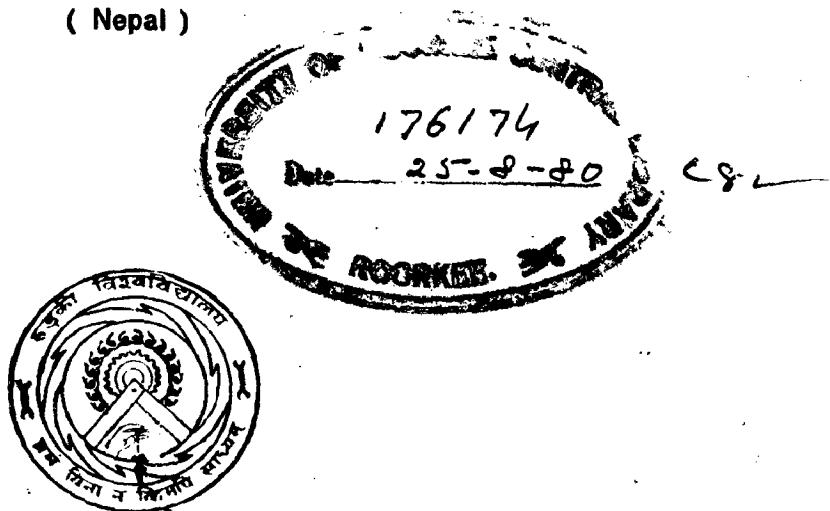


ANALYSIS FOR SNOWMELT RUNOFF DURING PREMONSOON MONTHS IN BEAS BASIN USING SATELLITE IMAGERIES

A DISSERTATION
submitted in partial fulfilment of
the requirements for the award of the degree
of
MASTER IN HYDROLOGY

By
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**UNESCO SPONSORED
INTERNATIONAL HYDROLOGY COURSE
UNIVERSITY OF ROORKEE
ROORKEE (INDIA)**

April, 1980

STATEMENT

This is to certify that the classification entitled "ANALYSIS FOR GROUND WATER INfiltration PREDICTION COURSE IN DRAIN DAKES USING CATEGORICAL MODELS" being delivered by Mr. R. B. Shinde as partial fulfillment of the requirement for award of the degree of Master in Hydrology of the University of Hyderabad, is a record of the candidate's own work carried out by him under our supervision and guidance. The material included in this classification has not been submitted for the award of any other degree or diploma.

This is further to certify that Mr. R. B. Shinde has worked for a period of 6 months since his admission to M.Sc. Hatch 1970 in the preparation of this classification under our guidance at this university.

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ACKNOWLEDGEMENTS

It is a great pleasure for me to express my deep sense of gratitude to Dr. S.M. Seth, Associate Professor, School of Hydrology, presently on deputation to the National Institute of Hydrology, Roorkee and Shri K.P. Sharma, Reader in Civil Engineering, ~~Survey~~ Survey and Photogrammetry Section for their keen interest, valuable guidance and encouragement throughout the course of this study.

I am also highly grateful to Dr. Satish Chandra, Professor, Dr. B.S. Mathur, Coordinator, and all other faculty staff members of the International Hydrology course, University of Roorkee, for their keen interest and encouragement given to me throughout the period of my stay in Roorkee.

I am also thankful to Mr. D.P. Goyal, Executive Engineer, H.P.S.E.B. for his cooperation in collection of various data required for this study.

Thanks are also due to the Government of Nepal for deputing me to undergo this training at the University of Roorkee. I am also highly thankful to UNESCO and the Government of India for providing me all the necessary facilities and financial assistance for undergoing training at the University of Roorkee, Roorkee.

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APPENDIX

The Appendix is divided for water sampled with the construction of multipurpose reservoirs to control and regulate the water availability, regulation of water availability and flow of water. It is required to determine the suitable techniques from the reservoirs for storage, regulation, irrigation, navigation, power generation, pollution control, flood control, etc.

Information available on the status of river characteristics during the different months is necessary for making appropriate prediction of ageing runoff. An integrated index of runoff during the different seasons is the total volume of the river cover, which is followed by the different sampling techniques. The conventional methods for estimating river data from remote areas are not only time consuming and expensive but by the time the results could be compiled, they would certainly be out-dated. Thus the application of遥感 technology to gauging popularity in the hydrological studies.

The status of Beas River is being utilised for operation of different water resources projects among which the PWD - BISI & LASH Project is the most important. The status of supply during the pre-monsoon period for the Beas River comes from the reservoirs. The general utility of the river reservoirs over the catchment during the winter months is to regulate the flow of water for the perennial character of the Beas River.

Photo-hydrological investigation of the Jees catchment, upstream of Sardai, and the estimation of the snowmelt runoff during the pre-monsoon period have been started. An attempt has been made to study the relationship between the snow cover, regulated with the help of the satellite images, and the cumulative discharges of the months of March, April and May of the years 1973, 1975, 1976 and 1977. An exponential trend has been observed in plotting. The snow covered areas in Boxes 5 and Box 7 of the DEMS images on the same day have been compared. A linear trend has been observed in plotting. An attempt has been made to identify and estimate the vegetal cover and land use features using remote identification techniques.

Due to the availability of the limited meteorological and hydrological data the study for the estimation of snowmelt runoff has been confined to the sub-basin upstream of Sardai. The sub-basin has been divided into permanent and temporary snow covered areas, provided that it is completely covered by snow. The Beaman-Ray method and the melt due to rainfall on snow have been used to estimate the snowmelt runoff. The calculated runoff across all the gauged stations give a reasonable agreement. With several yields the Jees - day factor of $0.0003 \text{ cm}^0.8^1 \text{ d}^{-1}$ for March and April and $0.0032 \text{ cm}^0.8^1 \text{ d}^{-1}$ for May have been obtained for the years 1977, 1978 and 1979. The routing of snowmelt after accounting for losses as well as the excess rainfall runoff from the permanent & temporary snow covered area has been done with the recession coefficient $\gamma = 0.80$ and the excess rain from the non-snow covered area has been ~~assumed~~ directly contributing for runoff on that same day as the time of concen-

Lastly, the runoff coefficient of 0.503 for the rainfall on the non covered area and 0.270 for rainfall on the non non covered area have been calculated. Since the time of concentration for the catchment is less than a day, the runoff due to rainfall on the non non covered area is incorporated on the same day on the calculated hydrograph obtained from the rainfall and the runoff from the area falling on the non covered area. There is an improvement in the results.

Zero hydroclimatological data, regular rainfall measurements, and area survey for determining the Precipitation-Runoff Relation, the water equivalent, and depth etc. are essential for a better estimation of surface runoff.

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CHAPTER 8

HYDROLOGY

8.1 General:

Water is one of the most essential requirements for the sustenance of all living beings. The total quantity of water available in the earth is not very, but it is widely distributed throughout a continuous hydrological cycle of conversion from atmosphere to land by precipitation and removing the earth again as precipitation. The hydrological cycle consists of four basic phases of activities. They are precipitation, evaporation and transpiration, runoff, and recharge or ground water.

Runoff is a hydrological part of the hydrological cycle. Accurate estimation of the volume of water stored in the snow cover zone and the volume of melt water can contribute to predict the flow during the snow period. For a particular area, yield information on snow, cover depth and water equivalent is a pre-requisite to calculate the energy transfer to the snowpack. The hydrologists find many hydrological problems especially in the mountainous areas, since very limited information is available relating to the hydrogeological and physical features affecting the snowmelt in addition. In contrast to rainfall, snowmelt is not generally measured quantitatively but data is collected mainly from meteorological gauges and information about the terrain, vegetative cover etc. A hydrological index of runoff during the snowmelt season is the total water of the snow cover.

Accordingly finding has been made on off-shore and near-shore morphology to measure area cover in which banks are relatively inaccessible and hazardous.

The Dosa catchment upstream of Lakkadlu Dosa collected for the study, shows it has a moderate slope and above 50 per cent of the catchment is covered by sand before the falling profile. Shows the sediment source of Dosa river during the Rabi period.

The present study can be broken down into two categories

- a) The analysis of lateral spreading for the Dosa catchment
- and b) The estimation of coastal areas in the catchment of Lakkadlu during the pre-monsoon period.

The photomagnetic section covers the general estimate for calculating the different physiographic parameters of the catchment of the Dosa tributary upstream of Lakkadlu. Perhaps the most difficult of the area cover is the coastal strip which is hardly measurable particularly since the offshore like the submerged land and sand depth in the marine areas. The sand area coverage is measured here by using the bathymetric (Bath) measurement. The relationship between the area cover and the coastal strip coverage of the falling section has been studied. The area covered areas from the location in Block 9 and Block 7 taken on the same day have been verified also.

Due to the limited data a small sub-catchment upstream of Kandy has been selected for estimating the runoff runoff during the pre-monsoon period. This section deals with the estimation of runoff due to rainfall in Dara river originating from the Minigama. The hydrological condition of the Minigama catchment is very complex since they are partly dry covered at higher altitudes and saturated at the lower altitudes. The year in Dara catchment is divided into the convection season, the southwest monsoon, the northeast season and the transition season.

The objective of the runoff from catchment computation is to ^{to} estimate annual water yield and the ratio of runoff generation. Both of these objectives may require rainfall computation in partly dry covered catchment either for the evaluation of existing projects or for the use of design; future projects.

CHAPTER IX

SNOW AND ITS CONTRIBUTION TO STREAM FLOW

2.1 INTRODUCTION :

In many areas snow is the dominant source of stream flow. Goodall (1956) has indicated that about 90 per cent of the yearly water supply in the high elevations of the Colorado Rockies is derived from snowmelt. The generation of snowmelt and sequential stream flow from the snowpack that accumulates in winter, forms one of the most important phases of the hydrologic cycle in the northern region of India. In India and many other countries snowmelt runoff estimations are vitally important in

- a) forecasting seasonal water yields for a diversity of water supply purposes.
- b) implementing flood control programmes.
- c) regulating rivers and storage works.
- and d) selecting design floods for particular watersheds.

Therefore, any programme for the effective control, conservation, and optimum development of water resources in these northern regions must take into account the vital contribution of snowmelt to the spring season runoff, or its potential for storage and subsequent utilization.

Despite the importance of snow hydrology, it is only in the last decades that intensive research has led to the formation of theory which yields a partly satisfactory understanding of the complex hydrodynamic processes producing

snowmelt and subsequent stream flow. The new techniques are being widely used for predicting design estimates and seasonal yield. However, for short range forecasting of peak flow rates, the agreement between prediction and actual observations has been found to be uncertain, and leaves room for much improvement.

2.2 ROLE OF SNOW AND ICE IN THE GLOBAL WATER BALANCE :

The quantitative assessment of the world water balance is still in the process of revision and refinement. Even so, reasonable estimates can be attempted in order to illustrate the relative importance of the different components.

The total volume of water present in the whole hydrosphere amounts , according to Ilevitch (1970), to approximately $1.45 \times 10^9 \text{ km}^3$. Ice and snow represent about $30 \times 10^6 \text{ km}^3$ of water (Hoinkes 1967). Other estimates put these values rather lower but, at any rate, ice and snow constitutes 2 per cent of the water in all its forms. Of course, the seas and oceans contain about 97.4 per cent of the world water, but if this saline water is discarded ice and snow become the major component (Volker 1970).

2.3 PHYSICAL PROPERTIES OF SNOW AND ICE :

Snow is defined as falling or deposited ice particles formed mainly by sublimation (UNESCO / IASH / WHO 1970). It can also be described as the solid form of water which

ගොන මල්ල පොකී, සිදු වෙමි විට ඇඟිල වැව්
තා සෙනෙනු (Cannula 2930), වැස්පි සෑ පොකී, පොෂ
ඩො පරිවෘතියේ 100 පැන (Batch 2932). මෙහි නිසාම
තෙව පැවතිල්ල වැට්ටිනු ලැබේ, මෙහි තෙව එහිට තෙ
වැට්ටිනු. වැව් සිදු වෙමි සෙනෙනු එළඹු වැව් එක්සිව
තැවතුමු සූ පොෂිත්, මෙහි පැවතිල්ල වැව්
වැට්ටිනු නැතුවෙන් පෙන්වී, මෙහි පැවතිල්ල වැව්
වැට්ටිනු නැතුවෙන් එහිට තෙව එහිට තෙව වැව් සැම්මුව සී
වැව් සිදු වෙමි පොකී, මෙහි පැවතිල්ල වැව්

The density of the earth before it is very
frequently around 6.3. The density of 6.3 is very often
described as it is old rock. There can naturally exist a
density of which due to pressure may go down, either by
roasting of iron casting or by the process of cutting down the
burnt. In case of iron the density is then considered to
have up to the transition from "iron to steel". The density
is 4.90 when the volume changes in such (a) per cent
by 1%. The density of the volume change of 10% to 20%
will be referred to density as follows:

$$\rho = \frac{\rho_1 - \rho}{\rho_1} = \lambda = \frac{\rho}{\rho \cdot \frac{1}{10}} = 10.000$$

ρ is the density in kg m^{-3}

ρ_1 is the density in 10 kg m^{-3}

λ is the density of 100 in 10 kg m^{-3} .

respond to world wide climatic change. During the flood period, the climatic conditions are from 600 to 2,200 mm less than at present.

2.9 SEDIMENTATION :

A great variety of methods and instruments has been developed for river surveys in order to meet different conditions and requirements. The most likely of primary importance for hydrological purposes are

- 1) River Survey
- 2) Sediment and water sampling
- and 3) River surveys.

All measurements are related to river morphology and sediment transport directly or the characteristics of the river and in particular to the exposure to wind and sun and to the frequency and velocity of the wind. Unless there is no deposition or erosion is exceeding a certain amount, a site for measuring must be found to

- 1) Dismounted
- 2) Free to current and inclination
- 3) Protected against strong wind and sunlight and
- 4) Where there are objects which could cause unnecessary error deposit.

These conditions partly connected with others, and in most cases a compromise has to be found.

(3) శాస్త్ర వ్యవస్థ

If the time average over days over a large area with locally variable snow accumulations is to be obtained, a great many observations must be taken. A network of observations gives a so called snow survey by comparison.

Show me three kinds of exaggeration:

- a) A number of cases and victims each of which is representative for certain criminal conditions. The cases given below are occurring generally and collected in Governmental police.
 - b) A large number of similar occurring events and indicate clearly the path which can be easily followed.
 - c) The single occurring events are supposed to be
in a definite relationship.

(2) ಈಗಾಗಿಯ ಏ ಪರಿಣಾಮವಿದೆ :

Mean Density is the ratio of the unit volume given in g cm^{-3} or kg m^{-3} . It can also be considered as a dimensionless ratio called specific gravity, which is the mean density relative to density of water at 4°C .

Water equivalent of snow cover is thus the product of snow depth and density. It is the total weight of water layer which could be obtained by melting the snow cover over

a given area (Nilwala / 2003 / no 2970).

Geographical distribution patterns are based on varying soil types which are taken by trees of different species and silviculture. The variability of tree growth is generally greater than that of tree density.

Considerable variations of densities in different species may be encountered, especially in solid silviculture. The average density of a given cover may also vary from one area to another due to different slopes and exposures. Fully stocked of each species, in terms of volume equivalent, can be measured by stem counts. In 2003, most solid silviculture plots had about 10000. Density of stems to be planted see table below. Comparative figures (U.S. Army Corps of Engineers, 1970) also show that for a standard basal area of 20 m²/ha there was a total volume of 20 m³ per ha for shrubs and 35 m³ per ha for trees. However such areas cannot be easily established due to a restriction in the following out of given reason in the forest. Other values are obtained by comparing the depth of fully stocked on a given basal area and calculating the volume equivalent. The use of different species to increase the variability of stock could be an interesting possibility.

(S) The basal area of trees:

An basal area is especially important in relation with a standard tree cover, since it can change from a 200 per cent coverage of a basin to zero in a relatively short time.

It is evident that the total production from a unit area may cover directly or indirectly all the surface area and yet, the possible occurrences of natural changes of the same cover have been limited, while recently, no agricultural areas. In the basin the same cover is gradually decreasing from the start of the catchment areas. At the present preoccupation the mainline records just from the lower catchments till it reaches the permanent inundation(3). Loos (1937) found the same cover disappeared owing to the cultivation.

$$A = \frac{200}{3 = 0.05}$$

- Ans A Is the percentage of area without cover
 b Is the area measured from an arbitrary origin
 c Is a constant
 d Is the base of natural logarithms which can be approximated as

$$0 = \frac{200}{3 = 0.05}$$

- Ans 3 Is the percentage of same cover
 0₂₀ Is the value of which $3 = 20$.

2.6 PASTURE MANAGEMENT AS A PRACTICE :

This management of pasture at a particular location in a catchment is essentially a thermodynamic process, the extent of which depends largely dependent on the net heat exchange

between the snowpack and its environment. The travel of melt water to another point in the pack and its time distribution at that point depend on physiographic (gradient, depth, etc.) and hydrodynamic (porosity) structure, storage etc.) properties of the snowpack[23].

The various sources and processes influencing heat transfer to or from a snowpack shown in figure (2.1) are listed below:

1. Absorbed shortwave (solar) radiation, R_s .
2. Net longwave (terrestrial and atmospheric) radiation , R_b .
3. Condensation (or vaporization) from the air, R_c .
4. Convective heat transfer (by wind) R_h .
5. Heat content of rain water, H_r .
6. Conduction of heat from ground, H_g .

The melt water produced by the net transfer of heat from all sources to the snowpack may be obtained from

$$M = \frac{\sum H}{203 B} \quad (1)$$

where M = water equivalent of snowmelt (in.)

H = algebraic sum of all heat contributions
(cal./cm²) , and

B = thermal quality of the snowpack, defined as the ratio of heat required to melt a unit weight of snow to that of ice at 0°C [averages from 0.95 to 0.97, for 3 to 5 per cent liquid water].

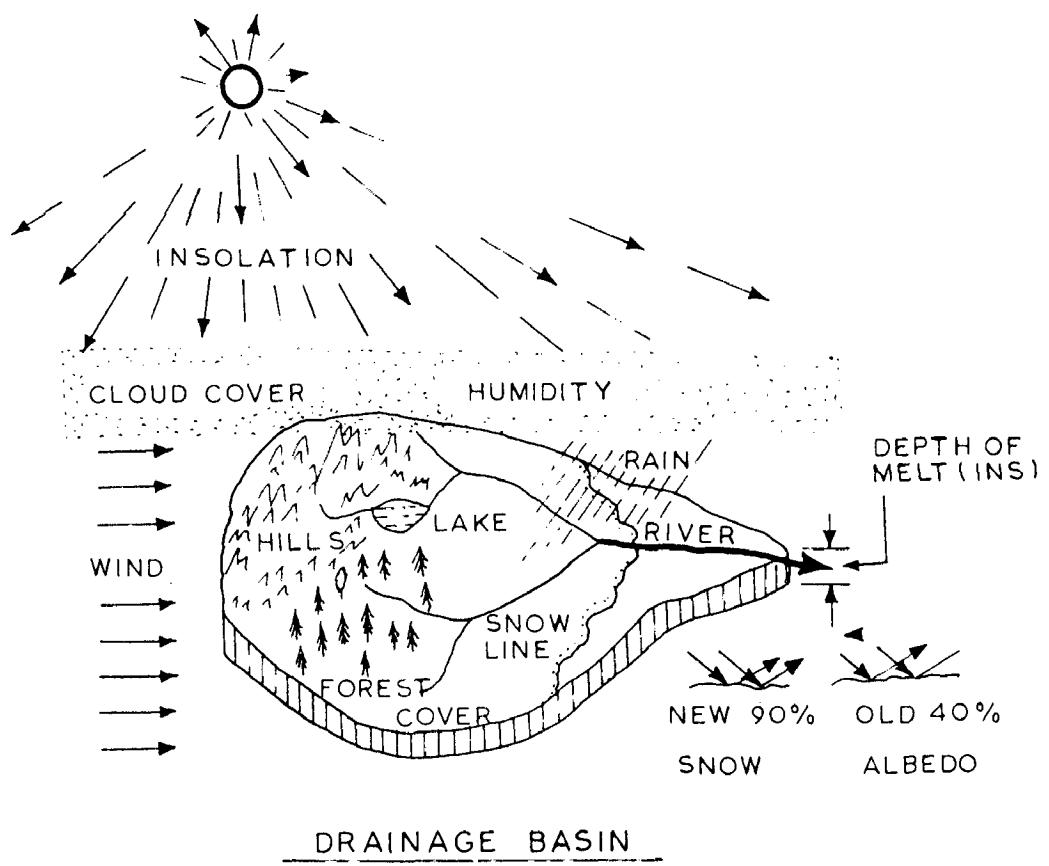
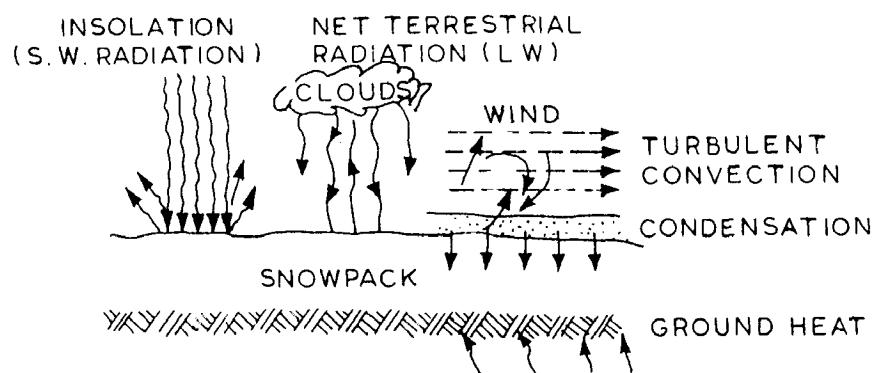


FIG. 2.1 SOURCES OF HEAT THAT GENERATE SNOWMELT

The constant k_1 in the heat transfer equation $\frac{d\theta}{dt} = k_1 \cdot \frac{\partial \theta}{\partial x}$, is proportional to $\frac{1}{\rho C_p}$ and $k_1 = \frac{1}{\rho C_p} \cdot \frac{h}{k} \cdot A \cdot \Delta T$ at 0°C , if ΔT is the temperature difference ($\text{deg}/\text{m}^2/\text{min}$).

2. Alternative methods (other) collection :

Alternative collection methods are usually more expensive than the conventional methods mentioned above as follows; the methods developed by the Bureau's Bureau of Measurement of Solid Materials. The cost analysis of how developed by the Bureau's Bureau of Measurement of Solid Materials depends on facilities, instrumentation and design, location, time of day, alternative collection (multiple, two, three), sensor cover, and reliability of the data (blocks).

The reliability of insulation or insulation value will depend on normally required in Amylum ($\text{deg}/\text{m}^2/\text{min}$) due to the ΔT of 10°C (mm, hr, or deg). The cost, design and insulation requirements of hot insulation will be determined by collection type or methodology. These insulations can be designed to give the insulation collection accuracy in $2\%/\text{hr}$ or $1\%/\text{deg}$.

In these insulation types and other types collection methods available are not available, either of the two approaches may be employed. The hot insulation is collected by allowing the differentiation of density of the insulation (block cover), sensor cover, slope, instrumentation, and data processing, the nature of the insulation, the ΔT , the cover and the surface area of the insulation, and good quality insulation. The good quality insulation collection will be used to calculate the heat transfer coefficient for each case, and

which occurs to isolated as well as continuous basis. The abode is generally taken as 60 per cent for fixed assets and reduced to depreciation exponentially to about 40 per cent depending on the nature of assets. The net component produced by depreciation will be 0.40 per cent of gross fixed assets.

$$I_{D0} = \frac{(2-a) I_{D1}}{200 D} = 0.0050 I_{D1} (2-a) \text{ Rs/LT}$$

where 'a' is the abode taken as a constant fraction, I_{D1} is the effective color pollution in kg/day and D is assumed to be 0.97 for a building complex.

A similar such empirical formulae can be a correlation between effective pollution and machine hours. The number of effective daily hours of machine in the plant usually varies from 8000 hours to complete the work. A recent study in IIT Roorkee by Rayguru (1990) has concluded that approach to be only slightly more conservative than using measured net incoloration is 27/kg.

2. Net Incoloration (Responsible and Nonresponsible) Pollution:

This is considered to be a most important factor which may affect the pollution to environment and responsible pollution caused by man can be controlled by industry's own. However, contribution of net incoloration pollution is relatively less than that of color pollution due to the circumstances under colour or already taken care of the same under colour cover; those activities are classified and those who are left in particular case by industry.

Based on the USSR Manual (1969) we can do the following calculations using the given information:

Water vapor flux density :

$$H_{w1} = 0.0232 (T_0 - 22) = 0.04 \quad (2)$$

where H_{w1} = the daily amount in Arches

and T_0 = the day temperature over land surface.

Water vapor density :

$$H_{w2} = 0.029 (T_0 - 22)$$

Computing cloud cover :

$$H_{w3} = 0.029 (T_0 - 22)$$

where T_0 is the temperature of cloud base in °C.

As the required temperatures are available, the informations can be used directly in the equations & other data available are also used in the same manner as discussed earlier. The results obtained are as follows:

3. Computation of Convection Rate :

The next step is to find the convection rate which is a mass transfer, the rate of condensation of water in the air is determined by the following. The various processes involved are rain and snow and considered to be the principal processes influencing the process.

The snowmelt produced by condensation may be estimated from the experimentally derived relation (USCE experiments as given in their Manual Sumoff from Snowmelt)

$$M_0 = 0.034 (z_a z_b)^{-1/6} (e_a - e_s) u_b \quad (1)$$

where M_0 = snowmelt in in/day

z_a and z_b = the heights of measurement (ft) of the air vapour pressure and wind speed above the snow surface.

e_a = the air vapour pressure in mb

e_s = the snow surface vapour pressure in mb
(6.11 mb at a melting snow surface).

and u_b = the wind speed in mph.

Salt produced by convection results mainly from heat transferred from warm air advected over the snow surface. The theory of turbulent transfer in the atmosphere is very complex, but experiments have indicated that simple approximation can be useful. The simplified expression considers chiefly the temperature gradient of the air above the snow surface, the wind speed, and the air density (taken as the function of the air pressure).

Convection melt may be estimated from the experimental equation

$$M_0 = 0.00629 (p/p_s) (z_a z_b)^{-1/6} (T_a - T_s) u_b \quad (2)$$

where M_0 = snowmelt in ins/day

p and p_0 = air pressure at the site and sea level, respectively

z_a and z_d = heights (ft) above the snow surface of air temperature and wind speed respectively

T_a and T_d = air and snow surface temperatures in $^{\circ}\text{F}$, the snow surface temperature being normally taken as $32\ ^{\circ}\text{F}$.

The contribution from convection is usually small relative to other factors. The equation for condensation and convection can be conveniently combined into a single equation to give

$$M_{cc} = 0.00629 (z_a z_d)^{-1/6} [(T_a - 32)p/p_0 + 0.39(T_d - 6.11)] ub$$

the total condensation - convection melt in ins/day. For practical applications in hydrology this equation can be further simplified. The ratio p/p_0 varies from 1.0 at sea level to 0.7 at an elevation of 10,000 ft. For areas with moderate topographic changes it may be assumed to have a constant value of approximately 0.8. Also the vapour pressure can be assumed to be adequately represented by dew point temperatures. By fixing the heights of measurement of T_a and T_d in $^{\circ}\text{F}$ at 10 ft. and that of wind speed at 50 ft. the preceding equation can be simplified to

$$M_{cc} = 0.0004 [0.22 (T_a - 32) + 0.78 (T_d - 32)] ub$$

where T_a and T_d = the mean air and dew point temperature respectively at the 10 ft. height
and u_b = the mean wind speed in mph at the 50 ft. height.

In some regions a linear regression relation between T_a and T_d gives a high degree of correlation, permitting further simplification.

4. Melt Content of Rain:

Rain falling on the snow surface at temperature above zero $^{\circ}\text{F}$ transfers heat to the snow thus producing melt. This can be stated directly by the equation

$$M_p = 0.007 P(T_a - 32)$$

where M_p = the snowmelt in ins/day due to rain

P = the mean rainfall in ins/day

and T_a = the mean free air temperature in $^{\circ}\text{F}$.

Ray K. Linsley Jr. [7] in his paper in June 1943 had also suggested this relation.

5. Heat conduction at ground:

Melt produced by heat conduction at the ground (M_g) is generally considered insignificant, unless there is a large underground source. A nominal value of 0.02 in/day is recommended.

for inclusion in design estimates.

In this subsection a semi-empirical theory developed mainly by the U.S. Corps of Engineers, has been given in outline; it is valid for very small plots of homogeneous character. Its chief purpose has been to provide an insight into the snowmelt process as influenced by various meteorological parameters, and to quantitate the effectiveness of each of these parameters in causing snowmelt.

The total snowmelt produced at a point location by the various factors will be

$$M = M_{rs} + M_{sl} + M_{ce} + M_p + M_g$$

2.7 SNOWMELT RUNOFF DETERMINATION

The manner in which runoff from either rainfall or snowmelt is affected by conditions prevalent within the snow pack is of primary interest to the hydrologist. Various views on storage characteristics of a snow pack have been suggested. These range from the concept that a snowpack can retain large amounts of liquid water to the hypothesis that snow pack storage is negligible. There is no universally applicable relationship, and it is important to base any runoff consideration on a knowledge of the character of a snowpack at the time of study. Winter runoff is related to snowpack condition whereas in the spring, once active melt begins, little or no delay in the transport of melt or rainfall through the snowpack occurs.

For drainage basins in mountainous areas, snowpack storage effects may be approximated by subdividing the watershed into relatively uniform areas. Normally, this will be accomplished by using elevation zones. Snowpack at the lowest levels may be conditioned readily transmit rain or meltwater, whereas in higher elevations a liquid water deficit may prevail. At upper most elevations, the snowpack may be very dry and cold and thus in a condition for the optimum storage of water. The storage potential of the watershed zones must be based on representative measurements of the snow depth, density, temperature, water equivalent, moisture content, and snowpack character. The snowpack character relates to the physical structure of the pack. Unfortunately, adequate measure of all these factors are not always available or easily obtained. Estimates of changes between sampling periods are usually indexed to readily observed meteorologic variables.

The formulation of snowpack storage and time delay characteristics can be fashioned by assuming a homogeneous pack. In this case storage is related directly to the liquid water deficit and cold content of the pack. Time delay is a function of inflow rate. It is considered that the snowpack storage potential must be entirely satisfied before runoff begins. This is not so in reality, but the assumption permits an analysis to be made. As melt proceeds, the storage potential of any snowpack diminishes.

The value of a freezing point coefficient is considered to be the ratio of the equivalent weight of sucrose to 2000 the freezing point of the compound is 0°C (solid sucrose) and the freezing point depression of the compound. If the value needed to bring a compound's temperature to 0°C , it may be calculated by

$$\eta_0 = \frac{W_0}{200} \cdot \frac{2}{\Delta T}$$

- Where η_0 = The mass fraction of sucrose present.
 W_0 = The equivalent weight of sucrose
 In liters for a normal solution based on the value of 200 of 0.01.

The value η_0 is kept equal to 2000 the freezing point depression of the compound is zero to this value by

$$\eta_0 = \frac{W_0}{200(1+\eta)} \cdot \frac{2}{\Delta T}$$

Where η = The osmotic pressure (mm/Hg)

W_0 = Mass of sucrose (kg/L)

Normal concentration is given the freezing point coefficient of the compound is given by

$$\eta_0 = \frac{2}{200} (U_0 \cdot \eta)$$

Where η_0 = The osmotic pressure of sucrose (mm)

U_0 = The mass concentration in mole per liter of the sucrose.

The time in hours t_p needed to fill the storage S_p is given by

$$t_p = \frac{S_p (V_o + V_c)}{100 (1 + m)}$$

It has been specified that the total storage potential S_p to be met prior to the runoff is given as

$$S_p = V_o + S_x$$

This is also known as 'permanent' storage since it is not available to the runoff until the snowpack has finally melted. An additional storage component transitory storage S_x is that water stored in the snowpack while moving through it to become runoff till initiation of runoff, the transitory storage in inches can be expressed as

$$S_x = \frac{D (1 + m)}{V}$$

where D = the depth of the snowpack (ft)

V = the rate of transmission through the snowpack (ft/hr)

The delay time of water in passing through the snowpack t_x is thus

$$t_x = D/V$$

for t_x in hours.

Assuming that t_x is very small compared to V_o , the depth of the snowpack is given by

$$D = \frac{V}{P_s}$$

with P_s the density of the snowpack.

then $t_s = V_s / (P_s V)$

Before the runoff commences, the total water stored in the snowpack, in inches, is given by

$$S = V_s + S_g + S_b$$

which can also be written as

$$S = V_s \left(\frac{2}{160} + \frac{2}{100} + \frac{(1+m)}{P_s V} \right)$$

The total time in hours which passes before runoff is produced is thus

$$t = t_s + t_g + t_b$$

or

$$t = V_s \left(\frac{2}{160(1+m)} + \frac{2}{100(1+m)} + \frac{1}{P_s V} \right)$$

After establishing the active runoff from the snowpack, the only significant term in equation $t = t_s + t_g + t_b$ is t_g , and this is usually small compared with the overall basin lag and can be neglected. With increased snowmelt and runoff, additional increments of water previously withheld by snow blockage to drainage outlets and other factors are released. Adequate quantification of this cannot be accomplished at

process. A case reported on 29 in having a mean temperature of $\sim 9^{\circ}\text{C}$, could store about 4 L. of liquid carbon dioxide till the end of summer [2].

2.7.1 Hydrograph Recording :

Hydrograph curves have the general form

$$\theta = \theta_0 e^{-kt}$$

where θ = the temperature at time t

θ_0 = the initial rate of θ

k = a constant.

Method of daily storage flow by hydrograph procedure overlaid with the amount of runoff derived from snowmelt [2]. The technique is essentially one of repetition of the daily hydrograph. Fig. (2.2) illustrates the procedure. Assume that the first, second and succeeding peaks, respectively, extended backward in time, at a point-A, the return time for constant days. If the ultimate recession curve is to be hydrograph a day later than it is. The area between recession from hydrograph 1 and hydrograph 2 (area unshaded) is the area attributed to day 1. In like manner, a series of successive hydrographs can be overlaid to determine their individual areas of contribution. By observing each hydrograph separately on the left side to peak I, the addition to trough II, and the sum of the successive volumes and ratio contribution of constant runoff can be made. A more comprehensive treatment of this subject can be found in [3].

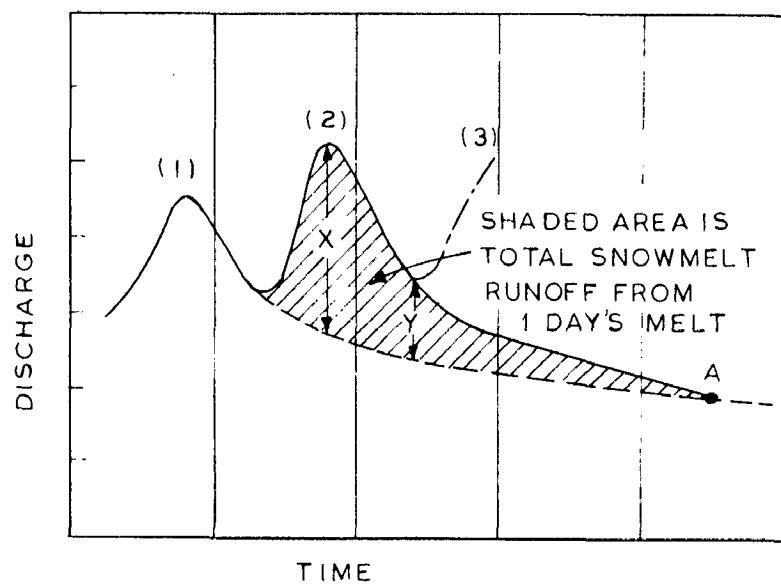


FIG. 2.2 SEPARATION OF A SNOWMELT HYDROGRAPH.

2.7.2 THE DEGREE - DAY METHOD :

This method was first suggested by W. E. Wilson [6]. As used in the U.S., a degree day in its broadest sense, is a unit expressing the amount of heat in terms of the persistence of a temperature for a 24 hr period of one degree - Fahrenheit departure from a reference temperature. As often applied in snowmelt studies, the degree day is computed by subtracting the average of the daily maximum and daily minimum temperature from 32°F . For example, if the daily mean thus computed were 32°F , there would be zero degree day. A daily mean of 37°F would yield 5 degree-days. Degree days above 32°F and degree days above reference temperature have been used in point-snowmelt and in runoff-snowmelt computation. Accordingly, Gerstke, Love, Goodell, and Bertle [4] used the commonly available maximum and minimum temperatures to estimate the degree days in a detailed interpretive study. The ratio of the water equivalent of the snowmelt away in 24 hrs to the number of degree days in the same period is called degree-day factor [5]. The relation needs

$$M = \alpha T_d \quad (1)$$

where M = the daily snowmelt depth (cm)

α = the degree-day factor ($\text{cm } ^{\circ}\text{C}^{-1} \text{ d}^{-1}$)

T_d = the number of degree-days ($^{\circ}\text{Cd}$)

Degree days ratios given in inches and degree days Fahrenheit can be converted to values in cm. and deg. celsius by a

coefficient of 4.57. It is pertinent at this point to look at the figures by species. Estimated contributions of the six bird species by species (unadjusted constant) have been noted.

