A STUDY ON LAND AREA DRAINAGE IN COASTAL AREA

A DISSERTATION

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CANDIDATE'S DECLARATION

I hereby certify that the work which is being presented in this dissertation entitled "A **STUDY ON LAND DRAINAGE IN COASTAL AREA**" in partial fulfillment of the requirement for the award of the degree of **Master of Technology** in **Water Resources Development (Civil)** in the Department of Water Resources Development and Management of Indian Institute of Technology Roorkee, is an authentic record of my own work carried out during the period from July 2015 to May 2016 under the supervision and guidance of Dr. U. C. Chaube, Emeritus Fellow and Dr. S. K. Mishra, Professor Department of Water Resources Development and Management, Indian Institute of Technology Roorkee, India.

The matter embodied in this dissertation has not been submitted by me for the award of any other degree.

Dated:

Place: Roorkee

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CERTIFICATE

This is to certify that the above statement made by the candidate is correct to the best of our knowledge.

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(SIDDARAJ H. P)

ABSTRACT

The drainage systems in the coastal region is predominantly different as compared to urban drainage systems. The coastal region is vulnerable to natural disasters such as storm surges, sea level rise, tidal variations, tsunami and cyclones.

The characteristics of the coastal region which includes climate, rainfall, soil, vegetation and terrain/topography varies from place to place. The major factor considered while designing coastal drainage system for any industrial or urban area is topography, availability of natural slope, constraints in land use and land cover and mean sea level. If the elevation of terrain/topography of coastal region is above compare to mean sea level, the industrial or urban area has to be protected with efficient drainage system which can flow with gravity to dispose the run-off generated within the short duration to avoid flooding in that region. Meanwhile, it has to be checked for constraints in pipeline systems and rectify for efficient dispose the runoff generated.

The elevation of terrain/topography is below/ equal/ slightly above as compare to mean sealevel, the coastal area will be more vulnerable to external flooding caused by tidal variation, cyclones, rise in sea level, storm surges, tsunami etc., these natural disasters may finally result in inundating the low lying areas, loss of valuable properties, loss of lives and waterlogging and it may also lead to accumulation of silts in agricultural land. To protect the area from external flooding, the measures that can be considered are flood plain zoning, planned urbanization, increasing the elevation of roads, providing adequate drainage system, adjustment in life style, cropping pattern and flood warning / preparedness system.

In the present study, the above problems were considered with the help of two case studies at two different coastal regions located at Pudimadaka village, Visakhapatnam, Andra Pradesh and Mithakhari, Port Blair, Andaman and Nicobar Island coastal. For the analysis, modern techniques such as Arc-GIS model, Auto-CAD model and SWMM model were applied and the results showed that, the effect of the flood can be minimized efficiently by making use of these modern techniques. It was observed that, the coastal area is more vulnerable to external flooding caused due to natural disaster. This study helps the planner to monitor the coastal environment due to natural hazards and it may also provide platform for the planning of drainage system.

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CHAPTER-1 INTRODUCTION

1.1 BACKGROUND

Designers of coastal drainage systems have to take into consideration the unique characteristics of coastal flooding, particularly the impacts of tides, low elevations, and high groundwater tables. The rate at which gravity can drain an area depends in part on the difference in elevation between the area being drained and the place to which the water flows. The greater the difference in elevation, the greater the slope of the "hydraulic head" and the faster the water can drain. Coastal areas generally are low-lying and thus vulnerable to flooding. High tides can decrease the elevation difference and further slow gravity drainage. Moreover, storm surges in coastal areas frequently occur during rainstorms, and can completely stop natural drainage. High water tables in coastal areas also limit natural drainage. With water tables just below the land surface, a rainstorm can rapidly saturate the soil (raise the water table to the surface). The saturated soil increases runoff by decreasing the ability of water to percolate into the ground. Coastal flooding can also be exacerbated by problems frequently not considered in designing the drainage system. Storm waves may overtop a seawall; and sediment and debris may block inlets, outlets, and storm sewer pipes and canals. During the worst storm surges, coastal areas may be completely inundated by the sea, leaving the drainage system ineffective until water levels have receded (James, 1987). Increasing concentrations of carbon dioxide and other gases are expected to warm the earth several degrees in the next century, which would raise sea level a few feet and alter precipitation patterns. Both of these changes would have major impacts on the operation of coastal drainage systems. The design of a coastal drainage system depends on the amount of runoff expected during a major storm and the elevation of the area being drained. Although the amount of rainfall and the severity of the worst storm vary from year to year, it has been reasonable to assume that historical weather records provide a reliable guide to future precipitation and runoff over the design life of the project. Recent developments in climatology, however, suggest that design conditions that have been fixed in the past may change substantially in the future. Further summarized from previous studies estimating sea level rise and climate change resulting from the greenhouse effect and examines the impacts on coastal drainage systems and possible responses (James, 1987). Storm surges associated with severe tropical cyclones constitute the world's worst coastal marine hazard. Storm surge disasters cause heavy loss of life and property, damage to the coastal structures and the losses of agriculture, which lead to annual economic losses in affected countries. Death and destruction arise directly from the intense winds characteristics of tropical cyclones blowing over a large surface of water, which is bounded by a shallow basin. As a result of these winds the massive piling of the seawater occurs at the coast leading to the sudden inundation and flooding of coastal regions (Dube, 2008). The National Academy of Sciences (NAS) and atmospheric scientists from around the world have concluded that increasing concentrations of carbon dioxide, methane, and other gases will raise the earth's average temperature a few degrees (C) in the next century. Such a warming would alter precipitation patterns and raise sea level. The former impact would change the load on coastal drainage systems, while the latter would reduce their efficiency (James, 1987).

The main factors contributing to disastrous storm surges in east coast may be summarized as (Dube, 2009) (Dube et al. 2010).

- (a) Shallow coastal water,
- (b) Convergence of the bay,
- (c) High astronomical tides,
- (d) Thickly populated low-lying islands,
- (e) Favorable cyclone track, and
- (f) Innumerable number of inlets in delta such as in the world's largest river system (Ganga-Brahmaputra-Meghna).

Frequency of tropical cyclones in east coast is not so high even then coastal regions of India suffers most in terms of loss of life and property caused by the surges. The reason is inadequate accurate prediction, and the low lands all along coasts are considerably low-lying huge deltas, such as, Gangetic delta and Irrawaddy delta (Dube, 2008). TABLE 1.1 lists the number of deaths associated with several deadly cyclone disasters where death tolls were in excess of 5000 lives. These major surges usually occurred unexpectedly (Dube, 2008)

Year	Countries	Death
1970	Bangladesh	3,00,000
1737	India	3,00,000
1886	China	3,00,000
1923	Japan	2,50,000
1876	Bangladesh	2,00,000
1897	Bangladesh	1,75,000
1991	Bangladesh	1,40,000
1833	India	50,000
1864	India	50,000
1822	Bangladesh	40,000
1780	Antilles (W. Indies) 22,000	
1965	Bangladesh	19,279
1999	India	15,000
1963	Bangladesh	11,520
1961	Bangladesh	11,466
1985	Bangladesh	11,069
1971	India	10,000
1977	India	10,000
1963	Cuba	7,196
1900	USA	6,000
1960	Bangladesh	5,149
1960	Japan 5,000	
1973	India 5,000	

TABLE 1.1: List of number of deaths associated with cyclone disaster.

(Source: Dube, 2008)

1.2 OBJECTIVE AND SCOPE OF STUDY

Objective

- To plan internal drainage of an industrial area located in coastal area.
- To analyze external flooding of a coastal area and suggest protection measures.

Scope of study

- Design flood estimation in ungauged coastal catchments.
- Study of constraints on availability of natural slope.
- External flooding due to man-made changes in land use/land cover, drainage pattern.
- External Flooding due to combination of tides and cyclones.

1.3 APPLICATION OF SWMM MODEL, AUTOCAD MODEL AND ARCGIS MODEL IN ANALYSIS OF FLOODING AND DRAINAGE.

The SWMM model is widely used for analyzing the flood and helps for decision making. applications of SWMM is used for various application such as Green infrastructure model, 2D modelling Integrated modelling, Dynamic minor/major system analysis, Mitigation, Water quality, Drainage design, Sanitary system design, Detention storage, Real time control, Wet weather sanitary sewer analysis, Flood mapping/risk analysis. For the present study, SWMM model is used for the design of Internal drainage for industrial area located in coastal area.

AUTOCAD software is used for creating blue prints for buildings, computer chips, bridge, drainage system, etc., this software is initially used for designing the internal drainage of Pudimadaka thermal power plant. It is also, used to get the measurements of pipe length, area, Layout plan of the drainage system, it is also used to know the topography by the means of contour map. Contour map is very reliable for the analysis and for DEM study using Arc-GIS than readily available SRTM, CARTOSAT, and ASTER data. Hence, In the present study, the AutoCAD model is used as 2D tool for drawing the 2D drawings for making the analysis simple and easier.

The basic applications of Arc-GIS are analyzing mapped information, helps creating and using of maps, sharing and discovering geographic information, compiling geographic data also manages the geographic information in a database. In the present study, Arc-GIS is used to view the spatial data, create layered maps, and perform basic spatial analysis which includes manipulation of shapefiles, geodatabases, editing and analysis.

1.4 ORGANIZATION OF THE REPORT

Literature review on the topics such as flooding in coastal regions, models for storm prediction, data input for surge prediction models, remedial measures, etc. are discussed in chapter 2.

Analysis tools, methodology, and applications such as, SWMM model, AUTOCAD model and ARCGIS model are discussed in chapter 3.

The study area location, characteristics are described in chapter 4.

Chapter 5 describes problem analysis of Pudimadaka thermal power plant and remedial measures to drain out generated runoff in the plant using SWMM, ARCGIS, and AUTOCAD models.

Chapter 6 describes flood control in Mithakhari (Andaman Nicobar), effect of tsunami, tidal analysis, flood problem and options for the flood control.

Conclusions and future scope of the work are discussed in chapter 7.

CHAPTER-2 REVIEW OF LITERATURE

2.1 INTRODUCTION

The flooding in coastal areas occurs due to various aspects, such as cyclones, tides, tsunami. Flooding takes place from the combined effect of tides and surges from the sea that penetrate into the land. Catastrophe due to storm surge need be seriously considered by the scientific community. About 90% of the damage is due to inundation of land by sea water. The main factors contributing to disastrous surges in east coast are shallow coastal water, convergence of bay, high astronomical tides, thickly populated low lying Islands and favorable cyclone track. Almost all the lives and most of the damage is due to the storm surges, Thus, it is necessary that the problem of the storm surge be seriously addressed by countries of various regions through collective efforts and integrated manner (Dube, 2009). Designers of coastal drainage systems recognize the unique characteristics of coastal flooding, particularly the impacts of tides, low elevations, and high groundwater tables (James, 1987). Coastal areas generally are low-lying and thus vulnerable to flooding. High tides can decrease the elevation difference and further slow gravity drainage. Moreover, storm surges in coastal areas frequently occur during rainstorms, and can completely stop natural drainage. High water tables in coastal areas also limit natural drainage. With water tables just below the land surface, a rainstorm can rapidly saturate the soil (raise the water table to the surface). The saturated soil increases runoff by decreasing the ability of water to percolate into the ground. Coastal flooding can also be exacerbated by problems frequently not considered in designing the drainage system. Storm waves may overtop a seawall; and sediment and debris may block inlets, outlets, and storm sewer pipes and canals. During the worst storm surges, coastal areas may be completely inundated by the sea, leaving the drainage system ineffective until water levels have receded (James, 1987).

