. |
| NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 6503. | 100. |
| NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 66. | 123. |
| 15 PEAK | 3.00 | 221. | 205. | 1235. | 2172. | 2110. | 100. |
| NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 6423. | 100. |
| PEAK | 4.00 | 217. | 209. | 926. | 1641. | 1612. | 100. |
| NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 6506. | 100. |
| NON-PEAK | 3.00 | 219. | 219. | 0. | 0. | 66. | 123. |

| | | | | | | | | | | | |
|----|----------|------|------|------|-------|-------|-------|-------|-----|------|-------|
| 16 | PEAK | 3.00 | 217. | 202. | 1235. | 2091. | 2078. | 6253. | 66. | 123. | 6376. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. | 247. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1616. | 1610. | 6451. | 66. | 100. | 100. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 165. | 6616. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| 17 | PEAK | 3.00 | 220. | 205. | 1235. | 2170. | 2108. | 6416. | 66. | 123. | 123. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1639. | 1610. | 6500. | 66. | 247. | 100. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 165. | 6664. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| 18 | PEAK | 3.00 | 220. | 205. | 1235. | 2171. | 2109. | 6420. | 66. | 123. | 123. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 6543. |
| | PEAK | 4.00 | 217. | 209. | 926. | 1640. | 1611. | 6503. | 66. | 165. | 100. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 19 | PEAK | 3.00 | 221. | 205. | 1235. | 2172. | 2110. | 6423. | 66. | 123. | 123. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 165. | 6668. |
| | PEAK | 4.00 | 217. | 209. | 926. | 1641. | 1612. | 6506. | 66. | 329. | 329. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| | NON-PEAK | 3.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 247. | 6546. |
| 20 | PEAK | 3.00 | 217. | 202. | 1235. | 2091. | 2078. | 6253. | 66. | 123. | 123. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1616. | 1610. | 6451. | 66. | 165. | 6671. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 21 | PEAK | 3.00 | 220. | 205. | 1235. | 2170. | 2108. | 6416. | 66. | 123. | 123. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1639. | 1610. | 6499. | 66. | 165. | 6615. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 22 | PEAK | 3.00 | 220. | 205. | 1235. | 2171. | 2109. | 6419. | 66. | 123. | 123. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 6543. |
| | PEAK | 4.00 | 217. | 209. | 926. | 1640. | 1611. | 6503. | 66. | 165. | 6664. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 23 | PEAK | 3.00 | 220. | 205. | 1235. | 2172. | 2110. | 6423. | 66. | 123. | 123. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 209. | 926. | 1641. | 1612. | 6506. | 66. | 165. | 6671. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 329. |
| | NON-PEAK | 3.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |

| | | AVERAGE & 10 DAILY IRR.SUPPLY = | | | | | | | | | |
|----|----------|---------------------------------|------|------|-------|-------|-------|-------|-----|---------|---------|
| 24 | PEAK | 3.00 | 217. | 202. | 1235. | 2091. | 2078. | 6253. | 66. | 123. | 100. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1616. | 1610. | 6451. | 66. | 165. | 100. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 25 | PEAK | 3.00 | 220. | 205. | 1235. | 2169. | 2108. | 6416. | 66. | 123. | 100. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1639. | 1610. | 6499. | 66. | 165. | 100. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 26 | PEAK | 3.00 | 220. | 205. | 1235. | 2171. | 2109. | 6419. | 66. | 123. | 100. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 209. | 926. | 1640. | 1611. | 6503. | 66. | 165. | 100. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 27 | PEAK | 3.00 | 220. | 205. | 1235. | 2172. | 2110. | 6423. | 66. | 123. | 100. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 209. | 926. | 1641. | 1612. | 6506. | 66. | 165. | 100. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 100. |