By E. Handig, Jr. Not estimated values of the unadjusted constant by dividing the total runoff from the basin for a day plotted by corresponding water level. (The term, $\frac{dy}{dx}$ is to be noted on the graph of runoff in inches over the entire drainage basin is 0.03 inch of runoff occurs in the unit time ratio for each degree day above 22°F . It is determined simply by dividing average degree days over the basin by 300). No case that the observed runoff should be corrected for runoff from rainfall. This may be done by the method of a rainfall-runoff relationship developed for the basin, but because of the possible errors in such a procedure, it is usually best unadjusted. The unadjusted constant from previous work is 0.09 or no runoff occurred. Contribution of the observed runoff for drainage basin probably represents the true value.

Figure [30] shows the unadjusted constants for Coochiching Creek, Lake, and River at 0.09 in. per degree day. If one would assume that the 0.09 in. is a laboratory and found the value of constant as 0.09 in./degree-day, he expected that the difference probably represents the error attributed to the fact that the basin does not contain any river which is not contained in the drainage area.

Figure 2 E. G. Peckham Davis and others indicated that the six bird species by species contribution is 0.09 and 0.25 in./degree day.

Studies have shown that the average Day factor decreases from 1.00 to 0.90 with time after a preceding cyclone. This effect is probably largely due to the reduction of early melt water in the snow and soil. In addition of Deacon & Western Pennsylvania Section [11] found the average Day factor to be slightly lower as having several stations with values ranging from 0.99 at Deacon with others to 0.95 during severe snow storm.

The U. S. Civil Service Bureau [12] found similar values of average Day factor (estimated monthly) for 48 different conditions and found that the estimated monthly value increased the insulation ratio of about 1%.

TABLE 2.1

<u>Estimated Insulation</u>	<u>Value of Average Day Factor</u>
1. New snowfall potential	0.92
2. Average monthly snowmelt due to snow melting index of cyclone	0.96 = 0.93
3. Average monthly snowmelt	0.95
4. Insulated building types of insulated buildings during cyclone	0.93 = 0.90
5. Wind insulation potential	0.90

Table 2.2 'A Guide for hydrological prediction' [15] also gives a table containing values of the degree day factors in monthly basis shown below:

TABLE 2.2

Month	Degree Day Factors ($^{\circ}\text{F}$)			
	Normal	Parity	Excess	
	Summer	Winter	Seasonal	
Jan	40.0	2	9	4
Feb	45.7	3	4	6
Mar	50.0	4	6	7

In the same publication, the value of the degree factor is given by a formulae collected here does gives a

TABLE 2.3

Weather condition	Degree-day factor ($^{\circ}\text{F}$)
Normal weather	9
Spring conditions and atmospheric humidity of normal range	9.00 4
Autumnal humidity of conditions above and below normal	9.7 9.0 8.0
Fall conditions	9.4 9.0 8.5

The considerations which can be drawn from earlier studies by different persons mentioned above, could be summarized as follows :

- 1) Unpublished constant for calculating the infiltration loss of each crop slice.
- 2) Published constants for varying for different periods of the varying seasons.
- 3) ^{For} This study do for establishing the published constants depend on the value of offset of crop coverage, or marketing process.
- 4) Unpublished constants may be varying if the conditions do not uniform in its practice.

Since the crop is not the only cause of heat and in view of the varying conditions in the tropics, the secondary factor cannot be expected to be constant. Values in the range from 0.07 to 0.9 have been reported (Bartlett, 1934). Thus a number of crop coverage & it is possible to measure degree day ratios in different conditions without changing the crop cover (Bartlett, 1934). Thus hardly expected to be a "a" parameter to which variations of the secondary factor could be attributed by the solution

$$\alpha = 2.3 P_g \quad (2)$$

where P_g = the crop coverage required to reduce (2.3) to unity
Equation (2) has been derived for average climatic condition. Substitution of deviations must be expected in periods with markedly

high or low wind speeds. However in larger banks, it might be necessary to take into account further possible effects of erosion by an increasing wind speed.

- (i) In general, when large dry stones are affected by oblique scission they are accompanied by a small amount of the loose debris from the scission which is included in the dry-stone scoria.
- (ii) The distance is the exposure of dry-stone walls which the loose debris from the scission which is included in the dry-stone scoria.
- (iii) On a slope the removable effects on density are minimised when the exposed area is greater than 100 square metres projection (i.e. a single layer of a given thickness on a slope requires a net density smaller than a double-layer of equal thickness, although obviously originally both would be equal).

In equation (2) the first density term is dependent other factors affecting the density: a greater density occurs in rocky slopes older ones with a low slope, which promotes the heat and scission. Furthermore, high densities are frequently associated with the increased mass per unit volume and the low thermal quality of rocks. Individually organisational rocks may also show this density to a gradually decreasing index of the thermal properties of rocks (Morgan and Coates, 1972).

According to a study by the U.S. Army Corps of Engineers the daily working time available is in practice not to be exceeded by the following corrections applied to a situation

Individual observations or groups of observations to explain unexplained values in time and space. The adequacy of an index is based on (1) the ability of the index to adequately account for the physical processes it represents, (2) the random variability of the observations, (3) the degree to which the point observation is typical of actual conditions and (4) the nature of variability between the point observation and the basin areas. Indices may be equations or simple coefficients, and variable or constant.

The type of data required to make comprehensive thermal budget analysis are usually unavailable in the case part for consideration other than those which themselves are observational areas. As a result, hydrologist must make the best use of information at hand. The most commonly available data are daily maximum and minimum temperatures, and wind velocity. Data products are continuous measurements of stream flow, and flow duration curves either available or the duration of the gauging. Hourly precipitation data can be combined with climatic factors to predict weather conditions.

A complete general index for relatively unchanging atmospheric conditions is difficult to derive for all basins but has been attempted. This indices are simple coefficients valid only for specific climatic regions, particular, hydrologic, and seasonal conditions and are therefore limited in applicability to other situations. The climate must be similar in terms of thermal budget before an

08 තුනක් සඳහා daily තැපෑලයෙන් R_{DSS} , තුනක් සඳහා daily තැපෑලයෙන් R_{DSS} සහ එම පැමිණීමෙන් තැබේ.

3. For open catchments

$$\Pi = 0.03 \left(\frac{R_{DSS}}{P_{DSS}} - 24 \right)$$

$$\Pi = 0.04 \left(\frac{R_{DSS}}{P_{DSS}} - 27 \right)$$

3a. For reservoirs at 1000

$$\Pi = 0.03 \left(\frac{R_{DSS}}{P_{DSS}} - 22 \right)$$

$$\Pi = 0.04 \left(\frac{R_{DSS}}{P_{DSS}} - 42 \right)$$

තොරතුරුවෙන් යථ ආක්‍රීමෙන් වෙත $\frac{R_{DSS}}{P_{DSS}}$ නිවැරදියෙන් 30 හෝ 60°P සහ සැලැසුම් නිවැරදියෙන් 44 හෝ 70°P සහ යොමු කළ මූලික ප්‍රමාණ නිවැරදියෙන් පෙර ලැබුවෙන් ප්‍රමාණ 32°P සහ මූලික ප්‍රමාණය ප්‍රමාණ 0.035 සහ මූලික ප්‍රමාණ 0.02 සහ ප්‍රමාණය. පෙර මූලික ප්‍රමාණ ප්‍රමාණය ප්‍රමාණය ප්‍රමාණය 0.03 හෝ 60°P සහ සැලැසුම් ප්‍රමාණය සහ සැලැසුම්.

2.7.3 INDEX :

Hydrologic indices are ratio type of hydrologic or hydro-
logic variables to describe their functioning. The indices variables
are more easily measured or handled than the original variables.
These indices relationships are known to assist decision problem
formulation and evaluation values. Indices can be used to compare
both actual and theoretical magnitude of basic values. Indices can be
of two types (1) basically obtainable observations to reflect hydrologic
variables or processes which themselves cannot be easily measured,
and (2) simplification of computation methods by selecting

individual observations or groups of observations to replace scattered values in time and space. The adequacy of an index is based on (1) the ability of the index to adequately describe the physical process it represents, (2) the random variability of the observation (3) the degree to which the point observation is typical of actual conditions and (4) the nature of variability between the point measurement and the basin areas. Indices may be equations or algebraic combinations, and variable or constant.

The type of data required to make computations of thermal budget indices are usually available in the report for publications other than those which themselves are operational areas. In a society, hydrologist must make the best use of information at hand. The most commonly available items are daily minimum and maximum temperature, and wind velocity. Wind prevalent and continuous measurements of these items, and low frequency record either summaries of the duration of the conditions. Hourly recordings data can be converted to annual sums and disrupt another methods.

A sample of General Index for randomly acceptable thermal balance indices is given below. It has not been carefully checked. Most indices are designed to be valid only for specific topography, precipitation, hydrology, and seasonal conditions and are therefore limited in applicability to other situations. The number ranges represent values in terms of thermal budget indices to

$$Y = a + b_1 I_1 + b_2 I_2$$

where Y = the demand amount

a = a regression constant

the b_1, b_2 = the regression coefficients

the I_1, I_2 = individual factors.

The table below shows some types of factors that have been successfully used in demand forecasting.

Table 2-4

Some factors used to determine the total sales volume.

Selected Factors Considered	Index
Alcohol	Proportion of consumption
Population distribution	Number of population
Seasonal variation	Use temperature for heavy
Geographical area	Geographic area
For each area longitude latitude should be considered.	For each area longitude latitude should be considered.
Constitutive body exchange	$(S_a - S_b) V$, where S_a is the air temp., S_b the ocean surface temp., or lake temp., and V wind velocity.
Cost of construction	$(O_a - O_b) V$, where O_a and O_b are value per square of air and land surface or a lake value, and V is the wind speed.

It should be noted that every item in the heat balance equation is not always constant for a particular analysis, and thus the number of steps will vary for different designs and conditions. A fixed rate equation developed by the Corps of Engineers for the partly covered bridge shown above gives $\dot{Q} = 3000, \text{ Btu}$

$$\dot{Q} = 0.00253 \theta + 0.0249 (\theta_{\max} - 77)$$

~~12000~~

θ = daily average windspeed (m/s) over the entire covered area

θ = an estimated value of the daily air-wave radiation exchange in the roof (Btu/day)

θ_{\max} = the daily maximum temperature at Duluth ($^{\circ}\text{F}$)

2.7.4 COMPUTED BASIS EQUATIONS:

Intensive studies by the U.S. Army Corps of Engineers at various laboratories in the U.S. have produced several general equations for outdoor cooling (1) summer periods and (2) periods of rain.

The term for cooling, heat transfer by convection and conduction is of prime importance. Solar radiation is direct, and long-wave radiation can be easily eliminated from the convective and conductive terms. The summer periods provide both solar and freeconvection radiation because insulation and air require direct evaporation. Convection and conduction are usually the principal cooling methods for roofs. The equations are

සුදුම්පත් පිළිගෙ :

3o. දුෂ්කාලීකාව වෙත යොමු කළ ප්‍රතිඵල් :

- a) සාර ගැය (සෙවා දේශග 20 උරු ඝණු) හෝ ප්‍රතිඵල් මෙටර් තුන් (සෙවා පිළිගෙ 20 එහි 60 උරු ඝණු නොවා ඇති).

$$\Pi = (0.029 + 0.004 V + 0.007 Z_p)(Z_0 = 52) + 0.09$$

- b) සාර ප්‍රතිඵල් පිළිගෙ (සෙවා එහි ප්‍රතිඵල් මෙටර්).

$$\Pi = (0.074 + 0.007 Z_p) (Z_0 = 58) + 0.05$$

සැයාම $\Pi =$ සාර ප්‍රතිඵල් පිළිගෙ (M^2/C^2)

$Z_p =$ සාර ප්‍රතිඵල් පිළිගෙ (M^2/C^2)

$Z_0 =$ සාර ප්‍රතිඵල් පිළිගෙ පිළි නියුත් නියුත් පිළි නියුත් ($^{\circ}\text{C}$)

V = සාර ප්‍රතිඵල් පිළිගෙ පිළි නියුත් (M^2)

E = සාර ප්‍රතිඵල් පිළිගෙ, ප්‍රතිඵල් පිළිගෙ පිළි නියුත් පිළි නියුත් පිළිගෙ, සාර ප්‍රතිඵල් පිළිගෙ පිළි නියුත් පිළිගෙ පිළි නියුත් පිළිගෙ පිළි නියුත් පිළි නියුත්.

වැඩිහිටි පිළිගෙ පිළිගෙ 4.0 නිසු පිළිගෙ පිළිගෙ පිළිගෙ පිළිගෙ 0.9 නිසු පිළිගෙ පිළිගෙ.

2o. දුෂ්කාලීකාව වෙත ප්‍රතිඵල් පිළිගෙ :

- a) සාර ප්‍රතිඵල් පිළිගෙ,

$$\Pi = 0.074 (0.92 Z_0^2 + 0.07 Z_p^2)$$

- b) සාර ප්‍රතිඵල් පිළිගෙ (සෙවා එහි 60 එහි 60 උරු ඝණු)

$$\Pi = E (0.0004 V) (0.92 Z_0^2 + 0.07 Z_p^2) + 0.029 Z_0$$

a) For partially cloudy areas,

$$\begin{aligned} D &= E^*(3-2)(0.0024 \text{ } I_g) \text{ } (k=0) \\ &\rightarrow E(0.0024 \text{ } V) \text{ } (0.22 \text{ } \frac{V}{100} + 0.70 \text{ } \frac{V}{100}) \\ &\rightarrow E(0.029 \text{ } \frac{V}{100}) \end{aligned}$$

b) For overcast areas

$$\begin{aligned} D &= E^*(0.00203 \text{ } I_g) \text{ } (k=0) \times (k=0) (0.0225 \text{ } - 0.04) \\ &\rightarrow E(0.0203 \text{ } \frac{V}{100}) \text{ } \rightarrow \\ &\rightarrow E(0.0006 \text{ } V) \text{ } (0.22 \text{ } \frac{V}{100} + 0.70 \text{ } \frac{V}{100}) \end{aligned}$$

Where $E, V, \text{ and } k = \text{ as previously described}$

$I_g = \text{ the direct solar radiation between the } 30^\circ \text{ N. and } 30^\circ \text{ S. and expressed in millimetre } (^{\circ}\text{C}) \text{ temperature}$

$V = \text{ the direct solar radiation between the } 30^\circ \text{ N. and } 30^\circ \text{ S. expressed in millimetre } (^{\circ}\text{C})$

$I_g = \text{ the observed or calculated insolation}$
(in millimetre)

o o the observed or calculated insolation during day and night.

II' o the direct shortwave radiation from the sun
(radiation from } 0.9 \text{ to } 2.1 \text{ } \mu\text{m}) which is related to
mean exposure of the sky when compared to an
unobstructed horizontal surface

V o the mean direct radiation = cloudy cover
(cloudless condition)

$\frac{V}{100} = \text{ the fraction of time when the direct sun and}$
clouds are less than one millimetre } (${}^{\circ}\text{C}$).

K o the continuous cloud cover (cloudy condition).

Note that the ratio of capacities of the two divas must be related to the total capacity of the two cover if scallable volumes are to be obtained. Present methods of determining this are not really adequate.

3.7.3 THE HYDRO MODULE :

This module requires data to model the hydrological runoff from a river basin [2]. Such an approach has potential merits for areas where hydroclimatological records are scarce. Inefficiency in the method is the usual lack of information due to properly specifying the various components. A hydrological budget equation for the catchment can be written as

$$R = P - E - \Delta I \quad (1)$$

where P = the gross precipitation

E = the runoff

ΔI = the storage

R = the change in storage.

For coastal catchments this equation is somewhat modified.

Gross precipitation for a given period P will now be defined as the sum of precipitation in the form of rain P_r and snow P_s . Or

$$P = P_r + P_s \quad (2)$$

This also may be written as

$$P = P_r + P_g + P_d + E_g \quad (3)$$

where P_D = net precipitation

L_1 = infiltration loss

A further refinement yields

$$P = P_{\text{mm}} + L_{\text{in}} + P_{\text{ex}} + L_{\text{et}} \quad (4)$$

where

P_{mm} and P_{ex} = net rainfall and runoff

L_{in} and L_{et} = the rain and snow infiltration.

The total loss L will be

$$L = L_{\text{in}} + L_{\text{et}} + L_0 + \theta_{\text{in}} \quad (5)$$

where

L_0 = the evapotranspiration loss

θ_{in} = change in available soil moisture. The storage term is then given as

$$\Delta = (V_2 - V_1) + \theta_{\text{in}} \quad (6)$$

where

V_2 and V_1 = final and initial total equivalent of the storage

θ_{in} = the ground surface storage.

Inserting values for V_0 , θ_0 and Δ from eqns. (4), (5) & (6) in equation (3)

$$\begin{aligned} B &= P_{\text{mm}} + L_{\text{in}} + P_{\text{ex}} + L_{\text{et}} = L_{\text{in}} + L_{\text{et}} = L_0 \\ &= \theta_{\text{in}} = (V_2 - V_1) = \theta_{\text{in}} \end{aligned} \quad ..(7)$$

and considering positive and negative values of L_{in} and L_{et} produces

$$B = P_{\text{mm}} + P_{\text{ex}} - (V_2 - V_1) = \theta_{\text{in}} = \theta_{\text{in}} = L_0 \quad (8)$$

The expression $P_{\text{ext}} = (U_2 - U_1)$ represents the amount of heat released,

$$\Delta = P_{\text{ext}} + H = Q_{\text{ext}} = Q_0 = E_0 \quad (9)$$

If reversible conditions of the system in eqn.(9) can be assumed, the heat released is also conserved.

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CHAPTER III

APPLICATION OF REMOTE SENSING TECHNIQUE FOR HYDROLOGICAL PURPOSES

3.0 INTRODUCTION :

The use of aerial photographs for mapping was popularised in the late 19th century, while some applications were made by mapping from balloon photography. The impact of the 2nd world war accelerated the modern trends of aerial photographic mapping. Aerial photo-mapping and photointerpretation are very useful as they provide the location, magnitude and quantitative information of the area under investigation as compared to the conventional ground survey mapping and investigation method.

Aerial photographs also aid in preparation of thematic maps of all types of natural resources and in applying qualitative and quantitative information about the ground conditions. The impact of aerial photo-interpretation has further vastly improved during the last decade or so by the introduction of Remote Sensing Technologies and computer aided photointerpretation system.

Remote sensing has already an overwhelming impact on hydrology and other environmental sciences. Broadly defined, remote sensing techniques in hydrogeology applied to study the physical and other characteristics of objects without coming into physical contact with them. Conventional survey methods are time consuming and cannot be easily employed due to adverse terrain and weather conditions.

As such, updating information at reasonably frequent intervals will be a strategy involving remote sensing techniques.

3.2 THE SATELLITES, SENSORS AND IMAGERY FOR PHOTO-ANALYSIS:

Artificial earth satellites can be used for research and analysis of hydrological features of water resources in the following :

- (i) as a platform for remote sensing
- and (ii) as a data relay device.

Whether the characteristics are natural or not, the types of clouds are generally the most useful (i) thin cumulus clouds, which are relatively low in altitude and have near vertical orientation, and (ii) dark cumulus clouds, which are relatively high and more horizontal.

The present satellite sensors available with our synchro-satellite include the three MSS, SIR-2, LISS-II and LISS-III sensors. The MSS sensor can identify the extent possible of the coverage from a single satellite to take any particular or general as the case may be, over during day light and over night. Sensors carried on the two satellites are generally visible to the naked eye, and the resolution of the two sensors are 10 m and 5, and 4 respectively, during the daylight portion of the orbit. These sensors are sensitive to broad bands of electromagnetic spectrum, 0.5 m to 0.7 m. The microwave picture obtained

present their information continuously between the aircraft and ground stations during the period 1000 hrs to 1800 hrs on successive days, transmitting them when required to a ground station.

The 7300S series aircrafts have been equipped with 0.25m² solar panels by removable plates on the left and right side panels of the aircraft, as well as by means of a removable panel assembly. The covering panel can be easily removed and reattached without removal of a ground station's signal. This occurs, which is conducive to increased utilization in the 20.5 - 12.5 m² area, as well as day time flights 1441cc.

During 1972 a research flight took place from Madrid 2250 ft to a military base in northern Spain. During this flight it was determined that the aircraft could fly at 1000 ft above sea level for 4500 km at 100 km/h. It was also determined that the aircraft could fly at 1000 ft above sea level for 1000 km at 100 km/h. These figures were obtained by standard meteorological instruments. The aircraft was able to fly at 1000 ft above sea level for 1000 km at 100 km/h. These figures were obtained by standard meteorological instruments. The aircraft was able to fly at 1000 ft above sea level for 1000 km at 100 km/h.

These improvements will be available through the increased number of aircrafts for conducting the aerial and ground surveillance of the atmosphere. Improvement of the ground-based remote sensing system is of great importance, since this should lead directly to improving the performance of aircrafts.

The computerized system developed by
Srivastava (1980) can work automatically and can also do real
time observations capability. Further, such a system is
able to collect data from a variety of in situ atmospheric
platforms and to broadcast specialised products to remote
areas. Local users can ^{can} receive and display this
information in a relatively simple manner [14].

It is to be noted that there are relatively clear
atmospheric windows in the range 0.9 to 1.9 μm , 3 to 5 μm ,
9 μm , and 10 to 12 μm which can be used effectively.
Band 5 has a resolution of 0.5 to 0.6 μm to be effectively
used for the study of sedimentation, turbidity and water quality
and for the discrimination of geological information. Band 6 is
operating in the range 0.6 to 0.7 μm to be used for the
study of vegetation, rock bottom, land use, crop cover, etc.
Band 7 (0.7 to 0.8 μm) and Band 8 (0.8 - 1.1 μm) are
mostly used for the analysis of land use and surface accumulation
features. The composite chart showing the sensor strategy,
discriminative discrimination, and range of operation of various
bands is given in the figure 10 [12].

Data analysis of any area includes recognition of
object and interpretation of imagery as well as making various
inferences automatically. The process of discriminating objects on
the basis of photographs and collecting certain information
characterised by analysis of the natural and cultural features and
make a photo-interpretation. The sensor can thus provide
a comparatively quick and automated solution to the problem.

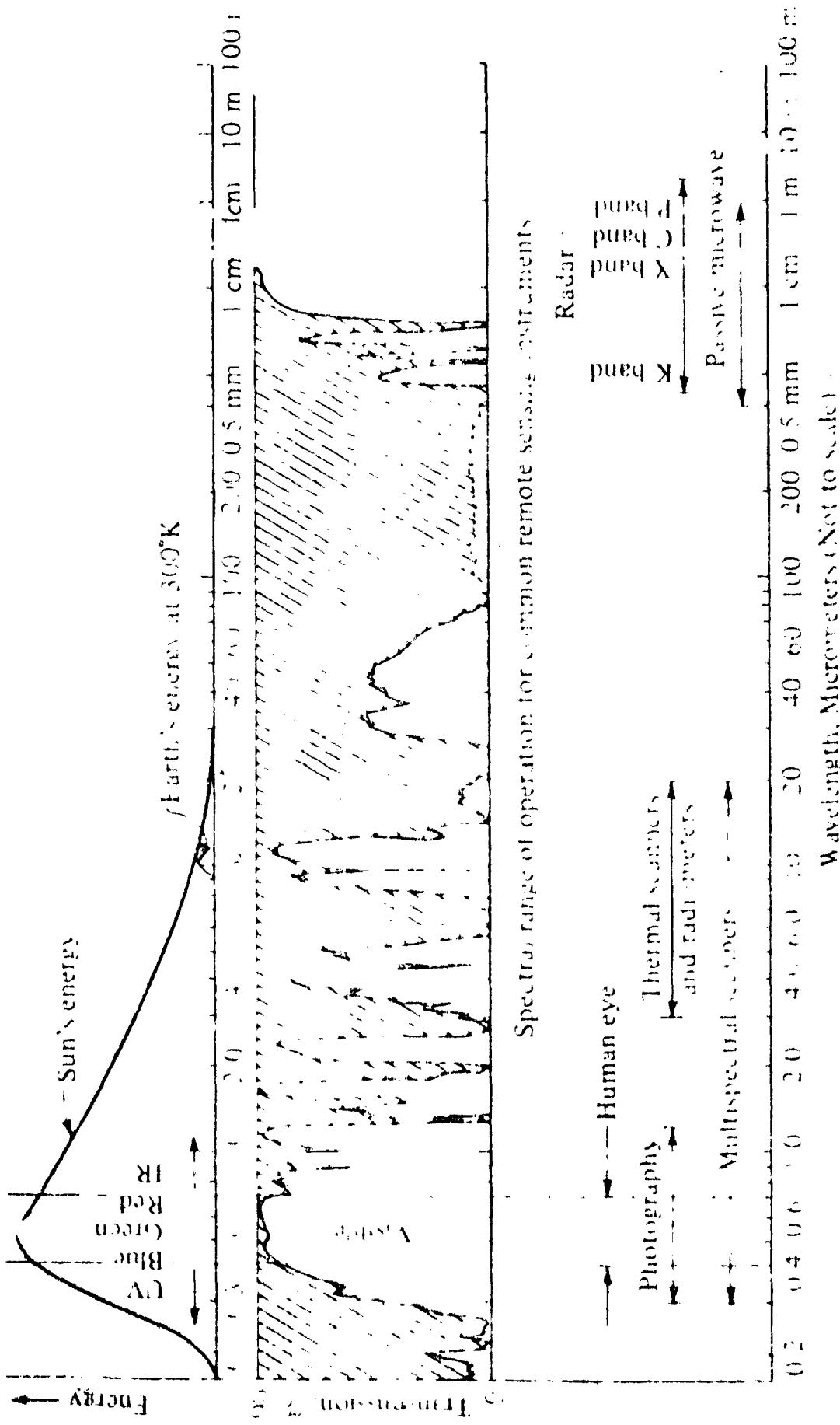


FIGURE 3.1
Composite chart showing source energy, atmospheric transmission, and range of operation of various sensors

Due to the satellite's fixed view and resolution requirements on this section the visible areas do not overlap much on successive orbits. Furthermore, repetitive orbits of an MSS are, in general, only once in a lifetime likely to contain one viewing cycle over a day apart. □. The MSS data are more useful than the current meteorological satellites because of (a) increased resolution and (b) simultaneous capability.

Simultaneous capability is achieved by the two of three sensors = total visible viewing capability, $0.9 - 0.9$, $0.9 - 0.6$, $0.6 - 0.7$ in broad categories. MSS's viewing resolution above the earth capability is the visible bands and, in addition, it also sees (about 3.0 □) and for (10 - 14 □) infrared.

Earth observation orbits are in the equatorial plane at a distance of 55,000 km above the earth's surface. The UNIKA Application Meteorology Satellite (AMS) of hydrological interest observes the earth from such orbits. The characteristics of this type of orbit are that it takes about 100 minutes to revolve the entire earth and that the area near the poles is poorly observed. A good characteristic of this type of orbits is that it possible the observe to take about one-fourth of the globe continually, or the number continually may be given characteristics that are distributed from the same portion of the globe. As can be seen from the chart, from pole to pole, once every twenty minutes of the time there is enough sun rise and sunset so the polar regions receive sufficient illumination continually.

3.2 NEW CLOUDS IN RAINY SEASONS :

3.2.1 New Clouds & Domes -

Investigation with multi-channel scanner used in LADME has indicated that the transient horizontal convective and cumulus clouds do exist in the 0.6 to 0.7 µm band. The vertical band 10.9 to 12.9 µm in the infrared window region of the atmospheric is very useful for distinguishing the ground vegetation. It has been developed to estimate the cloud cover in conjunction with the visible band due to identification of new convective areas as well as the region of raining areas.

3.2.2 Distinguishing between clouds and snow -

Both clouds and snow have high reflectance. Hence mapping area with cloud patterns are very difficult. Actual observation of cloud cover distribution can provide valuable information during periods of cloud cover that provide reliable snow-cover observations.

The following procedure is normally adopted for distinguishing snow from clouds (19).

a) Recognition of geographical features;

Determination of geographical features like villages, settlements and major roads etc., positively indicates absence of clouds.

b) Pattern recognition:

Snow cover on the mountain ridges follows the same color-coded pattern, as the mountain areas, which is different from the patterns of low-lying mountain areas. Thus possibility

As generally well defined.

(i) Uniformity of distribution :

Cloud cover in areas that are not forested have more uniform distribution than others. Even though the distributions of clouds and sun is nearly same, they covered areas are generally much smaller - because clouds are often very low or touch the ground.

(ii) Position variability :

Clouds do not remain the same always for more than a few hours. Thus, while position of high variability is caused by atmospheric and telegraphic of cloud cover. So when there is no change, observations for a day or more can, be regarded. The possible changes in cloud cover due either to shifting or transient cloud will be taken into account.

(iii) Intensity :

Clouds cast by clouds at low sun angles and in the northernly direction of prevailing sun to be taken into account while mapping cloud cover.

3.2.3 Protection to the Sun :

In non-forested areas which are identified to be cloudy skies, areas with continuous cloudiness definitely present when the sun's brightness should be mapped as overcast. Such areas represent the 25% of overcastness of approximately 1 km² area. Areas with partial cloudiness

(different grey and black) and each area of 2000 pixels is stored.

In quantitative terms the resolution is regarded as the edge of the brightest zone with regard to brightness variations due to forest and mountain shadows.

For more mapping purposes it is convenient to superimpose the satellite picture directly over the base map. This is normally difficult as the base image is dominated by the capability to have a non-uniform projection compared to the standard rectangular projections for the base map. An option available, 'Base ImageRegistration' is normally used for collecting project co-ordinates of the satellite picture on the base map with different alignment for the X and Y directions and the alignment can be continuously changed to facilitate direct superimposition of the landscapes. The map boundary is then marked out on the base map and a placement can be used to measure the area of new cover. Different methods for calculating area based on geometric calculations formulae have been given in software [29]. Both manual and computer-interactive methods are used for such calculations.

LATTICE Part 9 provides the best approximation of area from which calculations can be used for various areas methods listed (1) area based on scaling and comparison with a plumbline; (2) area methods derived from many locations; (3) calculations in 2-D or 2.5-D areas with reference to any shape image.

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The machine learning method is slow in execution and thus computationally costly, but relatively no expensive equipment is required. The mean absolute method is fast and not much equipment is required, thus the cost is low. The 2.322.5 km Box method, when used to obtain high precision is slow in execution but requires hardly any equipment.

The Stanford Research Institute Institute Estimate Satellite Image Analysis System (ESIAS), is an interactive measurement that employs classification, clustering and estimation techniques as a process intended to bridge the gap between traditional manual photointerpretation and completely automatic digital processing. Three operations procedures are available for working with ESIAS, (1) single threshold - threshold level method (2) multiple threshold setting locally called by reference to different contexts and other images and (3) two-band colour-composite threshold estimation, locally effect as in method (2). The enhanced threshold method using ESIAS is fast, but the methods are expensive. Multi-threshold-threshold techniques need more operations and training time and are therefore more expensive.

The general automated pattern recognition techniques are most equivalent to apply them and in conjunction with a decisional console and standard pattern recognition techniques and programs. Bands 4 to 5 versus Band 7 infrared images prove to be most useful to 'distinguish trees, ^{water} grass and rock areas, snow and vegetation areas, clouds or fog, water,

Snow can be clearly separated from rock, water, and vegetation but snow and vegetation mixed cannot always be clearly separated from rock.

The digital techniques are able to average the effect depending on the equipment available for separating the image, of the drainage basin boundary. The cost of the computer, the cost of memory and the labour for monitoring the image, and the computer time required for a few dimensional problems recognition program can be acceptable for a single application.

The following table give prostate in summary from the preliminary comparison of the various methods for precision, cost, ability to recognize snow in trees, and application to area like Finland; the distribution of snow cover with altitude or in sub-basin, which can be used in creating balance constraint matrix.

3.2.4 Determination of snow depth from satellite:

It was shown by H. Gruber et al. (1979) that estimation of snow depth is possible by relating the snow depth with its reflectivity as sensed by the satellite born sensors in the visible band.

3.2.5 Water equivalent of snow accumulation[16] :

Air borne technique, based on the detection by a snow layer of natural radiation emitted from ground, has proved successful to determine the water ^{equivalent} reflectivity. The resolution is said to be about 8 cm of snow and their work with snow coverage.

3.2.6 Snow density :

No. 7481 and No. 63210 studied the 45VCE Satellite in U.S.A. for snow density using SWIR & IRWY in 4 bands and CCRS (Computer Compatible Radios). One of the observations is such critical to the low threshold of detection. They have found a relation of the type

$$\text{Snow density} = 0.0125 + 0.0020 D + 2.0220^{\alpha} S \\ = 0.0125 + 0.0020$$

where

I = sum of the average daily precipitation above freezing
temperature ($^{\circ}\text{F}$)

D = Solar declination.

S = Ground level in ft.

α = Satellite measured parameter.

There is a very small; thin river in Maharashtra which has
been considered the best example for calculating area of catchment,
river equivalent and density of flow.

3.3 Area of basin cover used for calculating river basin flow characteristics:

Area cover used over the Modayya has been used by
Rao and Venkatesha (1973) for calculation of runoff flow in
the Indravati River. Runoff during area cover was measured
and obtained for the upper Indravati basin above 4000 ft
in elevation and compared to rainfall-runoff ratio measured during
the years 1967 to 1972. A linear regression equation quanti-
tatively expressing the relationship had a regression coefficient
of 0.92. Regression of April June 1972 determined using
the equation so derived produced a value that is within
2 per cent of the actual value. Similar work has been done
in many catchments of the U.S.A.

Vishwanath and Venkatesh (1977) studied area over and
runoff analysis using rainfall-runoff ratio for Gostwy. The relation
derived obtained is as follows:

$$\theta = 8.0 \left(e^{0.00204 - 3} \right)$$

$$\text{where } \theta = \text{runoff ratio } \text{mm}^{-1} \left(10^6 \text{ m}^3 \right)$$

$$\Delta = \text{area covered area } \text{m}^2$$

3.4 USES OF AERIAL PHOTOS IN HYDROLOGICAL INVESTIGATIONS

It is possible to study a vast area in short time with the analysis of aerial photos, which are quite reliable and fast, and give the latest information. Ground methods of investigation are not only time consuming and expensive but by the time results could be compiled, they could certainly be out-dated.

Photo hydrological investigations are carried out mainly for the following :

- 1) Preliminary evaluation of ground surface where no such information is available particularly for secondary studies to indicate potential water resources.
- 2) Setting maps for general purpose, revenue, planning etc.
- 3) Inventory of natural resources, e.g. agriculture, forestry, water resources, mineral exploration, soil surveys, etc.
- 4) Delimitation of watershed and their boundaries.
- 5) Topographic mapping for the study of the river basin characteristics, including geomorphic features.
- 6) Division of catchment into suitable maps scales for estimation of precipitation.
- 7) Site selection for locating rain gauge stations.
- 8) Preparation of special purpose maps showing ecological features, land use, soil characteristics, vegetal cover index etc., location of river valley, and good places etc.

- 9) River banking of river banks increase where no erosion threat exist and no soil loss, qualitative, quantitative information may be obtained from the occurrence of leakage, change, width, and depth of the channel.
- 10) Preparation of hydrological studies.
- 11) ~~Ground water~~ Ground water studies.
- 12) Keeping and monitoring the area field in order to predict runoff in streams, deriving part of which water from the rainfall.
- 13) Evaluation of intensity and frequency of floods and keeping flood inundation maps.
- 14) Property survey for automated area for solving scheduling problem while placing any structures.
- 15) Flood control, and hydropower generation potential.
- 16) Keeping chart books, studies and setting of the boundaries and river banks.

However, the use of aerial photographs has got certain limitations. One cannot completely do away with the field work but saving an area may be 2-3 times and an cost up to 9 times by according to the use of aerial photographs. It has been found that monitoring of snow cover by AERIAL-photograph is 6 times faster than the high altitude aerial photograph survey, and the cost of applying by aerial is about 1/2000 times the cost of the aerial photograph from aeronautics survey.