The purpose of this literature review is to understand recent developments in predicting the storm surges in Bay of Bengal and Arabian Sea. Dube et al., (1994, 1997, 2000, 2004, 2005, 2006), Chittibabu et al., (2004), Agnihotri et al., (2006), Jain et al., (2010), Sutapa et al., (2014), Mahendra et al., (2011), Saxena et al., (2012), Sindhu et al., (2012)., Paul et al., (2014), Mehra et al., (2015), have developed storm prediction models which have been successfully applied in the Bay of Bengal and the Arabian sea.

2.2 FLOODING DUE TO CYCLONES

A cyclone refers to the combination of very high speed wind, heavy rainfall, and/or high surge hitting coastal region. The occurrences of cyclones often cause huge loss to life and property particularly in coastal areas. The most devastating flood producing rains are generally associated with tropical cyclones. Besides, low-lying coastal areas suffer from most destructive floods. Floods created by tropical cyclones can reach catastrophic proportions when aggravated by wind induced surges along the coast line and can be felt a long distance inland due to back-up of rivers at high flow and subsequent flooding (Rao, 1997).

In general, all cyclones are dangerous. Some are more furious and cause havoc. To differentiate the destructive power of the cyclones based on the order of magnitude of the combined effect of wind velocity, surge height, rain amount, and other factors, National Oceanic and Atmospheric Administration (NOAA) classified the cyclone's-disaster-potential-scale into five categories widely known as the Saffir - Simpson hurricane scale, as show in TABLE 2.1.

Classification	Wind Speed	Pressure	Storm Surge	Damage
	(Kmph)	(mb)	(m)	
Tropical Depression	< 61			
Tropical Storm	62 to 118		0.3 to 1.0	
Category – ONE Cyclone	119 to 153	>980	1.1 to 1.7	Minimal
Category – TWO Cyclone	154 to 177	979-965	1.8 to 2.6	Moderate
Category –THREE Cyclone	178 to 209	964-945	2.7 to 3.8	Extensive
Category – FOUR Cyclone	210 to 249	944-920	3.9 to 5.5	Extreme
Category – FIVE Cyclone	> 249	<920	>5.5	Catastrophic

TABLE 2.1: The Saffir - Simpson cyclone scale chart (NOAA, 1994)

2.2.1 History of Cyclones

The coastal region of Andhra Pradesh is extremely vulnerable to cyclones, storm surges, and floods. The State risks are battered by cyclones of moderate to severe intensities every two to three years. Cyclones on the east coast originate in the Bay of Bengal, Andaman Sea or the

South China Sea, and usually reach the coastline of Andhra Pradesh, Odisha, Tamil Nadu, and West Bengal. The cyclones develop in the pre-monsoon (April to May) and post-monsoon seasons (October to December), but most of them tend to form in the month of November. History indicates that most of the tropical cyclones have occurred in late October, and November had been very severe. Since 1975, the State has faced more than 60 cyclones. Some of them were moderate, and a few of them very severe. Table 2 provides a brief description of very severe cyclones hitting Andhra coast. As seen, during the last 40 years, there was not a single year in which the State did not experience either a severe storm or a cyclone or heavy rain and flood. According to the State Disaster Management Department, about 44 per cent of the State is vulnerable to tropical storms and related disasters.

Vulnerability to storm surges is not uniform along the coast of Andhra. The stretch between Nizampatnam in Guntur district and Machilipatnam in Krishna district is most affected by storm surges. East and West Godavari districts, with vast stretches of paddy fields and irrigation, drainage canals always bear the brunt of cyclones accompanied by strong winds and pounding rains. In the aftermath of cyclones, these areas get flooded, leading to huge crop losses besides other damage.

The deadliest cyclone in the past 40 years (1975-2014) was the one that struck Andhra's coast in November 1977, killing about 10,000 people. About 2, 50,000 cattle heads perished, one million houses were damaged, and crops on 1.35 million hectares (ha) were destroyed.

Also, the pre-monsoon cyclone is not rare in the State. A severe cyclonic storm hit the Andhra coast in May 1990, in which the death toll was 817 and the State's revenue loss was assessed at Rs.2, 137 cr. In the cyclone of May 1979, more than 700 people lost lives. In 2010, seven people were killed in the coastal districts of Andhra when Cyclone Laila arrived. It made a landfall near Baptala in Guntur district on May 20 before monsoon. Harvested paddy in Krishna, Guntur and West and East Godavari districts was damaged badly, leaving farmers distraught. Historically, the occurrence of more than one cyclone in a season is not unusual in Andhra Pradesh. In 1996, the State experienced a severe cyclonic storm in November, which left 1,077 people dead. The state had suffered a loss of Rs.6, 129.25 cr. Again in December 1996, one more severe cyclone hit the State with the death toll of 27.

TABLE 2.2: LIST OF SEVERE TROPICAL CYCLONES OCCURRED IN THE COAST OF ANDHRA PRADESH

S1.	Date and	Category &	Description of Devastation & Impacts
no.	Name of	Technical	
	cyclone	description	
1	28 th Oct	Severe cyclonic	The most devastating in the past 40 years. Eight
	1 st Nov.	storm	coastal districts affected. About 10,000 people killed.
	1977		About 250,000 cattle heads perished; 1 million houses
	15-16 th	Severe Cyclonic	damaged and crops on 1.35 million hectares were
	Nov. 1977	storm with core	damaged. Estimated loss: Rs. 172 cr.
		of hurricane	
		winds	
2	15-13 th	Cyclonic storm	Heavy rains and floods. As many as 748,000 lakh
	May 1979	with core of	houses damaged. Estimated loss: Rs. 242 cr.
		hurricane winds	
3	15-16th	Cyclonic Storm	There were three cyclonic storms. First one in October,
	Oct. 1987		which was a severe storm but with no casualty. The
			second one, on 2-3 November was very severe. 10
	2 nd - 3 rd	Severe Cyclonic	districts affected. 119 people died; more than 100,000
	Nov. 1987	Storm	houses and 960,000 ha of crops damaged; estimated
			loss: Rs.126.48 cr.
6	July 1989	Severe Cyclone	Cyclone followed by heavy rains and floods. 22
		storm	districts affected. Death toll: 232; crops on about
			600,000 ha lost; estimated loss: Rs.913.5 cr. It was
			followed by a cyclonic storm with no casualty.
7	5-10 May	Severe cyclonic	14 districts affected. Death toll: 817; houses damaged:
	1990	storm with core	1.4 million; crop loss: more than 500,000 ha; loss
		of hurricane	Rs. 2,137.27 cr. It was followed by heavy rainfall in
		winds.	August in which 50 people died and the loss was
			assessed at Rs.179 cr.
8	November	Severe cyclonic	Four districts affected. Death toll: 1,077; houses
	1996	storm with core	damaged: 600,000; crop loss: 500,000 ha; loss Rs.

		of hurricane	6,129.25 cr. One more severe cyclone in December
		winds.	claimed 27 lives.
9	17-21 st	Severe Cyclone	14 districts affected. Death toll: 22; houses damaged:
	May 2010	'named as	14,298; crop loss: 260,000 ha; loss Rs.1, 603 cr.
	Way 2010		-
		Laila". Wind	Cyclone Laila battered Ongole town in Andhra
		speed 100-120	Pradesh; it received heavy rain of 320 mm on May 20
		Km/hr.	and 142 mm on May 21, and has made rivulets
			like Gundlakamma, Addavagu and swollen. Addanki
			received the highest rainfall of 522 mm, followed by
			Maddipadu with 510 mm and Kothapatnam 258 mm in
			24 hours on May 21. The cyclone caused heavy
			destruction in Prakasam, Krishna and Guntur districts
			and preliminary reports prepared by the State
			government put the loss at over Rs.500 cr.
10	28 Oct. to 1	Severe cyclone	Death toll: 30; crop loss: over 700,000 ha; loss: Rs.1,
	November	'Nilam' Wind	710 cr. Andhra Pradesh government conducted their
	2012	speed up to 100	review on the storm, it was revealed that the state
		Km /hr.	suffered huge economic losses of $\Box 200$ cr.
11	19-28 th	Very Severe	Lehar was the second most intense tropical cyclone of
	November	Cyclonic Storm	the 2013 season, as well as one of the two relatively
	2013	equivalent to a	strong cyclones that affected Southern India in
		category 1	November 2013, the other being Cyclone Helen.
		hurricane.	
		Named as	
		'Lehar'	
		Wind speed up	
		to 140 Km /hr.	
	19-23 Nov.	Very severe	Helen brought extensive damage to Machilipatnam
	2013	cyclone	in Krishna district, with uprooted trees and electric
		Named as	lines. The districts of Krishna, East
		'Helen'	Godavari and Srikakulam, and Guntur suffered heavy
		Wind speed	rainfall. Heavy damage to harvest crops was also
		100-130 Km/hr.	reported, with the West Godavari district being worst
L	l	1	

			affected. Paddy, coconut and banana crops have
			suffered damage. The total loss incurred by Krishna
			and West and East Godavari districts in the state of
			Andhra Pradesh due to the cyclone Helen was
			estimated to be Rs.1,628.73 cr.
12	7-14	Very Severe	Cyclone Hudhud pounded the coastal districts of
	October	Cyclonic storm	Andhra Pradesh and Odisha with heavy rain and winds
	2014	Equivalent to	of almost 200 kmph killing four people and left a trail
		category-4.	of destruction with Vishakhapatnam where the very
		Named as	severe storm made landfall the worst hit. According to
		Hudhud	Andhra Pradesh's Revenue (Disaster Management)
			Department a total of 2, 48,004 people were "affected"
		Wind speed	by Hudhud, which also damaged 70 houses and left 34
		185-215 Km/hr.	animals dead. Hudhud caused extensive damage to the
			city of Visakhapatnam and the neighboring districts
			of Vizianagaram and Srikakulam of Andhra Pradesh.
			Damages were estimated to be $\Box 21908 \text{ cr.}$ by the
			Andhra state government. At least 124 deaths could be
			confirmed, and a majority of them were from Andhra
			Pradesh

2.3 TSUNAMI

Tsunami (Soo-NAH-mee) is a Japanese word meaning harbor wave. A tsunami is a series of waves with a long wavelength and period (time between crests). Time between crests of waves can vary from a few minutes to over an hour. Tsunamis are often incorrectly called tidal waves; they have no relation to the daily ocean tides. Tsunamis can occur at any time of day or night.

2.3.1 Cause of Tsunami

Tsunamis are generated by any large, impulsive displacement of the sea bed. Earthquakes generate tsunamis by vertical movement of the sea floor. However, if the sea floor movement is horizontal, a tsunami is not generated. Generally, earthquakes of M > 6.5 cause Tsunami.

Tsunamis are also triggered by landslides into or under the water surface, and can be generated by volcanic activity and meteorite impacts.

2.3.2 Speed of Tsunami

Tsunami velocity is dependent on the depth of water through which it travels. The velocity is governed by the following equation

V = g h

Where,

- V is the velocity of Tsunami in m/sec.
- g is the gravitational force in m/sec²
- h is the depth of water in m.

Tsunamis travel approximately at a velocity of 700 kmph in 4000 m depth of sea water, but in 10 m of water depth the velocity drops to about 36 kmph. For example, the tsunami from Sumatra coastal earthquake travelled to Tamil Nadu coast in about two hours. Even on shore, Tsunami's speed could be 35 - 40 km/h, much faster than a person can run.