| | NON-PEAK | 3.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 28 | PEAK | 3.00 | 217. | 202. | 1235. | 2091. | 2078. | 6252. | 66. | 123. | 100. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1616. | 1609. | 6451. | 66. | 165. | 100. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 29 | PEAK | 3.00 | 220. | 205. | 1235. | 2169. | 2108. | 6416. | 66. | 123. | 100. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1639. | 1610. | 6499. | 66. | 165. | 100. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 30 | PEAK | 3.00 | 220. | 205. | 1235. | 2171. | 2109. | 6419. | 66. | 123. | 100. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 209. | 926. | 1640. | 1611. | 6503. | 66. | 165. | 100. |
| | NON-PEAK | 8.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 329. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| 31 | PEAK | 3.00 | 220. | 205. | 1235. | 2172. | 2110. | 6422. | 66. | 123. | 100. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 66. | 247. | 100. |
| | PEAK | 4.00 | 217. | 209. | 926. | 1641. | 1612. | 6506. | 66. | 165. | 100. |
| | NON-PEAK | 8.00 | 218. | 218. | 0. | 0. | 0. | 0. | 66. | 329. | 100. |
| | NON-PEAK | 3.00 | 219. | 219. | 0. | 0. | 0. | 0. | 66. | 123. | 100. |
| | | | | | | | | | | 394476. | |
| | | | | | | | | | | 100.00 | 100.00 |
| | | | | | | | | | | | 425085. |

MONTH OF : NOVEMBER YEAR : 1963 ENERGY GENERATION IN U/S, D/S POWER HOUSE AND % MEETING IRR.DEMAND

| | DATE | PERIOD | DURATION (HR) | GROSSH (M) | NETTH (M) | Q (M3/S) | STARTP (MW) | ENDP (MW) | AV. ENERGY (MWh) | QD (M3/S) | ENERGY (MWh) | TOT. ENERGY (MWh) | IRR. (%) |
|---|----------|--------|------------------|---------------|--------------|-------------|----------------|--------------|---------------------|--------------|-----------------|----------------------|-------------|
| 1 | PEAK | 3.00 | | 217. | 202. | 1235. | 2091. | 2077. | 6252. | 132. | 247. | 6499. | 100. |
| | NON-PEAK | 6.00 | | 218. | 0. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | | 217. | 208. | 926. | 1620. | 1609. | 6457. | 132. | 329. | 6786. | 100. |
| | NON-PEAK | 8.00 | | 226. | 0. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 2 | PEAK | 3.00 | | 221. | 205. | 1235. | 2171. | 2112. | 6425. | 132. | 247. | 6672. | 100. |
| | NON-PEAK | 6.00 | | 222. | 222. | 0. | 0. | ~ 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | | 217. | 208. | 926. | 1647. | 1608. | 6512. | 132. | 329. | 6841. | 100. |
| | NON-PEAK | 8.00 | | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 3 | PEAK | 3.00 | | 221. | 205. | 1235. | 2170. | 2112. | 6423. | 132. | 247. | 6670. | 100. |
| | NON-PEAK | 6.00 | | 222. | 222. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | | 217. | 208. | 926. | 1647. | 1608. | 6510. | 132. | 329. | 6839. | 100. |
| | NON-PEAK | 8.00 | | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 4 | PEAK | 3.00 | | 221. | 205. | 1235. | 2170. | 2111. | 6421. | 132. | 247. | 6668. | 100. |
| | NON-PEAK | 6.00 | | 222. | 222. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | | 217. | 208. | 926. | 1646. | 1607. | 6507. | 132. | 329. | 6837. | 100. |
| | NON-PEAK | 8.00 | | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | | 221. | 205. | 1235. | 2170. | 2111. | 6421. | 132. | 247. | 6668. | 100. |