3.9 PRINCIPLES OF PHOTO-ANALYSIS :

3.9.1 Procedural steps in photo-hydrological analysis

Photo-hydrologic studies are generally carried out in the following steps:

- 1) After proper collection of a watershed, the topographic map is required to be prepared by noting down details for distance directions, contours, elevations, etc. of the terrain features.
- 2) Identification of vegetative features and other details (geomorphic features) with the aid of image characteristics like shape, size, pattern, direction, tone, texture and others.
- 3) Correlation of image characteristics of various ground features (physical features of basin) to derive relevant hydro-hydrological features, geomorphology, rock-soil type, vegetation, land use etc. of the given area.

3.9.2 Preparation of topographic map:

For a hydrologic investigation, the hydrologist requires an up-to-date map of the project area. Aerial photographs help to prepare topographic map with the ground representations of tree species distribution, including features and other hydrologic details in a way which can depict those that obtained by the ground surveys. The topographic map reveals physiographic features like

- a) Hydrologic basin and related characteristics, etc
- b) Pedologic factors and texture.

S. 9.3 Characteristics of Basin :-

Basin characteristics available from photo-analysis are

- a) Area, slope, and shape of the basin including the nature of river bed.
- b) Shape factor.
- c) Ratio of concentration in the basin.
- d) Discharge ratio.
- e) Circum-Lottery ratio.
- f) Morphogenetic ratio.
- g) Shape of the water.
- and h) Relief condition.

These characteristics are described below:

S. 9.3.1 The area, slope and shape of the basin:-

A river, or drainage, basin is the entire area enclosed by a stream or system of connecting streams such that all overflows originating in the area is discharged through a single outlet. In large basins, it is assumed that all groundwater runoff originating from precipitation on the area is ultimately discharged from the basin as infiltration with the exception of that surface which is returned directly to the atmosphere by evapo-transpiration.

The drainage area which is the plan and horizontally projected area enclosed within the river is determined by planimetry from large scale map [17].

The shape and size of the basin considering sublimation form may affect much the stream discharge characteristics.

Horton [4] described the outline of a normal basin (मान्यता) as a polygonal void. The quantitative expression of irregular basin outline was made by him through form factors.

3.5.3.2 Basin Factor, R_2 :

Basin Factor, R_2 is the dimensionless ratio of the basin area A to the square of the basin length L .

$$R_2 = \frac{A^2}{L^2}$$

3.5.3.3 Shape Index S_3 :

In its inverted form, L^2/A , this ratio was used in unit hydrograph applications by the U.S. Army Corps of Engineers.

$$S_3 = \frac{L^2}{A}$$

where A = area of the watershed

L = Basin length along the river stream from the upstream point.

The plot of $\log L$ vs. $\log A$ gives linear relationship.

3.5.3.4 Circularity Ratio R_3 :

This defined circularity ratio as the ratio of basin area A to the area of a circle A_0 , having the same perimeter on the basin.

$$R_3 = A/A_0$$

3.5.3.5 Compaction Coefficient :

The compaction coefficient is given by the formula,

$$C_0 = 0.23 P_0 / \Delta$$

where P_0 = Parameter of the basin or sub basin

Δ = Area of the basin or sub basin

3.5.3.6 Effective slope :

It is given by the formula

$$S_e = 1.9 \frac{D.H./I}{L}$$

where S_e = effective slope of the basin

D = contour interval

H = the total number of contour lines intersected
by the grid lines (the grid is adopted)

3.5.3.7 bifurcation ratio :

In linear aspect of the channel system the number of stream segments of any given order will be lower than for the next lower order but same relation does not hold for the next higher order. The ratio of number of streams of a given order n_b to the number of streams of the previous n_{b+1} is known as bifurcation ratio, B_b .

$$B_b = \frac{n_b}{n_{b+1}}$$

3.5.3.8 stream order :

It is a classification according the degree of branching, or bifurcation, within a basin. Horton assigned order 1 to small, undivided unbranched, single-ray tributaries, order 2 to those which have branches of the first order only, order 3 to streams with branches of 2nd, and lower orders etc. This classification is the basis of the drainage system.

Based on Horton law of stream number

$$n_u = n_b (L^n)$$

3.5.3.9 Time of concentration :

Time of concentration, T_c , as per modified Manning formula is given as

$$T_c = \frac{L^{1.5}}{7700 R^{0.5}} \text{ in hours.}$$

where, L = length in feet along the channel from the steepest point in the area.

3.5.3.10 Edge of the catchment :

It is the change in gradient per unit length. Sudden changes in gradient of a slope may indicate cut-offs or areas of differential hardness or fault-line zones. The break of slope is easily identified as a sudden change in the contour density.

3.5.4 Drainage Patterns :

The following drainage patterns which give some structural or geological idea of a basin can easily be seen on the aerial photographs.

- a) dendritic
- ii) parallel form
- iii) trellis form
- iv) radial/annular form
- v) Parallel form
- vi) Isobatic form
- vii) Irregular form
- viii) Planar form

3.3.5 Discharge Factors :

Discharge factors refers to the number and relative spacing of discharge events per unit area in the drainage basin. The altitude, area and intensity of precipitation, etc. determine the drainage volume, drainage factors to some extent separated into

- a) Discharge density
- and b) Discharge frequency.

3.3.5.1 Discharge density :

An important indicator of the runoff characteristics and drainage density is the ratio of drainage density to drainage capacity, D, introduced by Horner

$$D = \frac{\sum L_i}{A} \quad (\text{in miles per square mile})$$

where $\sum L_i$ = total observed segment lengths cumulated for all orders within a basin.

$$A = \text{total area of basin}$$

Generally low drainage density (occurring during winter months) is found in regions of highly variable or highly permeable subsurface materials under sparse vegetation cover and vice versa. High drainage density (occurring fine months) is found in regions of rock or impermeable subsurface materials, dense vegetation, and continuous surface cover. All drainage factors discussed in this paper factors are to be equally included while drainage density is determined by physico-chemicals.

3.5.5.2 Drainage Frequency :

As per Norton, D.L., stream frequency or channel frequency, P is the number of stream segments per unit area of $P = L/A$.

3.5.6 Geomorphology :

Geomorphology analysis involves a systematic study of the relief and of drainage system. This is the landform study including the main feature of relief, local relief, fluvial forms, forms of mass transport, relation to lithology and structure, glacial forms, coastal forms, wind forms etc.

3.5.7 Soil Study :

The rock-soil type, permeable or nonpermeable, porous or nonporous, fractured or nonfractured, and moist or dry can be easily recognised on the aerial photographs from their tonal and textural variations. Certain species of trees also give good indication of soil type. The rock-soil type and the vegetative cover have direct effect on the infiltration capacity which itself, in turn has a bearing on the amount of runoff from the watershed.

3.5.8 Vegetation :

Photointerpretation is extensively used in delineating the areas having different natural vegetal cover densities, by correlating the tonal and texture variations those can be transferred on to the base map. The knowledge of the extent and type of vegetation, some important information regarding

while working with mercury in the boat 21 (D-7-1-2/10) found from District 3. Some particles of glass could be detected in the APM, while the visible band data, which was collected simultaneously, showed a considerable amount of glass. This phenomenon occurred during the melting conditions in operating. It is caused by a considerable increase in the reflected heat - i.e. radiation which in turn is apparently the result of a thin film of water at or near the surface of the glass which tends to absorb the radiation in the band.

Investigations show that for a given area there appears to be a normal pattern of sand transportation. The most significant finding of these studies was the coincidence of a close relationship between riverbank deposition and crevassed alluvium sites.

Investigations show the collection of sand may, under certain circumstances, be related to the river thickness, there is at present no visible method for determining sand thickness, or water equivalent, or density of sand.

Indiscriminate, predatory fishing, overfishing, overexploitation and ground water use be curtailed.

S.S.9 Land Use :

Land use mainly consists of forestation, cultivation, horticulture, urbanisation and urbanisation which can be easily identified on the coastal photographs by their specific image characteristics. All these features have a certain influence on the base flow which interacts with the underlying land use.

S.S.10 Hydrology of the coastal coastal areas :

For the hydrologists who want to forecast future levels, must probably appreciate the most complicated and most difficult = $R =$ runoff hydrological variable. Runoff area, precipitation, river equivalent, water content, soil + thickness and density all play a large part in the estimation of the runoff's contribution to runoff.

The choice of information according to climatic scenario output and depth of knowledge is a common problem. Remote sensing has been looked upon by many as a promising means of attacking the hydrologic problem.

Colour and infra-red techniques are currently being tried for classifying different types of crop growth and the presence of the drying water. A potentially useful discovery in remote sensing was made by Strong and co-workers (1971)

while cooling with energy in the form IR (0.7-1.2μ) from sun plus 3. The increase of time could indicate an error in the IR, while the visible band (400, 500) was collected simultaneously, showed a considerable amount of error. This phenomenon occurred during the melting temperature in spring. It is caused by a considerable decrease in the collected heat = IR radiation which in turn is apparently the result of a thin film of water at or near the surface of the mass which tends to absorb the radiation in the band.

Investigations show that for a given area there appears to be a normal pattern of snow accumulation. The most significant finding of these studies was the establishment of a close relationship between snowfall deposition and accumulated snow film.

Proposed recommendations that the collection of snow may, under certain circumstances, be related to the snow thickness, there is at present no visible method for determining snow thickness, or water equivalent, or density of snow.

CHAPTER-IV

ANALYSIS OF BEAS CATCHMENT FOR SNOW COVER AND SNOWMELT

4.1. THE BEAS CATCHMENT.

The source of Beas river is said to be Beas Kund a small spring near Rohtang pass. Unlike other major rivers of North India it is not fed by natural lakes. The catchment lies between longitude $76^{\circ} 56' E$ to $77^{\circ} 52' E$ and latitude $31^{\circ} 30' N$ to $32^{\circ} 25' N$ and occupies the area of about 4894 km^2 , out of which about 1400 km^2 is permanently covered by snow. River Beas is the principal tributary of river Satlej in the Indus river basin. Most of the catchment area comprises of precipitous slopes and the peaks are mainly bare. The river is mainly fed by snow and glacial melt besides the rainfall. The geographic pattern of the catchment is such that there are high mountains in the east as well as the north of the river valley. There is a high ridge on the West and a number of low hills ranging from 950 m to 1220 m in height. The river originating from Beas Kund takes a south-westerly direction upto Kulu and then takes a south-easterly direction upto its confluence with Tirath and Sainj rivers. It again flows in south-westerly direction, upto Pondoh, down stream of Larji.

The bed slope of river Beas in upper reaches is very steep, and the average value of the bed slope from Rotang pass to Manali is about 78 m/km, from Manali to Kulu, about 15.6 m/km, and from Kulu to Larji, about 8 m/km.

The principal tributaries of Beas river upto Larji site are Allun Nallah near Manali, Sarvari Khand, near kulu, Parvati river near Bhuntar, Thirthan and Sainj rivers near Larji (Appendix I). All these tributaries have got perennial flow which varies considerably during different months of the year. The catchment area at a scale of 1 inch to 6 miles (1, 253440), with contours at 2000 ft (611 m. approximately) interval is shown in the Appendix II.

4.2. COMPUTATION OF MORPHOMETRIC AND RELIEF FEATURES

4.2.1 MEASUREMENT OF BASIN AREA.

Area of Larji^{Basin} and its subbasins were measured with the help of a planimeter and the average values are given in the table number (4.1).

4.2.2. NUMBER OF STREAMS

All the streams according to their order in each sub-catchment were counted and the total number is tabulated in the table number (4.1).

4.2.3. TOTAL LENGTH OF STREAMS

As arranged in orders, the respective lengths

1	2	3	4	5	6	7	8	9
14. Watershed slope $S_B = H/L$								
15. Time of concentration $T_C = L^1.15$				0.204	0.053	0.039	0.082	0.074
16. Maximum number of order of streams	7700	40,385	40	2.24	6.19	6.42	10.79	11.56
17. Bifurcation ratio $R_b = n_u/n_{u+1}$				3	5	5	5	6
18. Stream frequency $P = N/A$				4.30	3.23	3.21	4.79	3.76
19. Stream density $D_s = S/A$				0.16	0.15	0.13	0.11	0.15
				0.39	0.37	0.26	0.21	0.30

of the streams were measured and these are given in table No. 44.1).

4.2.4. THE LOCAL RELIEF

It is generally found by selecting representative smaller sub-basins, finding the number of contours cut by a line and dividing it by the number of facets. Here the relief (H) is calculated by taking the elevation difference between basin mouth and the highest point on the basin perimeter. The values are given in table (4.1).

4.2.5. OTHER TYPICAL MORPHOMETRIC COMPUTATIONS

The other parameters like the stream density, stream frequency etc., have been calculated as according to the definition given in article (3.5.3) and tabulated in the table (4.1)

4.3. VEGETAL COVER AND LAND USE FEATURES

An attempt has been made to identify and delineate the vegetal cover and land use features using visual interpretation techniques, from 1:250,000 blow up of LANDSAT imagery dated 2nd December, 1972. Five distinct tonal variations could be recognized in the paper print. The interpretation includes the features like the snow covered area, Alpine pasture,

thin forest, thick forest and bare-and- cultivated land which are shown in the appendix III. The areal coverage of the features are given below in table No. (4.2). The hydrologic behaviour of forest and range lands and relationship of land use to water yield and stream flow has been studied quite extensively. These studies have gradually lead to an understanding of some of the basic relationships between land use and runoff, debris deposition, the schooling of stream channels, silting of reservoirs, storm flows, and other phenomena that have followed excessive logging, cultivating, burning, and grazing of forest lands and range lands.

TABLE 4.2.

VEGETAL COVER AND LAND USE FEATURE IN LARJI CATCHMENT

Sl.No.	VEGETAL COVER & LAND USE FEATURES	AREA Km ²	PERCENTAGE OF CATCHMENT(%)
1	Snow cover	1451	29.66
2	Alpine pasture	552	11.29
3	Thin Forest	523	10.69
4	Thick Forest	1359	27.78
5	Bare and Cultivated land	1006	20.57

X

6.4. SNOW COVERAGE IN LARJI CATCHMENT USING THE LANDSAT IMAGERIES.

6.4.1. THE LANDSAT IMAGERIES

The Beas catchment upstream of Larji was studied with the help of the multi spectral LANDSAT imageries from Space Application Centre, Ahmedabad of the following dates as 22, Sept., 1972, 3 December, 1972, 3 March, 1973, 21 March, 1973, 2nd March, 1975, 1 April, 1976 and 27 March, 1977. These imageries were in Band 5 and 7 and at a scale of 1: 1000 000. These are shown in figures (4.1, 4.2, 4.3).

6.4.2. STUDY OF SNOW-COVERED REGIONS ON LANDSAT IMAGERIES

LANDSAT imageries as above of the Beas catchment up stream of Larji were analysed. The overlays were traced from the imageries and areal extent of the snow cover in each sub basin was measured. These are shown in figures (4.1, 4.2, 4.3).

The results are tabulated in table number (4.3)

From the LANDSAT imageries it is clearly discernible that the extent of snow cover gradually increases from the month of September to March. This can be observed from the data in the table No.(4.3). Snow coverage is maximum in the month of March after which it depletes due to melting. From similar observation it has also been found that the Sutlej and Beas catchments

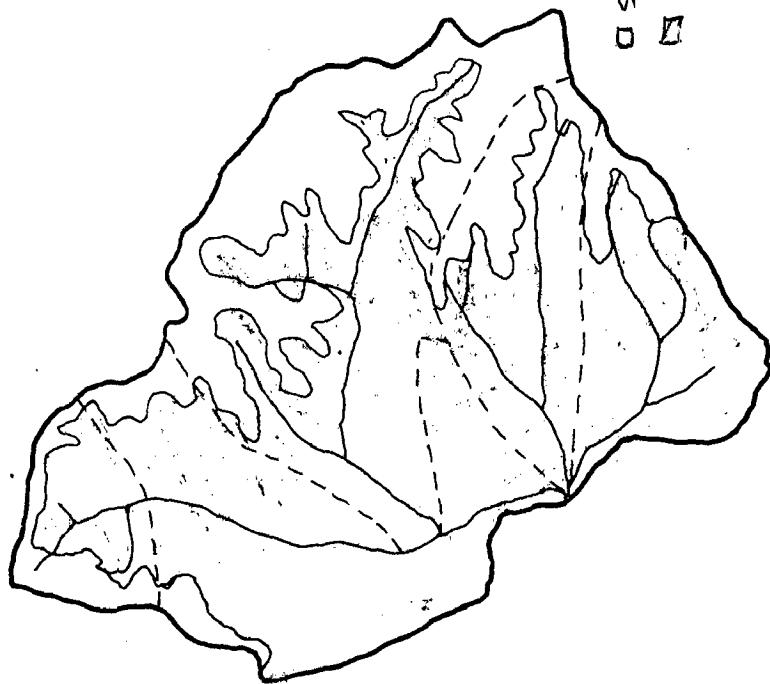


FIG. (i) LANDSAT IMAGE DATE 22 SEP. 1972
MSS 7



FIG.(ii) LANDSAT IMAGE DATE 3 DEC. 1972
MSS 7

FIG. 4.1 LANDSAT IMAGERIES OF BEAS CATCHMENT UP STREAM OF LARJI

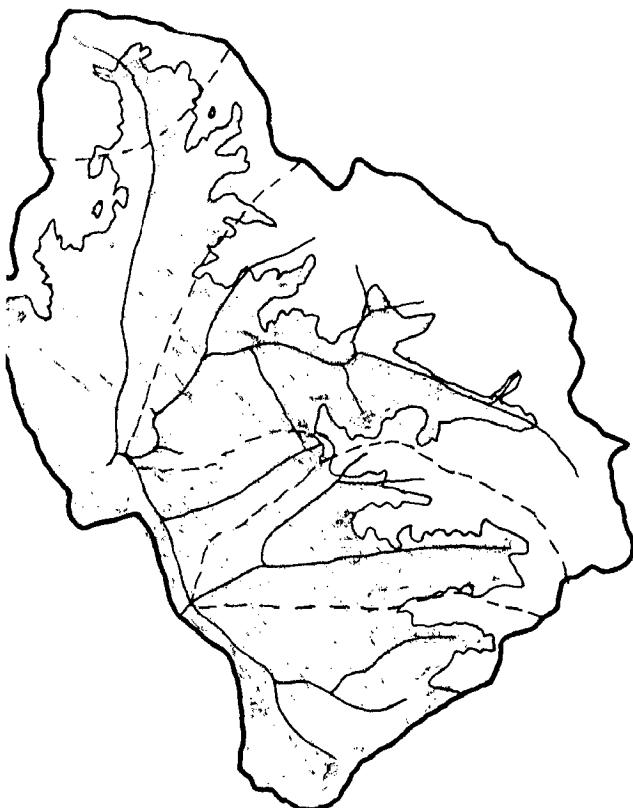


FIG. (iii) LANDSAT IMAGE DATE 22 SEP
1972 MSS 5

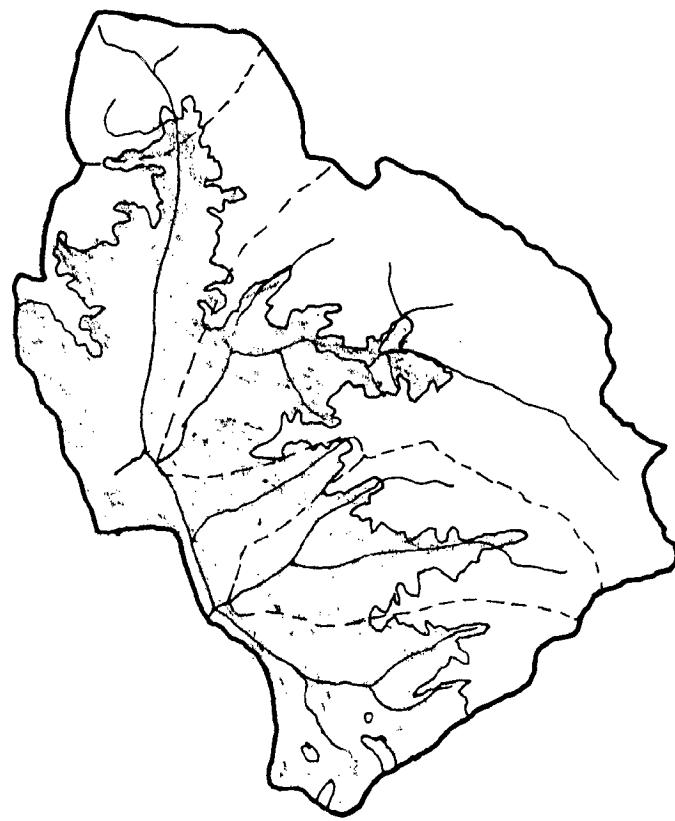


FIG. (iv) LANDSAT IMAGE DATE 3 DEC
1972 MSS 5

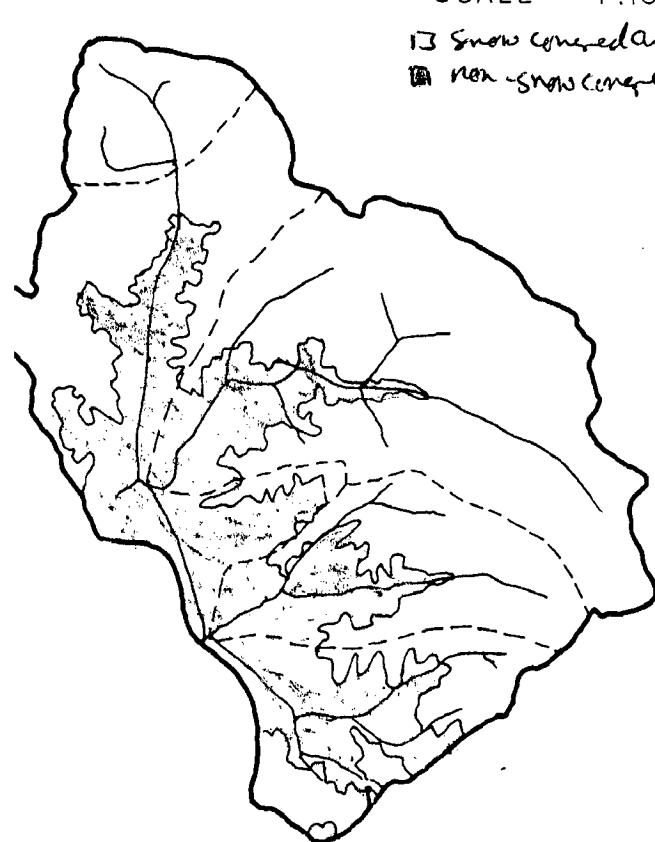


FIG. (v) LANDSAT IMAGE DATE 3 MAR
1973 MSS 5

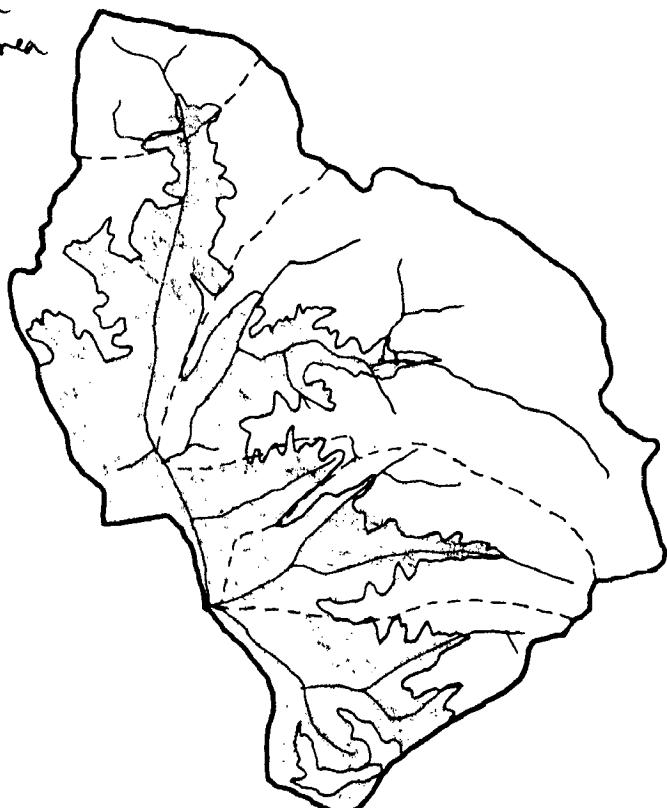


FIG. (vi) LANDSAT IMAGE DATE 21 MAR
1973 MSS 7

FIG. 4.2 LANDSAT IMAGERIES OF BEAS CATCHMENT UP STREAM
OF LARJI

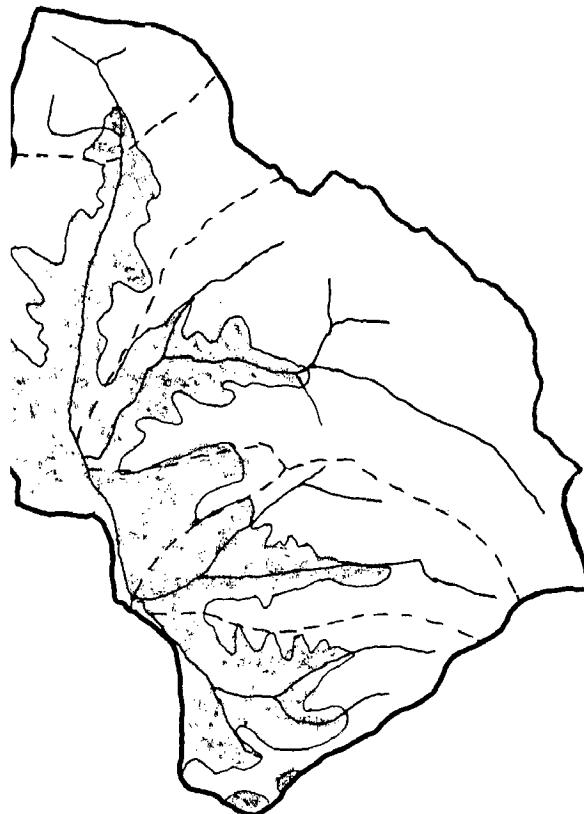


FIG.(Vii) LANDSAT IMAGE
DATE 21 MAR. 1973 MSS 5

FIG.(Viii) LANDSAT IMAGE
DATE 2 MAR. 1975 MSS 7

SCALE - 1: 1000,000

□ Snow covered area
■ non snow covered area



FIG.(ix) LANDSAT IMAGE
DATE 1 APR. 1976 MSS 5

FIG.(x) LANDSAT IMAGE
DATE 27 MAR 1977 MSS 5

G. 4 · 3 LANDSAT IMAGERIES OF BEAS CATCHMENT UP STREAM
OF LARJI

Areal Extent of snow-cover from LANDSAT Imageries

S.N.	Catchment	Area of catch-	ment in km ²	Date: 22 Sept. 1972		Date: 3 Dec. 1972		Date: 3 Mar. 1973 (BAND MSS 5)				
				(BAND MSS 5)	(BAND MSS 7)	(BAND MSS 5) (BAND snow-covered area in area in area in Snow-covered area in area in	(BAND MSS 7)	(BAND MSS 5) (BAND snow-covered area in area in area in Snow-covered area in area in	(BAND MSS 5)			
				km ²	%	km ²	%	km ²	%	km ²	%	
1.	Hanali	369.41	207	56.04	116	31.40	359	97.18	212	57.39	360	97.45
2.	Purnavati	1731.60	1100	63.53	724	41.81	1362	78.66	1080	62.37	1426	82.24
3.	Satnij	795.80	234	29.40	167	20.99	340	42.72	208	26.14	336	42.22
4.	Tirthan	697.40	234	32.73	71	10.15	119	17.01	95	13.88	265	37.89
5.	Lutjia	4394	1855	37.90	1216	24.89	50.86	1822	37.43	3025	61.81	

ANALYSIS OF CATCHMENT

S.N.	Catchment	Area of catchment in km ²	Dates 21 March 1973			Dates 2 March 1975			Dates 1 April 1976			Date: 27 Mar. 1976		
			(BAND MSS 5) (BAND MSS 3)	(BAND MSS 5) (BAND MSS 3)	Show-covered area in km ²									
1.	Ranikot	369.42	348	96.20	239	78.23	360	57.45	360	37.65	163	44.12		
2.	Pawat	1731.66	1553	89.69	1450	83.74	2513	67.30	1430	32.58	1306	75.42		
3.	Satnaj	797.80	480	61.57	365	45.87	462	58.05	475	59.69	336	41.97		
4.	Dittran	699.40	273	39.03	219	31.31	191	37.31	310	44.32	174	24.88		
5.	Lafj	4894	3273	66.83	2912	59.50	3057	62.46	3030	62.32	2194	64.83		

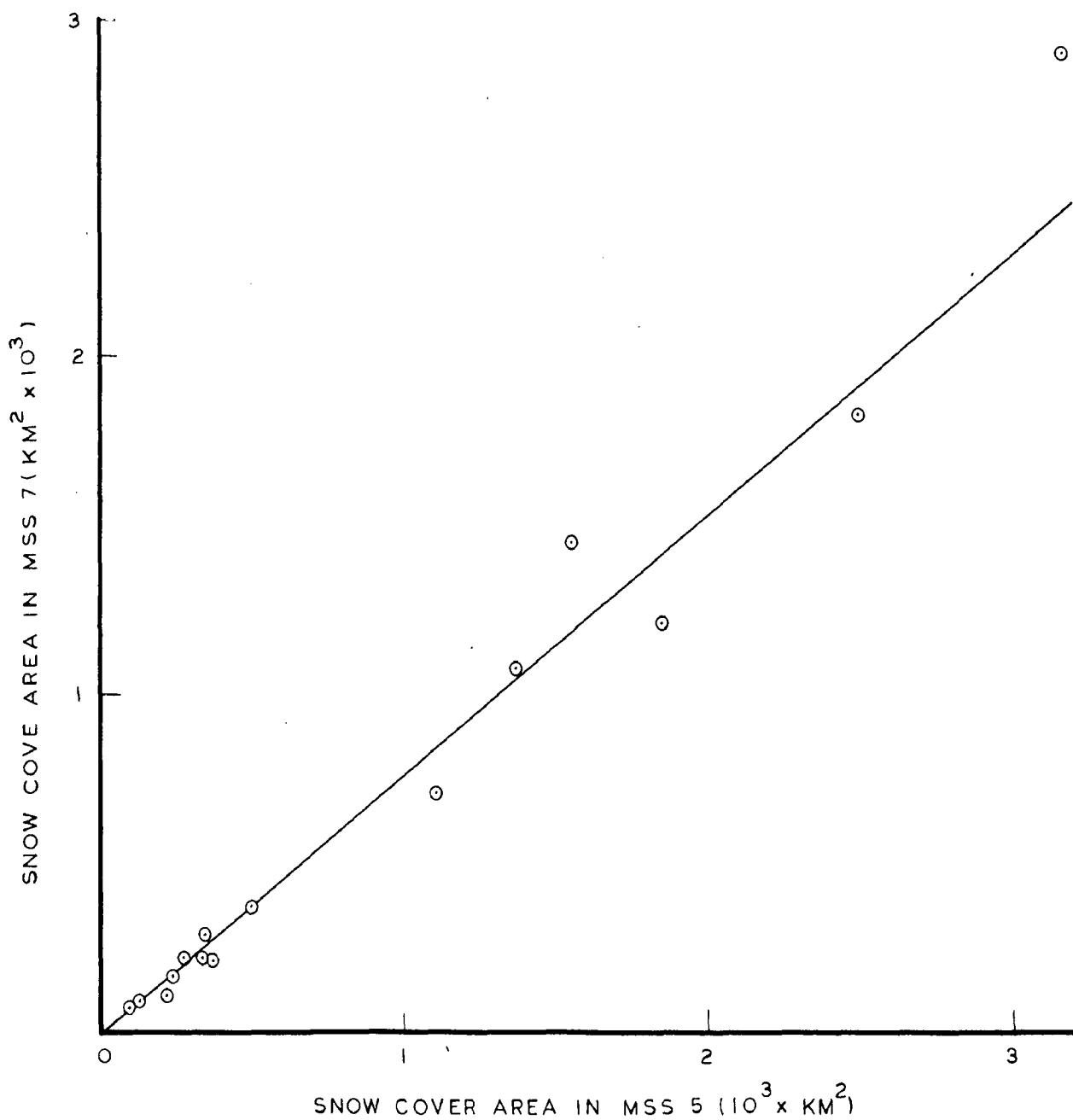


FIG. 4.4 SNOW COVER IN MSS 5 VS MSS 7 IN LARJI CATCHMENT

have maximum snow coverage in the months of February and March. (15) It is also interesting to note that the snow coverage in the imageries taken on the same day in Band 5 and Band 7 are not the same. These can be observed from the figures 4.1(i), 4.1(ii), 4.2(iii), 4.2(iv), 4.2(v) and 4.3(vii).

These imageries in the infra-red Band 7 indicates less snow than in those of the visible Band 5. These values of areal extent of snowcover as measured on Band 5 and Band 7 LANDSAT imageries at 1:100,000 scale have been tabulated in table No. (4.3) and also plotted as a graph in figure (4.4). A linear trend inclined at an angle of 37° from the X-axis of the HSS 5 has been observed from the graph.