2.3.3 Size of Tsunami

Tsunamis range in size from centimeters to over 30 m height. Most tsunamis are less than 3 m in height. A large tsunami can flood land up to 1.5 km from the coast. In deep water (greater than 200 m), tsunamis are rarely over 1m high and will not be noticed by ships due to their long period (time between crests). As tsunamis propagate into shallow water, the wave height can increase by over 10 times. Tsunami heights can vary greatly along a coast. The waves are amplified by certain shoreline and bathymetric (sea floor) features. The force of some tsunamis is enormous. Large rocks weighing several tones along with boats and other debris can be moved hundreds of feet inland by tsunami wave activity. Homes and other buildings are destroyed. All this material and water move with great force and can kill or injure people.

2.3.4 Frequency of Occurrence

On the average, there are two tsunamis per year in the Pacific Ocean which cause damage. Approximately every 15 years a destructive tsunami occurs in Pacific

The details of Tsunami in India are given below (National Disaster Management Division, Ministry of Home Affairs, Government of India, and January, 2006) TABLE 2.3: Details of tsunami (Source: Disaster prevention and management, volume 15,2006).

April 12, 1762	Earth Quake in the Bay of Bengal generated tsunami wave of 1.8	
April 12, 1702		
	m in coastal Bangladesh	
August 19, 1868	Earthquake Magnitude 7.5 in the Bay of Bengal. Tsunami wave	
	run-up level at Port Blair, Andaman Island 4.0 m.	
December 31,	Earthquake of magnitude Ms 7.9 in the Bay of Bengal, reported	
1881	tsunami run-up level of .76m at Car Nicobar, 0.3m at Dublat, 0.3	
	m at Nagapattinam and 1.22 m at Port Blair in Andaman Island	
1883	Karakatau, volcanic explosion in Indonesia. 1.5m tsunami at	
	Chennai, 0.6m at Nagapattinam	
1884	Earthquake in the western part of the Bay of Bengal. Tsunamis at	
	Port Blair & mouth of Hoogly River	
26-Jun-1941	Earthquake of magnitude MW 8.1 in the Andaman Sea at 12.90	
	N,92.50 E. Tsunamis on the east coast of India with Amplitudes	
	from 0.75 to 1.25 m. Some damage from East	
	Coast was reported.	
27-Nov-1945	Mekran Earthquake (Magnitude Ms. 8.3). 12 to 15 M wave height	
	in Ormara, 13 m at Pasni, and 1.37 m at Karachi (Pakistan). In	
	Gulf off Cambay of Gujarat wave heights of	
	11.0 m was estimated, and 2 m at Mumbai, where boats were	
	taken away from their moorings	
26-Dec-2004	An earthquake of rear Magnitude (MW 9.3) generated giant	
	tsunami waves in North Indian Ocean. Tsunami made extensive	
	damage to many coastal areas of Indonesia, India, Malaysia,	
	Maldives, Sri Lanka and	
	Thailand. A trans-oceanic tsunami, observed over areas beyond	
	the Ocean limit of origin. More than 2,00,000 people lost their	
	lives in above countries which is a record.	

2.4 TIDES

Tides are generated in the Bay of Bengal by the forces of attraction of mainly the sun and the moon upon the rotating earth. The effect of tide is manifested in a regular alteration of rise and fall of the water level of the sea and the estuarine channels and creeks. With the advent of rising tide, the water level of sea starts rising gradually and steadily till a highest level known as the "High Water Level" (H.W.L) is attained. This rising phase of the tide is called the "Flood tide" or the "Flow tide". After the attainment of H.W.L the tide water level starts falling gradually and steadily till a Lowest Water Level (L.W.L) is reached. This falling phase of the tide is called "Fbb tide". There upon the tide water starts rising once again till the occurrence of the next L.W.L is termed the "Period of Tidal Circle" which is on average is 12 hours 24 minutes. The tidal cycles are represented graphically by tidal curve.

With the advent of flow tide, the velocity of current which is in the inland direction starts increasing, reaches a maximum at about the middle of the flow tide and begins to decrease there after being zero at the H.W.L which is known as "High water slack". The reupon, the ebb tide commences and the current velocity which is in the seaward direction starts increasing once again and after attaining a maximum value begins to diminish gradually becoming zero at L.W.L which is known as the "low Water Slack". Two tides called "Semi-diurnal tides are also found to differ from each other. Another interesting feature of tides lies in the fact that the tidal range at any location fluctuates steadily and gradually from day to day in accordance with the lunar phase. The tidal range at the full and new moon is found to be the maximum. This phase is called the "Spring Tide". After the occurrence of the Neap Tide at the middle of moon cycle when the tidal range is the minimum.

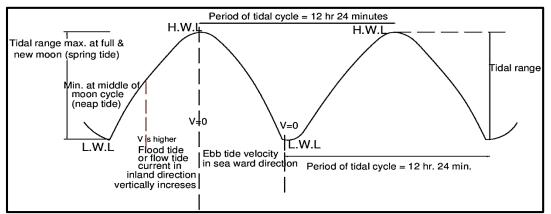


Figure 2.1: Graphically represented tidal cycles by tidal curve

2.5 MODELS TO PREDICT STORM SURGES IN COASTAL REGIONS

Chittibabu et al., (2004) addressed Mitigation of flooding and cyclone hazard in Orissa, India (Coastal districts of Orissa Gangam, Puri, Jagatsinpur, and kendrapara) considering two cyclone database has been used one from cyclone database from IMD (1877-2000) and second cyclone in Orissa (1804-1875) provided by British east India company, surge data from IMD, & Maximum sustained wind speed. IIT-D numerical surge model was used to compute storm surges along the Orissa coast. The model is a semi explicit finite difference model with the following characteristics, vertically integrated shallow water coastal zone numerical model, curvilinear representation of coastal boundaries, variable grid representation, Validation type boundary condition, & uses a dynamic storm model to simulate storm winds. The model was applied to estimate surge in coastal region of Orissa and found that the lowest value of surge was 3.0m and highest was 8.0m, and from the study it is suggested to construct a dykes and embankment at the areas of land that exists between major tributaries in the coastal area. The study concluded that no evidence of increase of storm surge amplitudes due to global warming.

Agnihotri et al. (2006) addressed A Bay-River coupled model for storm surge prediction along Andra coast of India (East coast of India) considering bathymetry data for the three cyclones events that struck east coast i.e. November 1977, may 1990 and November 1996 developed a two dimensional bay-river coupled numerical model for storm surges in east of India considering the effects of Krishna and Godavari river along with tropical cyclone, A rectangular cross section and uniform width was developed and coupled with twodimensional surge model in order to notice the effect of Krishna and Godavari rivers on the surge storm. Simulation showed that the discharge of fresh water carried by the river may modify the surge height in the bay significantly. The surge height was also computed with and without the inclusion of rivers, the maximum predicted surge values computed from two models were about 4.8m, and maximum sea surface elevation computed from two models were same expect where river Krishna and Godavari joins. the bay and conclude that the model may be used for operational prediction of storm surges.

Shahapure et al. (2010) advocated Coastal Urban Flood Simulation Using FEM, GIS and Remote Sensing in coastal urban watershed in Navy Mumbai, in Maharashtra state, in this model parameters considered for simulating the overland flow are bed slope and manning's roughness coefficient, and it was estimated using the DEM and satellite imaginary of the area depending upon land use land cover map. The developed rainfall runoff model also considered the effects of tidal variations using Finite Element Method. Galerkin's FEM was used for the approximation for the governing equations. Overland flow was modeled using the mass balance equation considering the impervious character of the urban watershed. Storm water flow through the channel was modeled using the diffusion wave form using Saint Venant's equations and considering the tidal variations. In this model 5 rainfall events were simulated & different tidal boundary conditions are developed for each event based on the tide table and the basic tidal equation, these tidal models are incorporated in coupled model as a boundary condition. Analysis concluded coupled model could predict the flooding satisfactorily. Further, Sensitivity analysis of the model was also, carried out altering some parameters, namely Manning's roughness coefficient for overland flow and channel flow, the grid element size and time step, observed results showed the values of computed peak discharge are more sensitive to manning's roughness coefficient for overland and channel flow. And finally, concluded developed model is quite useful for the flood simulation for coastal urban watersheds.

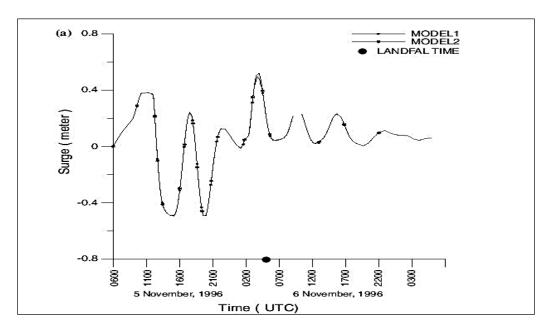


Fig 2.2: Temporal variation of surge height for Kakinada cyclone in Krishna river

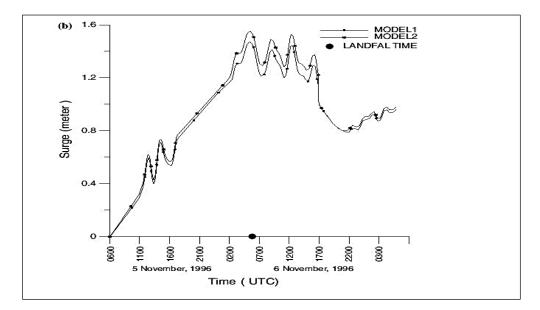
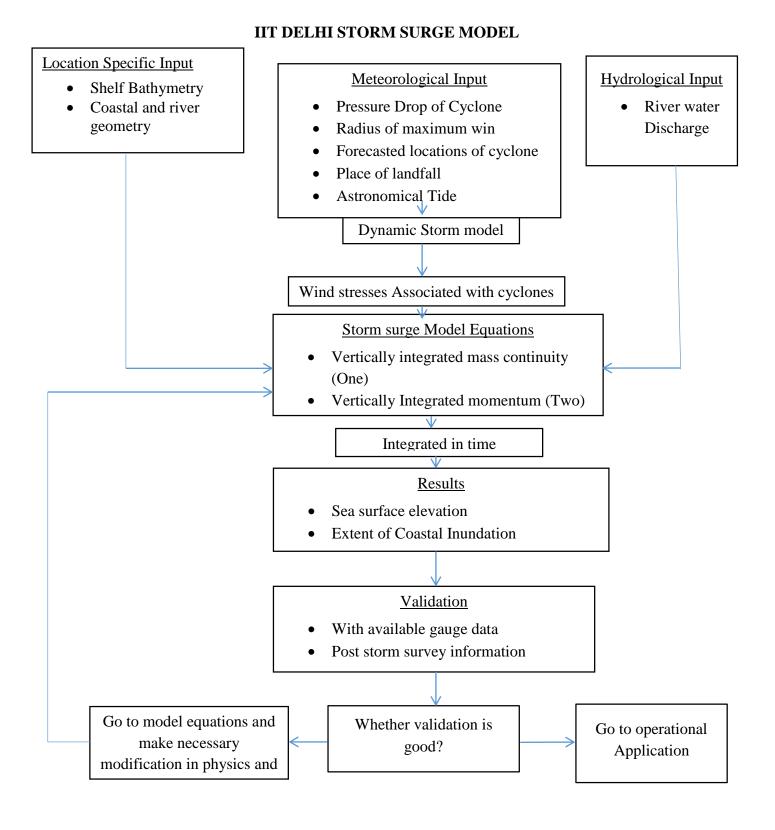


Fig 2.3: Temporal variation of surge height for Kakinada cyclone in Godavari river

Jain et al. (2010) studied the Computation of Expected Total Levels along the East Coast of India (Western sector of Bay of Bengal) considering 117 years' data for the major Historical storm surge (1891-2007), cyclonic tracks, and tide gauge data. The IITD (Indian institute of Technology, Delhi) storm surge model was used to compute the maximum probable surge amplitudes with the help of developed numerical models. A maximum probable surge at coast was simulated and TWL (Total water level) was computed by linearly adding the local tide and wave setup for the simulated surge along the coast. The model represented a balance between pressure gradient, centrifugal, Coriolis, and surface frictional forces for a stationary storm. The feasibility study was then carried out using the parameters of the cyclone based on a 50 yr. return period applied to synthesized tracks as an input to the numerical surge model, which may provide extreme water levels that could occur along the coast, and analysis showed that the lowest and highest values of the surge are about 4.3m and 10m, and finally the analysis from the model concluded that it may help coastal authorities to develop a long term and short term disaster management and vulnerability reduction action with respect to cyclones.