| 5 | PEAK | 3.00 | | 222. | 205. | 1235. | 2169. | 2110. | 6419. | 132. | 247. | 6666. | 100. |
| | NON-PEAK | 6.00 | | 222. | 222. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | | 217. | 208. | 926. | 1646. | 1607. | 6505. | 132. | 329. | 6835. | 100. |
| | NON-PEAK | 8.00 | | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | | 221. | 205. | 1235. | 2169. | 2110. | 6419. | 132. | 247. | 6666. | 100. |
| 6 | PEAK | 3.00 | | 220. | 205. | 1235. | 2168. | 2110. | 6417. | 132. | 247. | 6664. | 100. |
| | NON-PEAK | 6.00 | | 222. | 222. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | | 217. | 208. | 926. | 1645. | 1606. | 6503. | 132. | 329. | 6832. | 100. |
| | NON-PEAK | 8.00 | | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | | 220. | 205. | 1235. | 2167. | 2109. | 6414. | 132. | 247. | 6661. | 100. |
| 7 | PEAK | 3.00 | | 220. | 205. | 1235. | 2167. | 2109. | 6414. | 132. | 247. | 6661. | 100. |
| | NON-PEAK | 6.00 | | 222. | 222. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | | 217. | 208. | 926. | 1645. | 1606. | 6501. | 132. | 329. | 6830. | 100. |
| | NON-PEAK | 8.00 | | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | | 226. | 226. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |

| | | | | | | | | | | | |
|----|----------|------|------|-------|-------|-------|-------|-------|------|-------|-------|
| 8 | PEAK | 2.00 | 205. | 1235. | 2167. | 2108. | 6412. | 132. | 247. | 6659. | 100. |
| | NON-PEAK | 6.00 | 222. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1644. | 1605. | 6499. | 132. | 329. | 6828. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 9 | PEAK | 3.00 | 220. | 205. | 1235. | 2166. | 2107. | 6410. | 132. | 247. | 6657. |
| | NON-PEAK | 6.00 | 222. | 222. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | 217. | 208. | 926. | 1644. | 1605. | 6497. | 132. | 329. | 6826. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| 10 | PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| | NON-PEAK | 6.00 | 220. | 205. | 1235. | 2165. | 2107. | 6408. | 132. | 247. | 6655. |
| | PEAK | 4.00 | 222. | 222. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | NON-PEAK | 8.00 | 216. | 208. | 926. | 1643. | 1604. | 6494. | 132. | 329. | 6824. |
| | PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 6.00 | 226. | 226. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 11 | PEAK | 3.00 | 220. | 204. | 1235. | 2165. | 2106. | 6406. | 132. | 247. | 6653. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | 216. | 208. | 926. | 1643. | 1604. | 6492. | 132. | 329. | 6822. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 12 | PEAK | 3.00 | 220. | 204. | 1235. | 2164. | 2105. | 6404. | 132. | 247. | 6651. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | 216. | 208. | 926. | 1642. | 1603. | 6490. | 132. | 329. | 6819. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 13 | PEAK | 3.00 | 220. | 204. | 1235. | 2163. | 2105. | 6402. | 132. | 247. | 6648. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | 216. | 207. | 926. | 1642. | 1602. | 6488. | 132. | 329. | 6817. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 14 | PEAK | 3.00 | 220. | 204. | 1235. | 2162. | 2104. | 6399. | 132. | 247. | 6646. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | 216. | 207. | 926. | 1641. | 1602. | 6486. | 132. | 329. | 6815. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | 226. | 226. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 15 | PEAK | 3.00 | 220. | 204. | 1235. | 2162. | 2103. | 6397. | 132. | 247. | 6644. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| | PEAK | 4.00 | 216. | 207. | 926. | 1640. | 1601. | 6484. | 132. | 329. | 6813. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| | NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |

| | | | | | | | | | | | |
|----|----------|------|------|------|-------|-------|-------|-------|-------|------|-------|
| 16 | PEAK | 3.00 | 220. | 204. | 1235. | 2161. | 2102. | 6395. | 132. | 247. | 6642. |
| | NON-PEAK | 6.00 | 221. | 221. | 926. | 0. | 0. | 0. | 132. | 494. | 494. |
| | PEAK | 4.00 | 216. | 207. | 225. | 0. | 0. | 1601. | 132. | 329. | 6811. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 659. | 100. |
| | NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 247. | 247. |
| | NON-PEAK | 3.00 | 220. | 204. | 1235. | 2160. | 2102. | 6393. | 132. | 247. | 6640. |
| 17 | PEAK | 3.00 | 220. | 221. | 221. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 6.00 | 221. | 221. | 207. | 926. | 1600. | 6479. | 132. | 329. | 6809. |
| | PEAK | 4.00 | 216. | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 659. | 100. |
| | NON-PEAK | 3.00 | 220. | 204. | 1235. | 2160. | 2101. | 6391. | 132. | 247. | 6638. |
| 18 | PEAK | 3.00 | 220. | 221. | 221. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 6.00 | 221. | 216. | 207. | 926. | 1639. | 1600. | 6479. | 132. | 329. |
| | PEAK | 4.00 | 216. | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 659. | 100. |
| | NON-PEAK | 3.00 | 220. | 204. | 1235. | 2160. | 2101. | 6391. | 132. | 247. | 6638. |
| 19 | PEAK | 3.00 | 220. | 221. | 221. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 6.00 | 221. | 216. | 207. | 926. | 1639. | 1600. | 6477. | 132. | 329. |
| | PEAK | 4.00 | 216. | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 659. | 100. |
| | NON-PEAK | 3.00 | 220. | 204. | 1235. | 2160. | 2101. | 6389. | 132. | 247. | 6636. |
| 20 | PEAK | 3.00 | 219. | 204. | 1235. | 2158. | 2100. | 1599. | 1599. | 132. | 247. |
| | NON-PEAK | 6.00 | 221. | 221. | 224. | 0. | 0. | 0. | 0. | 0. | 100. |
| | PEAK | 8.00 | 224. | 224. | 225. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 0. | 100. |
| | PEAK | 4.00 | 216. | 204. | 1235. | 2158. | 2100. | 1599. | 6475. | 132. | 329. |
| | NON-PEAK | 8.00 | 224. | 224. | 225. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 0. | 100. |
| 21 | PEAK | 3.00 | 219. | 204. | 1235. | 2157. | 2100. | 1599. | 1599. | 132. | 659. |
| | NON-PEAK | 6.00 | 221. | 221. | 207. | 926. | 1638. | 1600. | 6473. | 132. | 329. |
| | PEAK | 4.00 | 216. | 224. | 224. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 8.00 | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 3.00 | 219. | 204. | 1235. | 2157. | 2099. | 6384. | 132. | 247. | 6633. |
| 22 | PEAK | 3.00 | 221. | 221. | 221. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 6.00 | 221. | 216. | 207. | 926. | 1637. | 1600. | 1598. | 132. | 329. |
| | PEAK | 8.00 | 224. | 224. | 224. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 3.00 | 219. | 204. | 1235. | 2157. | 2098. | 6382. | 132. | 247. | 6629. |
| 23 | PEAK | 3.00 | 219. | 221. | 221. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 6.00 | 221. | 216. | 207. | 926. | 1637. | 1598. | 6469. | 132. | 329. |
| | PEAK | 4.00 | 216. | 224. | 224. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 8.00 | 224. | 224. | 225. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 0. | 100. |
| | PEAK | 4.00 | 216. | 204. | 1235. | 2156. | 2097. | 6380. | 132. | 247. | 6627. |
| | NON-PEAK | 8.00 | 224. | 224. | 225. | 0. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 0. | 0. | 100. |

| TOTAL | | AVERAGE % 10 DAILY IRR. SUPPLY = | | | | | | | | | |
|----------|------|----------------------------------|------|-------|-------|-------|-------|------|------|-------|------|
| 24 PEAK | 3.00 | 219. | 204. | 2135. | 2155. | 2097. | 6378. | 132. | 247. | 6625. | 100. |
| NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| PEAK | 4.00 | 215. | 207. | 926. | 1636. | 1597. | 6464. | 132. | 329. | 6794. | 100. |
| NON-PEAK | 8.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 25 PEAK | 3.00 | 219. | 204. | 1235. | 2155. | 2096. | 6376. | 132. | 247. | 6623. | 100. |
| NON-PEAK | 6.00 | 220. | 220. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| PEAK | 4.00 | 215. | 207. | 926. | 1635. | 1596. | 6462. | 132. | 329. | 6792. | 100. |
| NON-PEAK | 8.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 26 PEAK | 3.00 | 219. | 203. | 1235. | 2154. | 2095. | 6374. | 132. | 247. | 6621. | 100. |
| NON-PEAK | 6.00 | 220. | 220. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| PEAK | 4.00 | 215. | 207. | 926. | 1635. | 1595. | 6460. | 132. | 329. | 6789. | 100. |
| NON-PEAK | 8.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 27 PEAK | 3.00 | 219. | 203. | 1235. | 2153. | 2095. | 6371. | 132. | 247. | 6618. | 100. |
| NON-PEAK | 6.00 | 220. | 220. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| PEAK | 4.00 | 215. | 206. | 926. | 1634. | 1595. | 6458. | 132. | 329. | 6787. | 100. |
| NON-PEAK | 8.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 28 PEAK | 3.00 | 219. | 203. | 1235. | 2152. | 2094. | 6369. | 132. | 247. | 6616. | 100. |
| NON-PEAK | 6.00 | 220. | 220. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| PEAK | 4.00 | 215. | 206. | 926. | 1634. | 1594. | 6456. | 132. | 329. | 6785. | 100. |
| NON-PEAK | 8.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| NON-PEAK | 3.00 | 225. | 225. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 29 PEAK | 3.00 | 219. | 203. | 1235. | 2152. | 2093. | 6367. | 132. | 247. | 6614. | 100. |
| NON-PEAK | 6.00 | 220. | 220. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| PEAK | 4.00 | 215. | 206. | 926. | 1633. | 1594. | 6454. | 132. | 329. | 6783. | 100. |
| NON-PEAK | 8.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| NON-PEAK | 3.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |
| 30 PEAK | 3.00 | 219. | 203. | 1235. | 2151. | 2092. | 6365. | 132. | 247. | 6612. | 100. |
| NON-PEAK | 6.00 | 220. | 220. | 0. | 0. | 0. | 0. | 132. | 494. | 494. | 100. |
| PEAK | 4.00 | 215. | 206. | 926. | 1632. | 1593. | 6452. | 132. | 329. | 6781. | 100. |
| NON-PEAK | 8.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 659. | 659. | 100. |
| NON-PEAK | 3.00 | 224. | 224. | 0. | 0. | 0. | 0. | 132. | 247. | 247. | 100. |

MONTH OF : DECEMBER YEAR : 1963 ENERGY GENERATION IN U/S, D/S POWER HOUSE AND & MEETING IRR.DEMAND

| DATE | PERIOD | DURATION (HR) | GROSSH (M) | NETTH (M) | Q (M3/S) | STARTP (MW) | ENDP (MW) | AV. ENERGY (MWh) | QD (M3/S) | ENERGY TOT. (MWh) | IRR. (%) |
|------|----------|------------------|---------------|--------------|-------------|----------------|--------------|---------------------|--------------|----------------------|-------------|
| 1 | PEAK | 3.00 | 219. | 203. | 1235. | 2150. | 2094. | 6366. | 174. | 326. | 6692. |
| | NON-PEAK | 6.00 | 221. | 221. | 0. | 0. | 0. | 0. | 174. | 653. | 653. |
| | PEAK | 4.00 | 216.. | 207. | 926. | 1637. | 1598. | 6470. | 174. | 435. | 6905. |
| | NON-PEAK | 8.00 | 223.. | 223. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.00 | 224.. | 224. | 0. | 0. | 0. | 0. | 174. | 326. | 326. |
| 2 | PEAK | 3.00 | 219. | 203. | 1235. | 2148. | 2092. | 6359. | 174. | 326. | 6686. |
| | NON-PEAK | 6.00 | 220.. | 220. | 0. | 0. | 0. | 0. | 174. | 653. | 653. |
| | PEAK | 4.00 | 215.. | 207. | 926. | 1635. | 1597. | 6463. | 174. | 435. | 6898. |
| | NON-PEAK | 8.00 | 223.. | 223. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.00 | 224.. | 224. | 0. | 0. | 0. | 0. | 174. | 326. | 326. |