4.4.3. THE SNOW COVER AND RUNOFF RELATION.

The imageries of the months of March indicate the extent of snow coverage in the basin before the melting season. Therefore, it is possible to get a relationship between the snow coverage of the basin before the melting season and the subsequent seasonal melt runoff. From the figures (4.3(vii), (viii), (ix) and (x)) the snow-covered areas of the sub-basins have been measured and the values tabulated in table No. (4.3). The cumulative sum of daily discharges in the months March-April-May as shown in table (4.4) and the snow coverage have been

C. A. . . .

22501150

22502800

22503000

16950050

57907395

37902550

13167000

50121200

50121300

31121200

31121300

31121400

31121500

31121600

31121700

31121800

356*95

343*50

354*85

352*65

352*40

352*35

352*30

352*25

352*20

352*15

352*10

352*05

352*00

352*95

352*90

352*85

357*55

357*50

357*45

357*40

357*35

357*30

357*25

357*20

357*15

357*10

357*05

357*00

357*95

357*90

357*85

357*80

357*75

357*70

357*65

357*60

357*55

357*50

357*45

357*40

357*35

357*30

357*25

357*20

357*15

357*10

357*05

357*00

357*25

357*20

357*15

357*10

357*05

357*00

357*95

357*90

357*85

357*80

357*75

357*70

357*65

357*60

357*55

357*50

357*20

357*15

357*10

357*05

357*00

357*95

357*90

357*85

357*80

357*75

357*70

357*65

357*60

357*55

357*50

357*45

SALY

Country wise analysis of daily disappearance for the same month-period

1	2	3	4	5	6	7
1975	March	1189.96	644.8	545.16	2460156500	1460156500
	April	1635.94	624	1011.94	2622948400	1003104900
	May	2533.94	644.3	1989.14	5059472500	1942977400
1976	March	1121.66	699.36	422.3	1131088360	1131088360
	April	1701.61	675.8	1024.81	2656307500	3787395800
	May	2526.57	699.36	1927.21	5161939200	3949235000
1977	March	789.41	699.36	90.05	241169920	241169920
	April	946.81	675.3	270.01	699865920	941055840
	May	1811.49	699.36	3112.12	9335502200	9276558040
1977	March	3712.72	1497.61	2215.11	5932950600	5932950600
	April	6241.7	2449.3	4792.4	12421900000	18354850600
	May	10139.18	1497.61	8661.57	23145591000	41500441600

1976	March	4591.08	1470.33	3120.75	1645.79	556.91	1491627700	11602025280
	April	7324.57	1422.90	5901.67	1592.70	1180.27	3209239800	4350887500
	May	8931.34	1470.33	7461.01	19983569184	4331.7	1645.79	1491627700
1977	March	1202.7	1645.79	3120.75	1470.33	4331.7	19983569184	43639313984
	April	2772.97	1592.70	1180.27	1422.90	5901.67	15297128000	23655744000
	May	3977.41	1645.79	1470.33	8931.34	1470.33	7461.01	19983569184
1978	March	623.08	139.3	281.58	281.58	275.48	1273.63	32091248000
	April	1549.03	2264.45	281.58	281.58	289.00	217.31	774057600
	May	2549.03	2264.45	281.58	281.58	289.00	217.31	774057600
		623.08	139.3	281.58	281.58	275.48	1273.63	32091248000
1979	March	5977.41	1645.79	1470.33	8931.34	1470.33	7461.01	19983569184
	April	1549.03	2264.45	281.58	281.58	275.48	1273.63	32091248000
	May	2549.03	2264.45	281.58	281.58	275.48	1273.63	32091248000
		623.08	139.3	281.58	281.58	275.48	1273.63	32091248000
1980	March	734.6	210.3	534.30	534.30	534.30	213043200	1358985800
	April	8931.34	210.3	534.30	534.30	534.30	213043200	1358985800
	May	999.88	217.31	782.57	782.57	782.57	2096033400	62229078600

7

6

5

4

3

2

1

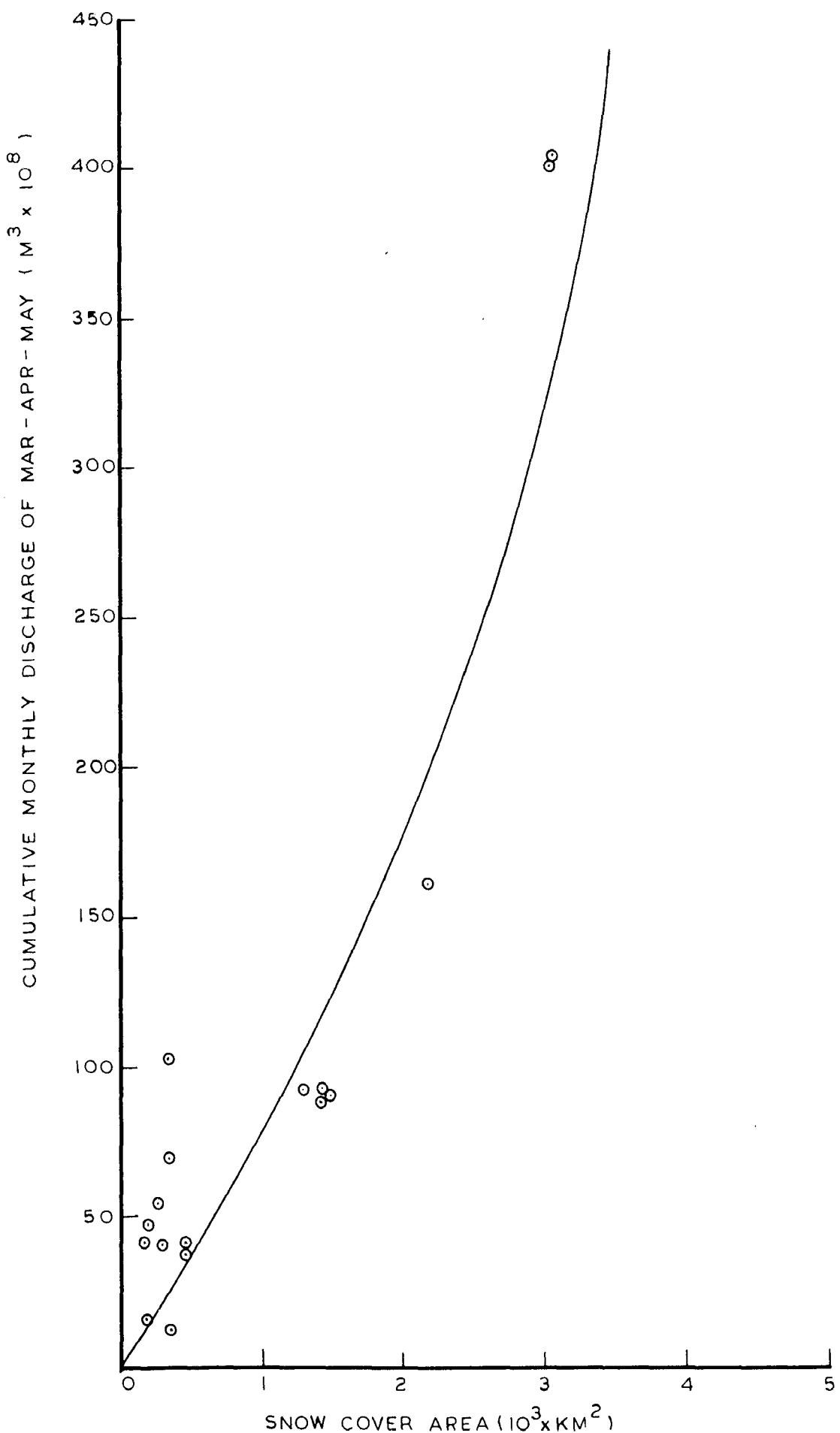


FIG. 4·5 RELATION BETWEEN THE SNOW COVERAGE AND CUMULATIVE MONTHLY DISCHARGE OF MONTHS MARCH-APRIL-MAY IN LARGI CATCHMENT

plotted as shown in figure (4.5). An exponential curve can be fitted to these limited plotted points. More discharge data of 1973, 1975, 1976 and 1977 have been used. A better relationship can be got by using more number of years of data.

The snow covered areas in the basins and the cumulative sum of average discharges obtained from the maximum and minimum discharges of the months March-April and May as shown in table no. (4.5) have been also used in getting a similar relationship. Here an exponential curve also can be fitted.

As shown in figure (4.6). It is giving a better fit than in the former case. From these curves it is evidently concluded that with more snow coverage more seasonal runoff can be expected.

No consideration of the change in the geological and geohydrological feature have been taken into account, where as this could change locally and affect the discharge.

4.5. METHODOLOGY FOR SNOWMELT RUNOFF COMPUTATION DURING MELT SEASON (MARCH TO MAY).

The basic phenomena involved in the snowmelt process has been of major interest to hydrologists and others involved in stream flow forecasting. It is

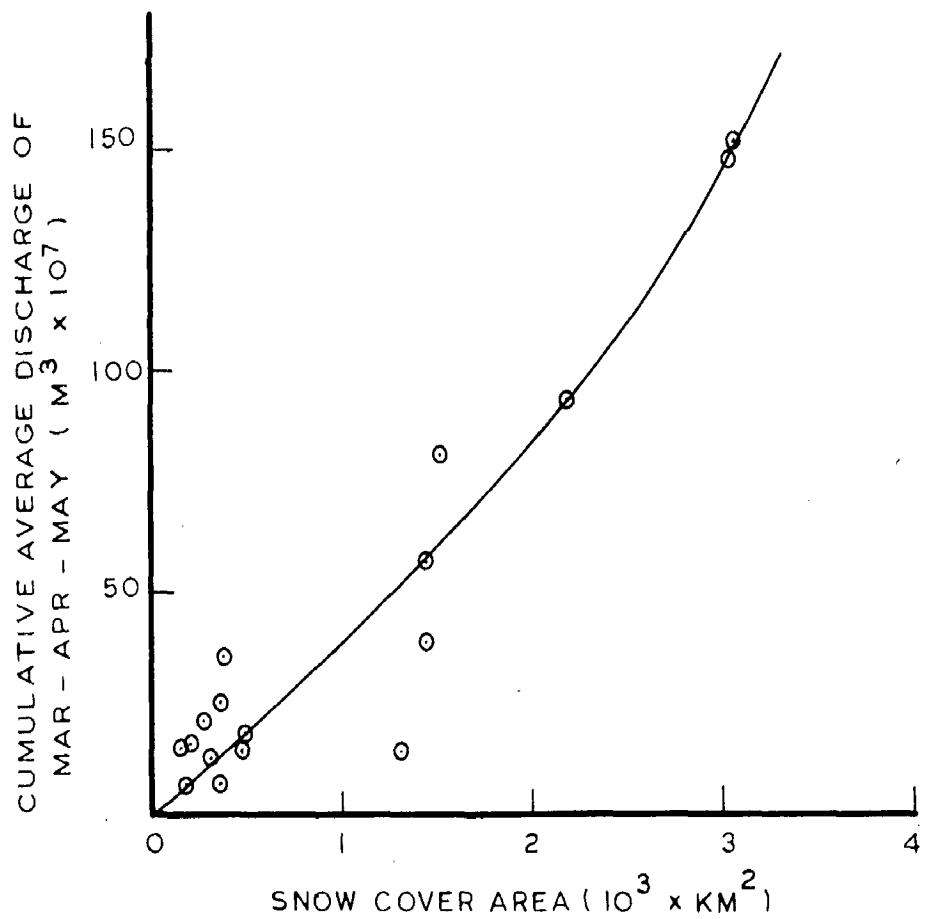


FIG. 4.6 RELATION BETWEEN THE SNOW COVERAGE AND CUMULATIVE AVERAGE DISCHARGE OF MONTHS MARCH - APRIL - MAY, IN LARGI CATCHMENT.

important that the hydrologist understand the nature and distribution of snowfall and mechanism involved in the snowmelt process if he is to make adequate estimates of the stream flow derived from this source.

Usually limited data is available in mountainous basins and generally temperature and precipitation are the only available ones.

In each basin the snow accumulation season (December to February) and the snowmelt season (March to May) are considered for the forecasting of the snowmelt runoff. During these seasons the basins can have permanent snow-covered area, temporary snow-covered area, and the nonsnow-covered area.

The aerial photography can provide the extent of snow coverage in such remote and inaccessible basins.

Due to the great elevation range, differences in temperature and precipitation have to be taken into consideration.

6.5.1. ASSUMPTIONS IN THE METHODOLOGY.

1. The catchment is divided into altitudinal bands to take into account the orographic effect on the precipitation and the temperature.

2. The contribution to snowmelt comes from both the temporary and permanent snow-covered areas.
3. The accumulation season is considered to extend from November to around Mid-March and the snow-melt season from around mid-March to May. This is to be judged by considering the meteorological conditions prevailing in the catchment.
4. The precipitation, rain as well as snow, received by the different altitudinal bands are substantially affected by the orographic effect. Therefore, each band gets different amount of precipitation increasing with the altitude.
5. During the accumulation season the snowmelt is negligible. The storage of snow in the various altitudinal band starts depleting during the melt season only.
6. The losses accounted from the snowmelt as well as the rainfall on the snow-covered area will including those due to evaporation and infiltration
7. The predominant factors affecting snow-melt ratio are the air temperature and rainfall. The other processes influencing heat transfer to the snow pack are relatively less important and are not taken into consideration.

6. During the accumulation season the base station can occasionally record rainfall and snow fall on the same day. During such time since the temperature is near freezing point, the rain falling on the accumulated snow pack is considered to be frozen through contact with the colder underlying snow. However, the higher altitudes can get snowfall instead due to the orographic effect.

4.5.2. THE DIVISION OF THE BASIN

The basin is divided into the temporary snow-covered zone, the permanent snow-covered zone, and the nonsnow-covered zone, provided that the basin is not completely covered by snow. These divisions can be made with the help of regular satellite or aerial photographs.

4.5.3. THE TEMPERATURE IN THE ELEVATION ZONES

The base station is used to provide input temperature data to the various elevation zones. The basin with a certain contour interval is divided into a number of elevation zones, the median heights of which are considered to be representative of the zone. The number of zones will depend on the size of the catchment and the availability of the contour maps.

By use of the lapse-rate approach, the

daily temperatures for each zone are computed by extending data from the base station.

$$\theta_i = \theta_b - \gamma (h_i - h_b) \quad (4.1)$$

where θ is the daily mean temperature (in °C)

h is the elevation (in m)

i and b are subscripts, referring to elevation zone i and the base station respectively

γ is an empirically derived coefficient which represents the lapse rate.

4.5.4. THE PRECIPITATION IN THE ZONES

The precipitation both rain as well as snow in the mountainous basin increases with height due to orographic effect. Instead of using a single value of the precipitation recorded at the base station, some reasonable incremental values of precipitation for the different elevation zones are assigned for taking into account the orographic effect. The precipitation received by a given zone will be given by the equation,

$$H_i = H_b + H_c \quad (4.2)$$

where H_i is the daily precipitation received by the zone i in mm.

H_b is the daily precipitation recorded at the base station in mm.

Δ_p is the incremental values of the precipitation
with elevation in mm per Xm

4.5.5. THE ACCUMULATION OF SNOW IN THE ELEVATION ZONES

Snowfall occurring from November to around mid-March can be taken into account as the stored water in the form of snow, keeping in view that negligible amount of snowmelt occur during this period as temperature generally remains near freezing point. Different amounts of snow is stored in various elevation zones due to the orographic effect on the snowfall.

4.5.6. COMPUTATION OF SNOWMELT

Since there is scanty rain during the snowmelt season, the flow in the streams are mainly contributed from the snowmelt.

(A) The degree-day method

The daily snowmelt depth in centimeter using the degree day method is given by

$$N = a \cdot T_d$$

where 'N' is the daily snowmelt in cm

'a' is the degree day factor in $cm \cdot ^\circ C^{-1} d^{-1}$

' T_d ' is the number of degree days in $^\circ Cd$.

(2) Snowmelt due to rain

The depth of water melted by rain in centimeter is given by

$$D = H \frac{T_x}{80} \quad (4.4)$$

Where D is the depth of water melted by rain in cm.

H is the rainfall depth in cm.

T_x is the temperature of rain in °C, which can be represented by the wet bulb temperature

80 is the ratio of heat of fusion of ice to the specific heat of water (dimension : °C)

Now taking into consideration an elevation zone A, the daily snowmelt in (m^3/s) is with the degree day method given by,

$$Q_A = s_A \cdot T_{dA} \frac{A_A}{86400(s)} \quad (4.5)$$

Where Q_A is the daily snowmelt in m^3/s

s_A is the degree day factor in $m^{\circ}C^{-1}d^{-1}$

T_d is the number of degree days in deg-cd
Snowmelt

A_A is the area of zone A in m^2

86,400(s) is the number of seconds per day, which converts the daily snow melt volume into daily discharge.

The snowmelt due to the rain in the elevation zone A is given by

$$Q_{RA} = H_A \cdot \frac{T_{RA}}{80} \cdot \frac{A_A}{86400(s)} \quad (4.6)$$

Where Q_{RA} is the snowmelt due to rain in zone A
in m^3/s

H_A is the rainfall depth in m.

T_{RA} is the temperature of the rain in zone A
in $^{\circ}\text{C}$

A_A is the area of the zone A in m^2

86400 (s) is the number of seconds per day

80 is the ratio of the heat of fusion of
ice to the specific heat of water
(dimension : $^{\circ}\text{C}$)

Therefore, the total daily snowmelt discharge
in m^3/s for the combined effect is given by

$$Q_{RA, RA} = Q_A + Q_{RA} \quad (4.7)$$

The term Q_{RA} exists only if rain is there on
the particular day.

The snowmelt continues till all the snow has
completely depleted out of the zone. Therefore, it is

important to keep in account the daily balance of the equivalent water stored in the temporary zone.

4.5.7. TRANSFORMATION OF SNOWMELT TO RUNOFF

In most cases, snowmelt calculations must be simplified owing to lack of detailed data on the energy balance. However, in accuracies which might result can be overshadowed by complications involved in extrapolating snowmelt relations from one point to the whole basin in order to determine the runoff. Apart from necessity of extrapolating meteorological data to the various parts of the basin, the retention of the meltwater on its way to the outlet must be considered in a broad variety of conditions.

In snow-lysimeter studies, the melt water is only delayed by percolation through the snow. Consequently the daily runoff ~~and~~ coincides with the daily snowmelt. Owing to the larger area of a basin and owing to the subsurface runoff, only a part of melt water appears in the outflow within the next 24 hours. If no further snowmelt were to take place, the remaining melt water would follow on subsequent days as recession flow according to the equation,

$$Q = Q_0 e^{-kt} \quad (4.8)$$

where Q_0 is the initial discharge of the snowmelt recession curve

k is the recession coefficient

t is the time as dimensionless number of time increments.

If k refers ~~to~~, for example, to discharge on two consecutive days, ~~K~~ is the number of days.

Runoff R is obtained by integrating the hydrograph.

$$R = \int_0^t Q dt = \int_0^t Q_0 k^t dt$$

$$= Q_0 \left[\frac{k^t}{k - 1} \right]_0^t = Q_0 \frac{k^t - 1}{k - 1} \quad (4.9)$$

With Q in units of m^3/s , R in m^3 and k referring to 1-day interval, the runoff R_1 in the first 24 hours starting with Q_0 and ending with Q_t is

$$R_1 = Q_0 \frac{k-1}{k} \times 86400 \text{ (s)} \quad (4.10)$$

The total run of R_t for $k < 1$, $t = \infty$ is

$$R_t = Q_0 \frac{-1}{k} \times 86400 \text{ (s)} \quad (4.11)$$

Substituting $Q_0 = -k \cdot R_t$ into equation (4.10)

$$R_1 = R_t (1-k) \quad (4.12)$$

Recalling the initial assumption that no further snowmelt takes place, R_t equals the first days snowmelt

(disregarding runoff losses). Thus the recession coefficient k determines (according to equation (4.12)) which part of the meltwater flows off in the first 24 hours.

If the successive daily runoff volumes are regarded as geometric series, equation (4.12) is simply derived as follows:

$$R_t = R_1 \frac{1-k^{t-1}}{1-k} = R_1 \frac{1-1}{k-1} \quad (4.13)$$

$$R_1 = R_t \frac{k-1}{1} = R_t (1-k) = M_1 (1-k)$$

Where M_1 is the daily snowmelt. Considering now that further snowmelt will take place on the second day, the total daily runoff is calculated as

$$R_2 = M_2 (1-k) + R_1 k \quad (4.14)$$

The practical computation values of k must be derived from the discharge data of the watershed. Thus taking into account the retention of melt water, the daily snowmelt runoff comprises of two components:

$$R_n = M_n (1-k) + k R_{n-1} \quad (4.15)$$

where R_n is the runoff on the n^{th} day in m^3
 M_n is the snow melt on the n^{th} day in m^3

n is an index indicating the sequence of days
 k is the recession coefficient in the melting
 period and is given by the relation,

$$k = \frac{R_n}{R_n - 1}$$

4.5.B. THE DAILY DISCHARGE FROM ALL THE VARIOUS ZONES

A particular zone A is first considered. Dividing the equation (4.15) throughout by 86400 seconds to get the discharge and snowmelt in m^3/s and including the snowmelt due to rainfall, the following equation is arrived at as given below.

$$(Q_s)_n = (Q_{A, EA})_n (1-k) + k (Q_s)_{n-1} \quad (4.16)$$

Where Q_s is the daily snowmelt discharge in m^3/s

k is the recession coefficient with 1 day interval.

$Q_{A, EA}$ is the total daily snowmelt discharge

(m^3/s) obtained by the degree-day method and due to the rain as given in equation (4.7)

Taking into account the losses and the retention of the snowmelt, the daily snowmelt discharge contributed by all the snow-covered zones, is given by the equation below

$$(Q_s)_n = C (Q_{A, EA} + Q_{B, EB} + Q_{C, EC} + Q_{D, ED}) (1-k) \\ (Q_s)_{n-1} \times (4.17)$$

Where Q_s is the daily snowmelt discharge in (m^3/s)

$Q_{A, ra}$, $Q_{B, rB}$, $Q_{C, rC}$, and $Q_{D, rD}$ are the total daily snow-melt discharge in m^3/s obtained due to rain and by the degree day method in four respective zones A, B, C, and D that have been assumed.

$Q_{P, rp}$ is the melt due to rain + temp. effect - in the permanent snow covered area.

k is the recession coefficient for 1 day interval.

n is an index expressing the sequence of day

C is an k coefficient accounting for the losses.

The rainfall during the snowmelt season is usually scanty and thus most of the flow in the river is contributed by the snowmelt. Therefore, with the degree day method snowmelt can be calculated with various different values of the degree-day factor so that the snowmelt hydrograph obtained from the daily computed discharges by the equation (4.17) match the observed direct runoff hydrograph (i.e. excluding the base flow). A typical year with scanty rain in the melt season is to be analysed first. With many trials the most suitable values of the degree-day factor for the month of March and April and that for the month of May are to be arrived at. The month of May having higher temperatures gets the higher value of the degree-day factor. These values of degree-day factors can be applied for computing the daily snowmelt discharge for other years provided that no large deviation in the meteorological conditions prevail from one year to other.

4.3.9. COMPUTATION OF THE RUNOFF COEFFICIENTS FOR THE TEMPORARY SNOW-COVERED AREA AND THE NONSNOW-COVERED AREA.

The cumulative sum of daily discharges due to snowmelt $\leq Q_s$ (in m^3/s) and the cumulative sums of gauged discharges excluding the base flow $\leq Q_0$ (in m^3/s) during the melt season can be calculated.

The difference between these values will give the amount of discharge $\leq Q_R$ (in m^3/s) contributed from the rainfall during the melt season.

$$\leq Q_R = \leq Q_0 - \leq Q_m \quad (4.18)$$

Generally during the melt season $\leq Q_R$ will be a small quantity in comparison to $\leq Q_m$.

This amount contributed by the rainfall must equal to two components as given below:

$$Q_R = C_1 \frac{(\leq H_1)}{86400} A_1 + C_2 \frac{(\leq H_2)}{86400} A_2 \quad (4.19)$$

Where $\leq Q_R$ is the total discharge contributed from the rainfall in m^3/s during the melt season.

C_1 is the runoff coefficient which takes into account loss due to evaporation from the temporary snow-covered area A_1 in m^2 .

C_2 is the runoff coefficient to consider the loss due to evaporation and infiltration from the nonsnow-covered area A_2 in m^2 .

ΣH_1 and ΣH_2 are the total of the daily rainfall depth
(m) in the temporary snow covered area and the non-snow
covered area respectively during the melt season.
86400 is the number of seconds in a day which converts
the volume of rainfall (m^3) into discharge(m^3/s)

Working with different years similar equations like that
of equation (4.19) are obtained. The solution to such
linear equations can be done by an algebraic method as
outlined in the subsequent paragraph.

4.5.10. THE ALGEBRAIC METHOD TO SOLVE A SET OF LINEAR EQUATIONS.

In the mathematical discussion of the
results of observations, it is required to derive from
the data the best or plausible results which they are
capable of affording.

When the quantities which are observed
directly are function of several unknown quantities which
are to be determined, the problem can be generally reduced
to a formulation such as the following.

The immediate problem is to find values
for a set of unknown quantities X, Y in such a way that
a set of given equation.

$$\begin{aligned} a_1 X + Y &= n_1 \\ a_2 X + Y &= n_2 \\ a_3 X + Y &= n_3 \end{aligned} \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} \quad (4.20)$$

Called the equation of conditions may be satisfied as nearly as possible, when the number of equations is greater than the number of unknowns X, Y and the equations are not strictly compatible with each other.

The solution to such linear equation is may be done in the following steps.

1. Multiply each linear equation by its own constants a_1, a_2, \dots, a_n and then add them to get a single equation i.e.

$$a_1^2 X + a_1 Y = a_1 n_1$$

$$a_2^2 X + a_2 Y = a_2 n_2$$

$$a_n^2 X + a_n Y = a_n n_n$$

$$(a_1^2 + a_2^2 + \dots + a_n^2) X + (a_1 + a_2 + \dots + a_n) Y = (a_1 + a_2 + \dots + a_n) n_n \quad (4.21)$$

2. All the linear equations may be added as such to obtain a single equation as

$$(a_1 + a_2 + \dots + a_n) X + Y = (n_1 + n_2 + \dots + n_n) \quad (4.22)$$

Now equation (4.21) and (4.22) can be solved simultaneously to get the values of X and Y

4.5.11. SNOWMELT DISCHARGE INCLUDING THE RAINFALL RUNOFF

Part of the rainfall on the temporary snowcovered area also flows along with the melt water. With this consideration the daily discharge can be expressed as

$$(Q_{sx})_n = (Q_s + Q_x) (1-k) + (Q_{sx})_{n-1} k \quad (4.23)$$

Where Q_{sx} is the daily discharge in m^3/s due to the melting of snow and the daily discharge in m^3/s contributed by the rain, if any, on the temporary snow-covered area.

$$Q_x = \frac{C_1 H_1 A_1}{86400} \quad (4.24)$$

Where Q_x is the discharge contributed by the rainfall on the temporary snowcovered area

C_1 is the runoff coefficient accounting the loss in the temporary snow covered area A_1 in m^2

H_1 is the rainfall in m in the temporary snow covered area.

86400 is the number of seconds in a day.

Using the equation (4.23) hydrograph can be plotted. The daily discharge (m^3/s) due to the rainfall, if any, falling on the nonsnow-covered area is given by

$$Q_y = \frac{C_2 H_2 A_2}{86400} \quad (4.25)$$

Where Q_y is the discharge contributed by the rainfall on the non snowcovered area.

C_2 is the run off coefficient in the snow-covered area A_2 in m^2

H_2 is the rainfall in m in the non-snow-covered zone.

86400 is the no. of seconds in the day.

This discharge Q_y can be superimposed on the same day on the hydrograph obtained by equation (4.23), if the time of the concentration of catchment, provided small and having appreciable gradient, is less than a day. Hence the the total daily discharge thus obtained is

$$Q_{(total)} = (Q_{ex}) + (Q_y) \quad (4.26)$$

The hydrograph thus obtained by using the equation (4.26) should lead to a better agreement with the observed hydrograph excluding the base flow.

This methodology can be used in small remote catchments where data are limited. Usually a valley station considered as the base station provides the input data to the computation of the daily snowmelt discharge. This methodology has been extended to be used in the Hanali catchment.

4.4 ANALYSIS OF BEAS CATCHMENT FOR SNOWMELT RUNOFF:

The hydrological condition of the Himalayan catchments is a complex one, since most of them are partly covered with snow at the higher elevation, and rain fed, at lower elevation.

The weather system that generally causes precipitation in the Himalayan regions are the Monsoon and the western disturbances. The year in the Beas catchment may be divided into the following four seasons.

a) The snow accumulation period.

This period refers to the months from December to mid March. Precipitation in the form of snow and sleet, which generally occurs in the catchment is associated with the movement of the Western Disturbances across the region. The flow in the Beas catchment is mainly due to the groundwater supplemented by some rain and snowmelt in the lower hilly region.

b) The snowmelt period.

This period refers to the months from around mid March to mid June. The freezing level is mostly maintained in the catchment upto ^{mid} March, and the subsequent lifting of the freezing level in this period due to above normal heating causes heavy snowmelt. Therefore, high inflow into the river are observed.

c) The monsoon period.

This period spans from mid June to mid September. Basin catchment receives bulk of its annual rain during this period.

d) The groundwater period.

This period spans from October to mid February. During this period, virtually, all the precipitation is in the form of snow, and consequently river flow is entirely dependent on ground water discharge.

4.6.1 THE HYDROLOGIC AND METEOROLOGIC DATA AVAILABLE FOR THE STUDY.

4.6.1.1 THE TEMPERATURE DATA.

for Manshi Station.

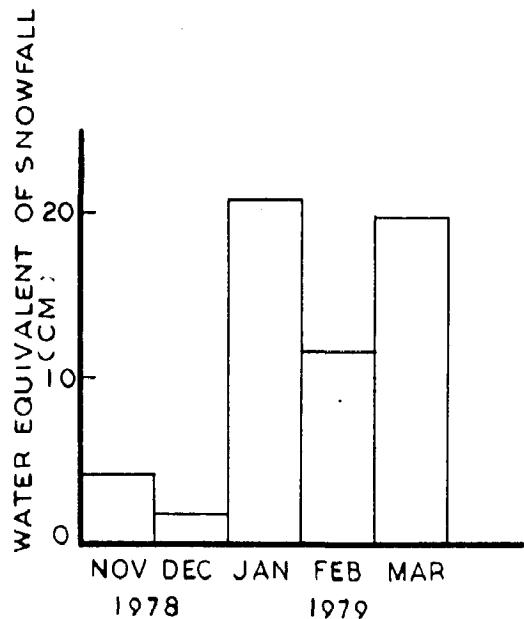
The daily maximum and minimum data has been collected for the years 1976, 1977, 1978 and 1979 from the Beas outlet; link project, Reservoir sub Division, Pandoh (H.P.).

The daily mean temperature for the melting period considered in this study is tabulated in Appendix (IV a, IV b, IV c) and plotted in figures 4.7(a), 4.7(b), 4.7(c).

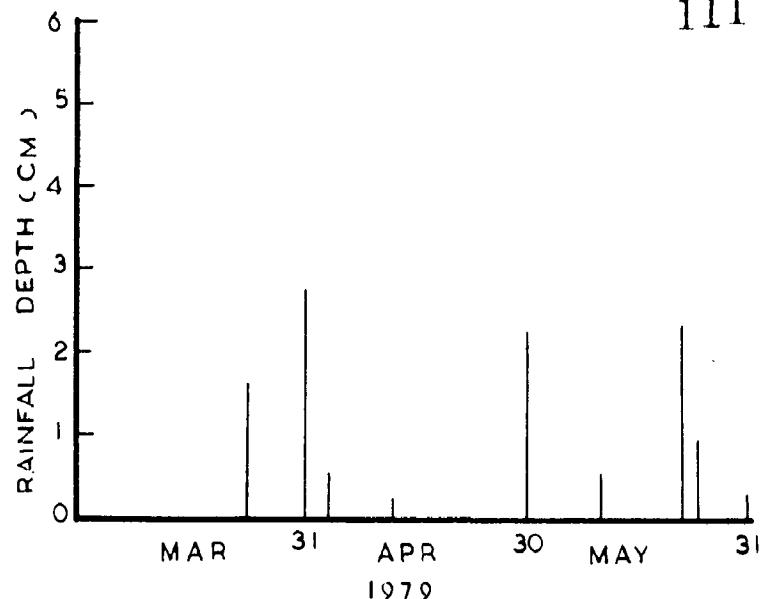
4.6.1.2 THE DISCHARGE DATA.

The daily discharge data collected for Parvati river, Sainj river, and Tirthan river from 1973 to 1979 has been obtained from the Director of Plant Design, Sunder nagar (H.P.).

The daily discharge data for the Nanell and Larji gauging stations for the period 1976 to 1979 and 1973 to 1979 respectively has been collected from the Beas outlet; link project, Reservoir sub Division, Pandoh (H.P.). The discharge data at Larji for the months



WATER EQUIVALENT OF
THE SNOWFALL IN MANALI



DAILY RAINFALL DEPTH
RECORDED MANALI

FIG. 4 8 (a)

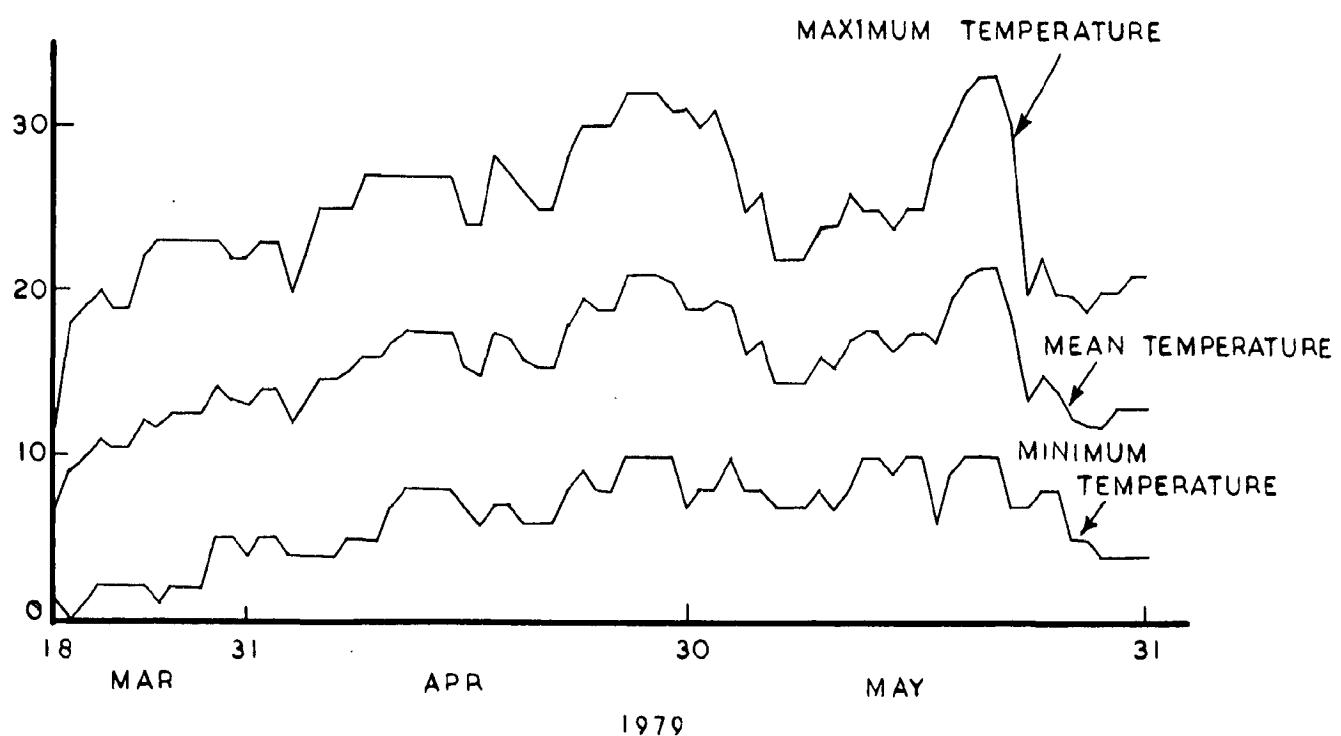
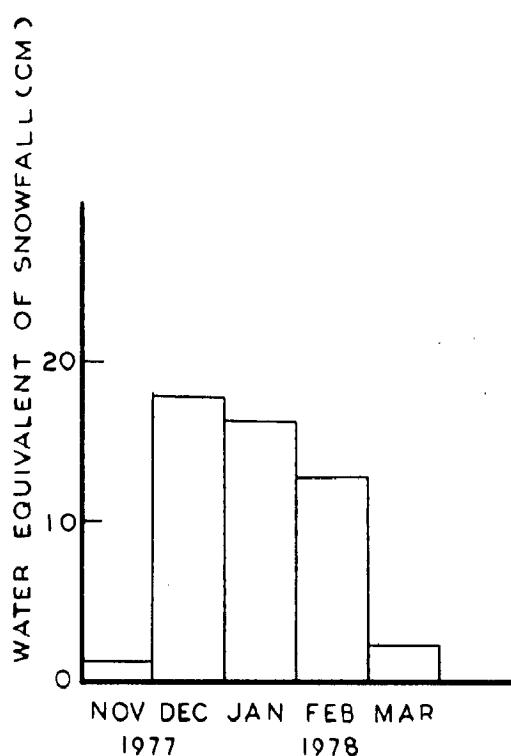
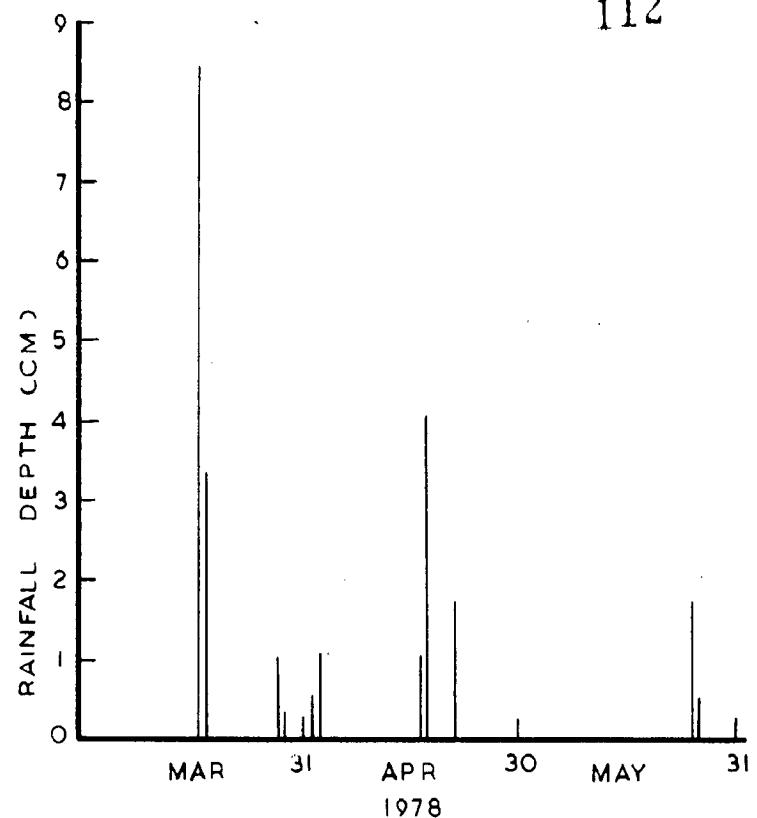


FIG.4.7(a) DAILY MAXIMUM, AVERAGE, AND MINIMUM TEMPERATURE
RECORDED IN MANALI



WATER EQUIVALENT OF THE
SNOWFALL IN MANALI



DAILY RAINFALL DEPTH
RECORDED IN MANALI

FIG. 4.8 (b)

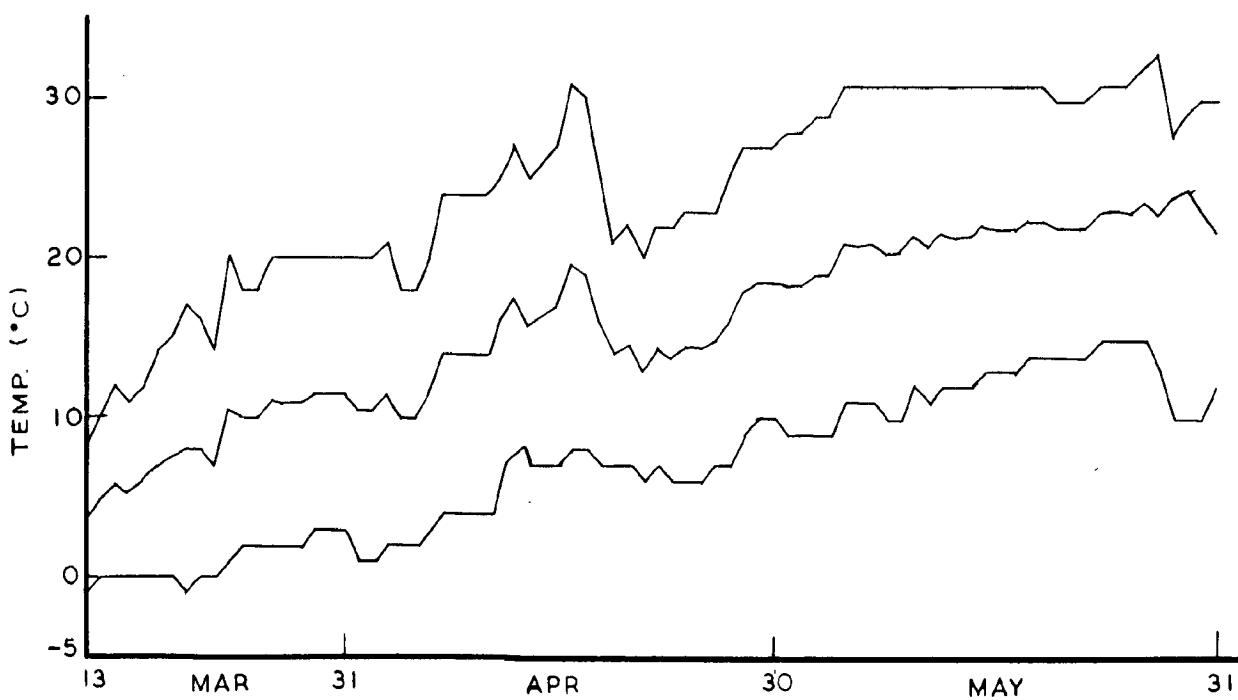


FIG 4.7(b) DAILY MAXIMUM, AVERAGE, AND MINIMUM TEMPERATURE
RECORDED IN MANALI

of April and May is missing for the year 1973. The daily discharge of Beas river at Manali gauging station excluding the base flow for the years 1977, 1978 and 1979 during the melting period considered in the study is tabulated in Appendix (XI a, XI b, XI c).