WRD&M, IIT ROORKEE

Mahendra et al. (2011) have discussed Assessment and Management of coastal multi-hazard vulnerability along the Cuddalore Villupuram, east coast of India using geospatial techniques in Tamilnadu state covering the districts of Cuddalore, Villupuram, and Pondicherry considering parameters of sea level rate change, shoreline change rate, elevation contours and historical storm surge. Sea level rate change was found by plotting linear best fit line using least squares method by using recorded monthly mean values of tide gauge data. ArcGIS and ERDAS model were used to calculate shoreline change and to obtain elevation contours, and storm surges were calculated using Probability of non-exceedance by assigning the rank series by Gringorten method. MHVM of the study area was prepared by overlaying the multi – hazard areas on the base maps. Sea level change indicated a value of 0.085mm/y. The shoreline projected for the next 100 years for the open coast indicated that an area of 3.77 km² is going to be eroded. Study showed total area of 360 km² has been delineated hazard zone with 314 km² under Cuddalore, Villupuram and Pondicherry respectively, and finally Concluded that MHVM can help in planning for aftermath of an event, rehabilitation, civil disturbances, restoration of the utilities, health problems etc.,

Saxena et al., (2012) have discussed Coastal hazard mapping Cuddalore region, south India (Cuddalore, State of Tamilnadu, south India) using data source for Analysis of shoreline change, LANDSAT-1, LANDSAT-TM, IRS, LISS III, EO-I, CARTOSAT-II, and past 20 years' gauge data from Chennai port. Hazard mapping involves identification of shoreline vulnerable to impact of storm surge; arise in sea level and erosion. The model proposed in this study are erosion mapping by (LRR, DSAS model), coastal flood hazard mapping by (statistical distribution or Gumbel's distribution), land use/land cover (ERDAS model, LISS III, ArcGIS model) and socio economic impacts. The result showed that volume of annual net sediment transport is estimated to be 0.40x106 m³. Extreme flood level calculated using Gumbel's distribution (for 100yr return period) 2.98 m MSL, and annual MSL Chennai was 0.041 m, and maximum limit of inundation towards landward was found to be 2050 m .The study concluded that the coastal stretches of Cuddalore district are in the high risk zones for multi hazard, and the results from the study would assist local state govt. in the preparing for the impacts of erosion, inundation risk & future sea level rise along the Indian ocean.

Sindhu et al., (2012) studied Return period estimates of extreme sea level along east coast of India from numerical simulations (East coast of India) considering Visakhapatnam Chennai storm surge events associated with meteorological events, cyclonic tracks occurred during 1989-2000 ETOPO-5 data sets, Radius of maximum wind, core pressure, and position of core of cyclone (Holland model) 2D vertically integrated model was used to simulate storm surge due to 136 low-pressure that occurred during past 27 years (1974-2000) in the bay of Bengal, model includes Atmospheric forcing and storm surge and Holland model. In this present study model is selected in such a way that it is taken care of both tidal force and storm surge simultaneously to calculate the total sea level and further it is subtracted from tidal elevation in order to obtain storm surge. The 5-50nyear return period levels of total sea level along the east coast of India showed considerable increase from south to north. High Return period surges were 0.84m & 0.57m respectively. The model simulation showed considerably good result as compared with the observed surge levels due to cyclone events (Details provided at table 3), from the it is analyzed that 5-50 year return period of surge component considerably high at shallow & wide self-regions such as gudur, karaali, surya lanka, Machilipatnam. The study illustrates that storm surge simulation results can be used to derive return estimates of extreme events at location where long-period observations of sea level don't exist. The estimated return levels can be used as preliminary estimates for the design of marine structures for the coastal areas.

Cyclone event	Observed surge	simulated surge	mean error model- observed	RMS error
Para dip				
Aug-81	0.12	0.08	-0.0001	0.08
Jun-82	0.17	0.07	0.0001	0.15
Aug-84	0.15	0.06	0.0001	0.12
Visakhapatnam				
Nov-76	0.04	0.04	0.02	0.06
Aug-86	0.15	0.05	0.02	0.12
Chennai				
Nov-78	0.06	0.07	0.04	0.05

Matt Lewis et al., (2013) have discussed a storm surge inundation model of the northern Bay of Bengal using publicly available data developed computationally inexpensive inundation model from freely available data sources for the northern Bay of Bengal region to estimate flood risk from storm surges. Shuttle Radar Topography Mission (SRTM) terrain data has

been used in a dynamic coastal inundation model. A sub-grid routine allowed estuary channels with widths less than this resolution to be simulated efficiently, and allowed six major river flows to be represented. The inundation model was forced with an IIT-D model hind cast of the 2007 cyclone Sidr flood event, using parameters from two cyclone databases (IBTrACs and UNISYS). Validation showed inundation prediction accuracy with a root mean squared error (RMSE) on predicted water level of ~ 2 m, which was of the same order of magnitude as the forcing water-level uncertainties. Concluded that SRTM and other publicly available data can be useful for coastal flood risk management in data-poor regions. SRTM processing techniques may also improve inundation model performance.

Sutapa et al.(2014) addressed Predictability of landfall location and surge height of tropical cyclones over North Indian Ocean (NIO) In this study models were developed to predict storm surge heights and to know exact landfall location of tropical cyclones over NIO basin, for this Artificial neural network (ANN) model with multilayer perceptron (MLP) is developed to forecast exact location of landfall (lat. and long.) and neuro fuzzy coupled (NFC) is developed for precise forecast of surge heights. The result revealed that the prediction error with NFC model in forecasting the surge height is 2.448% with 6-h lead time, whereas the error is observed to increase with increase in lead time, for forecasting the surge height with 18-h lead time, the accuracy is observed to be 11.4%. The study concluded that the lat. & long. Position of landfall can be predicted with acceptable accuracy with ANN model. Further, the study revealed that neuro-fuzzy coupled model is found to be suitable model for forecasting the surge height over NIO with more than 88% accuracy when the lead time is 18-h.

Paul et al., (2014) have reviewed and discussed Implementation of method of lines to predict water levels due to storm along the coastal region of Bangladesh considering April 1991 cyclone as base data to validate the simulated result in comparison with observation, and the track of storm & other meteorological data was collected from BMD. The model was developed based on MOL (method of line), in addition to the classical fourth order Runge-Kutta method, to solve vertically shallow equations for the prediction of water levels due to a storm along the coast of Bangladesh. The developed model was applied to estimate water levels along the coast of Bangladesh due to interaction of tide & surge associated with the storm. Table 2.5 shows computed water levels with respect to MSL associated with 1991 storm along the coast of Bangladesh. The study concluded that the MOL could provide an

effective algorithm for solving shallow water equation in comparison with a standard finite difference solution.

	Simulated max.	Simulated overall peak
Coastal	surge level in this	water level by this
location	study (m)	study (m)
Hiron point	3.92	4.01
Tiger point	4.21	4.57
Kuakata	3.52	3.86
Rangabali	4.1	4.5
Char madras	5.5	5.81
Char Jabbar	6.19	6.35
Char chenga	5.11	5.81
Companiganj	6.7	7.28
Sandwip	5.24	5.63
Sitakunda	4.83	5.78
Chittagang	5.17	6.26

TABLE 2.5: The computed water levels with respect to MSL associated with 1991 storm along the coast of Bangladesh

Mehra et al., (2015) have given overview on Coastal sea response to the tropical cyclone forcing in the Northen Indian Ocean in areas such as Rathnagiri, Verem, karwar, Tuticorin, mandapam, Gopalpur, gangavaram, Kakinada, and port Blair, considering Cyclonic parameters during E1& E2, Wind speed, Sea level pressure, and Storm forward translation speed Multi-linear regression Analysis model is used to examine the characteristics of the sea level oscillation at different topographic locations in AS & BOB due to metrological events.

i.e., $\eta = B0+B1\tau u+B2\tau v+B3Ap+\epsilon$,

 $Tu = PA*CD*UVu^2+v^2$

Where,

η=sea level rise residual,

B0, B1, B2, &B3 = co-efficient of regression,

E=Difference b/w measured SLR & estimated SLR.

PA=density of air,

CD= drag co-efficient

The present study indicated that surge peak lagged up to Verem, at Ratnagiri & Karachi surge peak leads the E1 with constant amplitude. (Ref.table.2.6)

Location	Peak (cm)	Propagation speed ms ⁻¹
Columbo	31.6	7.9
Mandapam	24.3	1.8
Turticorin	21.4	13.1
kochi(Peak1)	12.9	
kochi(Peak2)	14.14	
Karwar	36.9	7.6
Verem	35.5	5

TABLE 2.6: Peak and Propagation speed of the areas near North Indian Ocean

The study concluded that multi-linear regression using local daily mean winds (cross and along shore) in association with the atmospheric pressure is able to account for up to 69% of daily mean sea level residual (SLR) at Ratnagiri, Verem and Karwar during E1. However, in BOB up to 57% of daily mean SLR is accounted for at Gopalpur, Gangavaram and Kakinada.

2.6 DATA INPUT FOR STORM PREDICTION MODELS (Dube, 2008).

To obtain confidence in surge prediction the good knowledge regarding input parameters for the model plays a vital role. These parameters include oceanographic parameters, hydrological inputs, basin characteristics, coastal geometry, astronomical tides, and meteorological parameters (Dube, 2008). It is evident that these input parameters strongly influence surge development. The brief details of this parameters are discussed below.

1. Meteorological data

The main characteristics required are i) The pressure drop (difference between ambient pressure surrounding the storm and the central pressure), maximum sustained winds and radius of maximum wind these parameters are estimated by satellite imageries (Dube, 2008). ii) Point of rainfall, duration of the storm, and vector motion of storm are obtained from IMD (Indian meteorological department).

2. Oceanographic data

Data on oceanographic are concerned with the following i) bathymetry ii) astronomical tides and iii) inshore currents in closed regions (Dube, 2008).

3. Basic characteristics and coastal geometry

The location of the highest surge depends upon the coastal geometry of the basin.

4. Hydrological input

The main hydrological information needed is a) river discharge in the sea and b) rainfall distribution (Dube, 2008).

2.7 REMEDIAL MEASURES (Dube, 1997)

Risk Assessment:

Evaluation of risks of tropical cyclones should be undertaken and illustrated in a hazard map indicating analysis of climatological records to determine how often cyclones have struck and their intensity. Map should incorporate information of past history of winds speeds, frequencies of flooding, possible height & location of storm surges etc. A master plan for flood plain management should be developed to protect critical assets from flash, riverine, and coastal flooding.

Land Use Control:

It refers to controlling land use so that the least critical facilities of the proposed plant are placed in most vulnerable areas. Policies regarding future development may regulate land use and enforce building codes for areas vulnerable to the effects of tropical cyclones. For example, in coastal areas, regulation can stipulate maximum building heights, types of land and staff residences. Another option includes the development of vulnerable areas for use of parks, sports facilities and open tree planting/ grazing land.