| 3 | PEAK | 3.00 | 218.. | 203.. | 1235.. | 2146.. | 2089.. | 6353.. | 174.. | 326.. | 6679.. |
| | NON-PEAK | 6.00 | 220.. | 220.. | 0.. | 0.. | 0.. | 0.. | 174.. | 653.. | 653.. |
| | PEAK | 4.00 | 215.. | 206.. | 926.. | 1633.. | 1595.. | 6456.. | 174.. | 435.. | 6891.. |
| | NON-PEAK | 8.00 | 223.. | 223.. | 0.. | 0.. | 0.. | 0.. | 174.. | 870.. | 100.. |
| | NON-PEAK | 3.00 | 224.. | 224.. | 0.. | 0.. | 0.. | 0.. | 174.. | 326.. | 326.. |
| 4 | PEAK | 3.00 | 218.. | 203.. | 1235.. | 2144.. | 2087.. | 6346.. | 174.. | 326.. | 6672.. |
| | NON-PEAK | 6.00 | 220.. | 220.. | 0.. | 0.. | 0.. | 0.. | 174.. | 870.. | 100.. |
| | PEAK | 4.00 | 215.. | 206.. | 926.. | 1632.. | 1593.. | 6450.. | 174.. | 435.. | 6885.. |
| | NON-PEAK | 8.00 | 223.. | 223.. | 0.. | 0.. | 0.. | 0.. | 174.. | 870.. | 100.. |
| | NON-PEAK | 3.00 | 224.. | 224.. | 0.. | 0.. | 0.. | 0.. | 174.. | 326.. | 326.. |
| 5 | PEAK | 3.00 | 218.. | 202.. | 1235.. | 2141.. | 2085.. | 6339.. | 174.. | 326.. | 6665.. |
| | NON-PEAK | 6.00 | 220.. | 220.. | 0.. | 0.. | 0.. | 0.. | 174.. | 653.. | 653.. |
| | PEAK | 4.00 | 215.. | 206.. | 926.. | 1630.. | 1592.. | 6443.. | 174.. | 435.. | 6878.. |
| | NON-PEAK | 8.00 | 222.. | 222.. | 0.. | 0.. | 0.. | 0.. | 174.. | 870.. | 100.. |
| | NON-PEAK | 3.00 | 223.. | 223.. | 0.. | 0.. | 0.. | 0.. | 174.. | 326.. | 326.. |
| 6 | PEAK | 3.00 | 218.. | 202.. | 1235.. | 2139.. | 2083.. | 6333.. | 174.. | 326.. | 6659.. |
| | NON-PEAK | 6.00 | 220.. | 220.. | 0.. | 0.. | 0.. | 0.. | 174.. | 653.. | 653.. |
| | PEAK | 4.00 | 215.. | 206.. | 926.. | 1628.. | 1590.. | 6436.. | 174.. | 435.. | 6871.. |
| | NON-PEAK | 8.00 | 222.. | 222.. | 0.. | 0.. | 0.. | 0.. | 174.. | 870.. | 100.. |
| | NON-PEAK | 3.00 | 223.. | 223.. | 0.. | 0.. | 0.. | 0.. | 174.. | 326.. | 326.. |
| 7 | PEAK | 3.00 | 218.. | 202.. | 1235.. | 2137.. | 2080.. | 6326.. | 174.. | 326.. | 6652.. |
| | NON-PEAK | 6.00 | 219.. | 219.. | 0.. | 0.. | 0.. | 0.. | 174.. | 653.. | 653.. |
| | PEAK | 4.00 | 214.. | 206.. | 926.. | 1626.. | 1588.. | 6430.. | 174.. | 435.. | 6865.. |
| | NON-PEAK | 8.00 | 222.. | 222.. | 0.. | 0.. | 0.. | 0.. | 174.. | 870.. | 100.. |
| | NON-PEAK | 3.00 | 223.. | 223.. | 0.. | 0.. | 0.. | 0.. | 174.. | 326.. | 326.. |

| | | | | | | | | | | | |
|----|----------|------|------|------|-------|---------|-------|-------|------|-------|-------|
| 8 | PEAK | 3.00 | 217. | 202. | 1235. | 2135. | 2078. | 6319. | 174. | 326. | 6645. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 174. | 653. | 653. |
| 9 | PEAK | 4.00 | 214. | 205. | 926. | 1625. | 1587. | 6423. | 174. | 435. | 6858. |
| | NON-PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 174. | 970. | 100. |
| 10 | PEAK | 3.00 | 223. | 223. | 0. | 0. | 0. | 0. | 174. | 326. | 326. |
| | NON-PEAK | 3.00 | 217. | 202. | 1235. | 2132. | 2076. | 6312. | 174. | 326. | 6639. |
| 11 | PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 174. | 653. | 653. |
| | NON-PEAK | 4.00 | 214. | 205. | 926. | 1623. | 1585. | 6416. | 174. | 435. | 6851. |
| 12 | PEAK | 8.00 | 222. | 222. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| | NON-PEAK | 3.00 | 222. | 222. | 0. | 0. | 0. | 0. | 174. | 326. | 100. |
| 13 | PEAK | 3.00 | 217. | 201. | 1235. | 2130. | 2074. | 6306. | 174. | 326. | 6632. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| 14 | PEAK | 4.00 | 214. | 205. | 926. | 1621. | 1583. | 6410. | 174. | 435. | 6845. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| 15 | PEAK | 3.00 | 222. | 222. | 0. | 0. | 0. | 0. | 174. | 326. | 100. |
| | NON-PEAK | 6.00 | 217. | 201. | 1235. | 2128. | 2071. | 6299. | 174. | 653. | 6625. |