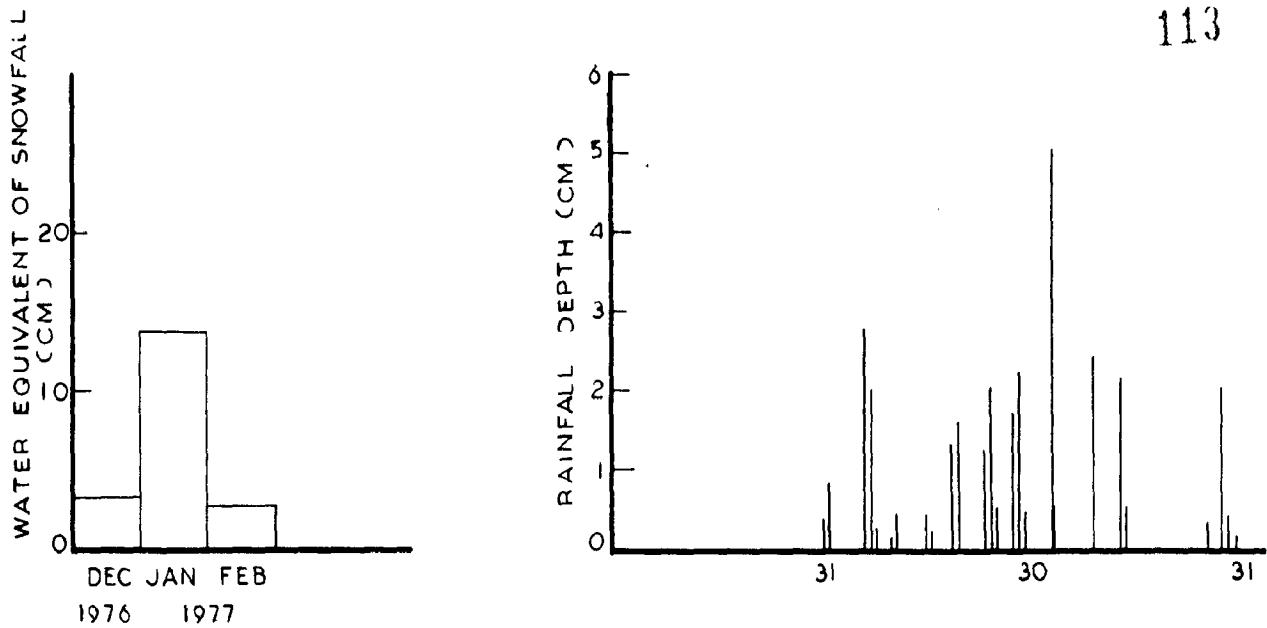
4.4.1.3 THE RAINFALL AND SNOWFALL DATA.

The rainfall and snowfall data for the Manali station for the years 1976 to 1979 was obtained through the office of S.E., Planning and Design (c)-^{hong} XI, H.P.S.B.B., Sunder Nagar (H.P.).

The data are tabulated in Appendix (V a, V b, V c, and VI a, VI b, VI c). The rainfall data and the water equivalent of the snowfall are plotted in the figures (4.8(a), 4.8(b), 4.8(c)).

4.4.1.4 TEMPERATURE IN DIFFERENT ELEVATION ZONES.

The Manali catchment has been divided into five elevation zones at the contour interval of 2000 ft (610 m) as indicated in the table no. (4.6) below.



WATER EQUIVALENT OF
THE SNOWFALL IN MANALI

DAILY RAINFALL DEPTH
RECORDED MANALI

FIG. 4.8(c)

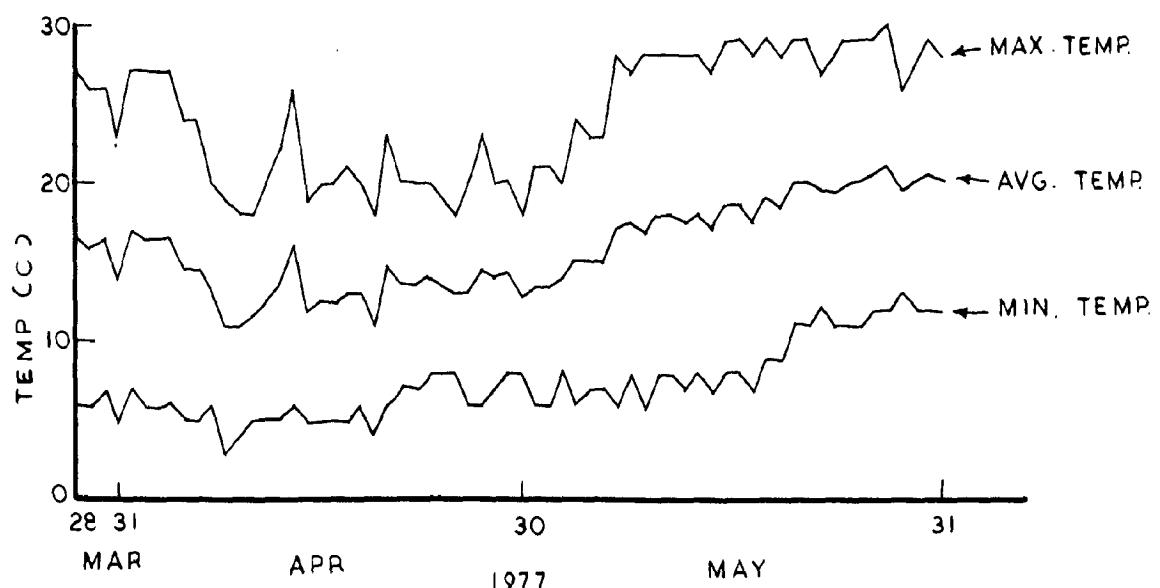


FIG.4.7(c) DAILY MAXIMUM , AVERAGE , AND MINIMUM TEMPERATURE
RECORDED IN MANALI

of April and May is missing for the year 1973. The daily discharge of Beas river at Manali gauging station excluding the base flow for the years 1977, 1978 and 1979 during the melting period considered in the study is tabulated in Appendix (XI a, XI b, XI c).

4.6.1.3 THE RAINFALL AND SNOWFALL DATA.

The rainfall and snowfall data for the Manali station for the years 1976 to 1979 was obtained through the office of S.E., Planning and Design (^{hmg} J.), M.P.S.E.B., Sunder Nagar (H.P.).

The data are tabulated in Appendix (V a, V b, V c) and VI a, VI b, VI c). The rainfall data and the water equivalent of the snowfall are plotted in the figures (4.8(a), 4.8(b), 4.8(c)).

4.6.1.4 TEMPERATURE IN DIFFERENT ELEVATION ZONE.

The Manali catchment has been divided into five elevation zones at the contour interval of 2000 ft (610 m) as indicated in the table no. (4.6) below.

Table no. (4.6) Area between elevation zones.

S.No.	elevation zones ft	Area of the zones (km^2)
1	6000 - 8000	23.53
2	8000 - 10000	49.89
3	10000 - 12000	104.61
4	12000 - 14000	109.65
5	14000 and above	81.73
Total		369.61

The medium height is considered to be representative of each elevation zone. Using the lapse rate for every 1000 ft as 1.53°C , ^(ref 22) the daily temperature for each zone is calculated by the equation (4.1) with respect to the temperature recorded at Manali station, which is considered to be the base station at a height of 5984.02 ft. Similar values of lapse rate as 1.53°C per 1000 ft (305 m) have been observed in the catchment by using temperature data of Manali and Bhuntar. Bhuntar has an elevation of 3555.25 ft (1084.4m) and is located further down stream of Manali (1830 m). The position temperatures obtained in the different zones by this lapse rate are tabulated in the degree - day column in the Appendix (X_a, X_b, X_c).

4.6.1.5 THE SNOW COVERED AREA FROM THE SATELLITE IMAGERY.

The only satellite imagery available for the year 1977 (Fig.4.9) has been incorporated in this study (19). The satellite imagery of scale 1:250,000 is shown in the figure (4.9).

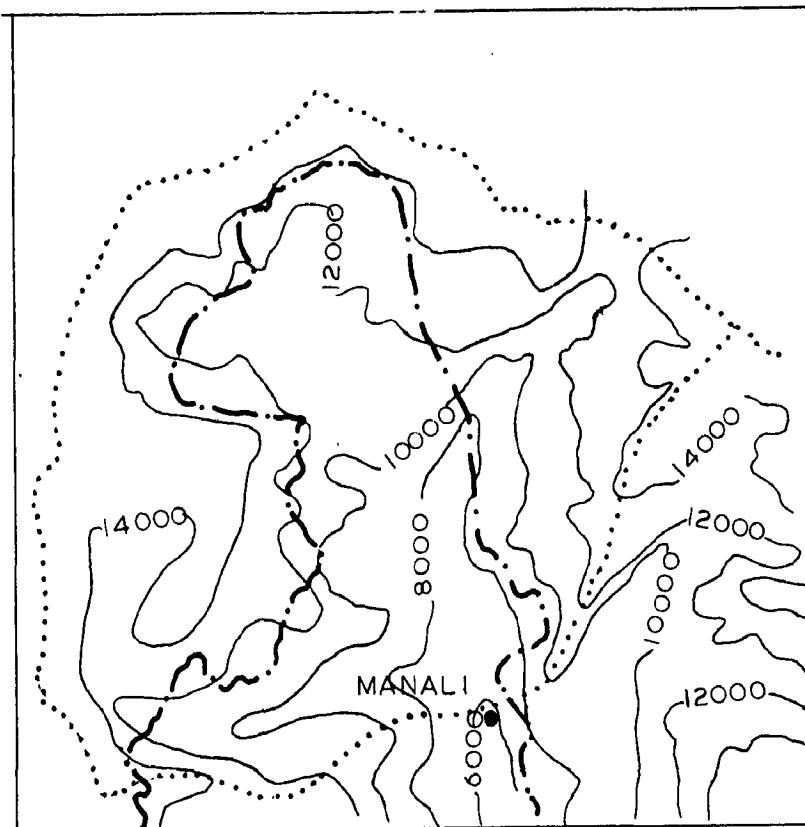
Since the other satellite imagaries of 1973, 1975 and 1976 indicate that Manali catchment ^{generally can be} is completely snow covered and since the snowfall of 1978 and 1979 is 2.5 to 3 times that of 1977, it is concluded that the Manali catchment is completely covered by snow before the melting period of 1978 and 1979.

(In '77 about 59% of the catchment is covered by snow.)

4.6.1.6 THE PRECIPITATION IN THE DIFFERENT ZONES.

a) It is found that the precipitation, snow as well as rain, in the mountainous regions increase with altitude due to orographic effect. The incremental values for the rainfall and snowfall for each 2000 ft rise in altitude have been adopted from the similar studies conducted in British Columbia (9); since no Indian data was available for estimating the same, the incremental values for the rainfall and snowfall are given in Appendix (VII a, VII b). The snowfall and rainfall depths for different elevation zones using these incremental values are given in Appendix (Va, Vb, Vc and VI a, VI b, VI c).

b) It is observed that Manali catchment generally receives the snowfall from November to around mid March. The snowfall occurring from November to around mid March has been considered to be accumulated as the stored water in the form of snow, keeping in view that negligible melt occurs during this season as



LEGEND

SNOW LINE - - - - -

MANALI CATCHMENT

CONTOUR LINE ~~~~~

FIG. 4.9 SNOW COVER MAP OF MANALI CATCHMENT
LANDSAT IMAGE DATE 27 MAR. 1977 MSS 7

SCALE - 1: 250,000

CONTOUR VALUES IN FEET

the temperature remains near freezing for elevations above 6000 ft. The water equivalent of the snowfall data during the accumulation period in Manali station has been worked out assuming a water equivalent value of 10%. This has been plotted in the figure (4.8(a), 4.8(b), 4.8(c))

The volume of water stored in the form of snow in each elevation zone is calculated with equation.

$$V_s = d \cdot H_s \cdot A_s \quad (4.651)$$

where V_s is the volume of water stored in the accumulated snow (m^3) in an elevation zone, d is the water equivalent, H_s is the computed depth of snowfall (m) for the considered zone & A is the area of the zone under consideration (m^2).

It is generally observed from the satellite imagery that the snowline remain near the altitude of 14000 ft. Hence we consider the permanent snow covered area to be above 14000 ft. For each elevation zone up to 14000 ft. the volume of water stored in the form of snow during the accumulation seasons is calculated with the equation (4.6.1). The volume of water stored in the form of snow during the accumulation period for different zones in different years are given in Appendix (VIII a, VIII b, VIII c)

4.6.1.7 THE RECESSION FACTOR

The daily recession discharge in Manali are plotted against the daily discharge on the previous day for the years 1977 to 1979 during the melting seasons as shown in figure (4.10).

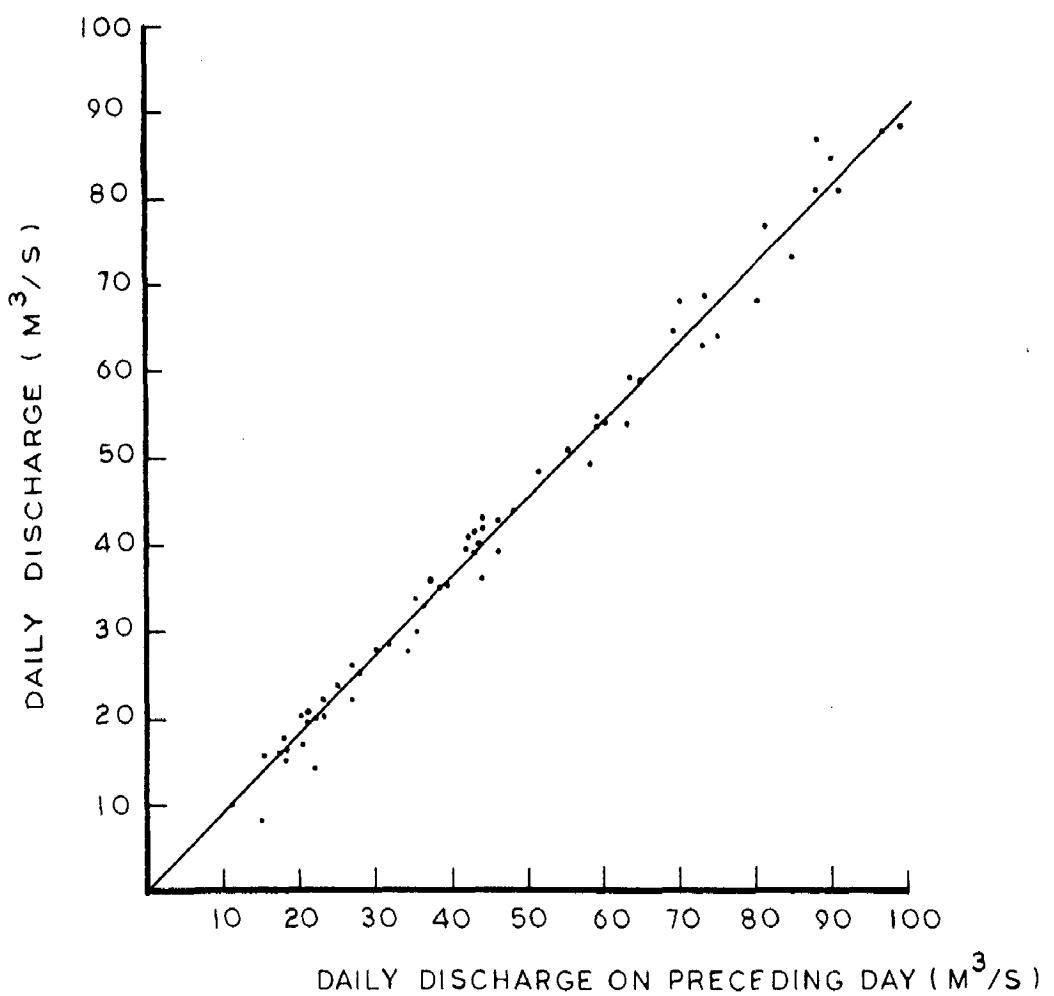


FIG. 4.10 DAILY RECESSION ANALYSIS FOR MANALI DURING SNOW MELT PERIOD 1976, 1977, 1978 AND 1979

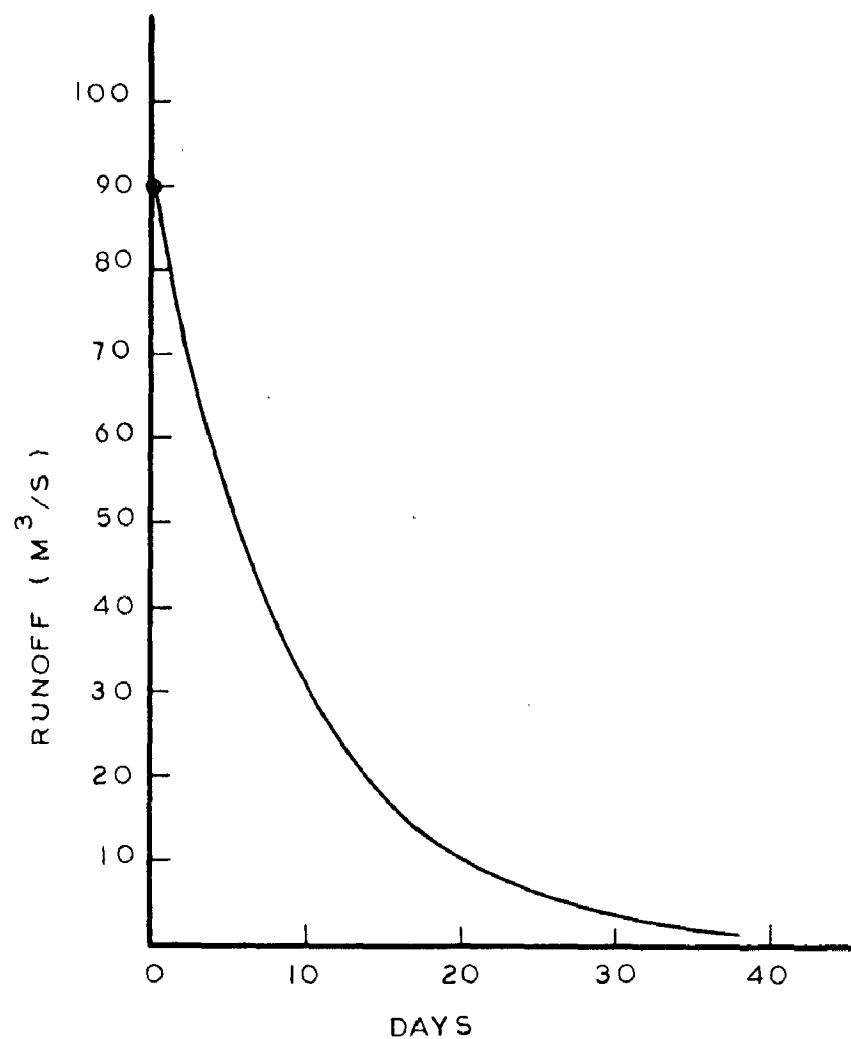


FIG. 4.II SNOW MELT - RUNOFF RECESSION
CURVE FOR MANALI

The recession factor k is derived from the slope of the straight line fitted to the plotted points as 0.90. Similar values also have been obtained in recession analysis carried out in St. Louis creek near Fraser, Colorado (4). The snowmelt runoff recession curve for Manali is shown in the figure (4.11).

4.6.1.8 THE BASE FLOW

The base flow for the considered year has been taken to be the minimum discharge in the groundwater period. During this period virtually, all the precipitation is in the form of snow and consequently river flow is entirely dependent on the ground water discharge. The base flows for the years 1977, 1978 and 1979 are observed to be $9.27 \text{ m}^3/\text{s}$, $11.79 \text{ m}^3/\text{s}$ and $14.27 \text{ m}^3/\text{s}$ respectively.

4.6.1.9 COMPUTATION OF SNOWMELT DISCHARGE

for both temporary & permanent zones
With the degree day method equation (4.5) snowmelt
is computed with different values of the degree day factor so that
the hydrograph plotted with these computed daily snowmelt discharge
is reasonable matching the observed direct runoff hydrograph.
The year 1979 has been treated first because it has less rainfall
as compared to 1978 and 1977 during the melting season. The
suitable value for degree day factor for the months of March and
April is working out to be $0.0018 \text{ cm}^{-1} \text{C}^{-1} \text{d}^{-1}$ and that for the

month of May as $0.00315 \text{ cm}^{-2} \text{C}^{-1} \text{d}^{-1}$. These values are coming around the average value of the ~~snowmelt~~^{degree day factor} as $0.0027 \text{ cm}^{-2} \text{C}^{-1} \text{d}^{-1}$ given in reference (23).

The month of May gets the higher value of the degree day factor since more snowmelt is to be observed as the temperatures in this month is relatively higher and persists for more hours of the day than the other two months. The degree day factor is also related to the snow density as has been discussed in chapter 2 from reference (3). The snow density in May due to heavy melting can have higher values than those of March and April.⁷ The melt due to the rainfall as computed by equation (4.6) is also included now. The melting of snow due to the rainfall in each zone is calculated and tabulated in Appendix (IX a), With the equation (4.7) the melt in all the zones are calculated and summed up. There are tabulated in the last column, under the elevation zone above 14000 ft. table, in Appendix (Xa). Now taking into account the retention effect and the losses due to infiltration and evaporation equation (4.17) is used to get the daily snowmelt discharge considering the melt from all the elevation zones. The losses in equation (4.17) is given a value of 10%. Hence the coefficient "C" in the equation (4.17) gets a value of 0.90. Such a value has been found and used in a similar study in ~~Glueckauf~~^{Disch HMA} water shed in Switzerland (9). These computed daily discharge are plotted against the observed direct runoff hydrograph.

The degree day factor depend on the density of snow. Old snow means higher density. ~~These~~ old snow has less albedo. Thus more radiation penetrates into the snow mantle to produce more melt. Thus the Month of May gets higher value of the degree day factor as compared to Mar - April.

as shown in figure (4.12 a) A reasonable agreement is observed. The daily calculated snowmelt discharge for the year 1977 and 1978 are also calculated. These are tabulated in the last column, under the elevation zone above 14000 ft table, in Appendix (X b and X c). The melt due to the rainfall effect in each zone for these years are calculated and tabulated in Appendix (IX b; IX c). The computed daily discharge are plotted against the observed direct runoff hydrograph as shown in figure (4.12.b, 4.12.c). The daily snowmelt discharge is calculated by the equation (4.17) and the values are tabulated in the 2nd column of Appendix (XI a, XI b, XI c)

4.6.1.D COMPUTATION OF THE RUNOFF COEFFICIENTS FOR RAIN ON THE SNOW-COVERED AREA AND THE NON-SNOW-COVERED AREA,

Taking into account the water budget for the concerned snow-covered melting period the difference between the cumulative sum of the daily observed discharge $\sum Q_{\text{O}}$, excluding the base flow and the cumulative sum of the daily snowmelt discharge $\sum Q_{\text{SM}}$, is equal to the total discharge contributed due to the rainfall $\sum Q_{\text{R}}$ as given by the equation (4.18) i.e.

$$\sum Q_{\text{R}} = \sum Q_{\text{O}} - \sum Q_{\text{SM}}$$

The total discharge $\sum Q_{\text{R}}$ can be written as

$$\sum Q_{\text{R}} = \frac{C_1 (\sum H_1) A_1}{86400} + C \frac{C_2 (\sum H_2) A_2}{86400}$$

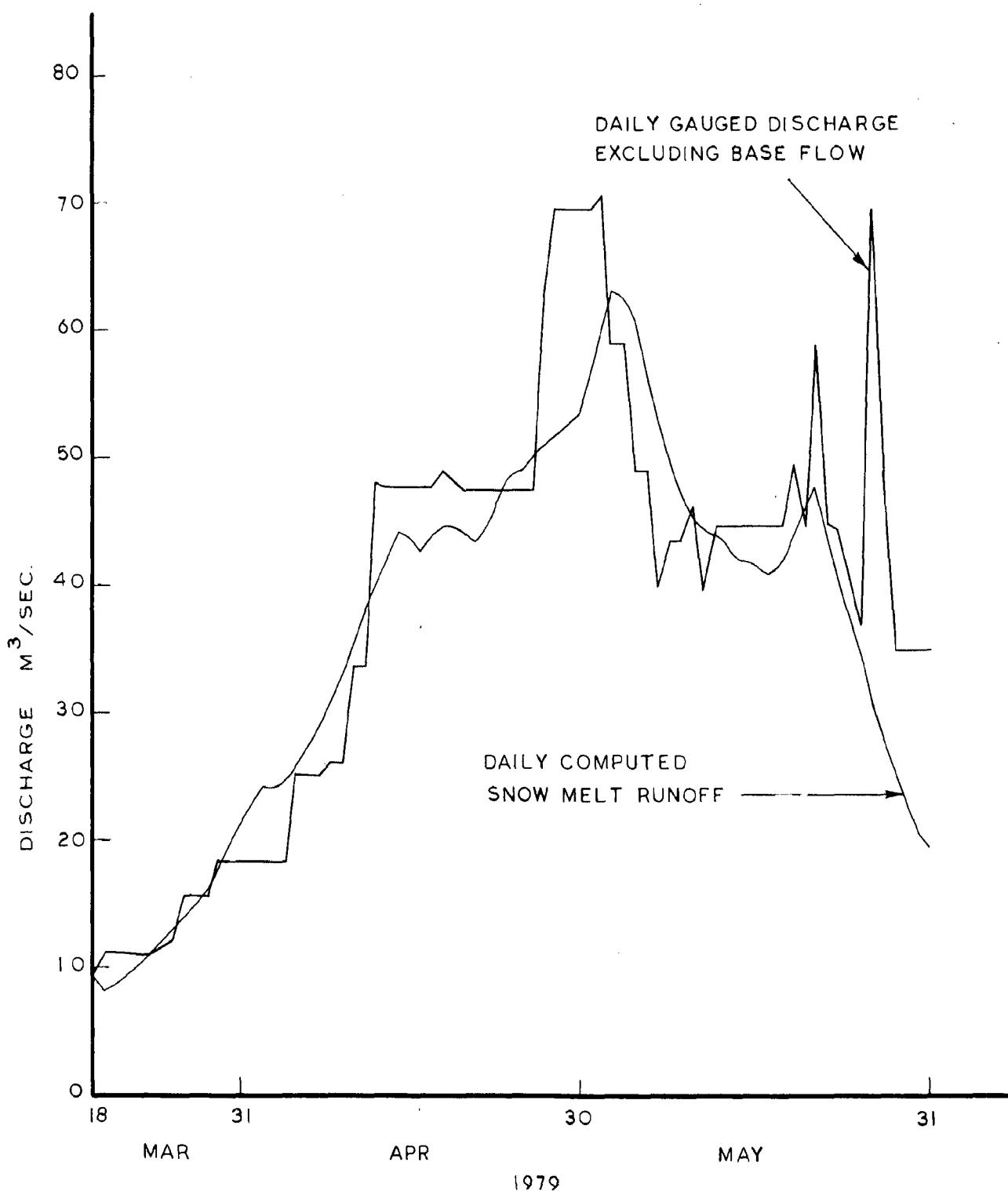


FIG.4.12(a) DAILY COMPUTED SNOWMELT RUNOFF AND DAILY GAUGED DISCHARGE (EXCLUDING BASE FLOW) IN MANALI

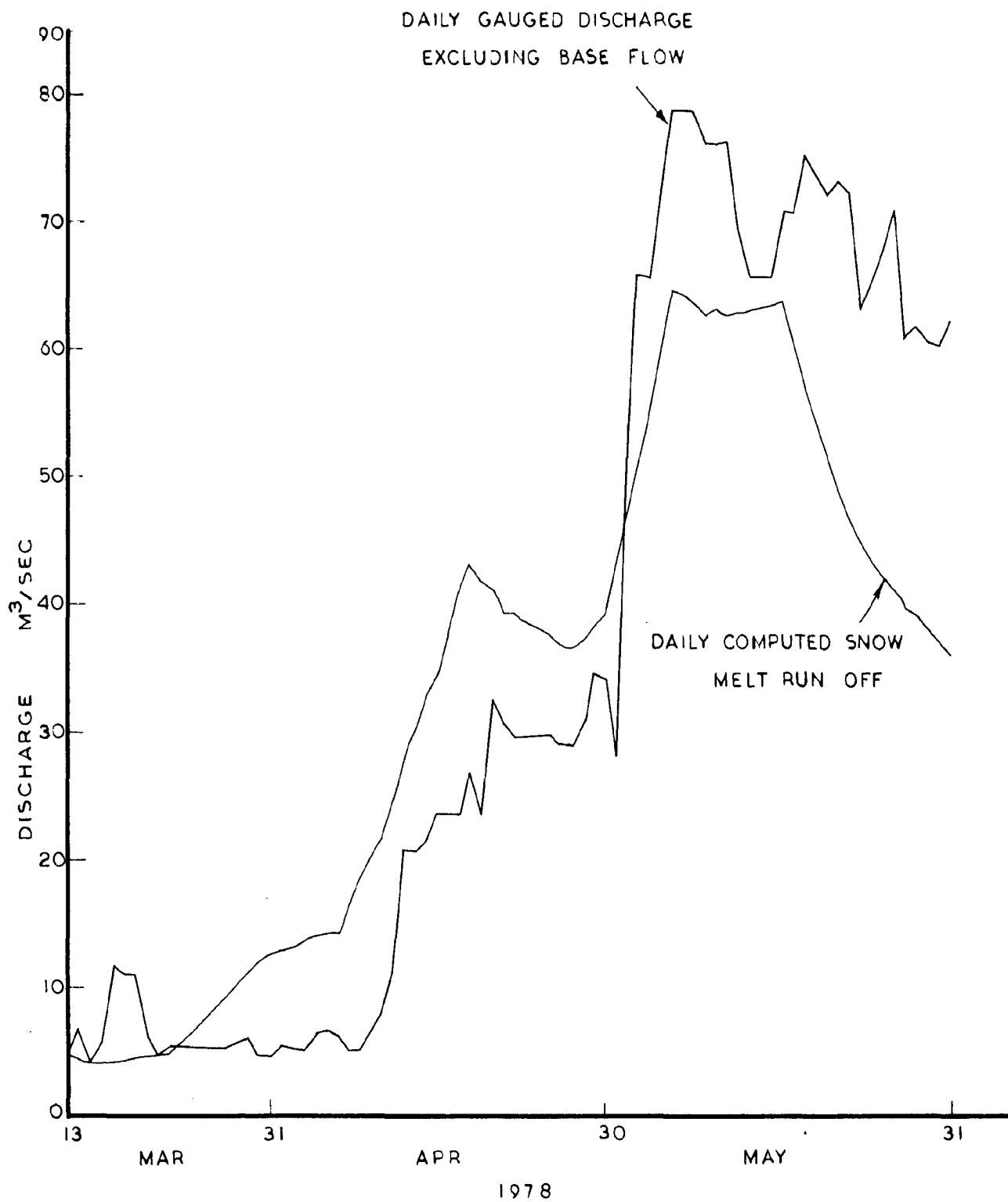


FIG.4.12(b) DAILY COMPUTED SNOWMELT RUNOFF AND DAILY GAUGED DISCHARGE (EXCLUDING BASE FLOW) IN MANALI

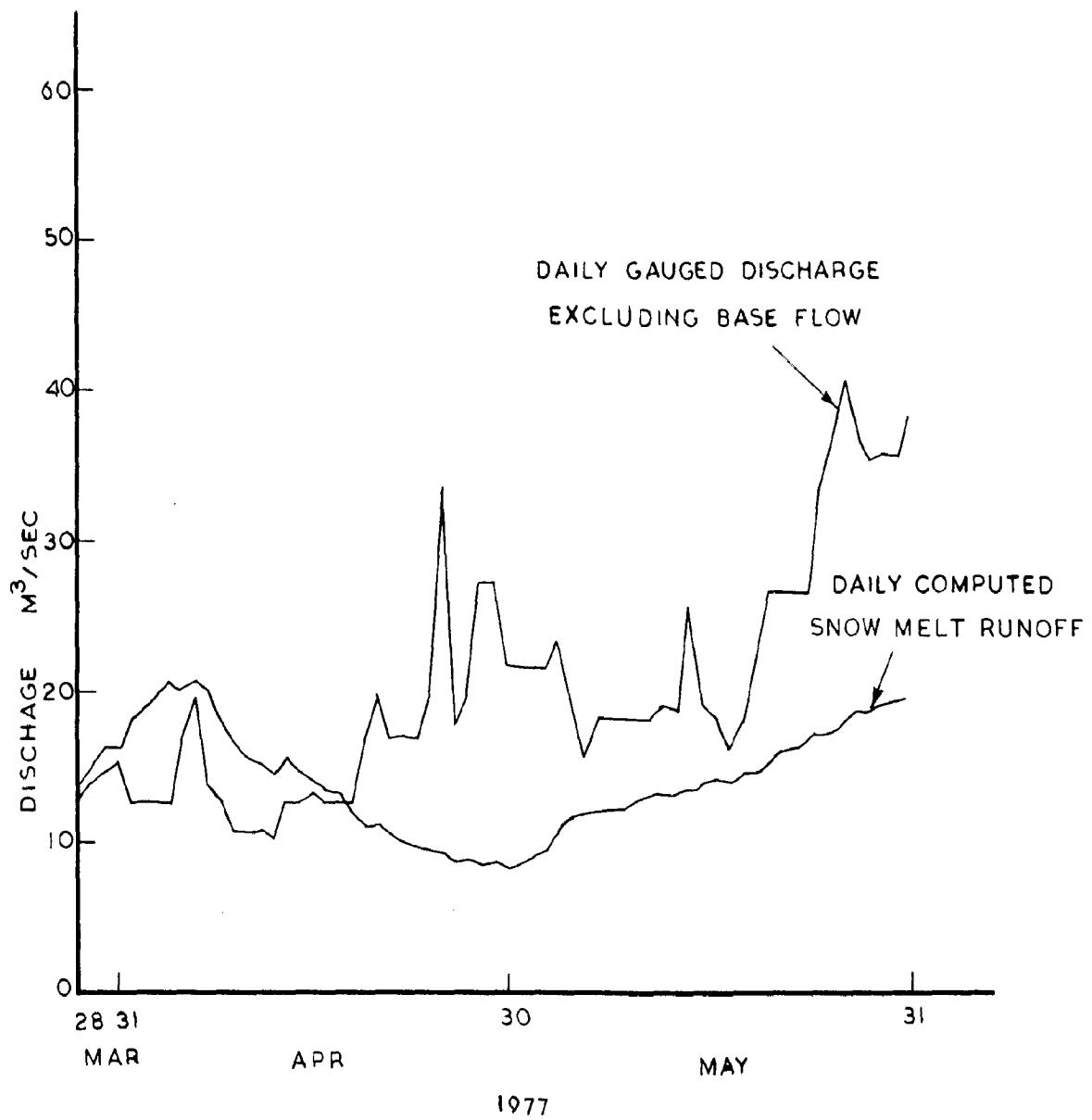


FIG. 4.12(c) DAILY COMPUTED SNOWMELT RUNOFF AND DAILY GAUGED DISCHARGE (EXCLUDING BASE FLOW) IN MANALI

where ΣQ_R is the total discharge contributed by the rainfall in m^3/s during the melting period. C_1 and C_2 are the runoff coefficients for the snow covered area and non snow-covered area respectively. ΣH_1 and ΣH_2 are the total of the daily rainfall depth (m) in the temporary snow covered area A_1 (m^2) and the non-snow covered area A_2 (m^2). 86400 is the number of seconds in a day. The recession flows prior to and subsequent to the respective melt periods of 1977 to 1979 have been obtained with the help of the snowmelt runoff recession curve in figure (4.11). These have been accounted to get the values of ΣQ_o and ΣQ_m .