Reducing Vulnerability of Structures and Infrastructures

- New buildings should be designed as wind and water resistant. Design standards are usually contained in building codes;
- Communication and utility lines should be located away from coastal area or installed underground;
- Improvement of building sites by raising the ground level to protect against flood and storm surges;

- Protective river embankments, levees and coastal dikes should be regularly inspected for breaches due to erosion and opportunities taken to plant mangroves to reduce breaking wave energy;
- Improved vegetation covers to reduce soil erosion and landslides and facilitate the absorption of rainfall to reduce flooding.
- Disaster preparedness
- Educating the community in the risk hazard areas.
- Practical training how to reduce damage in the event of disaster.
- Promoting ingenious way for coping with the consequences.

CHAPTER-3 ANALYSIS TOOLS

3.1 INTRODUCTION

The Analysis tools used in the present study follow the standard sequence of drainage, landforms, cover and the integration of their results for geological and hydrogeological assessment. In this study, ARCGIS model and SWMM model are used i) to simulate and understand the topography, land use and land cover ii) to obtain economic design to drain generated storm water in plant location of study area, and iii) to level undulated topography by identifying areas requiring cutting and filling.

3.2 ARC-GIS MODEL (DEM STUDY)

3.2.1 Geo-referencing of topography map

The actual survey contour maps prepared in AutoCAD format was converted to raster files (tiff format). In order to Geo-reference these data the projections used in this project is WGS – 1984 zone 44N by listing the four corners coordinates (x and y, in meters) in the map. The coordinates are also used to create a GIS layer representing the topographic maps index of the topographic coverage. This layer was created with the GIS software, with a command that generates regular grids, represented by lines and polygons, according to a specified distance on the x and y axes. The distance was given by the difference between the coordinates of map corners. The topographic maps index GIS layer has been then converted in shape file format in order to be integrated in ArcView with the other layers of the database.

The geo-referencing procedure was carried out using Ground Control Point (GCP) method. For each map file, the four corner co-ordinates have been entered as GCPs and a first order polynomial transformation was used to re-calculate the coordinates of each pixel in the raster layer. The Root Mean Square error (RMS) resulted less than the pixel value. Carrying the correct UTM -WGS 44 coordinates. An evaluation of the quality of geo-referencing was carried out by loading in Arc map both the topographic maps and geo-referenced maps are checked for mismatching. Slight differences found can be auto adjusted.

3.2.2 Generation of DEM

Digital elevation model (DEM) is the digital representation (digital map) of the ground elevation data in meters. ARC-GIS software is used for preparation of the DEM. Given file format of the contour map (DWG) of study area has been converted into shape file (SHP) which is the working format in GIS environment. Each contour was assigned its value. The contours in shape file are interpolated to obtain digital elevations of the equally sized gridded cells. Variation in elevation is depicted through different colors. The DEM can be used to identify areas requiring cutting and filling and to estimate the volume of earthwork required to level the undulating topography of the study area.

3.2.3 Generation of Stream Network and Basin Delineation

The derived digital elevation model has been used for further processing in the context of stream generation and basin delineation. DEM has been smoothened out for eliminating uneven irregularities (such as pits) using filter size. Corrected DEM has been used as input data to generate pattern of flow directions and for identification of flow accumulation through each pixel of given elevation. Generated information on flow pattern and flow accumulation considers Eight-Point Pour model for the purpose of computing flow directions for use in basin delineation with DEMs directions. With the flow directions assigned for each DEM point, the flow accumulation at each DEM point has been computed. The flow accumulation at a given DEM point is defined as the number of earlier DEM points whose flow paths eventually pass through that point. Streams are identified by large values of flow accumulation since the flow paths of many points pass through the outlet point. Streams have been identified by displaying all DEM points with a flow accumulation value.

3.2.4 Distribution of Land Area in Different Elevation Ranges

The Digital Elevation Model has been used to compute the natural drainage area (within plant boundaries) between different elevation ranges. The DEM computes number of pixels in each interval. The graphical depiction of the cumulative area distribution shows different elevation in the plant area. This information will be derived from DEM study can be used to arrive at cost effective levels at which different plant components should be finally located.

3.3 DESIGN STORM SCENARIOS OF VARIOUS RETURN PERIODS

Design storm scenarios are required for

- (i) estimation of design flood and planning of internal drainage in the plant area and
- (ii) for assessing possible submergence in the plant area from external flooding.

The areal distribution and time distribution of the rainfall of a given duration are two main meteorological factors deciding the flood peak and the shape of the flood hydrograph. This input has to be converted into excess rainfall and convoluted with synthetic unit hydrograph to obtain a flood hydrograph after addition of base flow.

3.3.1 Estimation of Storm Rainfall of 25 Year, 50 Year and 100 Year Return Periods

The following procedure has been adopted for estimation of critical distribution of storm rainfall to cause the maximum flood due to rainfall of a specified duration:

 The duration of the storm rainfall which causes the maximum discharge in a drainage basin is called the design storm duration (T_D). Central Water Commission (CWC 1994) has recommended that T_D may be estimated as:

 $t_p(hrs.) = 1.1808 (LLc/\sqrt{S})^{0.285}$

 t_p is basin lag (hours), L is longest length of main river from farthest point on watershed boundary to outlet and S is equivalent stream slope. Lc is length of Main River from a point near the centroid of catchment to the outlet of catchment.

- 2. Locate catchment area under study on the T-yr., 24-hour isopluvial map and obtain the T-yr, 24-hour point rainfall value in cm. For catchment covering more than one isohyets, compute the average point storm rainfall.
- 3. Use the conversion ratio for T_D hours and multiply the T-yr 24 –hr rainfall in step-2 by the ratio to obtain T year T_D -hr point rainfall.
- Convert the T-yr T_D-hr point rainfall to T-yr T_D-hr areal rainfall by multiplying with the area reduction factor (ARF) corresponding to catchment area and for T_D-hr duration.
- 5. Apply the time distribution coefficients corresponding to design storm duration T_D to obtain the cumulative rainfall depths at 1-hr interval since the unit duration of synthetic U.G. is 1-hour.

6. Obtain the 1-hourly rainfall increments from subtraction of successive 1-hour cumulative value of rainfall in step-5

Apply appropriate design loss rate to obtain effective rainfall in each hour.

3.3.2 Extrapolation of Storm Rainfall for Other Return Periods

A plot of 24 hr storm rainfall of 25 yr, 50 yr and 100 year return periods (isopluvial map) on extreme value probability paper has been used for extrapolation of 24-hour storm rainfall of various return periods.

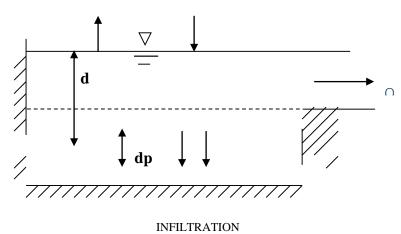
3.4 STORM WATER MANAGEMENT MODEL

3.4.1 Plant Area Drainage Planning

The Storm Water Management Model (SWMM) is a dynamic rainfall – runoff simulation model which has been used in the present study for design of drainage system. The runoff component of SWMM operates on a collection of sub-catchment areas that receive rainfall and generate runoff. The kinematics wave flow routing portion of SWMM transports this runoff through a system of open channels to specified outfall locations. SWMM tracks the quantity of runoff generated within each sub-catchment and the flow rate and flow depth in each channel during a simulation period comprised of multiple time steps (source: SWMM manual 5.1). In the present study SWMM 5 software running on Windows has been used for the analysis.

3.4.2 Overview of Computational Methods

SWMM is a physically based discrete – time simulation model. The conceptual view of surface runoff used by SWMM is shown below ^[31].



EVAPORATION RAINFALL

Each sub-catchment surface is treated as non-linear reservoir. Inflow comes from rainfall and any designed upstream catchments. There are several outflows, including infiltration, evaporation and surface runoff. The capacity of this reservoir is the maximum depression storage, which is the maximum surface storage provided by ponding, surface welling and interception. Surface runoff per unit area Q occurs only when the depth of water in the reservoir exceeds the maximum depression storage d_p in which case the outflow is given by Manning's equation. Depth of water over the sub-catchment (d) is continuously updated with time (t in seconds) by solving numerically a water balance equation over the sub-catchment.

Infiltration: Green-Ampt method has been used in this study for modeling infiltration. This method assumes that sharp wetting front exist in the soil column, separating soil with some initial moisture content below from saturated soil above. The input parameters required are the moisture deficit of the soil, the soil's hydraulic conductivity and the suction head at the wetting front.

Flow routing: flow routing within a conduit link in SWMM is governed by the conservation of mass and momentum equations for gradually varied, unsteady flow (i.e. Saint Venant's flow equation). Kinematic wave routing method has been used for flow routing in channels. This routing method solves the continuity equation along with a simplified from of the momentum equation in each channel. The latter requires that the slope of the water surface equal the slope of the channel.

The maximum flow that can be conveyed through conduit is the full flow Manning equation value. Any flow in excess of this entering the inlet node is either lost from the system or can pond atop the inlet node and be introduced into the conduit as capacity becomes available.

Surface ponding: normally in flow routing when the flow into junction exceeds the capacity of the system to transport it further downstream, the excess volume overflows the system and is lost. An option exists to have instead the excess volume be stored atop the junction in a ponded fashion and be reintroduced into the system as capacity permits. Under kinematic flow routing the ponded water is stored simply as an excess volume. Alternately the ponded water may have separate surface overflow system.

3.5 AUTOCAD MODEL

The AUTOCAD software was developed and marketed by Autodesk, which is a multinational software corporation and it was released in December 1982. AUTOCAD software is an application program used for 2D and 3D computer aided design (CAD) and

technical drawing. CAD is used to create precision drawings by drafters, artists, engineers, architects.

AUTOCAD software is used for designing mechanical components, analyzing piping systems and solving design issues. AUTOCAD can be used in MS windows, Mac OS X, and iOS Android. This software is initially used for designing the internal drainage of Pudimadaka thermal power plant. It is used to get the measurements of pipe length, area. The AUTOCAD drawing of the pudimadaka thermal power plant is shown in the Fig 3.1 and it is further divided into two parts as shown in Fig 3.2 & 3.3. The commands used for drawing are in the Table 3.1

COMMANDS	DESCRIPTION
ARC	Creates an arc.
BLOCK	Creates a block definition from selected object.
BREAK	Breaks the selected object between two points.
CLOSE	Closes the current drawing.
CLOSEALL	Closes all currently open drawings.
CIRCLE	Create a circle.
СОРҮ	Create a copy of an object.
DIST	Measures the distance and angle between two points.
DIVIDE	Creates evenly spaced point objects.
ERASE	Delete an object.
EXTEND	Extends the object to meet the edges of other objects.
EXPLODE	Breaks an object into component object.
EXTERNALREFERENCE	Opens the External References pallet.
FILLET	Rounds and fillets the edges of the objects.
НАТСН	Fills an enclosed area.
LAYER	Manages layers and layer properties.
LINE	Creates straight line segments.
LIST	Displays property data for selected objects
MATCH PROP	Applies the properties of selected objects to other objects.

Table 3.1: AUTOCAD commands.