| 16 | PEAK | 4.00 | 218. | 218. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 174. | 326. | 100. |
| 17 | PEAK | 3.00 | 222. | 222. | 0. | 0. | 0. | 0. | 174. | 653. | 6619. |
| | NON-PEAK | 6.00 | 217. | 201. | 1235. | 2126. | 2069. | 6292. | 174. | 435. | 6838. |
| 18 | PEAK | 4.00 | 218. | 218. | 0. | 0. | 0. | 0. | 174. | 653. | 100. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| 19 | PEAK | 3.00 | 222. | 222. | 0. | 0. | 0. | 0. | 174. | 326. | 326. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 174. | 6612. | 100. |
| 20 | PEAK | 4.00 | 213. | 205. | 926. | 1618. | 1580. | 6396. | 174. | 435. | 6831. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| 21 | PEAK | 3.00 | 222. | 222. | 0. | 0. | 0. | 0. | 174. | 326. | 326. |
| | NON-PEAK | 6.00 | 216. | 201. | 1235. | - 2124. | 2067. | 6286. | 174. | 326. | 100. |
| 22 | PEAK | 4.00 | 213. | 205. | 926. | 1618. | 1580. | 6396. | 174. | 435. | 6831. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| 23 | PEAK | 3.00 | 216. | 201. | 1235. | - 2124. | 2067. | 6286. | 174. | 326. | 6612. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 174. | 435. | 6831. |
| 24 | PEAK | 4.00 | 213. | 204. | 926. | 1616. | 1578. | 6390. | 174. | 435. | 6825. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| 25 | PEAK | 3.00 | 222. | 222. | 0. | 0. | 0. | 0. | 174. | 326. | 326. |
| | NON-PEAK | 6.00 | 216. | 200. | 1235. | 2121. | 2065. | 6279. | 174. | 326. | 6605. |
| 26 | PEAK | 4.00 | 213. | 204. | 926. | 1615. | 1577. | 6383. | 174. | 435. | 6818. |
| | NON-PEAK | 8.00 | 221. | 221. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| 27 | PEAK | 3.00 | 221. | 221. | 0. | 0. | 0. | 0. | 174. | 326. | 326. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 174. | 653. | 653. |
| 28 | PEAK | 4.00 | 213. | 204. | 926. | 1613. | 1575. | 6376. | 174. | 435. | 6811. |
| | NON-PEAK | 8.00 | 220. | 220. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |
| 29 | PEAK | 3.00 | 221. | 221. | 0. | 0. | 0. | 0. | 174. | 326. | 326. |
| | NON-PEAK | 6.00 | 218. | 218. | 0. | 0. | 0. | 0. | 174. | 6599. | 100. |
| 30 | PEAK | 4.00 | 213. | 204. | 926. | 1613. | 1575. | 6376. | 174. | 435. | 6811. |
| | NON-PEAK | 8.00 | 220. | 220. | 0. | 0. | 0. | 0. | 174. | 870. | 100. |

| | | | | | | | | | |
|----|----------|------|------|------|-------|-------|-------|-------|------|
| 16 | PEAK | 3.00 | 216. | 200. | 1235. | 2117. | 2060. | 6266. | 326. |
| | NON-PEAK | 6.00 | 217. | 217. | 0. | 0. | 0. | 174. | 100. |
| | PEAK | 4.00 | 212. | 204. | 926. | 1611. | 1573. | 6370. | 100. |
| | NON-PEAK | 8.00 | 220. | 220. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 221. | 221. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 215. | 200. | 1235. | 2115. | 2058. | 6259. | 100. |
| 17 | PEAK | 3.00 | 215. | 217. | 0. | 0. | 0. | 0. | 100. |
| | NON-PEAK | 6.00 | 217. | 217. | 0. | 0. | 0. | 174. | 100. |
| | PEAK | 4.00 | 212. | 203. | 926. | 1610. | 1572. | 6363. | 100. |
| | NON-PEAK | 8.00 | 220. | 220. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 221. | 221. | 0. | 0. | 0. | 174. | 100. |
| 18 | PEAK | 3.00 | 215. | 200. | 1235. | 2112. | 2056. | 6252. | 100. |
| | NON-PEAK | 6.00 | 217. | 217. | 0. | 0. | 0. | 174. | 100. |
| | PEAK | 4.00 | 212. | 203. | 926. | 1608. | 1570. | 6356. | 100. |
| | NON-PEAK | 8.00 | 220. | 220. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 221. | 221. | 0. | 0. | 0. | 174. | 100. |
| 19 | PEAK | 3.00 | 215. | 199. | 1235. | 2110. | 2054. | 6246. | 100. |
| | NON-PEAK | 6.00 | 217. | 217. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 4.00 | 212. | 203. | 926. | 1606. | 1568. | 6349. | 100. |