The values of the ΣQ_o , ΣQ_m and ΣQ_R are given in the table no (4.3) below.

Table no. (4.3). The cumulative sum of daily observed discharge, the cumulative sum of daily snowmelt discharges, and the total discharge due to the rainfall during the melting period.

Year	Cumulative sum of the daily observed discharge (m^3/s) during the melting period (ΣQ_o) (excluding base flow)	Cumulative sum of the daily snowmelt discharge (m^3/s) during the melting period (ΣQ_m)	Total discharge due to rainfall (m^3/s) during the melting period (ΣQ_R)
1979	3071.27	2775.05	296.21
1978	3215.72	2858.75	357.04
1977	1462.45	962.78	499.87

The total runoff due to rainfall on snow covered area and non snow covered area during the melting period is given in the table no. (4.8) below.

Table no. (4.9). The total discharge due to rainfall on snow covered area and non snow covered area during the melting period.

Year	Total discharge due to rainfall during melting period on	
	snow covered area	non snow covered area.
	$(\sum h_1 A_1 / 86400) \text{ (m}^3/\text{s})$	$(\sum h_2 A_2 / 86400) \text{ (m}^3/\text{s})$
1979	282.23	355.98
1978	532.45	142.41
1977	619.02	649.61

By using the values in table no. (4.7), and (4.8) in equation (4.19), three linear equations are obtained as given below.

$$296.21 = C_1 282.23 + C_2 355.98$$

$$357.04 = C_1 532.45 + C_2 142.41$$

$$449.67 = C_1 619.02 + C_2 649.61$$

The linear equations are solved by using the method given in section (4.5.10). The values of C_1 and C_2 thus obtained equal 0.593 and 0.278 respectively.

4.6.1.16 SNOWMELT DISCHARGE AT MANALI GAUGE SITE INCLUDING THE RAINFALL RUNOFF.

Part of the rain falling on the snow-covered area flows along with the snowmelt. The daily discharge for the melting period for 1977 to 1979 ^{ave} was thus calculated by the equation (4.23) and tabulated in the 6th column Appendix (XIa, XIb, XIc). The discharge contributed due to rainfall on the non-snow-covered area is super imposed on the hydrograph obtained by the equation (4.23) on the very same day since the time of concentration for the catchment is less than a day. The discharge including the runoff due to rainfall on the non-snow covered area is tabulated in the 5th column Appendix (XIa, XIb, XIc). The hydrographs thus obtained by these computed discharges are shown in figures (4.13a, 4.13b, 4.13c). With this consideration there is an improvement in the result. A reasonable agreement is there between the computed hydrograph and the observed ~~due-to runoff~~ ^{direct} hydrograph.

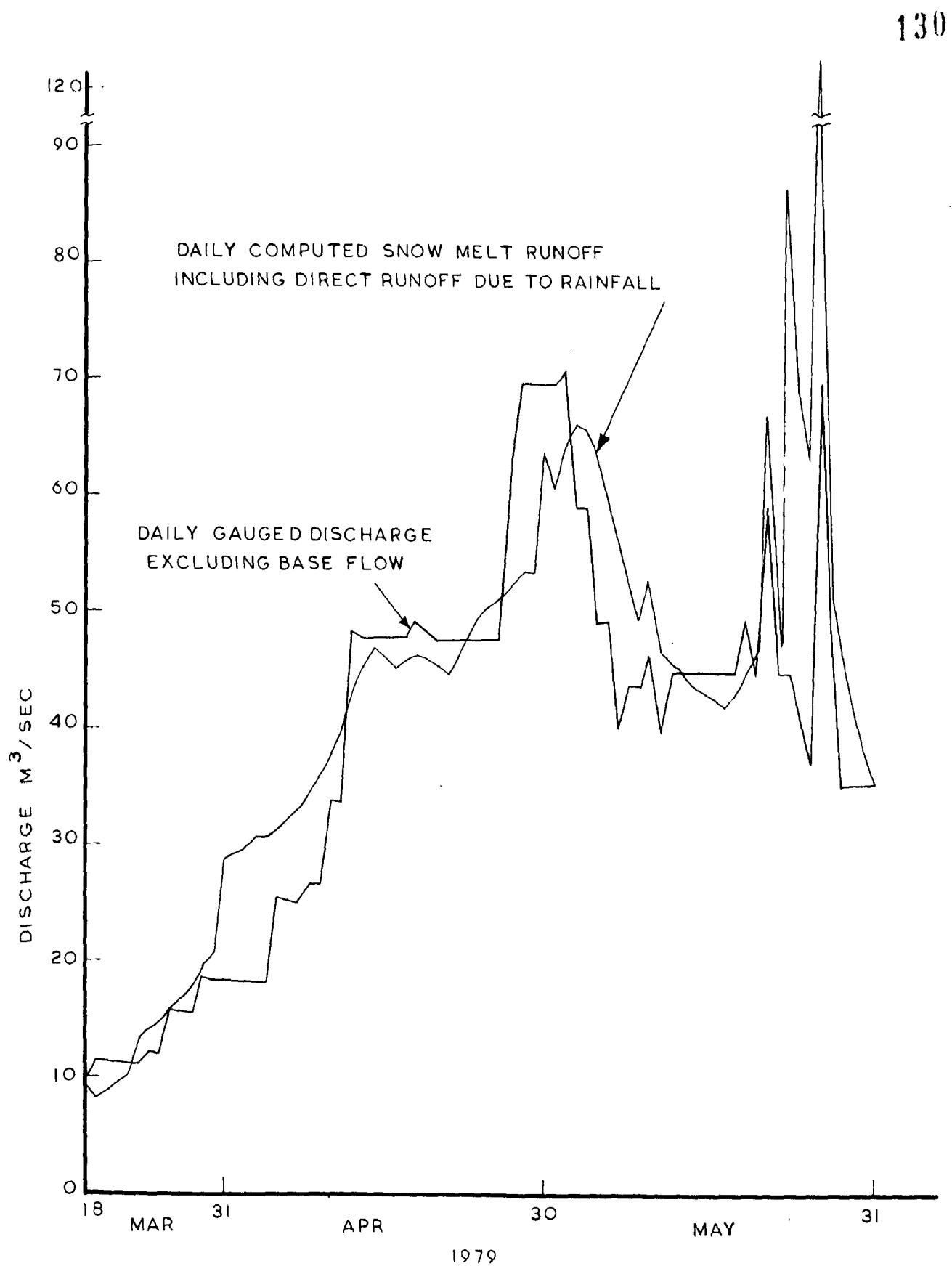


FIG.4.13(a) DAILY COMPUTED SNOWMELT RUNOFF INCLUDING DIRECT RUNOFF DUE TO RAINFALL AND DAILY GAUGED DISCHARGE (EXCLUDING BASE FLOW) IN MANALI

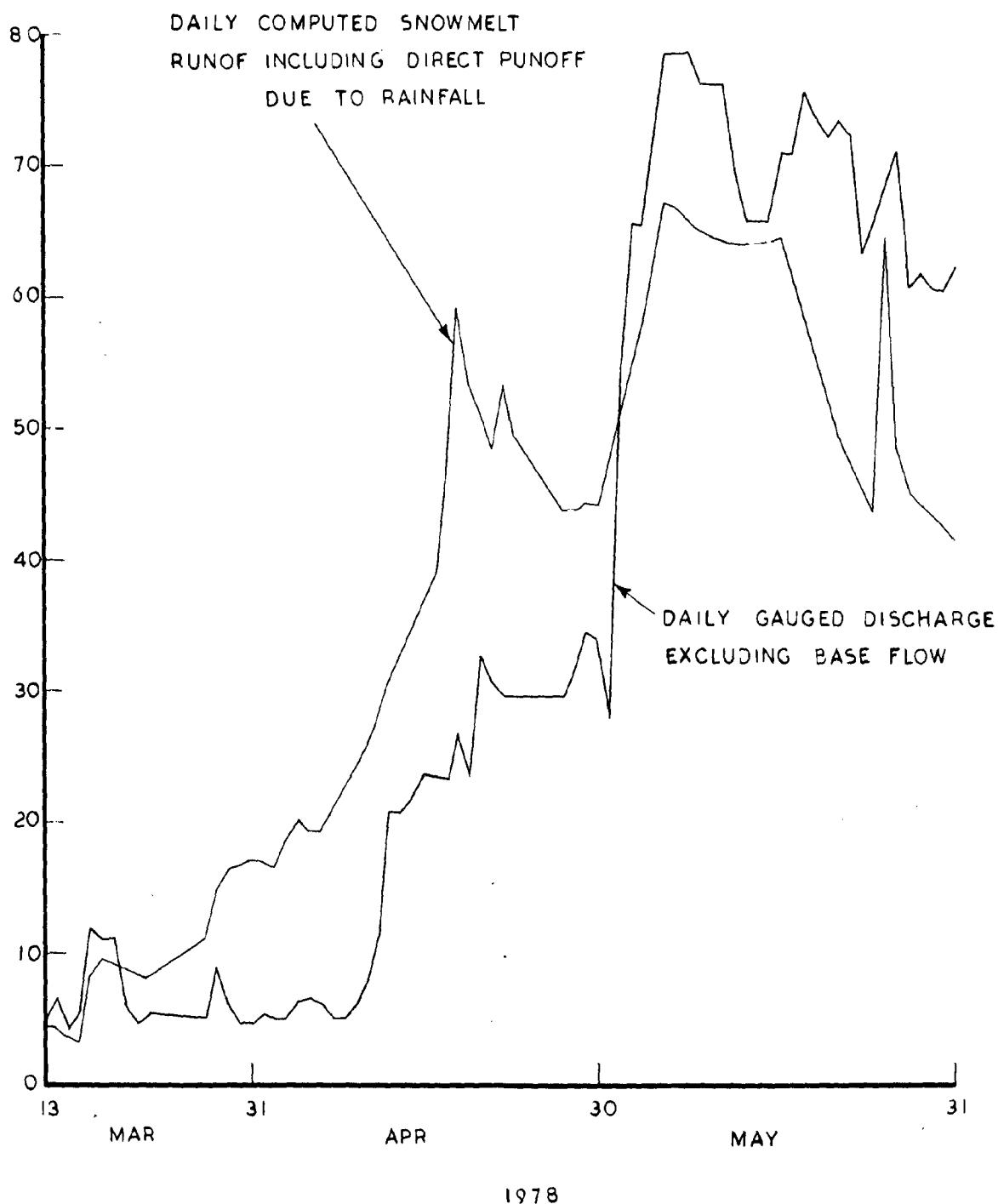


FIG.4.13(b) DAILY COMPUTED SNOWMELT RUNOFF INCLUDING DIRECT RUNOFF DUE TO RAINFALL AND DAILY GAUGED DISCHARGE (EXCLUDING BASE FLOW) IN MANALI

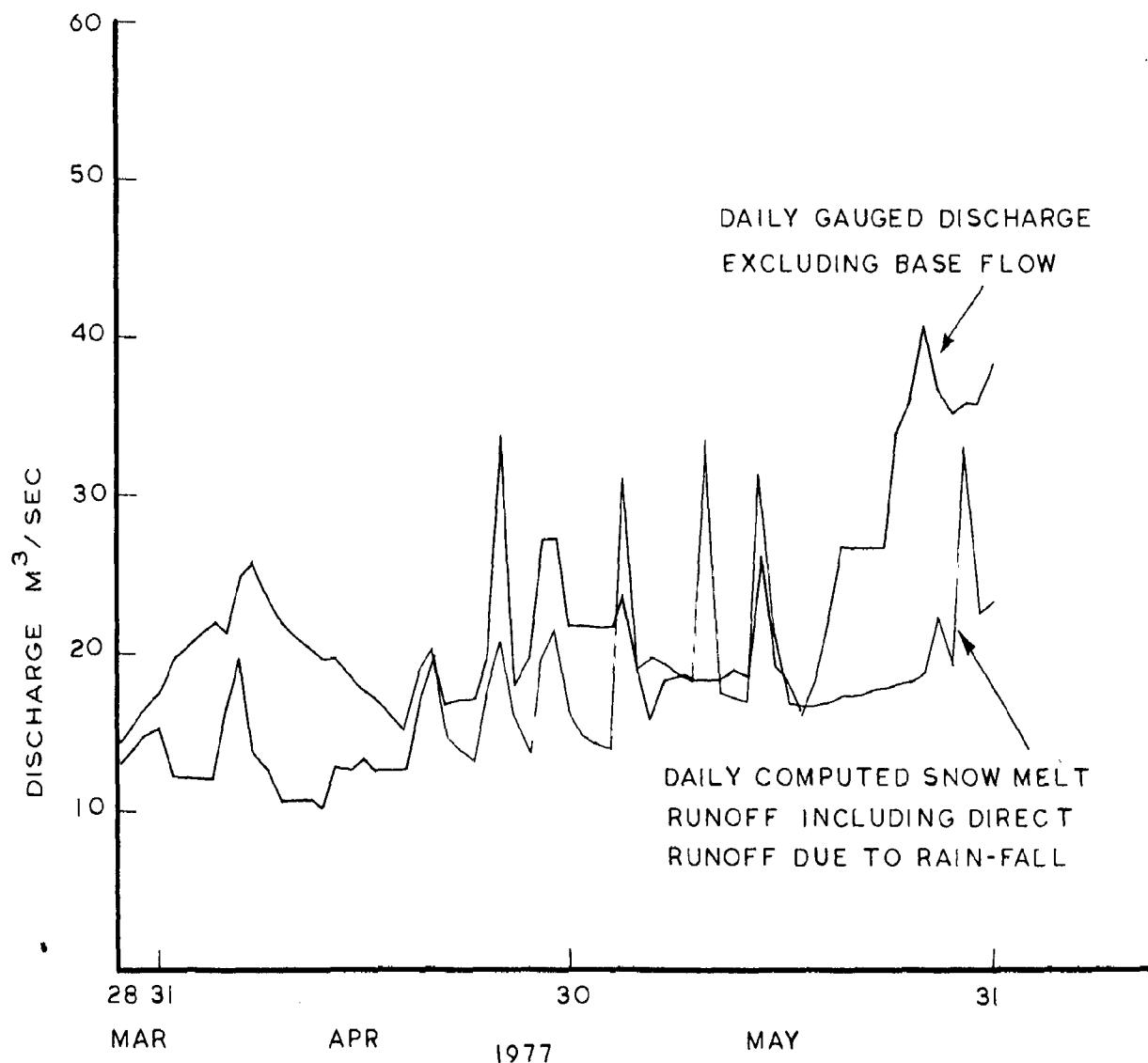


FIG.4.13(c) DAILY COMPUTED SNOWMELT RUNOFF INCLUDING DIRECT RUNOFF DUE TO RAINFALL AND DAILY GAUGED DISCHARGE (EXCLUDING BASE FLOW) IN MANALI

CHAPTER - V

DISCUSSION, CONCLUSION AND SCOPE FOR FURTHER STUDY

5.1. DISCUSSION

Remote sensing has proved to be an invaluable aid in monitoring resources in inaccessible regions. Snowcapped Himalayas from which many rivers originate pose a formidable problem for ground survey or even aerial surveys for the estimation of snow-cover. Orbital remote sensing systems particularly with the advent of LANDSAT series of satellites, has opened up new vias for monitoring snow and estimating the total quantity of water stored as snow.

Snow melting is a thermodynamic process. Thus the investigation of the processes depends basically on the accurate measurement of the various factors influencing the transmission of heat to the snow mantle. It is found that the heat within the atmosphere is the main factor. The problem is then largely compatible with an adequate snow cover, precipitation in the form of rain on snow area and the relationship of these values to the rate of snow melt.

Considerable differences in altitude, and therefore in climate, soil, and vegetative conditions, are

specific features of mountainous river basin. Therefore, such basins are usually divided into elevation zones for the study. Because of the time difference between the accumulation of seasonal snowpack and its melting, the forecast of seasonal flow may be prepared well in advance. The possibilities for forecasting are most favourable for those areas where rainfall during the melting period is scarce in comparison to the accumulated winter precipitation in the form of snow and the total heat inflow is sufficient every year for complete melting of the seasonal snow pack (i.e. from the temporary snow covered areas).

Conditions for runoff in high land river basins are such that losses of melt water will not vary greatly from year to year. Under such conditions, there should exist a relationship between the accumulated winter precipitation and seasonal runoff. In principle, such a relationship can be established empirically for any basin if observational data are available over a number of years. In practice for Indian catchments, however, the problem of determining such relationship is far from easy particularly because of very limited relevant data being available. In Indian mountain basins the water equivalent data of the snowpack is not available and the measurements of precipitation and snow cover do not make it possible to determine the true amount of accumulated water and may serve only for obtaining some indices of this value.

At least two factors have an influence on runoff and, consequently on the degree of correlation between runoff and the snow accumulation index. These factors are the amount of precipitation for the melting season and the antecedent water storage in a basin. Both of these factors must be taken into account in the development of seasonal snowmelt runoff relations and in the preparation of forecasts.

In the Manali catchment due to the availability of limited data some assumptions are made keeping in view the physics of melting process so as to arrive at a reasonable estimate of snow melt runoff. The data available for this study comprises of some satellite imageries, daily record of temperature, snowfall, and rainfall at Manali gauging station, which is the outlet of the catchment situated at an elevation of about 6000 ft. (1830 m). The elevation in Manali catchment varies from 6000 ft (1830 m) to 14000ft.(4270 m) for the area under temporary snow cover and above 14000 ft(4270 m) for area under permanent snow cover. This information about the temporary and permanent snow cover has been obtained by comparison of a few available satellite imageries. In the present study the area under temporary snow cover from 6000 ft to 14000 ft. has been divided into four elevation zones at an interval of 2000 ft. each. The variation of the precipitation (snowfall as well as rainfall) with elevation (as given Appendix : VII a, VII b) and the β parameter (as 1.53°C decrease for every 1000 ft (305 m) rise in elevation) have

(22)

been assigned from literature survey. These assumptions have been proved to reasonably correct as the total volume as well as the rate of snowmelt runoff at the Manali gauging site has been predicted reasonably well.

The snowmelt has been estimated by considering melt due to the influence of the temperature and due to the influence of the rainfall on the snow covered area. The water equivalent of snow has been assumed as 0.1. The losses from snowmelt under permanent as well as temporary cover have been taken as 10%. Such a value has been found and used in a similar study in the mountainous watershed of Dischma in Switzerland. The losses of rain falling on temporary snow covered area and rain falling on the non-snow covered area have been accounted for by computing the coefficients C_1 and C_2 respectively. The values of these coefficients, C_1 as 0.595 and C_2 as 0.278, are reasonable, though some further study will require to investigate the physical significance of the values. The routing of snowmelt after accounting for losses as permanent & temporary well as excess rainfall from the snowcovered area has been made using equation (4.23) with the recession coefficient for one day K taken as 0.90 and the excess rain from non-snow covered area has been assumed as directly contributing for the runoff for that day. The direct snowmelt runoff computed using the above procedure for the period March to May of 1977 to 1979 compare quite well with the observed direct runoff for the corresponding periods.

5.2. CONCLUSIONS

The results obtained from this study are quite encouraging particularly in view of limited data having been used. The following conclusions can be drawn on the basis of the results.

- (1) The satellite imageries reveal that the snowline start descending to lower altitudes from September to around the first week of March. Thus this is the accumulation season. After the first or second week of March the snowline starts receding indicating the onset of the melting season. The snow accumulation is the maximum in the year 1975 and minimum in the year 1977. With these imageries one can make reasonable judgement about temporary and permanent snow cover.
- (2) The imageries taken in MSS 5 indicate more snow cover than in those taken in MSS 7 on the same day. The imageries of 22 September, 1972, 3 December, 1972 and 21 March, 1973 are studied in this respect. The snow covered areas of the subcatchments in Larji catchment in MSS 5 and MSS 7 are plotted and a straight line has been fitted with an inclination of 37° from the X-axis of the MSS 5. This phenomenon refers to the melting condition near the snowline causing considerable decrease in the reflected near I.R. radiation. MSS 5 is thus found to be more appropriate for snow survey since moisture increases in MSS 7.

- (3) The snow covered areas in various subcatchments have also been plotted against their cumulative discharges for March-April-May. An exponential curve has been fitted. This evidently shows that with larger areal snow coverage more snowmelt discharge can be expected in the melting season. However, the snow extents from the imageries must be considered alongwith other factors very carefully to get a meaningful estimate. Better results can be expected working with enlarged imageries and identifying snow in shadows. However, due to the ruggedness of the terrain the ^{true} snow covered area cannot be estimated.
- (4) Using the blown up LANDSAT image in MSS 5 of scale 1:250,000 dated Dec. 2, 1972 the vegetal cover and the land use features have been interpreted and delineated as snowcover, Alpine pasture, thin forest, thick forest and bare and cultivated land. The Larji catchment is covered by snow more than the other features, which can also be concluded from table (4.2).
- (5) The division of Manali catchment in five zones of 2000 ft. interval in altitude has been adequate.
- (6) A lapse rate of 1.53°C per 1000 ft. (305 m) has been assigned from literature survey. Similar values of lapse rate have been observed in the catchment using the temperature data of Manali and Bhuntar which is further down stream of Manali at an elevation of 3525.25 ft(1084.35 m). However, it is better to establish this relationship ^{or do} if a station at 10,000 ft (3050 m) were available.

- (7) Only assumed values of the variation of precipitation with elevation were based on literature survey. They have performed reasonably well. However, further study and data is needed to establish this relation.
- (8) The snowline before the snowmelt season for the year 1977 was taken with the help of the satellite image. The span of accumulation season was also concluded from the satellite imagorics. However, more satellite imagorics are needed for better result.
- (9) The water equivalent of the snow was taken as 0.1 since the actual condition of the snowpack ^{was} not known.
- (10) The idea of using temperature as predominant factor in the process of snowmelt has given quite an encouraging result. The degree-day factors of $0.0018 \text{ cm}^{\circ}\text{C}^{-1} \text{ d}^{-1}$ and $0.00315 \text{ cm}^{\circ}\text{C}^{-1} \text{ d}^{-1}$ for Mar - April ^{for May} have been used. These values are coming around the average value of $0.0027 \text{ cm}^{\circ}\text{C}^{-1} \text{ d}^{-1}$ given in the literatures reviewed. Since the rainfall on the snow-covered area is scanty, no definite conclusion can be arrived by ascertaining the suitability of the snowmelt due to rain falling on the snow covered area.
- (11) The calculated values of the losses C_1 and C_2 as 0.595 and 0.278 of the rain falling on snow covered area and rainfall on the non-snow covered area respectively are reasonable though further study is required to investigate the physical significance of these values.

5.3. SCOPE FOR FURTHER STUDIES

The observations of snowline, depth, and density of snow, are essential for the proper evaluation of the snowmelt runoff. Study is also needed for estimating the base flow, the losses from the snowmelt, the phreatic level rate, the degree day factor and the runoff coefficient.

The availability of the satellite remote sensed data used in conjunction with conventional methods is likely to improve the accuracy of the snowmelt forecasts. A thorough study should be made to see whether the methods used abroad are to be modified to suit the conditions prevailing in the Himalayan catchments.

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78° 0'

77° 45'

77° 30'

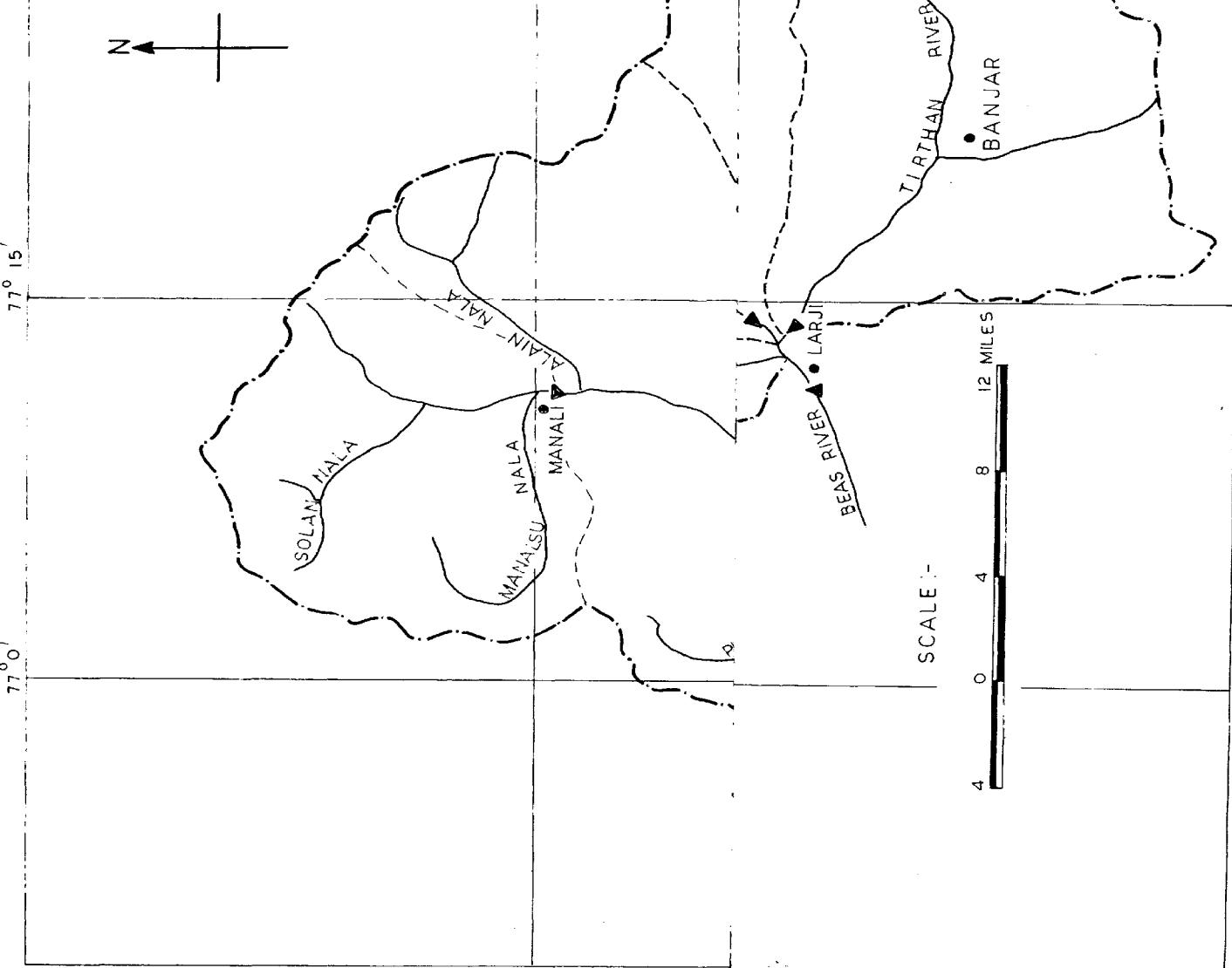
77° 15'

77° 0'

32° 15'

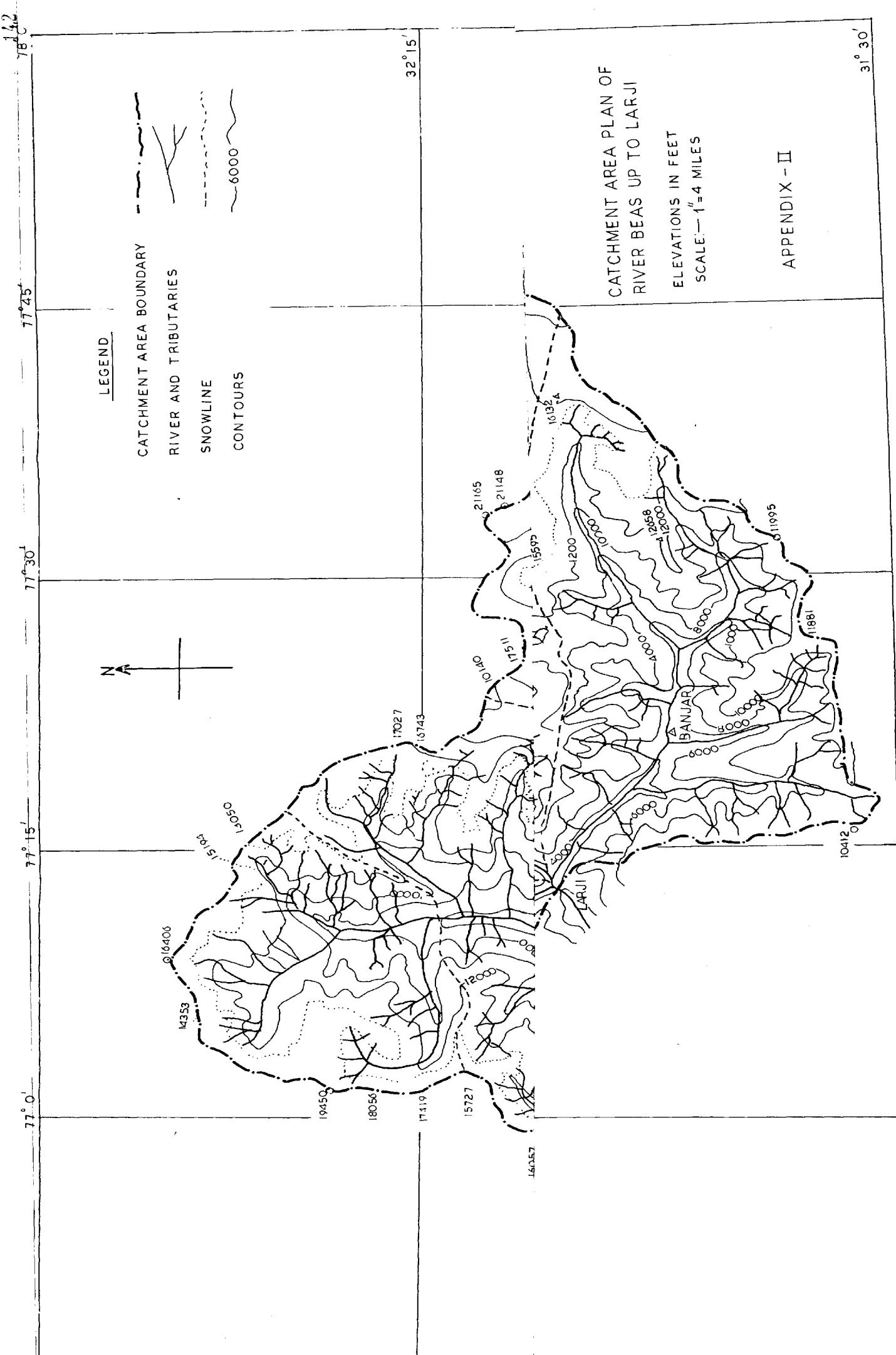
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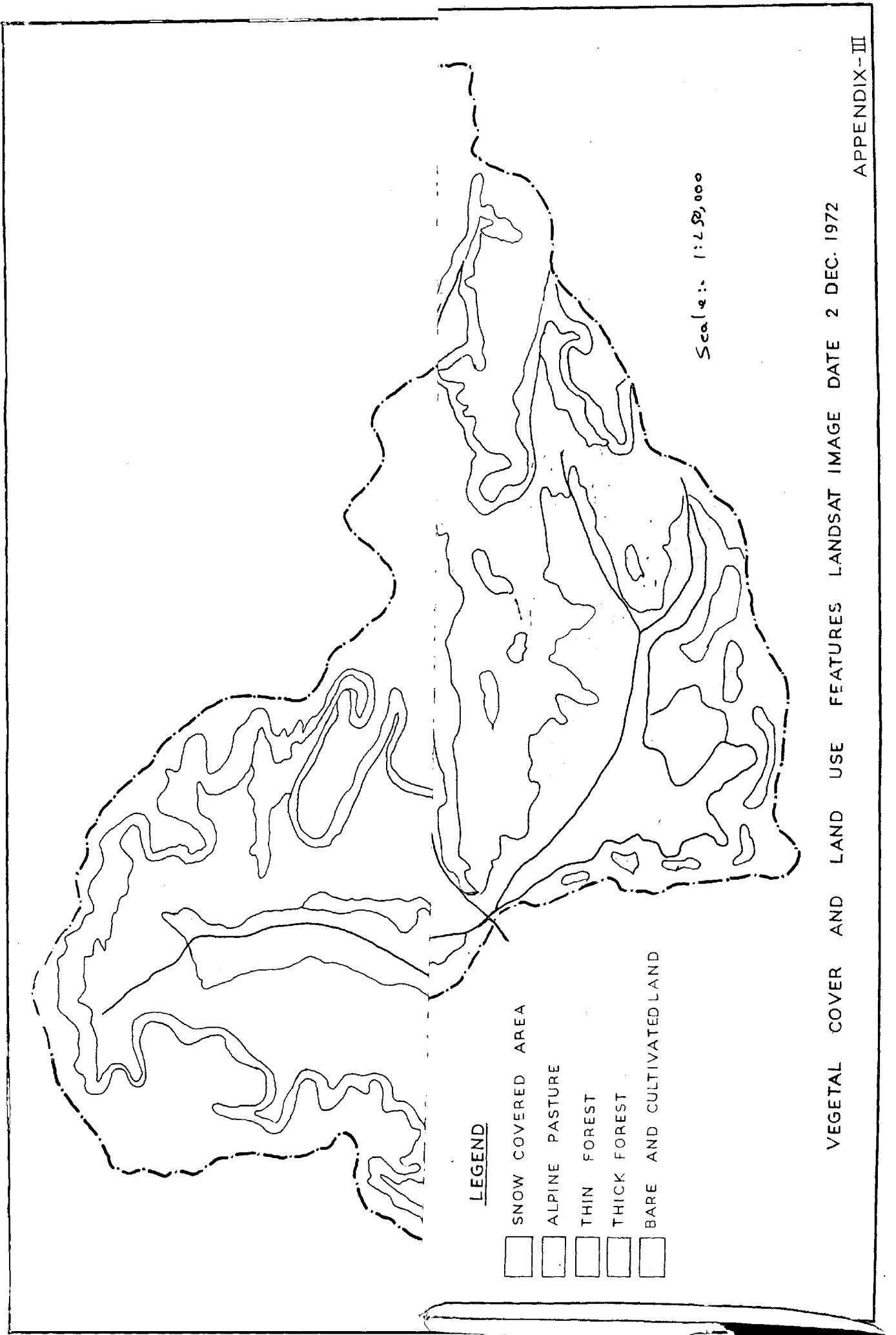
- RIVER AND TRIBUTARIES
- Boundary of Catchment
- - Sub Catchment
- ▲ Discharge Site

BEAS CATCHMENT
UP TO LARJI

APPENDIX - I

31° 30'





APPENDIX I IV (a)

Daily Mean temperature data in Manali - year 1977

Date	Daily mean Temp (°c)	Date	Daily mean Temp (°c)	Date	Daily Mean Temp (°c)
March					
18	6.5	12	17.5	7	14.5
19	9	13	17.5	8	14.5
20	10	14	17.5	9	16
21	11	15	15.5	10	15.5
22	10.5	16	15	11	17
23	10.5	17	17.5	12	17.5
24	12	18	17	13	17.5
25	12	19	16	14	16.5
26	12.5	20	15.5	15	17.5
27	12.5	21	15.5	16	17.5
28	12.5	22	16	17	17
29	14	23	19.5	18	19.5
30	13.5	24	19	19	21
31	13	25	19	20	21.5
		26	21	21	21.5
April					
1	14	27	21	22	18.5
2	14	28	21	23	19.5
3	12	29	20.5	24	15
4	13	30	19	25	14
5	14.5			26	12.5
6	14.5	May 1	19	27	12
7	15	2	19.5	28	12
8	16	3	19	29	13
9	16	4	18.5	30	13
10	17	5	17	31	14
11	17.5	6	14.5		

APPENDIX : IV(b)

Dail Mean temperature data in Manali Year: 1978.