MIRROR	Create a mirror copy of other object.
MODEL	Switches from layout tab to model tab.
MSPACE	In a layout, switches from paper space to model space in viewport.
MTEXT	Creates a multiline text object.
OPTIONS	Customizes the program settings.
ORTHO	Constraints cursor movement to horizontal or vertical direction
OSNAP	Sets running object snap model
PROPERTIES	Controls properties of existing objects.
PRINT	Prints the 2D drawing.
PAN	Moves view planner to the screen
PLINE	Creates a 2D polyline.
POLYLINE EDIT	Edits the polyline.
PURGE	Removes unused items
REGEN	Regenerates the entire drawing from the current viewport.
RECTANG	Creates the rectangular polyline
ROTATE	Rotates the selected object.
SCALE	Enlarges or reduces selected object.
SELECT	Places selected objects in the previous selection set.
TEXT	Creates a single- line text objects.
STRETCH	Stretches objects crossed by a selection window.
TRIM	Trim object to meet the edges of other objects.
TEXTSCR	Opens the text window.
UNITS	Controls coordinates and angle display format and precision.
ZOOM	Increases or decreases the magnification of the view in the viewport.



Figure 3.1: Plan of Pudimadaka Thermal Power Plant

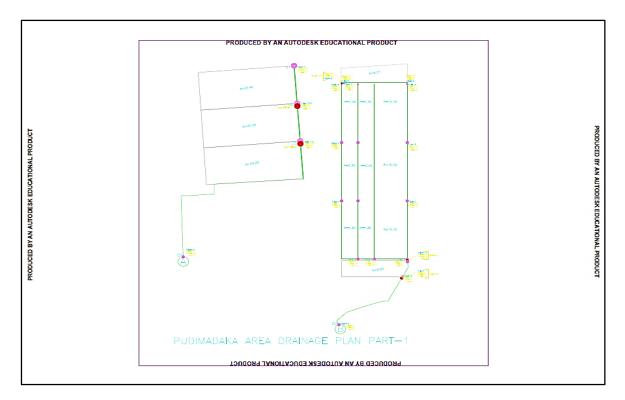


Figure 3.2: Plan showing Pudimadaka Thermal Power Plant Part 1

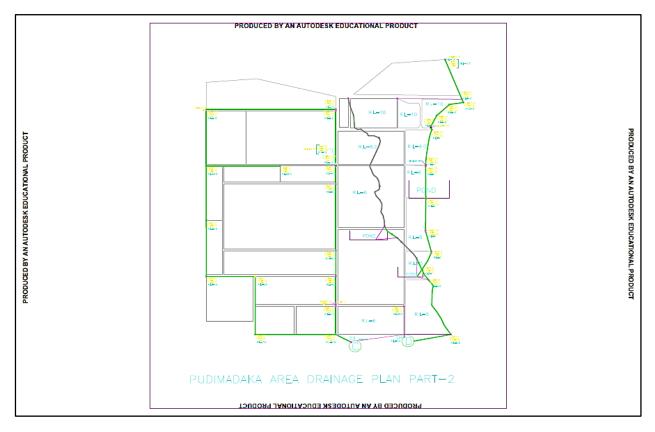


Figure 3.3: Plan showing Pudimadaka Thermal Power Plant Part 2

CHAPTER - 4 STUDY AREA

4.1 CHARACTERISTICS OF STUDY AREA-I

4.1.1 Location

The site is located at Andra Pradesh state, Vishakhapatnam district, near Pudimadaka village, Achutapuram & Rambilli Mandals and is approximately 40 km from district headquarters Visakhapatnam. The site is well connected through Pudimadaka road to NH-16 at a distance of 12.2 km and by SH-97 at a distance of 3.5 km. Gangavaram port is about 35 km NE of the site and Vizag port is at a distance of 47 km from the site. Figure 4.1 shows the Index map of Pudimadaka Power Plant.

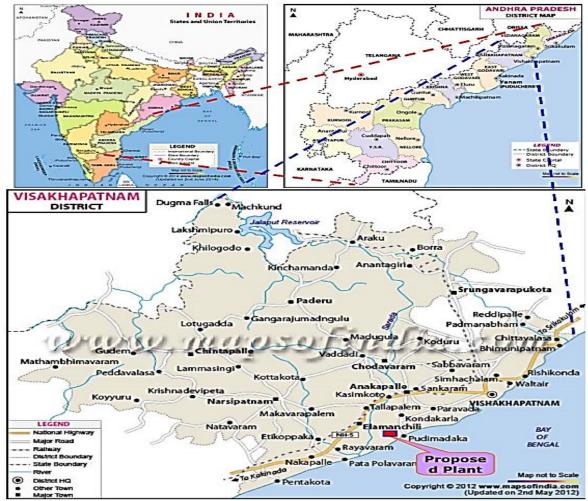


Figure 4.1: Index Map of Pudimadaka Power Plant

4.1.2 Topography

The study area is predominantly plain with few hillocks observed adjacent to the project site. Maximum difference in levels would be about 36 - 40m.

4.1.3 Rainfall & Climate

Climatologically the district experiences tropical sub-humid type of climate with moderate summer and good seasonal rainfall. The southwest monsoon sets in the second week of June and lasts till September end. October and November receive rainfall from northeast monsoon. Winter season with cool and fine weather prevails from December to February followed by summer season up to early June. The average annual rainfall of the district is 1116 mm. and monthly rainfall ranges from nil rainfall in January to 207.5 mm in October. October is the wettest month of the year. The mean seasonal rainfall distribution is 673.5 mm. in southwest monsoon (June September), 271.8 mm. in northeast monsoon (October-December), 10.9 mm. rainfall in winter (Jan-Feb) and 159.6 mm in summer (March–May). The percentage distribution of rainfall, season-wise, is 60.36% in southwest monsoon, 24.36 % in northeast monsoon, 0.97 percentage in winter and 14.3 % in summer.

4.1.4 Soils

The different soils in the district are red loams, sandy loams, sandy soils and black cotton soils. Red loamy soils are predominating and occupy about 70% in the district. Sandy loamy soils are largely confined to the coastal areas and to certain stretches in the interior mandals of Chodavaram, Narsipatnam, K. Kotapadu and Madugula. Black cotton soils occur in parts of K. Kotapadu, Devarapalli, Chedikada, Paderu and Hukumpeta mandals.

4.1.5 Drainage

The most important rivers drained in the district are Machikund, Tandava, Varaha, Sarada and Gostani. Most of the rivers are ephemeral in nature. However, some of the tributaries of Machikund are perennial with indications of substantial ground water discharge. Almost all the rivers and streams experience flash floods during rainy season. A good number of springs exist in Paderu and Araku areas. The district is characterized by sub-dendritic to dendritic nature of drainage pattern and is of coarse texture. In general, the density is in the range of 0.6 to 1/Km2. Many of the hill streams in Paderu valley disappear on entering the plains due to high permeability of the pediment gravels. The disappearance of streams in and along the

hill slopes is contributing to the ground water, which is again discharged through the silty soils at lower elevations.

4.1.6 Land cover and land use

The plant area lies mostly in the agricultural fields with coconut and cashew plantation area. The area is selected excluding the existing villages Kothakudur, Vasattipalem, Laxmipuram and Nalapalem. There are some scattered huts in the agricultural fields inside the plant area. The village Pudimadaka is about 300m from the proposed plant area. Overall the area is plain with gentle slope the total level difference in the site is about 30m. There is no water logging area in the plant site. There are some salt beds on the south of the plant area. Small village ponds are seen inside the plant area and adjacent to the plants area as well.

4.1.7 Data Used for The Study of Study Area -I:

- Daily rainfall records for Vishakhapatnam for 2000 to 2011 and daily rainfall data for Kakinada for 1996 to 2014 were obtained from National Institute of Hydrology, Roorkee.
- Natural drainage within plant area and vicinity based on reconnaissance survey of the area.
- Plant layout map and contour map for the plant area and the nearby area based on recent topographic survey.

4.2 CHARACTERISTICS OF STUDY AREA-II

4.2.1 Location

The second study area is located in Andaman and Nicobar islands. There are 572 islands in the territory having an area of 8,249 km² (3,185 sq. mi). Of these, only 38 are permanently inhabited. The islands extend from 6 ° to 14 ° North latitudes and from 92 ° to 94 ° East longitudes. The Andaman's are separated from the Nicobar group by a channel (The Ten Degree Channel) some 150 km (93 mi) wide. The highest point is located in North Andaman Island (Saddle Peak at 732 m (2,402 ft.)). The Andaman group has 325 islands which cover an area of 6,408 km² (2,474 sq. mi) while the Nicobar group has only 24 islands with an area of 1,841 km² (711 sq. mi).

The capital of the union territory, Port Blair, is located 1,255 km (780 mi) from Kolkata, 1,200 km (750 mi) from Visakhapatnam and 1,190 km (740 mi) from Chennai. The

northernmost point of the Andaman and Nicobars group is 901 km (560 mi) away from the mouth of the Hooghly River and 190 km (120 mi) from Burma. Indira Point at 6° 45' 10"N and 93° 49' 36"E at the southern tip of the southernmost island, Great Nicobar, is the southernmost point of India and lies only 150 km (93 mi) from Sumatra in Indonesia.

The proposed site is located near Mithakhari village, and is approximately 30km from Port Blair. The Index map is shown in Figure 4.2(a). Figure 4.2(b) is the site vicinity map.

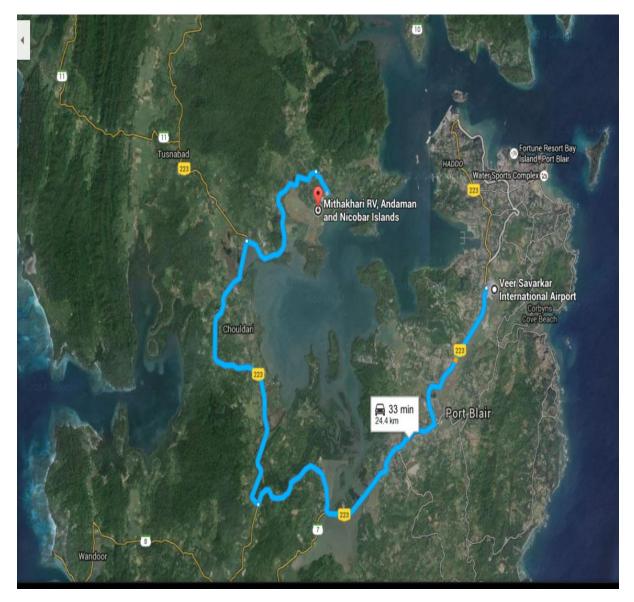


Figure 4.2(a) Index map of Mithakhari solar plant site



Figure 4.2(b) Mithakhari solar plant site vicinity map

4.2.2 Soil and Vegetation

Andaman and Nicobar Islands soil and vegetation are favorable for tropical evergreen forest and semi-evergreen forests; in some regions, the soil and vegetation of Andaman and Nicobar Islands also supports tropical monsoon.

Andaman and Nicobar Islands experiences a tropical climate, without any extremes except for the rains and thunder storms. Rainfall is common in the Islands, and is generally divided into two phases: May to mid-September and November to mid-December. Thus, the climate of Andaman and Nicobar Islands is highly favorable for the evergreen forest.

The soil and vegetation at Andaman and Nicobar Islands supports the growth of epiphytic vegetation (plants that grow on other plants). In fact, the vegetation of Andaman and Nicobar Islands mostly comprise of ferns and orchids.

The vegetation of Middle Andaman mostly includes moist deciduous forests. The monsoon rains largely supports the deciduous type of vegetation in the Andaman and Nicobar Islands. Further, the vegetation of North Andaman is characterized by wood climbers: the type of vegetation found here is moist evergreen type. Another aspect of vegetation in Andaman and Nicobar Islands is that throughout the length and breadth of the islands, the coastline is dotted with coconut trees. The entire fringe of the island is outlined with coconut trees.