| | PEAK | 8.00 | 219. | 219. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 220. | 220. | 0. | 0. | 0. | 174. | 100. |
| 20 | PEAK | 3.00 | 215. | 199. | 1235. | 2108. | 2051. | 6239. | 100. |
| | NON-PEAK | 6.00 | 217. | 217. | 0. | 0. | 0. | 174. | 100. |
| | PEAK | 4.00 | 212. | 203. | 926. | 1605. | 1567. | 6343. | 100. |
| | NON-PEAK | 8.00 | 219. | 219. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 220. | 220. | 0. | 0. | 0. | 174. | 100. |
| 21 | PEAK | 3.00 | 215. | 199. | 1235. | 2106. | 2049. | 6232. | 100. |
| | NON-PEAK | 6.00 | 216. | 216. | 0. | 0. | 0. | 174. | 100. |
| | PEAK | 4.00 | 211. | 203. | 926. | 1603. | 1565. | 6336. | 100. |
| | NON-PEAK | 8.00 | 219. | 219. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 220. | 220. | 0. | 0. | 0. | 174. | 100. |
| 22 | PEAK | 3.00 | 214. | 199. | 1235. | 2103. | 2047. | 6226. | 100. |
| | NON-PEAK | 6.00 | 216. | 216. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 4.00 | 211. | 203. | 926. | 1601. | 1563. | 6329. | 100. |
| | PEAK | 8.00 | 219. | 219. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 220. | 220. | 0. | 0. | 0. | 174. | 100. |
| 23 | PEAK | 3.00 | 214. | 199. | 1235. | 2101. | 2045. | 6219. | 100. |
| | NON-PEAK | 6.00 | 216. | 216. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 4.00 | 211. | 202. | 926. | 1601. | 1563. | 6329. | 100. |
| | PEAK | 8.00 | 219. | 219. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 220. | 220. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 6.00 | 214. | 214. | 0. | 0. | 0. | 174. | 100. |
| | PEAK | 4.00 | 211. | 202. | 926. | 1601. | 1563. | 6329. | 100. |
| | NON-PEAK | 8.00 | 219. | 219. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 220. | 220. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 6.00 | 219. | 219. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 4.00 | 211. | 202. | 926. | 1600. | 1562. | 6323. | 100. |
| | PEAK | 8.00 | 219. | 219. | 0. | 0. | 0. | 174. | 100. |
| | NON-PEAK | 3.00 | 219. | 219. | 0. | 0. | 0. | 174. | 100. |

| TOTAL | | AVERAGE % | 10 DAILY IRR. SUPPLY = |
|-----------|------|-----------|------------------------|
| 24 PEAK | 3.00 | 214. | 198. |
| NON-PEAK | 6.00 | 216. | 2099. |
| PEAK | 4.00 | 216. | 0. |
| NON-PEAK | 8.00 | 216. | 0. |
| NON-PEAK | 8.00 | 218. | 0. |
| NON-PEAK | 3.00 | 219. | 0. |
| 25 PEAK | 3.00 | 214. | 198. |
| NON-PEAK | 6.00 | 215. | 1235. |
| PEAK | 4.00 | 211. | 202. |
| NON-PEAK | 8.00 | 218. | 218. |
| NON-PEAK | 3.00 | 219. | 219. |
| 26 PEAK | 3.00 | 214. | 198. |
| NON-PEAK | 6.00 | 215. | 1235. |
| PEAK | 4.00 | 211. | 202. |
| NON-PEAK | 8.00 | 218. | 218. |
| NON-PEAK | 3.00 | 219. | 219. |
| 27 PEAK | 3.00 | 214. | 198. |
| NON-PEAK | 6.00 | 215. | 1235. |
| PEAK | 4.00 | 210. | 202. |
| NON-PEAK | 8.00 | 218. | 218. |
| NON-PEAK | 3.00 | 219. | 219. |
| 28 PEAK | 3.00 | 213. | 198. |
| NON-PEAK | 6.00 | 215. | 215. |
| PEAK | 4.00 | 210. | 201. |
| NON-PEAK | 8.00 | 218. | 218. |
| NON-PEAK | 3.00 | 219. | 219. |
| 29 PEAK | 3.00 | 213. | 197. |
| NON-PEAK | 6.00 | 215. | 215. |
| PEAK | 4.00 | 210. | 201. |
| NON-PEAK | 8.00 | 217. | 217. |
| NON-PEAK | 3.00 | 218. | 218. |
| 29 PEAK | 3.00 | 213. | 197. |
| NON-PEAK | 6.00 | 215. | 215. |
| PEAK | 4.00 | 210. | 201. |
| NON-PEAK | 8.00 | 217. | 217. |
| NON-PEAK | 3.00 | 218. | 218. |
| 30 PEAK | 3.00 | 213. | 197. |
| NON-PEAK | 6.00 | 214. | 214. |
| PEAK | 4.00 | 209. | 201. |
| NON-PEAK | 8.00 | 217. | 217. |
| NON-PEAK | 3.00 | 213. | 197. |
| 31 PEAK | 3.00 | 212. | 197. |
| NON-PEAK | 6.00 | 214. | 214. |
| PEAK | 4.00 | 209. | 200. |
| NON-PEAK | 8.00 | 217. | 217. |
| NON-PEAK | 3.00 | 218. | 218. |
| TOTAL | | 391693. | 472612. |
| AVERAGE % | | = | 100.00 |
| TOTAL | | = | 1343101 |