Date	Daily Mean temp. (°c)	Date	Daily Mean Temp (°c)	Date	Daily Mean Temp (°c)
March					
13	3.5	4	10	27	16
14	5	5	10	28	18
15	6	6	11.5	29	19.5
16	5.5	7	14	30	19.5
17	6	8	14	May	
18	7	9	14	1	19.5
19	7.5	10	14	2	18.5
20	8	11	16	3	19
21	9	12	17.5	4	19
22	7	13	16	5	21
23	10.5	14	16.5	6	21
24	10	15	17	7	21
25	10	16	19.5	8	20.5
26	10	17	19	9	20.5
27	11	18	16	10	21.5
28	11	19	14	11	21
29	11.5	20	14.5	12	21.5
30	11.5	21	13	13	21.5
31	11.5	22	14.5	14	21.5
April					
1	10.5	23	14	15	22
2	10.5	24	14.5	16	22
2	10.5	25	14.5	17	22
3	11.5	26	15	18	22.5

Appendix : IV(b) Contd..

Date	Daily Mean Temp (° c)
19	22.5
20	22
21	22
22	23
23	23
24	23
25	23
26	23.5
27	23
28	24
29	24.5
30	23
31	22

Dally Rain & Temperature in Manaus. Year = 1977

Date	Daily Mean Temp. (°C)		Daily Rain mm	Daily Mean Temp. (°C)	Daily Rain mm
	R	S			
March 1	23.0	20	12.0	20	20
2	25	23	20	21	20
3	25.0	23	19	22	20.0
4	24	27	20.0	20	19.0
5 April	17	20	12.0	17	20
6	23.0	20	20	20	20
7	23.0	20	50	23	20.0
8	20.0			27	21
9	20.0	17	18.0	20	20.0
10	20.0	2	18.0	20	20
11	20.0	0	16	20	20.0
12	22	0	19	21	20
13	22	0	19	21	20
14	21.0	6	19		
15	22.0	7	17		
16	19.0	0	17.0		
17	20	0	17		
18	22.0	10	10		
19	22.0	11	10		
20	22.0	80	19.0		
21	20	80	19		
22	22	85	18.0		
23	16.0	80	18.0		
24	19.0	17	17.0		
25	19.0	80	19		
26	19	80	19		
27	21	85	18.0		
28	16.0	17	17.0		
29	19.0	80	19		
30	19.0	80	19.0		

APPENDIX V (a)

**Estimated daily rainfall in different zones in Manali
catchment**

Year 1979.

Date	Daily rainfall depth recorded at Manali (cm)	Computed daily rainfall depth for different elevation zones. (cm)				
		6000 to 8000	8000 to 10000	10000 to 12000	12000 to 14000	above 14000ft
		ft	ft	ft	ft	ft
23.3.79	1.620	1.745	1.995	2.495	2.495	2.745
31.3.79	2.720	2.845	3.095	3.345	3.595	3.845
3.4.79	0.52	0.57	0.67	0.77	0.87	0.97
12.4.79	0.22	0.27	0.37	0.47	0.57	0.67
30.4.79	2.22	2.345	2.595	2.845	3.095	3.345
10.5.79	0.52	0.57	0.67	0.77	0.87	0.97
21.5.79	2.32	2.445	2.695	2.945	3.195	3.445
23.5.79	0.94	0.99	1.09	1.19	1.29	1.39
26.5.79	5.98	6.18	6.58	6.98	7.38	7.78
Total	17.06	17.96	19.76	21.56	23.36	25.16

APPENDIX -V(b)

Estimated daily rainfall in the different zones in Manali catchment

Year 1978.

Date	Daily rainfall depths recorded at Manali(cm)	Computed daily rainfall depths for different elevation zones. (cm)					
		6000ft to 8000ft	8000ft to 10000ft	10000ft to 12000ft	12000ft to 14000ft	Above 14000ft	
		6000ft to 8000ft	8000ft to 10000ft	10000ft to 12000ft	12000ft to 14000ft		
17.3.78	0.48	0.68	9.08	9.48	9.89	10.28	
18.3.78	3.77	3.495	3.745	3.995	4.245	4.495	
28.3.78	1.02	1.145	1.395	1.645	1.895	2.145	
29.3.78	0.34	0.39	0.49	0.59	0.69	0.79	
3.4.78	0.38	0.63	0.73	0.83	0.93	1.03	
4.4.78	1.12	1.245	1.495	1.745	1.995	2.245	
17.4.78	1.22	1.345	1.595	1.845	2.095	2.345	
18.4.78	4.08	4.28	4.68	5.08	5.48	5.88	
22.4.78	1.72	1.945	2.095	2.345	2.595	2.845	
25.5.78	1.76	1.885	2.135	2.385	2.635	2.885	
26.5.78	0.54	0.59	0.69	0.79	0.89	0.99	
31.5.78	0.22	0.27	0.37	0.47	0.57	0.67	
Total	24.45	25.80	28.50	31.20	33.90	36.60	

APPENDIX V (a)

Estimated daily rainfall in different zones in Manali catchment, year 1977.

Date	Daily rainfall depths recorded in Manali (cm)	Computed daily rainfall depths for different elevation zones (cm)					
		6000 ft to 8000 ft	8000 ft to 10000 ft	10000 ft to 12000 ft	12000 ft to 14000 ft	14000 ft to 16000 ft	above 16000 ft
1	2	3	4	5	6	7	
31.3.77	0.40	0.45	0.55	0.65	0.75	0.85	
1.4.77	0.84	0.89	0.99	1.09	1.19	1.44	
6.4.77	2.82	2.945	3.195	3.445	3.695	3.945	
7.4.77	2.08	2.185	2.435	2.685	2.935	3.185	
8.4.77	0.22	0.27	0.37	0.47	0.57	0.67	
10.4.77	0.12	0.17	0.27	0.37	0.47	0.57	
11.4.77	0.44	0.48	0.59	0.69	0.79	0.89	
13.4.77	0.44	0.49	0.59	0.69	0.79	0.89	
15.4.77	0.22	0.27	0.37	0.47	0.57	0.67	
19.4.77	1.38	1.505	1.755	2.005	2.255	2.505	
20.4.77	1.62	1.745	1.995	2.245	2.495	2.745	
24.4.77	1.24	1.365	1.615	1.865	2.115	2.365	
25.4.77	2.04	2.165	2.415	2.665	2.915	3.165	
26.4.77	0.52	0.57	0.67	0.77	0.87	0.97	
28.4.77	1.72	1.865	2.095	2.345	2.595	2.845	
29.4.77	2.26	2.305	2.635	2.885	3.35	3.355	
30.4.77	0.42	0.47	0.57	0.67	0.77	0.87	
4.5.77	5.08	5.28	5.68	6.08	6.48	6.88	

Contd....

1	2	3	4	5	6	7
10.5.77	2.42	2.545	2.795	3.045	3.295	3.545
14.5.77	2.16	2.285	2.535	2.785	3.035	3.285
15.5.77	0.52	0.57	0.67	0.77	0.87	0.97
27.5.77	0.32	0.37	0.77	0.57	0.67	0.77
29.5.77	2.08	2.205	2.455	2.705	2.955	3.205
30.5.77	0.42	0.47	0.57	0.67	0.77	0.87
Total	31.76	33.935	38.285	42.635	46.985	51.335

APPENDIX VI (a)

Estimated daily snow fall in different zones in Manali Catchment.

Year 1978-1979

Date	Daily snow depths recorded at Manali (cm)	Computed daily snowfall depths for different elevation zones (cm)			
		6000 ft	8000 to 10000 ft	10000 to 12000 ft	12000 to 14000 ft
		8000 ft	10000 ft	12000 ft	14000 ft
1	2	3	4	5	6
25.11.78	10.80	12.05	14.95	17.05	19.55
26.11.78	17.20	15.45	17.95	20.45	22.95
27.11.78	16.20	17.75	19.95	22.45	24.95
2.12.78	16.20	17.45	19.95	22.45	24.95
14.1.79	22.20	23.45	25.95	28.45	30.95
15.1.79	49.20	51.20	55.20	59.20	63.20
16.1.79	36.40	17.65	20.15	22.65	25.15
17.1.79	8.20	8.70	9.70	10.70	11.70
20.1.79	8.20	8.70	9.70	10.20	11.70
21.1.79	25.20	26.45	28.95	31.45	33.95
26.1.79	47.20	49.20	53.20	51.20	61.20
29.1.79	6.20	6.70	7.70	8.70	9.70
30.1.79	18.00	19.25	21.75	24.25	26.75
2.2.79	16.20	17.45	19.95	22.45	24.95
16.2.79	3.20	3.70	4.70	5.70	6.70

Contd...

1	2	3	4	5	6
17.2.79	4.20	4.70	5.70	6.70	7.70
19.2.79	14.20	15.45	17.95	20.45	22.95
20.2.79	49.20	51.20	55.20	59.20	68.20
21.2.79	9.00	9.50	10.50	11.50	12.50
23.2.79	14.80	16.05	18.55	21.05	23.55
26.2.79	4.20	4.70	5.70	6.70	7.70
2.3.79	16.20	17.45	19.95	22.45	24.95
3.3.79	45.20	47.20	51.20	55.20	59.20
4.3.79	17.40	18.65	21.15	23.65	26.15
5.3.79	22.40	23.65	26.15	28.65	31.15
6.3.79	26.60	27.85	30.35	32.85	35.35
7.3.79	30.40	31.65	34.15	36.65	39.15
8.3.79	14.20	15.45	17.95	20.45	22.95
9.3.79	9.20	10.45	12.95	15.45	17.95
17.3.79	16.20	17.45	19.95	22.45	24.95
Total	571.00	605.25	676.75	747.25	817.75
6					

APPENDIX - VI(b)

Estimated daily snow fall in different zones in Manali catchment.

Year : 1977 - 78

Date	Daily snow depths recorded at Manali	Computed daily snow fall depths for different elevation zones (cm)			
		6000 ft to 8000 ft	8000 ft to 10000 ft	10000 ft to 12000 ft	12000 ft to 14000 ft
		6000 ft	to 10000 ft	12000 ft	to 14000 ft
3.11.77	4.00	5.30	6.30	7.3	8.30
6.11.77	7.40	7.90	8.90	9.9	10.90
30.11.77	10.00	10.50	11.50	12.50	13.50
1.12.77	46.40	48.40	52.40	56.40	60.40
10.12.77	4.00	5.10	6.10	7.10	8.10
17.12.77	16.20	17.45	19.95	22.45	24.95
20.12.77	42.60	44.60	48.60	52.60	56.60
25.12.77	42.20 (4.20)	15.45	17.95	20.45	22.95
26.12.77	39.20	40.45	51.95	45.45	47.95
23.12.77	12.00	13.25	15.75	18.25	20.75
28.12.77	2.00	2.50	3.50	4.50	5.50
29.12.77	2.00	3.50	3.50	4.50	5.50
13.1.78	14.60	16.85	18.35	20.85	23.35
14.1.78	19.20	20.45	22.95	25.45	27.95
23.1.78	9.00	9. ⁵⁰ 00	10.50	11.50	12.50
26.1.78	45.40	47.40	51.40	55.40	59.40
28.1.78	36.90	39.05	40.55	43.05	45.55
29.1.78	38.00	39. ²⁵ 00	40. ⁷⁵ 35	46.25	46.75
5.2.78	3.20	3.70	4.70	5.70	6.70
6.2.78	4.00	4.50	5.50	6.50	7.50
7.2.78	21.60	22.85	25.35	27.85	30.35

<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>
8.2.78	5.00	5.50	6.50	7.50	8.50
11.2.78	13.00	14.25	16.75	19.25	21.75
13.2.78	12.20	13.45	25.95	18.45	20.95
15.2.78	4.20	4.70	5.70	6.70	7.70
16.2.78	21.20	22.45	24.95	27.45	29.95
17.2.78	26.60	27.85	30.85	32.85	35.35
18.2.78	17.80	19.05	21.55	24.05	26.55
3.3.78	2.00	2.50	3.50	4.50	5.50
11.3.78	12.00	13.25	15.75	18.25	20.75
12.3.78	10.00	10.50	11.50	12.50	13.50
Total	517.20	548.45	610.95	673.45	735.95

APPENDIX: VI (c)

Estimated daily snowfall in different zones in Manali catchment. year 1976 - 1977

Date	Daily snow depths recorded at Manali (cm)	Computed daily snowfall depths for different elevation zones (cm)			
		6000 ft to 8000 ft	8000 ft to 10000 ft	10000 ft to 12000 ft	12000 ft to 14000 ft.
		1	2	3	4
3.12.76	5.80	6.30	7.30	8.30	9.30
26.12.76	19.20	20.45	22.95	25.45	27.95
29.12.76	6.00	6.50	7.50	8.50	9.70
12.1.77	6.20	6.70	7.7	8.70	8.70
20.1.77	20.00	21.25	23.75	26.25	28.75
24.1.77	27.70	28.65	31.15	33.65	36.15
25.1.77	36.20	37.45	39.95	42.45	44.95
26.1.77	40.00	41.25	43.75	46.25	48.75
27.1.77	6.00	6.50	7.50	8.50	9.50
28.1.77	2.00	2.50	3.50	4.50	5.50
5.2.77	6.00	6.50	7.50	8.50	9.50
21.2.77	3.20	3.70	4.20	5.70	6.70
27.2.77	17.20	18.45	20.95	23.45	25.95
27.2.77	17.20	18.45	20.95	23.45	25.95
Total	195.2	206.2	228.2	250.2	272.2

APPENDIX VII (a)

Values adopted for the increment of snowfall due to
orographic effect.

Snowfall at base station (in cm)	Incremental values of snowfall with elevation cm per 2000 ft (610 m)
0 - 10	1
10 - 40	2.5
above 40	40

APPENDIX VII (b)

Values adopted for the increment of rainfall due to the
orographic effect.

Rainfall at the base station (in cm)	Incremental values of rainfall with elevation cm per 2000 ft. (610 m)
0 - 1	0.1
1 - 4	0.25
above 4	0.40

APPENDIX-VXXX(a)

Estimated equivalent water stored in the snow during the accumulation season for different elevation zones in Arnold catchment.

accumulation season: 1970 Nov. to 1979 Nov.

Col.1.	Elevation zone	Volume of equivalent water stored in deposited snow under constant precipitation regime (m ³)
1	2	3
1.	0000-6300	16035009
2.	6300-10000	33052061
3.	10000-12000	77919309
4.	12000-30000	69973649

APPENDIX-VXXX(b)

accumulation season: 1977 Nov. to 1979 Nov.

1	2	3
1.	0000-6300	12005028
2.	6300-10000	30350109
3.	10000-12000	70442306
4.	12000-30000	60040107

APPENDIX-VXXX(c)

accumulation season: 1973 Nov. to 1977 Nov.

1	2	3
1.	0000-6300	20000000
2.	6300-10000	20050000
3.	10000-12000	30510000
4.	12000-30000	23400200

APPENDIX IX (a)

Calculated snowmelt due to rain and calculated rainfall runoff in different elevation zones.

Year 1979

Elevation zone 6000 ft to 8000 ft.

Date	Rainfall (mm)	Degree days (°Cd)	Snowmelt volume (m ³)	Snowmelt m ^{3/5}	Runoff (in m ^{3/5}) from rainfall when the zone is	
					snow covered	nonsnow covered
1	2	3	4	5	6	7
March						
23	0.01745	9.95	46303.10	0.54	2.85	-
31	0.02845	11.45	98578.40	3.12	4.61	-
April						
3	0.0057	10.45	17659.70	0.20	0.92	-
12	0.0027	15.95	12767.80	0.15	0.44	-
30	0.02345	(no snow-cover in the zone)		-		1.77
May						
10	0.0057			-		0.43
21	0.02445			-		1.95
23	0.0099			-		0.75
26	0.0610			-		4.67

Elevation zone 9000 ft. to 10000 ft.

1	2	3	4	5	6	7
March						
23	0.01995	5.89	73569.40	0.85	6.83	-
31	0.03095	6.39	162576.10	1.88	10.59	-
April						
3	0.0067	7.39	30999.70	0.35	2.29	-
12	0.0037	12.09	29850.3	0.35	1.26	-
30	0.02595	(no snow-cover in the zone)		-	4.14	
May						
10	0.0067			-	1.07	
21	0.02695			-	4.31	
23	0.0199			-	1.74	
26	0.0558			-	10.52	

Elevation zone 10000 ft. to 12000 ft.

March						
23	0.02245	2.83	82977.80	0.96	16.17	-
31	0.03345	5.33	234999.5	2.72	24.09	-
April						
3	0.0077	4.33	43946.30	0.51	5.54	-
12	0.0047	9.83	60896.80	0.70	3.38	-
30	0.02845	11.33	424869.80	4.92	20.49	-
May						
10	0.0077	(no snow-cover in the zone)		-	2.59	
21	0.02945			-	9.90	
23	0.0119			-	4.00	
26	0.0598			-	23.49	

Contd.....

Elevation zone 12000 ft. to 14000 ft.

1	2	3	4	5	6	7
March						
23	0.02495	-	-	-	-	-
31	0.03595	2.27	112952.30	1.31	27.19	-
April						
3	0.0087	1.27	15293.00	0.18	6.58	-
12	0.0057	6.77	53411.40	0.62	4.31	-
30	0.03095	8.27	354271.90	4.10	23.41	-
May						
10	0.0087	4.77	57439.10	0.66	6.58	
21	0.03195	10.77	476274.30	5.51	24.60	
23	0.0124	(no snow cover in the zone)			-	4.38
26	0.0738					26.08

Elevation zone above 14000 ft.

March					
23	0.02745	-	-	0.339	
31	0.03845	0.74	-	0.339	
April					
3	0.0097	-	-	-	
12	0.0057	5.24	-	0.42	
30	0.03345	6.74	-	2.69	
May					
10	0.0097	3.24	-	0.37	
21	0.03445	9.24	-	3.80	
23	0.0139	0.24	-	0.04	
26	0.0778	0.24	-	0.219	

APPENDIX : ZX (b)

Calculated snowmelt due to rain and calculated rainfall runoff in different elevation zones.

(Year 1978)

Elevation more 6000 ft. to 8000 ft.

Date	Rainfall (in)	Degree days (c.d)	Snowmelt volume (m ³)	Snow melt (m ³ /a)	Round off (in 3/a) from rainfall when the zone is		
					snow covered	Now covered	low covered
1	2	3	4	5	6	7	
March							
17	0.0868	4.46	114774.9	1.33	14.06	-	
18	0.03495	5.45	56472.3	0.65	5.86		
28	0.01148	9.45	032079.6	0.37	1.85		
29	0.0039	9.45	10926.6	0.13	0.63		
April							
3	0.0063	(No snowcover in the zone)			1.02		
4	0.01245				2.02		
17	0.01345					1.02	
18	0.0428					3.24	
22	0.01945					1.39	
May							
23	0.01895					1.42	
26	0.0059					0.446	
31	0.0027					0.204	

Elevation zone 8000 ft to 10000 ft

1	2	3	4	5	6	7
March						
17	0.0909	1.39	79020.5	0.91	31.07	-
18	0.03745	2.39	56039.5	0.65	12.01	-
28	0.01395	6.39	55910.3	0.65	4.77	-
29	0.0049	6.39	21137.9	0.24	1.67	-
April						
3	0.0073	6.89	31490.6	0.36	2.49	-
4	0.01495	5.39	50450.9	0.58	5.11	-
17	0.01995	14.39	143701.4	1.66	9.45	-
18	0.0468	14.45	423602.3	4.90	16.01	-
22	0.02095	9.89	129723.8	1.50	7.17	-
March						
25	0.02135	(no snow cover in the zone)				3.41
26	0.0069			-		1.103
31	0.0039	?				0.59

Elevation zone 10000 ft to 12000 ft.

March						
17	0.0948	-				
18	0.03995	-				
28	0.01645	3.23	72202.7	0.83	11.0	-
29	0.0059	3.03	29784.7	0.34	4.2	-

Contd...

1	2	3	4	5	6	7
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April

3	0.0093	3.82	41900.6	0.48	5.9	-
4	0.01745	2.33	93591.3	0.61	12.57	-
17	0.01845	11.33	272894.5	3.12	13.29	-
19	0.0598	8.33	557766.5	6.45	36.59	-
22	0.02345	6.83	211109.2	2.44	16.89	-

May

25	0.02385	(no snow cover in the zone)	-	-	8.02	
26	0.0079			-	-	2.65
31	0.0047			-	-	1.58

Elevation zone 12000 ft to 14000 ft.

March

17	0.0988	-	-	-	-	-
18	0.04245	-	-	-	-	-
28	0.01895	0.27	7081.79	0.08	14.33	-
29	0.0069	0.77	7353.77	0.09	5.22	-

April

3	0.0093	0.77	9911.61	0.11	7.03	
4	0.02995	-	-	-	15.09	
17	0.02095	8.27	239806	2.77	15.89	-
19	0.0348	5.27	399725.1	4.62	41.46	-
22	0.02595	3.77	135609.5	1.56	19.63	-

1	2	3	4	5	6	7
May						
25	0.02635	12.27	447502.8	5.17	-	9.31
26	0.0089	(no snow cover in the zone)		-		3.14
31	0.0057	-	-	-	-	2.01
Elevation zone above 14000 ft.						
March						
17	0.1028					
18	0.04495					
28	0.02145					
29	0.0079					
April						
3	0.0103					
4	0.02245					
17	0.02345	6.74		1.87		
18	0.0588	3.74		2.62		
22	0.02845	2.24		0.76		
May						
23	0.02895	10.74		3.69		
26	0.0099	11.24		1.33		
31	0.0067	9.74		0.78		

Calculated snowmelt due to rain and calculated rainfall runoff
in different elevation zones. Year - 1977

Elevation zone 8000 ft. to 10,000 ft.

no	Rainfall (mm)	Degree days (°cd)	Snowmelt volume (m ³)	Snowmelt m ³ /a	Runoff (in m ³ /a) from rainfall when the zone Snow- covered	Non snow- covered
1	0.0055	9.39	5853.63	0.07	0.34	-
2	0.0099	12.39	13909.7	0.16	0.61	-
3	0.03195	9.39	35832.7	0.42	1.98	-
4	0.02635	6.39	23147.1	0.3	1.51	-
5	0.0037	6.39	26914.81	0.03	0.11	
6	0.0059	7.00	5275.88	0.06	0.17	
7	0.0059				0.17	
8	0.0039				0.17	
9	0.0037				0.11	
10	0.01755				0.51	
11	0.01995				0.58	
12	0.01615				0.47	
13	0.02415				0.70	
14	0.0037				0.19	
15	0.02095				0.61	
16	0.02625				0.76	
17	0.0057				0.16	
18	0.03568				0.74	
19	0.02795				0.81	
20	0.02535				0.73	
21	0.0067				0.194	
22	0.0047				0.14	
23	0.02455				0.71	
24	0.0057				0.16	

Elevation zone 10000 ft. to 12000 ft.

1	2	3	4	5	6	7
March 31	0.065	6.33	30076.9	0.35	2.31	-
April 1	0.0109	9.33	26340.5	0.06	3.70	-
6	0.03445	6.33	171999.5	1.99	11.69	-
7	0.02665	5.33	104613.7	1.21	9.11	-
8	0.0047	3.33	11440.8	0.13	1.59	-
10	0.0037	3.33	1035.9	0.12	1.26	-
11	0.0069	4.33	26254.2	0.277	2.34	-
15	0.0069	4.33	24354.2	0.20	2.34	-
16	0.0047	4.33	16593.7	0.19	1.59	-
19	0.02005	3.33	48600	0.56		3.74
20	0.02245					4.19
24	0.01865					3.49
25	0.02665					4.97
26	0.0077					1.44
28	0.02345					4.38
29	0.02885					5.34
30	0.0062					1.23
May 4	0.0606					11.35
10	0.03045					3.69
14	0.02785					5.19
15	0.0077					1.44
27	0.0057					1.06
29	0.02705					3.05
30	0.0057					1.23

Elevation zone 12000 ft. to 14000 ft.

T	2	3	4	5	6	7
March 31	0.007	3.27	25585.1	0.31	4.64	
April 1	0.0119	6.27	00080.4	0.93	7.03	
2	0.03695	3.27	151602.8	1.74	21.88	
7	0.02935	2.27	71809.5	0.83	17.38	
8	0.0057	0.27	1668.27	0.02	3.38	
10	0.0077	0.27	3121.99	0.04	2.76	
11	0.0079	1.27	15154.3	0.18	4.68	
15	0.0079	2.27	15184.3	0.18	4.68	
16	0.0057	2.27	10936.4	0.13	3.38	
19	0.02355	0.27	6359.39	0.08	13.38	
20	0.02495	3.27	10196.1	1.18	14.78	
24	0.02115	2.27	6350.66	0.73	12.52	
25	0.02915	2.27	71728.8	0.81	17.16	
26	0.0087	2.27	21407.9	0.23	3.15	
28	0.02595	2.27	77919.5	0.69	15.37	
29	0.03135	3.27	311125.7	1.27	19.57	
30	0.0077	2.27	18947.2	0.19	4.36	
May 4	0.0448	6.27	239938.4	3.48	38.38	
10	0.03195	(no snow cover in the zone)			9.12	
14	0.03035				6.39	
15	0.0087				2.41	
27	0.0087				1.05	
29	0.02935				0.17	
30	0.0077				2.13	

Elevation zones above 14000 ft.

Date	Degree day ($^{\circ}\text{C}$)	Daily snowmelt m ³ /s	Sum of daily snowmelt for all the zones m/s
1	2	3	4
Mar. 31	0.0085	1.74	0.1752
April 1	0.0144	4.74	0.8130
2	0.03945	2.24	1.052
7	0.03185	0.74	0.2891
8	0.0067	-	-
10	0.0057	-	-
11	0.0087	0.24	0.0247
15	0.0099	0.24	0.02547
16	0.0067	0.24	0.01916
19	0.02505	-	-
23	0.02745	2.24	0.7329
24	0.02385	1.24	
25	0.03165	0.74	0.27
26	0.0097	0.74	0.060
28	0.02845	1.24	0.42
29	0.03305	1.74	0.69
30	0.0077	0.74	0.06
May 4	0.0088	2.74	2.23
10	0.03545	5.74	2.24
14	0.03205	4.74	1.96
15	0.0097	6.24	0.72
27	0.0077	6.74	0.6
29	0.03205	7.74	2.96
30	0.0087	6.24	0.85

APPENDIX X (a)

Computed daily snowmelt in different elevation zones
in Manali catchment

Year 1979

ELeVELATION ZONE: 6000 ft to 8000 ft

Date	Degree-Day (°C d)	Dail snow melt volume (m ³)	Daily snow melt (m ³ /s)	Equivalent volume of water remaining in the form of snow (m ³)
1	2	3	4	5
March				
18	4.95	209652.3	2.43	13845756
19	7.45	315537.3	3.65	13530219
20	8.45	357891.3	4.14	13172328
21	9.45	400245.3	4.63	12772082
22	8.95	379068.3	4.39	12393013
23	8.95	379068.3	4.39	11967642**
24	10.45	442599.3	5.14	11525042
25	10.45	442599.3	5.14	11082443
26	10.95	463776.3	5.37	10618667
27	10.95	463776.3	5.37	10154890
28	10.95	463776.3	5.37	9691113.7
29	12.45	527307.3	6.10	9163806.4
30	11.95	506130.3	5.86	8657676.1
31	11.45	484953.3	5.61	8076144.4**
April				
1	12.45	527307.3	6.10	7548837.1
2	12.45	527307.3	6.10	7021529.8

1	2	3	4	5
3	10.45	442599.3	5.12	6561270.8**
4	11.45	484953.3	5.61	607631.5
5	12.95	548484.3	6.34	5527833.2
6	12.95	548484.3	6.34	4979348.9
7	13.45	569561.3	6.59	4409587.5
8	14.45	612015.3	7.00	3797672.2
9	14.45	612015.3	7.00	3185656.9
10	15.45	654359.3	7.57	2531287.6
11	15.95	67554613	7.62	1855741.3

Elevation zone 6000 ft. to 10000 ft.

19	2.89	169045.3	1.96	3328941.5
20	4.39	393650.3	4.54	3289396.5
21	5.39	482092.3	5.53	3241487.3
22	5.39	571534.3	6.61	3184333.8
23	5.39	526813.3	6.10	3131452.5
24	7.39	660976.3	7.65	3005516.6
25	7.39	660976.3	7.65	2939419.0
26	7.89	705697.3	8.17	2868849.2
27	7.89	705697.3	8.17	2798279.5
28	7.89	705697.3	8.17	2798272.5

Contd... .

1	2	3	4	5
29	9.39	839860.3	9.72	25605284
30	8.89	795739.3	9.20	25311144
31	9.39	750418.3	8.69	24898148**
April				
1	9.39	839860.3	9.72	24058288
2	9.39	839860.3	9.72	23218427
3	7.39	660976.3	7.65	22526451**
4	8.39	750418.3	8.65	21778033
5	9.89	884581.3	10.29	20891452
6	9.89	884581.3	10.24	20006557
7	10.39	929302.3	10.76	19077558
8	11.39	1018744.3	11.79	18058824
9	11.39	1018744.3	11.79	17040079
10	12.39	1108186.3	12.83	15931693
11	12.89	1152907.3	13.34	14778986

Elevation Zone 10000 ft to 12000 ft.

March				
18	-	-	-	77919385
19	1.83	250426.3	2.89	7766948
20	2.33	438734.3	5.08	77230214
21	3.33	627032.3	7.26	76603193
22	2.83	532683.3	6.17	76070298

Contd.

<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>
23	2.83	532883.3	6.17	75454437 **
24	4.83	815330.3	8.44	74639107
25	4.83	815330.3	9.44	73823777
26	4.83	909479.3	10.53	72914297
27	4.83	909479.3	10.53	72004841
28	4.83	909479.3	10.53	71095339
29	6.83	1191926.3	13.80	69903412
30	5.83	1097777.3	12.71	68805635
31	5.83	1003528.3	11.62	67767007**
<u>April</u>				
1	6.83	1191926.3	13.80	66575081
2	6.83	1191926.3	13.80	65383155
3	4.83	815330.3	9.44	64523878**
4	5.83	1003528.3	11.62	63520250
5	6.83	1286075.3	14.86	62234175
6	6.83	1286075.3	14.86	60948099
7	7.83	1380224.3	15.97	59567875
8	8.83	1568522.3	18.15	57999353
9	8.83	1568522.3	18.15	56481267
10	9.83	1756620.3	20.33	54724446
11	9.83	1850969.3	21.42	52873477
Elevation zone 12000 ft. to 14000 ft.				
18	-	-	-	-
19	-	-	-	-

Contd.....

1	2	3	4	5
20	-	-	-	89776489
21	0.27	53387.1	0.62	89723061
22	-	-	-	
23	-	-	-	
24	1.27	25117.1	2.91	89471944
25	1.27	25117.1	2.91	89220827
26	1.77	349982.1	4.05	88870845
27	1.77	349982.1	4.05	88520863
28	1.77	349982.1	4.05	88170881
29	3.27	646577.1	7.48	87524304
30	2.77	547712.1	6.34	86976592
31	2.27	448847.1	5.19	85414792**
April				
1	3.27	646577.1	7.48	85768215
2	3.27	646577.1	7.48	85121639
3	1.27	25117.1	2.91	84855228**
4	2.27	448847.1	5.19	84406381
5	3.27	745442.1	8.63	83660939
6	3.27	745442.1	8.63	82915497
7	4.27	844307.1	9.77	82071189
8	5.27	1042037.1	12.06	81029152
9	5.27	1042037.1	12.06	79987115
10	6.27	1239767.1	14.35	78747348
11	6.27	1338632.1	15.69	777462104

Elevation zone above 16000 ft.

Date	Degree days (°ad)	Snow daily snow melt (m³/s)	Sum of daily snow melt from all the zones (m³/s)
1	2	3	4
March			
19	-	-	4.39
19	-	-	11.08
20	-	-	14.86
21	-	-	18.59
22	-	-	18.66
23	-	-	19.01*
24	-	-	25.14
15	-	-	25.14
26	0.24	0.41	28.53
27	0.24	0.41	28.53
28	0.24	0.41	28.53
29	1.74	2.96	40.06
30	1.24	2.11	33.22
31	0.74	1.26	39.74*
April			
1	1.74	2.96	40.06
2	1.74	2.96	40.06
3	-	-	27.00 *
4	0.74	1.26	32.37
5	2.24	3.61	43.90

Contd...

1	2	3	4	5
6	2.24	3.81	43.90	
7	2.74	4.66	47.75	
8	3.74	6.37	55.45	
9	3.74	6.37	55.45	
10	4.74	8.07	63.15	
11	5.24	8.92	66.99	

Elevation zone 6000 ft to 8000 ft.

April

12	15.95	675546.3	7.82	1377082.2**
13	15.95	675546.3	7.82	701535.9
14	15.95	675546.3	7.82	25989.6
15	13.95	25969.6	0.30	0

Elevation zone 8000 ft to 10000 ft.

April

12	12.89	1152907.3	13.34	13596217**
13	12.89	1152907.3	13.34	12443310
14	12.89	1152907.3	13.34	11290403
15	10.89	974023.3	11.27	10316379
16	9.39	839860.3	9.72	9476519.9
17	12.89	1152907.3	13.39	8323612.2
18	12.39	1108186.3	12.03	7215425.9

Contd....

1	2	3	4	5
19	11.39	1018744.3	11.79	6198681.6
20	10.89	974023.3	11.27	4248535
21	10.89	974023.3	11.27	4248535
22	13.39	1197626.3	13.85	3051805.7
23	14.89	1331791.3	15.41	1719215.4
24	14.89	1287070.3	14.90	432145.1
25	14.89	432145.1	5.00	0

Elevation zone 10000 ft. to 12000 ft.

April

12	9.83	1850969.3	21.42	50961610**
13	9.83	1850969.3	21.42	49110640
14	9.83	1850969.3	21.42	47259672
15	7.83	1474373.3	17.06	45765299
16	7.83	1380224.3	15.97	44403056
17	9.83	1850969.3	21.42	42552088
18	9.83	1756620.3	20.33	40795266
19	8.83	1569522.3	18.15	39226744
20	7.83	1474373.3	17.06	3775237
21	7.83	1474373.3	17.06	36277996
22	10.83	1945116.3	22.51	34332878
23	11.83	2227565.3	25.78	32105313
24	11.83	2133416.3	24.69	29971898
25	11.83	2133416.3	24.69	27936480
26	13.83	2516012.3	29.05	25328466

Contd....

1	2	3	4	5
27	13.33	2510012.3	29.05	22810455
28	13.33	2510012.3	29.05	20308443
29	12.83	2415853.3	27.96	17892580
30	11.33	2133416.3	24.69	15334294**
May				
1	11.33	3733478.5	43.21	11600815
2	11.33	3898239.3	45.12	7702576.2
3	11.33	3733478.5	43.21	3969097.7
4	8.83	2909674.8	33.68	1059422.9
5	9.33	1059422.9	12.26	0

Elevation range 12000 ft. to 14000 ft.

April				
12	6.77	13386321	15.49	7607006**
13	6.77	13386321	15.49	74731427
14	6.77	13386321	15.49	73392795
15	4.77	9431721	10.91	72449622
16	6.27	8443071	9.77	71605315
17	6.77	13386321	15.49	70266683
18	6.27	12397671	14.34	69026916
19	5.27	10420371	12.05	67984879
20	4.77	9431721	10.91	67041707
21	4.77	9431721	10.91	66098535
22	7.27	14374971	16.64	62926945

Contd.....

1	2	3	4	5
24	8.27	16352271	18.92	61291718
25	8.27	16352271	18.92	59655491
26	10.27	20306871	23.50	57625804
27	10.27	20306871	23.50	55595117
28	10.27	20306871	23.50	5356443
29	9.77	19318221	23.35	51632608
30	8.27	16352271	18.92	49643109**
May				
1	8.27	28616474	33.10	46701461
2	8.77	30346611	35.12	437468
3	8.27	28616474	33.10	40889153
4	5.77	199965706	23.11	38888574
5	6.27	21695924	25.11	36710982
6	3.77	13045236	15.10	35414458
7	3.77	13045236	15.10	34109934
8	3.77	13045236	15.10	32805411
9	5.27	18235649	21.10	30991646
10	4.77	10305511	19.10	29571295**

Elevation zone above 14000 ft.April

12	5.24	8.92	69.23*
13	5.24	8.92	66.99
14	5.24	8.92	66.99
15	3.24	5.52	45.08

Contd.....