4.2.3 Climate

Like most islands in the Bay of Bengal, Andaman and Nicobar too have a tropical climate with humidity about 80% and temperatures varying from 23 ° C to 31 ° C. The North East Monsoon sets in November whereas the South West Monsoon towards the end of May. Weather remains more or less uniform throughout the year with neither extreme hot summers nor chilly winters.

4.2.4 Rainy days and monthly rainfall at port Blair

Fifteen years (from 2000 to 2014) daily rain fall data at Port Blair has been analyzed. Study of rainy days and seasonal rainfall is also relevant as efficiency of solar plant in electricity generation depends on sunshine duration in a period. Months having more amounts of rainfall and more number of rainy days are less effective as far as electricity generation is concerned.

1. Rainy days

Table 4.3 shows number of rainy days in different months. A day is considered to be rainy day if rainfall on that day is more than 6 mm. On an average there are 100 rainy days in a year. May to October is the rainy season sometimes extending in the month of November also. February is the driest month with only one rainy day on an average.

2. Monthly rainfall

Table 4.4 shows monthly rainfall in year's 2000 to 2014. Average annual rainfall is 3114 mm. 2796 mm rainfall (89.8%) is received during May to November. September is the rainiest month with an average rainfall of 500 mm followed by May month with average rainfall of 491 mm. February is the driest month with average rainfall of 23 mm.

Table 4.3 Number of Rainy Days (Considering Rainfall More Than 6 mm) at Port Blair

Yr.	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sept	Oct	Nov	Dec	Total
2000	2	3	4	6	15	14	11	17	12	10	5	3	102
2001	4	0	5	1	23	11	12	14	12	10	6	4	102
2002	0	0	0	3	12	9	14	9	14	4	9	4	78
2003	1	0	4	1	11	9	22	15	14	9	3	4	93
2004	1	3	0	1	17	18	11	13	12	15	5	0	96
2005	0	0	0	3	8	15	17	15	15	10	12	8	103
2006	1	0	0	7	14	18	8	14	23	11	4	1	101
2007	0	0	0	3	15	14	10	15	16	11	9	1	94
2008	1	3	4	9	16	14	18	14	12	9	11	0	111

2009	0	0	1	7	11	16	9	10	12	10	6	2	84
2010	2	0	0	0	10	14	18	16	13	18	11	11	113
2011	6	3	11	2	11	12	19	17	20	11	3	4	119
2012	1	1	0	4	16	9	12	13	19	11	11	5	102
2013	2	0	0	2	14	19	18	14	22	7	12	3	113
2014	0	0	0	0	11	13	17	10	13	14	7	0	85
Avg.	1.4	0.867	1.933	3.267	13.6	13.667	14.4	13.73	15.27	10.67	7.6	3.333	99.73

Table 4.4 Monthly Rainfall (mm)	at Port Blair
---------------------------------	---------------

Yr.	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sept	Oct	Nov	Dec	Total
2000	32.5	85.5	200	210.6	468.3	383.6	230.9	572.5	258.3	300.7	141.1	79.6	2963.6
2001	122.3	5.1	121.5	16.4	942.5	228.6	305.1	454.2	431.6	290.4	117.7	79.2	3114.6
2002	0	0	0	84.4	386.1	354.6	441.1	294.2	421.8	78.3	313.5	122	2496
2003	21.4	0.1	127.3	13.3	316.2	225.2	535	352.6	420.2	290.1	56.8	69.9	2428.1
2004	104.2	25.9	1	33.7	662.8	601.3	401.4	362.9	431	270.3	143.9	0.9	3039.3
2005	0	0	3.4	51.7	312.3	912.4	546.4	463.7	609.7	207.5	366.7	285.4	3759.2
2006	6.7	1.9	0.9	149.8	403.8	481.2	177.3	314.1	791.7	561.4	79	34.4	3002.2
2007	0	0	0	40.7	274.2	402.5	251.6	489.1	473.2	320.9	263.8	9.6	2525.6
2008	10.5	43	80.6	287.9	976	374.4	632.8	527.5	479.8	274.1	443	0.8	4130.4
2009	0	0	27.2	157.4	405.1	566.1	178.8	418.5	411.2	237.6	86.9	62.6	2551.4
2010	88.9	0	0	7	320.1	390.7	594.2	423	314.5	420.7	222.3	328.8	3110.2
2011	132.1	77.4	456.2	54.2	409.3	450.1	607.6	535.2	643.6	150.7	70.6	240.6	3827.6
2012	36.1	109.4	8.5	63.2	597	395.2	298	406.3	904.8	252.4	249.1	155.1	3475.1
2013	28.9	0.1	5.7	21.3	659.1	616.8	597.1	235.2	493.2	267.1	352.7	129.4	3406.6
2014	0.4	0	0	0	229.9	501.7	696.6	283.5	409.4	564.9	174.6	16	2877
Avg.	38.93	23.23	68.82	79.44	490.85	458.96	432.93	408.83	499.6	299.14	205.45	107.62	3113.79

4.2.5 Data Used for The Study of Study Area -II:

Daily rainfall data for IMD station at Port Blair

- WAPCOS Report on Flood Control Works in Mithakhari
- Data tidal observations at Port Blair
- Layout details of existing 5 MW solar plant at Port Blair
- Natural drainage within proposed plant area and vicinity based on reconnaissance survey of the area.

CHAPTER 5

INTERNAL DRAINAGE PLANNING OF STUDY AREA-I

Storm water management model can be used for the planning of drainage scheme in a proposed industrial area. A variety of options can be tried to arrive at appropriate plan satisfying various physical and technical constraints such as topography, plant layout etc.,

This chapter illustrates potential use of AUTOCAD, SWMM and Arc-GIS model in coastal drainage planning through case study of proposed Pudimadaka thermal power plant (study area-I). Fig 5.1 shows the plant area details with their components.

The Auto-CAD model and Arc-GIS model combined is used for the DEM study the brief procedure followed has been explained as below.

5.1 Procedure for Digital Elevation Model (DEM)

The contour map prepared using AutoCAD software was converted to raster format. The converted contour map was geo-referenced providing X and Y co-ordinates i.e. (Latitude and Longitude) in ARC-GIS by selecting four or more points in clockwise direction. The geo-referenced values were verified using Link table. Further, for the minor changes in the co-ordinates during the selection are adjusted by selecting Auto adjusts in Link table and geo-referenced raster file is rectified.

The geo-referenced rectified file saved in image format i.e. (.img). The same file is opened from catalog of Arc-GIS. Using Arc toolbar, from Data Management Tool, Projection and Transformation select Define projection, provide input parameter as Universal Transverse Mercator (UTM) projected coordinate system and Zone 44 N WGS 1984 for geo-referencing and click ok the file is Geo-referenced.

Open the contour map (.dwg file) using AutoCAD software, switch off all the layers except contour layer and save the file. From ArcGIS software open the same file, the opened file can be viewed at Table of contents, Right click on it and open attribute table and view the contour elevations. After that, again right click, go to Data and Export data to create a Shape file.

Using, spatial adjustment and editor tool, start editing by selecting four points on the map to set adjustment data and select save edit and stop editing. Also, if necessary using editor tool bar start editing by deleting unnecessary things and join the missing contours.

For creating DEM in ArcGIS from the contours exported from AutoCAD, first identify whether the contour lines are belonging to respective contour elevations or else assign elevation values for each of the contour lines in ArcGIS. Further, after assigning the values create TIN file using 3D analyst tool, Data Management, TIN, create TIN, for input class give contour and at Height field select Elevation.

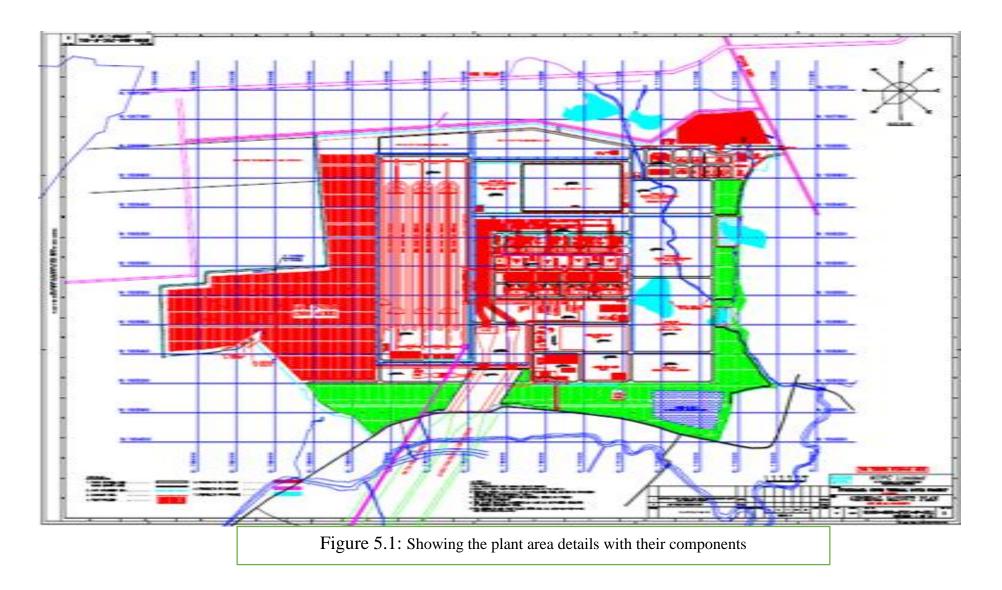
Convert TIN to raster in order to get DEM for that go to 3D Analyst tool, Conversion, TIN to raster, create TIN, and give input file name as (.img) click ok. Further, Extract the boundary file by Extract by mass using Spatial Analyst Tool, Extraction, Extract by mask and provide input parameter as (dem.img) that was created in previous step and output parameter as Boundary shape file. Now, only plant area is ready for further analysis.

Further, reclassify in-order to obtain Area-Elevation-capacity calculations using, Arc toolbar, Spatial Analyst tool, Reclass, Reclassify, provide extracted file as input raster and enter the value up to which elevation point is maximum and provide breakages manually.

ARC-GIS software has been used for preparation of the DEM. The contours in shape file have been interpolated to obtain digital elevations of the equally sized gird cells. Size of a grid cell is $0.5 \text{ m} \times 0.5 \text{ m}$ in this study. The DEM of the plant area is shown as contour zoning map in Fig 5.4 and variation in elevation from 0 m to 20.5 m is depicted through different colors. The DEM of the study area is also shown as single color intensity map in Fig 5.4(a).

Fig 5.4 shows, the existing ground levels varying from 0.0 m to 20.5 m in the project area. The north-west part of the area has elevations in the range of 1.6 m to 20.5 m. The south-west part and eastern part of the project area have lower elevations in the range of 0 m to 6.0 m. The plant area can be leveled in order to economize cost of earthwork in excavation and filling and plant components can be kept at different levels as per the requirement.

The DEM can be used to identify areas requiring cutting and filling and to estimate the volume of earthwork required to level the undulating topography of the study area.



5.1.1 Distribution of land area in different elevation ranges

The Digital Elevation Model prepared in Geographic Information System (GIS) has been used to compute the natural drainage area (within plant boundaries) between different elevation ranges. The DEM computes the number of pixels in each interval. Table 5.1 shows distribution of area from 0 m to 20.5 m elevation. The DEM pixel size used in this study is $0.5m \times 0.5$ m.

5.1.2 Distribution of land area in Pudimadaka project area

Table 5.1 show that, in the pudimadaka project area 486.09 ha (65.39%) of land area lies below 9 m elevation (317.85ha) and the project area having elevation higher than 9 m elevation is 168.24 ha (34.61%).