1	2	3	4	5
16	1.74	2.96	38.42	
17	5.24	8.92	59.17	
18	4.74	8.07	55.57	
19	3.74	6.37	48.37	
20	3.24	5.52	44.76	
21	3.24	5.52	44.76	
22	5.74	9.77	62.78	
23	7.24	12.33	73.59	
24	6.74	11.46	69.99	
25	6.74	11.46	60.09	
26	8.74	14.86	67.43	
27	8.74	14.86	67.43	
28	8.74	14.86	67.43	
29	8.24	14.03	64.34	
30	6.74	11.46	66.80*	
May				
1	6.74	20.08	96.39	
2	7.24	21.57	101.81	
3	6.74	20.08	96.39	
4	4.24	12.63	69.42	
5	4.74	14.12	51.49	
6	2.24	6.67	21.77	
7	2.24	6.67	21.77	
8	2.24	6.67	21.77	
9	3.74	11.14	32.24	
10	3.24	9.65	29.78*	

Centd.....

Elevation zone 12000 ft. to 14000 ft.

1	2	3	4	5
Key				
11	6.27	2169592.4	25.10	26501702
12	6.27	2342606.1	27.11	24159098
13	6.27	2342606.1	27.11	2181649
14	5.77	1986576.6	23.11	19819911
15	6.27	2342606.1	27.11	17477305
16	6.27	2342606.1	27.11	15134699
17	6.27	2169592.4	25.10	12965107
18	8.77	3034661.1	35.12	99304461
19	10.27	3553702.4	41.13	63767437
20	10.27	3726716.1	43.13	26500278
21	10.27	2690027.6	36.183	0

Elevation zone above 14000 ft.

May			
11	4.74	14.12	39.22
12	5.24	15.61	42.72
13	5.24	15.61	42.72
14	4.74	12.63	35.74
15	5.24	15.61	42.72
16	5.24	15.61	42.72
17	4.74	17.12	39.22
18	7.24	21.57	56.69

Contd.....

1	2	3	4	5
19	9.79	26.04	67.17	
20	9.24	27.53	70.46	
21	9.24	27.53	73.02*	
22	6.24	18.59	18.59	
23	1.24	3.69	3.73*	
24	4.27	12.72	12.72	
25	3.27	9.74	9.74	
26	0.24	0.72	0.939*	
27	-	-	-	
28	-	-	-	
29	0.74	2.20	2.20	
30	0.74	2.20	2.20	
31	3.27	9.74	9.74	

** the volume of snowmelt due to rainfall is also considered.

* the snowmelt due to rainfall is also included.

APPENDIX - X(b)

Computed daily amount in different elevation zones in Manali

Catchment Year : 1978

Elevation zone 6000 - 8000 ft.

(1) Date Days (deg. cd)	(2) Degree Days	(3) Daily Melt Vol (m ³)x	(4) Daily snow melt (m ³ /s)	(5) Equivalent vol. of water remaining in the form of snow (m ³)x
1	2	3	4	5
March				
13	1.95	828903	0.96	12079125
14	3.45	146121.3	1.69	11933003
15	4.46	188898.8	2.19	11744104
16	3.95	167298.3	1.94	11576806
17	4.46	188898.8	2.19	11273132**
18	5.45	230829.3	2.67	10985831**
19	5.95	282006.3	2.92	10733825
20	6.45	273183.3	3.16	102160641
21	6.45	273183.3	3.16	10107458
22	5.45	230829.3	2.67	9956629.1
23	8.95	379068.3	4.39	9577560.8
24	8.45	357891.3	4.14	9219669.5
25	8.45	387891.3	4.14	8861778.2
26	9.45	400248.3	4.63	8461532.9
27	9.45	400248.3	4.63	8061287.6
28	9.45	400248.3	4.63	7628962.7**
29	9.95	421423.3	4.88	7196613.0**
30	9.95	421423.3	4.88	6775191.5
31	9.95	421423.3	4.88	6353769.2

1	2	3	4	5
April				
1	0.93	379068.3	4.39	5974700.9
2	0.93	379068.3	4.39	5595632.6
3	0.93	421422.3	4.39	5132309.7**
4	0.45	357891.3	4.14	4720827.1
5	0.45	357891.3	4.14	4362935.6
6	0.93	421422.3	4.39	3941513.5
7	12.45	527307.3	6.10	3414206.2
May 13	-	ELEVATION ZONE 8000 - 10000 ft-	-	30358105
14	0.39	34882.3	0.40	30323222
15	1.39	124324.3	1.44	30198898
16	0.89	79603.3	0.92	30119295
17	1.39	124324.3	1.44	29915950**
18	2.39	213766.3	2.47	29646145**
19	2.89	258487.3	2.99	29387657
20	3.29	303208.3	3.51	29084449
21	3.39	303208.3	3.51	28791241
22	2.39	213766.3	2.47	28567475
23	5.89	526813.3	6.10	28040661
24	5.39	482092.3	5.58	27558569
25	5.39	482092.3	5.58	27076477
26	6.39	571534.3	6.60	26504942 25933408
27	6.39	571434.3	6.60	25900000000
28	6.39	571534.3	6.60	25306063**
29	6.89	616255.3	7.13	24668671**
30	6.89	616255.3	7.13	24052415
31	6.89	616255.3	7.13	23436160

Contd...

1	2	3	4	5
April				
1	5.09	526813.3	6.10	22909347
2	5.09	526813.3	6.10	22382533
3	5.09	616255.3	7.13	21734782**
4	5.09	482092.3	5.58	21202243**
5	5.09	482092.3	5.58	20720151
6	6.09	616255.3	7.13	20103898
7	9.09	819860.3	9.72	19264036
May	13	Elevation zone 10000 - 12000 ft		
14	-	-	-	-
15	-	-	-	-
16	-	-	-	-
17	-	-	-	-
18	-	-	-	-
19	-	-	-	70449604
20	0.33	62138.3	0.72	70381469
21	0.33	62138.3	0.72	70325327
22	0	0	-	*
23	2.83	53288.3	6.07	69792444
24	2.83	438734.3	5.08	69353709
25	2.83	438734.3	5.08	68914975
26	3.83	627032.3	7.26	68287943
27	3.83	627032.3	7.26	67660910
28	3.83	627032.3	7.26	66961675**
29	3.83	721181.3	8.35	66210709**
30	3.83	721183	8.35	65489526
31	3.83	721183	8.35	64768343

1	2	3	4	5
---	---	---	---	---

Appl	2.82	531000.3	6.15	64238343
2	2.12	531000.3	6.15	63706343
3	3.83	721183	8.35	62943259**
4	2.33	438734.3	5.08	62450934**
5	2.33	438734.3	5.08	62012199
6	2.83	438734.3	5.08	61573465
7	6.33	1191926.3	13.80	60381539

Mar 13 Elevation zones 12000 ft-14000 ft

14	-	-	-	-
15	-	-	-	-
16	-	-	-	-
17	-	-	-	-
18	-	-	-	-
19	-	-	-	-
20	-	-	-	-
21	-	-	-	-
22	-	-	-	-
23	-	-	-	-
24	-	-	-	-
25	-	-	-	80844107
26	0.27	53387.1	0.62	80790719
27	0.27	53387.1	0.62	80737332
28	0.27	53387.1	0.62	80676864**
29	0.77	152252.1	1.76	80654285**
30	0.77	152252.1	1.76	80532033
31	0.77	152252.1	1.76	80349780

Contd.....

1	2	3	4 *	5
April				
1	-	-	-	-
2	-	-	-	-
3	0.77	152252.1	1.76	80187617*
4	-	-	-	-
5	-	-	-	-
6	0.77	152252.1	1.76	80035365
7	3.27	646577.1	7.48	79388788

Elevation zones above 1400 ft.

Date	Degree days (.cd)	Daily snow melt (m ³ /s)	Sum of daily snowmelt from all the zones (m ³ /s)
1	2	4	6
Nov 13	-	-	0.96
14	-	-	3.13
15	-	-	3.11
16	-	-	2.86
17	-	-	3.87
18	-	-	6.44
19	-	-	5.91
20	-	-	7.39
21	-	-	7.39
22	-	-	5.14
23	-	-	16.41
24	-	-	14.60
25	-	-	14.00
26	-	-	19.11
27	-	-	19.11
28	-	-	21.09

1	2	4	6
29			22.92*
30			22.12
31			22.12
April 1			16.64
2			16.64
3			23.55*
4			16.60*
5			15.54
6	0.24	0.41	19.26
7	1.74	2.95	40.06
	Elevation 6000-8000		
April 8	12.45	527307.3	6.10 2896898.9
9	12.45	527307.3	6.10 2359591.6
10	12.45	527307.3	6.10 1832284.3
11	14.45	612015.3	7.08 1220269
12	15.95	679540.3	7.82 544722.7
13	14.45	544722.7	6.30 0
	Elevation 8000-10000 ft		
April 8	9.39	839960.3	9.72 184241.75
9	9.39	839960.3	9.72 17584314
10	9.39	839960.3	9.72 1674445.4
11	11.39	1018744.3	11.79 15662580
12	12.89	1152907.3	13.34 141335070
13	11.39	1018744.3	11.79 13114762
14	11.39	1063965.3	12.31 12051297

Contd....

	1	2	3	4	5
15	12.39	1108186.3	12.82	10943111	
16	14.89	1331791.3	15.39	9611319.8	
17	14.39	1287070.3	14.90	8180548.3**	
18	14.45	1292436.9	14.93	6464709.1**	
19	9.39	839860.3	9.72	5624848.8	
20	9.89	884581.3	10.24	4740267.5	
21	9.39	750410.3	9.68	3989849.2	
22	9.87	884581.3	10.23	2975544.1	
23	9.39	839860.3	9.72	2135683.8	
24	9.89	884581.3	10.23	1251102.5	
25	9.89	884581.3	10.23	366521.2	
26	14.45	368521.2	4.24	0	
27	-	-	-	-	
28	-	-	-	-	
29	-	-	-	-	
30	-	-	-	-	
May	-	-	-	-	
1	-	-	-	-	
2	-	-	-	-	
3	-	-	-	-	
4	-	-	-	-	
5	-	-	-	-	
6	-	-	-	-	
		Elevation Zone	10000 - 12000 ft		
8	6.33	1191926.3	13.80	59189612	
9	6.33	1191926.3	13.80	57997686	

Contd...

<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>
April				
11	8.33	1568522.3	18.15	55237237
12	9.33	1850969.3	21.41	53806260
13	8.33	1568522.3	18.15	51837746
14	8.33	1662671.3	19.24	50155074
15	9.33	1756820.3	20.33	48398257
16	11.33	2227565.3	25.78	46170689
17	11.33	2133416.3	24.69	43764378**
18	8.33	1568522.3	18.15	41638089**
19	6.33	1191926.3	13.80	40446163
20	6.33	1286075.3	14.88	39160088
21	5.33	1093628.3	11.62	38186459
22	6.33	1286075.3	14.88	36659275**
23	6.33	1191926.3	13.80	35467349
24	6.33	1286075.3	14.88	34181273
25	6.33	1286075.3	14.88	32995190
26	7.33	1380224.3	15.97	31514974
27	8.33	1568522.3	18.15	29946451
28	10.33	1945118.3	22.91	28001333
29	10.33	2039267.3	23.60	25961066
30	10.33	2039267.3	23.60	23922798
May				
1	10.33	3568717.3	41.30	20031282
2	10.33	3568717.3	41.30	16462564
3	11.33	3733478.3	43.17	12729085
4	11.33	3733478.3	43.17	8995407.4
5	13.33	4391521.3	50.84	4603085.9
6	13.33	4392521.3	50.84	210964.4

Cont'd...

1	2	3	4	5
Elevation zone 12000 ft ~14000 ft.				
April				
8.	3.27	646577.1	7.48	78742210
9.	3.27	646577.1	7.48	78095633
10.	3.27	646577.1	7.48	77449056
11.	5.27	1042037.1	12.06	76407019
12.	6.77	1338632.1	15.49	76068387
13.	5.27	1042037.1	12.06	74026350
14.	5.27	1140902.1	13.20	72885448
15.	6.27	1239767.1	14.35	71645681
16.	6.27	1734092.1	20.07	69911589
17.	6.27	1635227.1	18.92	68936556**
18.	5.27	1042037.1	12.06	66594793**
19.	3.27	646577.1	7.48	65948213
20.	3.77	745442.1	8.63	65202774
21.	2.27	448847.1	9.19	64753927
22.	3.77	745442.1	8.63	64618517**
23.	3.27	646577.1	7.48	63971940
24.	3.71	745442.1	8.63	63226498
25.	3.77	745442.1	8.63	62481056
26.	4.27	644307.1	9.77	616336749
27.	5.27	1042037.1	12.06	60594712
28.	7.72	1437497.1	16.64	50157215
29.	7.77	1536363.1	17.78	57620853
30.	7.77	1536363.1	17.73	56084490
May				
1	7.77	2688629.5	31.11	53395860
2	7.77	2688629.7	31.11	50707230

Contd...

1	2	3	4	5
3	8.27	286164342	33.12	47845587
4	10.27	3553697.2	41.13	44291890
5	10.27	3553697.2	41.13	40738193
6	10.27	3553697.2	41.13	37184495

Elevation zone above 14000 ft.

Date (1)	Degree days (cd) (2)	Daily snow melt (m ³ /s) (4)	Sum of daily snow melt from all the zones (m ³ /s) (6)
7. 8	1.74	2.96	40.06
9	1.74	2.96	40.06
10	1.74	2.96	40.06
11	3.74	6.37	55.45
12	5.24	8.92	66.98
13	3.74	6.37	55.45
14	4.24	7.23	59.31
15	4.74	8.07	55.45
16	7.24	12.33	73.57
17.	6.74	11.48	79.41*
18.	3.74	6.37	70.10*
19.	1.74	2.96	33.96
20.	2.24	3.81	37.56
21	0.74	10.26	26.75
22.	2.24	3.81	43.81*
23	1.74	2.96	33.96
24	2.24	3.81	37.55
25	2.24	3.81	37.55

1	2	4	6	8
26.	2.74	4.67	34.95	
27.	3.74	6.37	36.58	
28.	5.74	9.77	48.92	
29.	6.24	10.62	52.00	
30.	6.24	10.62	52.00	

May

1	6.24	18.59	91.00
2	6.24	18.59	91.00
3	6.24	20.08	96.37
4	6.24	20.08	96.37
5	8.74	26.04	118.01
6	8.74	26.04	118.01

x1xx22

Elevation 10000 ft - 12000

May 7	13.33	210564.4	2.44	5
8	12.83	-	-	-
9	12.83	-	-	-

Elevation 12000 ft 14000 ft

May 7	10.27	3553697.2	41.13	33630798
8	9.77	3380693.7	39.12	30250116
9	9.77	3380693.7	39.12	26869431
10	10.77	3726710.7	43.12	23142730
11	10.27	3553697.2	41.12	19589023
12	10.77	3726710.7	43.12	15862312
13	10.77	3726710.7	43.12	12135601
14	10.77	3726710.0	43.12	8408890.3
15	11.27	3899724.3	45.14	4509166.1

<u>ELEVATION ZONE ABOVE - 14000-ft.</u>			
1	2	3	6

Mar 29			22.92
30			22.12
31			22.12
1			16.64
2			16.64
3			23.55*
4			16.60*
5			15.54
6	.24	0.41	19.26
7	1.74	2.96	40.06
8	1.77	2.96	40.06
9	1.74	2.96	40.06
10	1.74	2.96	40.06
11	3.74	6.37	55.45
12	5.24	8.92	66.98
13	3.74	6.37	55.45
14	4.24	7.23	59.31
15	4.74	8.07	55.45
16	7.24	12.33	73.57
17	6.74	11.48	79.41*
18	3.74	6.37	70.10*
19	1.74	2.96	33.96
20	2.24	3.81	37.56
21	0.74	1.26	26.75
22	2.24	3.81	43.81*

ELEVATION ZONE ABOVE 14000ft-

<u>1</u>	<u>2</u>	<u>3</u>	<u>6</u>
23	1.74	2.96	33.96
24	2.24	3.81	37.55
25	2.24	3.81	37.55
26	2.74	4.67	34.65
27	3.74	6.37	36.58
28	5.74	9.77	48.92
29	6.24	10.61	52.00
30	6.24	10.62	52.00

May

1	6.24	18.59	91.00
2	6.24	18.59	91.00
3	6.74	20.08	96.37
4	6.74	20.08	96.37
5	8.74	26.04	118.01
6	8.74	26.04	118.01

elevation zone 1200ft to 14000ft

1	2	3	4	5
16	11.27	3899726.2	45.14	609461.9
17	11.27	609461.9	7.05	0

ELEVATION ZONE ABOVE 14000ft

1	2	4	6
May 7	8.74	26.04	69.61
8	8.28	24.55	63.67
9	8.24	24.55	63.67
10	9.24	27.53	70.65
11	8.74	26.04	67.16
12	9.24	27.53	70.65
13	9.24	27.53	70.65
14	9.24	27.53	70.65
15	9.74	29.02	74.16
16	9.74	29.02	74.16
17	9.74	29.02	36.52
18	10.24	30.51	30.51
19	10.24	30.51	30.51
20	9.74	29.02	29.02
21	9.74	29.02	29.02
22	9.74	29.02	29.02
23	10.74	32.00	32.00
24	10.74	32.00	32.00
25	10.74	32.00	35.69*
26	11.24	33.49	34.82*
27	10.74	32.00	32.00
28	11.74	34.98	34.98
29	12.24	36.47	36.47

197

1	2	4	6	5
30	10.74	32.00	32.00	
31	9.74	29.02	29.80*	

* the snowmelt due to rainfall is also included.

** the volume of snowmelt due to rainfall is also included.

APPENDIX: X (a)

Computed daily snowmelt in different elevation zones
in Manali catchment year 1977

ELeVELATION ZONE C 8000 - 10000 ft.

Date	Degree day (°C)	daily vol. of snowmelt (m ³)	daily snowmelt (m ³)	equivalent vol. of water namely in the (m ³)
1	2	3	4	5
March				
28	11.89	192618	2.23	1861162
29	11.39	184518	2.14	1676664
30	11.89	191970	2.23	1484694
31	9.39	152118	1.76	1326719.4 **
Apri. 1	12.39	202218	2.32	1112091.7 **
2	11.89	192618	2.23	919463.7
3	11.89	192618	2.23	726835.7
4	11.89	192618	2.23	534217.7
5	9.89	160218	1.85	373979.7
6	9.89	160218	1.85	177949 ***
7	8.39	135918	1.57	10053.9 **
8		18853.9	0.22	0

ELeVELATION ZONE D 10000 - 12000 ft.

28	8.83	921852	10.66	13589748
29	8.83	689652	10.06	12720096
30	8.83	921852	10.66	11798244
31	6.33	660852	7.65	11107315 **

Contd....

	1	2	3	4	5
April					
1	9.33	974052	11.27	10058922	* *
2	8.83	921852	10.67	9137070.6	
3	8.83	921852	10.67	8215218.6	
4	8.83	921852	10.67	7293356.6	
5	6.83	713052	6.25	5695263.1	* *
7	5.33	556652	6.44	5034197.6	* *
8	3.33	347652	4.02	4751045.6	* *
9	3.33	347652	4.02	4327452.6	
10	3.83	399052	4.63	3917241.6	* *
11	4.83	504252	5.84	3389637.6	* *
12	5.03	608652	7.04	2779985.6	
13	6.33	859652	10.06	1910433.6	
14	4.33	452052	5.23	1458381.6	
15	4.83	504252	5.84	929767.6	* *
16	4.83	504252	5.84	408921.9	* *
17	5.33	408921.9	4.75	0	
	<u>Elevation range 12000.0 - 14000. ft.</u>				
May					
20	5.77	893196	10.34	22516004	
20	5.27	815796	9.44	21700208	
30	5.77	893196	10.34	20807612	
31	3.27	506196	5.83	20274230	* *

Contd.....

	1	2	3	4	5
brij	1	6.27	970596	11.23	19222754 **
	2	5.77	893196	10.34	13329558
	3	5.77	893196	10.34	17436362
	4	5.77	893196	10.34	16543165
	5	3.77	583596	6.75	15959570
	6	3.77	583596 583596	6.75	15214971 **
	7	2.27	351396	4.07	14801765 **
	8	0.27	41796	0.48	14758302 **
	9	0.27	41796	0.48	14716566
	10	0.27	119196	1.38	14593387 **
	11	1.77	273996	3.17	14304235 **
	12	2.27	428796	4.93	13873440
	13	5.27	815796	9.44	13059844
	14	1.27	196596	2.28	12863048
	15	1.77	273996	2.28	12573598 **
	16	1.77	273996	2.28	12286956 **
	17	2.27	351396.6	4.07	11937570
	18	2.27	351396	4.07	11586174
	19	0.27	41796	0.480	11537808 **
	20	3.77	583596	6.75	10944016 **
	21	2.27	428796	4.93	10515220
	22	2.27	428796	4.93	10086424
	23	3.27	508196	5.88	95802287
	24	2.27	428796	4.93	9122316.6 **
	25	2.27	351396	4.055	714997 **

Elevation zone above 14000 ft.

Date	Degrees & day	Daily snow- melt	Sum of daily snowmelt from all the zones (in ³ /s)
1	2	4	6
Mar 28	4.24	7.21	30.44
29	3.74	6.34	28.01
30	4.24	7.21	30.44
31	1.74	2.95	19.13 *
Apr 1	4.74	8.81	35.09 *
2	4.24	7.22	30.46
3	4.24	7.22	30.46
4	4.24	7.22	30.46
5	2.24	3.81	20.69
6	2.24	3.81	25.85 *
7	0.74	1.26	15.96
8			4.87
9			4.50
10			6.17
11	0.24	0.41	9.98 *
12	1.24	2.11	14.11
13	3.74	6.37	25.87
14	-	-	7.51
15	0.24	0.41	9.24 *

Contd.....

1	2	4	6
16	0.24	0.41	8.94 *
17	0.74	1.26	10.00
18	0.74	1.26	5.33
19	-	-	0.96
20	2.24	3.81	11.97 *
21	1.24	2.11	7.04
22	1.24	2.11	7.04
23	1.74	2.95	9.81
24	1.24	2.11	8.12 *
25	0.74	1.26	6.41 *

Elevation 12000 ± 14000 ft.

April	1	2	3	4	5	6
	26	2.27	0.351396	4.07	8.3969085	*
	27	3.27	0.593596	6.75	7.1633125	
	28	3.27	0.428796	4.95	7.2565985	* *
	29	3.27	0.506196	2.27	6.7609625	* *
	30	2.27	0.351396	4.07	6.2930623	* *
May	1	2.27	0.614943	8.68	5.6780593	
	2	2.27	0.614943	8.68	5.0631163	
	3	3.27	0.885943	10.25	4.1772733	
	4	4.27	1.156743	13.2	3.0205383	* *
	5	4.27	1.156743	13.39	1.9537873	
	6	4.27	1.156743	13.39	0.7070443	
	7	6.27	0.7070443	8.18	0.7070443	

Elevation 5500 above 14000 ft.

Date	Degree Days (cd)	Daily Snowmelt in'/s	Sum of daily snowmelt from all the slopes in' s
1	2	3	4
Nov 26	0.24	0.08	5.59 *
27	1.24	5.81	10.40
28	1.24	2.11	9.37 *
29	1.74	2.95	10.77 *
30	0.74	1.25	5.88 *
Dec 1	1.24	3.69	12.37
2	1.24	3.69	12.37
3	1.74	5.18	15.43
4	2.74	8.16	27.14 *
5	3.74	8.16	21.35
6	2.74	8.16	16.34
7	4.74	14.13	14.32
8	5.24	15.61	15.61
9	4.74	14.13	14.13
10	5.74	17.10	19.52 *
11	5.74	17.10	17.10
12	5.24	15.61	15.61
13	5.74	17.10	17.10
14	4.74	14.13	13.98 *
15	6.24	18.59 ^{18.59} 19.31	18.59 *
16	6.24	18.59	18.59
17	5.24	15.61	15.61
18	6.74	20.08	20.08
19	6.24	18.59	18.59

1	2	4	6
21	7.74	23.06	23.06
22	7.24	21.57	21.57
23	7.24	21.57	21.57
24	7.74	23.06	23.06
25	7.74	23.06	23.06
26	8.24	24.55	24.55
27	8.74	26.84	27.64*
28	7.24	21.57	21.57
29	7.74	23.06	26.02*
30	8.24	24.55	24.55*
31	7.74	23.06	23.91*

* the snowmelt due to rainfall is also included.

** the volume of snowmelt due to rainfall is also included.

APPENDIX XI (a)

Daily gauging discharge (excluding base flow) and computed daily snowmelt discharge including runoff due to rainfall on the snow-covered area and on non snow covered areas.

Year 1979

Date	Daily gauged discharge (excluding base flow) (m^3/s)	computed snowmelt discharge (m^3/s)	computed snowmelt discharge including runoff due to rainfall on the snow-covered area (m^3/s)	computed snowmelt discharge including runoff due to rainfall on the snow-covered area and non snow-covered area. (m^3/s)
1	2	3	4	5
March				
18	9.69	9.11	9.11	9.11
19	11.42	8.30	8.30	8.30
20	11.34	8.80	8.80	8.80
21	11.34	9.59	9.59	9.59
22	11.34	10.13	10.13	10.13
23	11.34	10.83	13.13	13.13
24	12.08	12.01	14.08	14.08
25	12.08	13.06	14.93	14.93
26	15.80	14.33	16.00	16.00
27	15.74	15.47	15.95	15.95
28	15.74	16.49	17.82	17.82
29	16.50	16.45	19.64	19.64
30	18.64	19.86	20.93	20.93
31	18.64	21.46	28.40	28.40

Contd... .

1	2	3	4	5
April				
1	18.44	22.92	29.16	29.16
2	18.44	24.24	29.84	29.84
3	18.44	24.25	30.67	30.67
4	18.44	24.73	30.51	30.51
5	25.36	26.21	31.41	31.41
6	25.12	27.96	32.22	32.22
7	25.12	29.08	33.29	33.29
8	26.57	31.17	34.95	34.95
9	26.57	33.04	35.44	35.44
10	33.67	35.42	38.48	38.48
11	33.65	37.90	40.66	40.66
12	48.08	40.96	43.66	43.66
13	47.91	42.34	45.32	45.32
14	47.91	44.13	46.82	46.82
15	47.91	43.78	46.18	46.18
16	47.91	42.86	45.60	45.60
17	47.91	43.91	45.85	45.85
18	49.02	44.52	46.26	46.26
19	48.37	44.41	45.98	45.98
20	47.54	44.00	45.92	45.92
21	47.57	43.63	44.91	44.91
22	47.57	44.92	46.05	46.05
23	47.57	47.03	48.07	48.07
24	47.54	48.64	49.55	49.55
25	47.54	49.19	50.00	50.00

Centd....

1	2	3	4	5
26	47.54	50.34	51.13	51.13
27	63.37	51.38	52.08	52.08
28	69.74	52.31	52.94	52.94
29	69.71	52.87	53.34	53.34
30	69.71	53.59	57.97	63.88
April				
1	69.71	56.91	60.84	60.84
2	70.76	60.38	63.92	63.92
3	59.20	63.02	66.19	66.19
4	59.14	62.97	65.82	65.82
5	49.62	61.30	63.56	63.56
6	49.45	57.13	59.42	59.42
7	40.24	53.38	55.44	55.42
8	43.76	50.00	51.84	51.84
9	43.79	47.90	49.56	49.56
10	46.76	45.79	47.67	51.96
11	39.96	44.74	46.60	46.60
12	44.96	44.11	45.78	45.78
13	44.99	43.54	45.04	45.07
14	44.99	42.40	43.76	43.76
15	44.99	42.00	43.22	43.22
16	44.99	41.64	42.74	42.74
17	44.99	41.01	41.99	41.99

Contd....

1	2	3	4	5
18	44.99	42.01	42.89	42.89
19	49.45	43.85	44.64	44.64
20	44.99	45.03	46.54	46.54
21	59.14	47.82	50.62	55.48
22	44.99	44.70	47.23	47.23
23	44.64	40.57	75.51	75.38
24	40.98	37.66	69.10	69.10
25	37.37	34.77	63.05	63.05
26	69.71	31.37	57.59	122.35
27	49.45	28.24	51.83	51.83
28	35.07	25.41	46.64	46.64
29	35.04	23.07	42.18	42.48
30	35.04	20.96	39.16	38.16
31	35.04	19.75	35.21	35.21

1	2	3	4	5
April 1	5.12	19.04	20.93	20.93
2	5.60	19.33	20.73	20.73
3	5.09	14.03	18.09	18.09
4	6.37	20.33	20.09	20.09
5	6.6	20.21	19.49	19.49
6	6.03	10.03	19.21	19.21
7	5.09	10.59	20.00	20.00
8	9.10	20.50	22.94	22.94
9	6.91	20.33	23.00	23.00
10	8.35	22.08	23.10	23.10
11	81.2	24.60	27.03	27.03
12	20.65	20.20	30.99	30.99
13	20.86	20.41	32.02	32.02
14	21.74	22.71	30.83	30.83
15	23.59	24.03	33.39	33.39
16	23.50	37.00	39.37	39.37
17	23.59	40.06	45.09	45.09
18	23.61	43.26	55.89	55.89
19	23.59	43.04	53.33	53.33
20	22.08	43.83	51.40	51.40
21	20.7	39.03	40.67	40.67
22	29.86	39.02	43.09	43.09
23	29.59	30.54	40.93	40.93
24	29.50	33.07	40.01	40.01
25	29.7	37.64	40.99	40.99
26	29.93	25.09	45.00	45.00
27	29.02	21.59	42.03	42.03

APPENDIX V (n)

Daily gauged discharge (excluding baseflow) and computed daily snowmelt discharge including runoff due to rainfall on the snow covered area and non snow covered area, Year-1970

Date	Daily gauged discharge excluding baseflow (m^3/s)	Computed snowmelt discharge (m^3/s)	Computed snowmelt discharge including runoff due to rainfall on the snow covered area (m^3/s)	Computed snowmelt discharge including runoff due to rainfall on the snow covered area and non snow covered area (m^3/s)
1	2	3	4	5
Mar. 13	6.93	6.93	6.92	6.92
14	6.91	6.93	6.93	6.93
15	4.04	4.19	4.19	4.20
16	5.99	4.03	4.03	4.03
17	11.77	6.33	6.31	6.32
18	11.03	6.32	6.06	6.06
19	21.09	6.02	9.20	9.20
20	0.48	4.05	0.93	0.93
21	4.93	4.05	0.73	0.73
22	9.12	4.03	0.31	0.32
23	5.23	5.03	5.53	5.53
24	5.29	6.57	9.40	9.40
25	5.20	7.25	9.78	9.78
26	5.29	6.36	20.59	20.59
27	3.20	3.10	11.19	11.19
28	0.90	10.18	14.92	14.92
29	6.00	11.13	20.54	20.54
30	4.93	12.04	20.00	20.00
31	4.09	12.02	17.10	17.10

1	2	3	4	5
April 1	5.12	19.04	20.93	20.93
2	5.00	19.23	20.73	20.73
3	5.09	16.03	20.09	20.09
4	6.37	20.22	20.09	20.09
5	6.6	20.11	19.48	19.48
6	6.03	14.43	19.23	19.23
7	5.09	16.59	20.00	20.00
8	5.10	20.54	22.94	22.94
9	6.91	20.39	23.00	23.00
10	6.39	21.08	29.10	29.10
11	11.2	24.68	27.06	27.06
12	20.65	20.26	30.93	30.93
13	20.84	20.41	32.02	32.02
14	21.74	32.71	34.83	34.83
15	23.59	34.63	35.33	35.33
16	22.50	37.00	39.37	39.37
17	23.59	40.06	45.09	45.71
18	23.81	43.26	55.80	55.10
19	25.56	41.04	59.33	59.33
20	22.08	43.83	51.60	51.40
21	20.7	39.03	40.67	40.67
22	20.96	39.02	41.09	41.09
23	20.50	30.64	40.93	40.93
24	20.50	30.07	40.01	40.01
25	20.7	37.04	40.93	40.93
26	20.03	23.09	43.09	43.09
27	20.02	24.59	43.09	43.09

1	2	3	4	5
April 28	31.1	37.33	43.85	43.85
29	34.8	38.28	44.15	44.15
30	34.22	39.13	44.41	44.41
May 1	38.22	43.41	48.16	48.16
2	34.06	47.36	51.53	51.53
3	65.51	51.80	55.05	55.05
4	65.51	54.75	58.21	58.21
5	72.03	59.89	63.01	63.01
6	78.5	64.53	67.33	67.33
7	78.5	64.34	66.86	66.86
8	78.5	63.83	65.90	65.90
9	76.40	62.99	65.04	65.04
10	76.20	63.06	67.89	64.89
11	76.37	62.79	64.45	64.45
12	69.58	62.87	64.36	64.36
13	65.86	62.95	64.29	64.29
14	65.85	63.01	64.23	64.22
15	65.85	63.38	64.47	64.47
16	70.9	63.71	64.69	64.69
17	70.9	60.63	63.51	61.51
18	73.14	57.32	58.11	58.11
19	73.79	54.34	55.05	55.05
20	72.37	51.51	52.15	52.15
21	73.37	48.97	49.54	49.54
22	72.37	46.60	47.20	47.20
23	63.48	46.89	45.35	45.35
24	63.16	43.29	43.71	43.71

1	2	3	4	5
23				
May	25	60.27	42.17	42.95
	26	70.97	41.00	41.42
	27	60.97	39.05	40.15
	28	61.93	39.03	39.30
	29	60.68	39.39	38.65
	30	60.49	37.44	37.66
	31	62.35	35.37	40.56

APPENDIX-XI (a)

Daily gauging discharge (excluding baseflow) and computed daily snowmelt discharge including runoff due to rainfall on the snow covered area and non snow covered area. YRSP = 1977

Date	Daily gauged discharge excluding baseflow(m ³ /s)	Computed snowmelt discharge (m ³ /s)	Computed snowmelt discharge including runoff due to rainfall on the snow-covered area (m ³ /s)	Computed snowmelt discharge including runoff due to rainfall on the snow-covered area and non snow-covered area (m ³ /s)
1	2	3	4	5
Mar. 28	12.62	14.097	14.097	14.097
29	13.98	15.21	15.206	15.206
30	14.69	16.43	16.42	16.42
Apr. 1	15.08	16.50	17.13	17.13
April 2	12.62	16.01	19.59	19.59
3	12.62	16.95	20.37	20.37
4	12.62	19.00	21.07	21.07
5	12.62	20.50	21.71	21.71
6	16.00	20.36	21.40	21.40
7	19.55	20.66	24.79	24.79
8	13.95	20.03	25.59	25.59
9	12.62	18.47	23.89	24
10	10.54	17.03	21.91	21.91
11	10.54	15.89	20.91	21.06
12	10.54	15.20	20.33	20.5
13	10.37	14.95	19.57	19.57
14	12.62	15.78	19.62	19.62
15	13.22	14.33	17.95	17.77

1	2	3	4	5
16	12.62	13.60	17.06	17.17
17	12.62	13.13	16.26	16.26
18	12.62	12.32	15.11	15.11
19	16.94	11.14	14.65	19.1
20	19.90	11.10	16.76	20.53
21	16.97	10.62	14.82	14.82
22	17	10.19	13.97	13.97
23	17	9.96	13.36	13.36
24	19.78	9.69	13.89	17.84
25	33.71	9.30	14.56	20.33
26	17.76	9.87	14.16	15.79
27	19.67	9.94	13.69	13.69
28	27.31	8.79	14.47	19.45
29	27.22	8.88	15.66	21.80
30	21.62	8.49	13.01	16.42
May	1	21.54	8.76	14.61
	2	21.54	8.99	14.62
	3	21.54	9.48	14.23
	4	23.56	10.98	18.71
	5	18.98	11.82	19.29
	6	18.86	12.11	19.81
	7	18.10	12.17	19.19
	8	18.19	12.35	18.67
	9	18.19	22.39	18.08
	10	18.19	22.91	23.63
	11	18.19	23.16	17.76
	12	18.92	13.24	17.30

1	2	3	4	5
May 13	18.76	13.46	17.18	17.18
14	25.81	13.55	16.90	31.21
15	19.04	13.94	16.95	30.995
16	18.19	14.21	16.92	16.92
17	16.31	14.19	16.63	16.63
18	18.19	14.58	16.77	16.77
19	22.45	14.79	16.69	16.69
20	26.62	15.39	17.09	17.09
21	26.60	15.93	17.46	17.46
22	26.60	16.28	17.65	17.65
23	26.60	16.59	17.83	17.83
24	33.55	17.01	18.14	18.14
25	36.46	17.39	18.43	18.43
26	40.75	17.86	18.39	18.39
27	36.52	18.57	19.34	22.79
28	35.30	18.65	19.34	19.34
29	35.52	19.13	19.51	33.44
30	35.52	19.62	19.77	19.77
31	38.28	19.63	19.97	23.41

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