Elevation	No. of pixels	Area (sq.m)	Area (Ha)	Cum. Area (Ha)	Area (%)	Cum. Area (%)
1	31	16998	1.7	1.70	0.35	0.35
2	465	254973	25.5	27.20	5.25	5.60
3	623	341610	34.2	61.36	7.03	12.62
4	642	352028	35.2	96.56	7.24	19.86
5	823	451275	45.1	141.69	9.28	29.15
6	1106	606453	60.6	202.33	12.48	41.62
7	848	464984	46.5	248.83	9.57	51.19
8	672	368478	36.8	285.68	7.58	58.77
9	587	321870	32.2	317.87	6.62	65.39
10	473	259360	25.9	343.80	5.34	70.73
11	387	212204	21.2	365.02	4.37	75.09
12	328	179852	18.0	383.01	3.70	78.79
13	285	156274	15.6	398.64	3.21	82.01
14	335	183691	18.4	417.00	3.78	85.79
15	268	146952	14.7	431.70	3.02	88.81
16	234	128309	12.8	444.53	2.64	91.45
17	206	112956	11.3	455.83	2.32	93.77
18	208	114053	11.4	467.23	2.35	96.12
19	257	140921	14.1	481.32	2.90	99.02
20	87	47705	4.8	486.09	0.98	100.00
	Total Plan	nt Area = 486.09	44		100.00	

Table 5.1 Cumulative areal	distributions with	elevation in the	Pudimadaka ni	niect area
Table 5.1 Culturative areas	distributions with	elevation in the	гишпацака рі	oject alea.

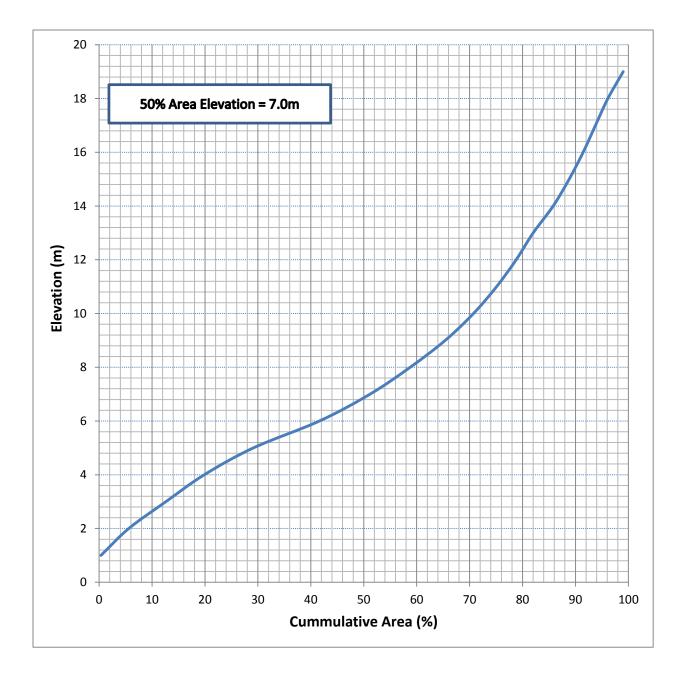


Figure 5.2: Cumulative areal distributions with elevation in the Pudimadaka Project area.

Fig 5.2 is graphical depiction of the cumulative area distribution up to different elevation. The information derived from the DEM study can be used to arrive at cost effective levels at which different plant components should can be finally located.

Elv	No. of pixels	Area (sq.m)	Area (Ha)	Area (%)	Cum. Area (Ha)	Cum Area (%)	H-h (m)	Avg. Area (ha)	Vol. (ha-m)	Vol. (%)	Cum. Vol.	Cum. (%)
1	31	16998.2	1.70	0.35	1.70	0.35	1	1.70	1.70	0.35	1.70	0.35
2	465	254973.4	25.50	5.25	27.20	5.60	1	13.60	13.60	2.81	15.30	3.16
3	623	341609.5	34.16	7.03	61.36	12.62	1	29.83	29.83	6.16	45.13	9.31
4	642	352027.8	35.20	7.24	96.56	19.86	1	34.68	34.68	7.16	79.81	16.47
5	823	451275.5	45.13	9.28	141.69	29.15	1	40.17	40.17	8.29	119.97	24.76
6	1106	606452.9	60.65	12.48	202.33	41.62	1	52.89	52.89	10.91	172.86	35.67
7	848	464983.7	46.50	9.57	248.83	51.19	1	53.57	53.57	11.06	226.43	46.73
8	672	368477.7	36.85	7.58	285.68	58.77	1	41.67	41.67	8.60	268.11	55.33
9	587	321869.6	32.19	6.62	317.87	65.39	1	34.52	34.52	7.12	302.62	62.45
10	473	259360.0	25.94	5.34	343.80	70.73	1	29.06	29.06	6.00	331.68	68.45
11	387	212203.7	21.22	4.37	365.02	75.09	1	23.58	23.58	4.87	355.26	73.32
12	328	179852.2	17.99	3.70	383.01	78.79	1	19.60	19.60	4.05	374.87	77.36
13	285	156274.0	15.63	3.21	398.64	82.01	1	16.81	16.81	3.47	391.67	80.83
14	335	183690.5	18.37	3.78	417.00	85.79	1	17.00	17.00	3.51	408.67	84.34
15	268	146952.4	14.70	3.02	431.70	88.81	1	16.53	16.53	3.41	425.20	87.75
16	234	128309.2	12.83	2.64	444.53	91.45	1	13.76	13.76	2.84	438.97	90.59
17	206	112956.0	11.30	2.32	455.83	93.77	1	12.06	12.06	2.49	451.03	93.08
18	208	114052.6	11.41	2.35	467.23	96.12	1	11.35	11.35	2.34	462.38	95.42
19	257	140920.8	14.09	2.90	481.32	99.02	1	12.75	12.75	2.63	475.13	98.05
20	87	47704.7	4.77	0.98	486.09	100	1	9.43	9.43	1.95	484.56	100.0 0
			486.09	100.0				484.56	484.56	100.0		

Table 5.2: Elevation-Area- volume Computation for entire Project area

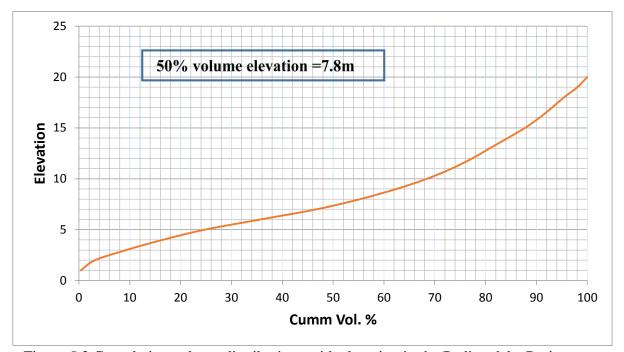
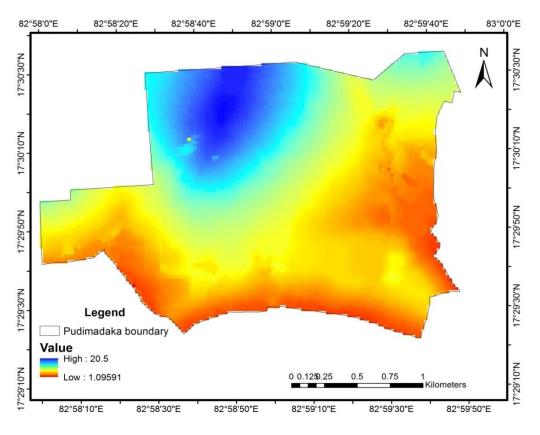
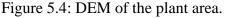


Figure 5.3 Cumulative volume distributions with elevation in the Pudimadaka Project area Fig 5.3 is graphical depiction of the cumulative volume distribution up to different elevation. The information derived from the DEM study can be used to arrive at cost effective levels at which different plant components should can be finally located.





5.1.3 Generation of stream network

The Spatial analyst tools of ARC-GIS software has been used in the present study for further processing in the context of stream generation. DEM has been smoothened out for eliminating uneven irregularities using Fill tool to remove the sinks. Corrected DEM has been used to generate pattern of flow directions and for identification of flow accumulation through each pixel of given elevation. Generated information on flow pattern and flow accumulation considers Eight-Point Pour model for the purpose of computing flow directions for use in basin delineation with DEMs directions.

With the flow directions assigned for each DEM point, the flow accumulation at each DEM point has been computed. The flow accumulation at a given DEM point is defined as the number of earlier DEM points whose flow paths eventually pass through that point. Streams are identified by large values of flow accumulation since the flow paths of many points pass through the stream points. Outlet of a watershed has the highest value of flow accumulation of any of the DEM points since the flow paths of all points in the watershed will eventually pass through the outlet point. Streams have been identified by displaying all DEM points with a flow accumulation value. Fig 5.5 shows the generated stream network in the study area.

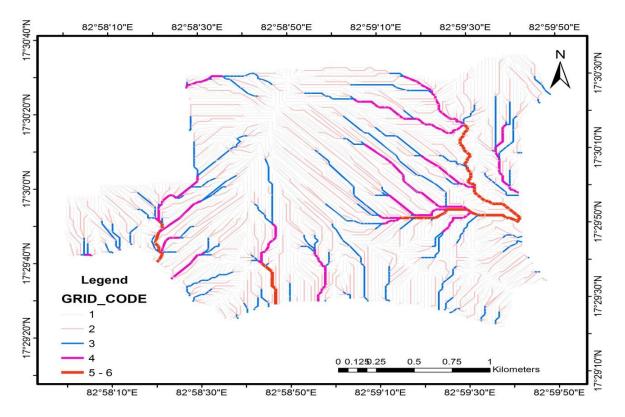


Figure 5.5: DEM stream network of the plant area.

5.1.4 Summary Results of DEM Study

From the DEM study it is evident that the plant natural ground varies from 0 to 20.5m, the F.G.L in the plant area ranges from 7 to 15m. The average elevation corresponding to balancing the cut and fill volume of earthwork is 7.8m. It means earth may have to be brought from outside for filling. (Based on the Table 5.2 for which area/volume above a certain elevation is of the order of 50%).

5.2 INTERNAL DRAINAGE FOR THERMAL POWER PLANT

Storm water management model can be used for planning and drainage scheme in a proposed industrial area. A variety of options can be tried to arrive appropriate plan satisfying various technical and physical constraints such as plant layout, topography, soil characteristics etc.

The potential use of SWMM software in planning for internal drainage through case study of proposed thermal power plant in Vishakhapatnam, Andra Pradesh.

5.2.1 Plant Area Characteristics

STPP area is about 358 ha (= 885 acres) consisting of different land uses. The plant area having undulating topography exhibits large difference in its ground levels. DEM study using recent topographic data has been presented previously. Based on this study, the existing ground levels vary from 1m to 20.5 m in the project area. The north-west part of the area has elevations in the range of 1.6m to 20.5 m. The south-west part and eastern part of the project area have lower elevations in the range of 1 m to 6.0 m. The plant area to be levelled. In order to economize cost of earthwork in excavation and filling.

Elevation (m)	Space for various components	Area (ha)
14	Crushed coal stock pile unit	60.65
16	Space for transmission line (in north of coal yard)	5.26
15	Space for transmission line (in north of switch yard)	11.33
12	Switch yard (16.99 ha), space for preassembly north of Boiler unit (8.09ha)	25.08
10	Residential and Office complex area	17.75
9	Main plant (Boiler Unit)	44.1
8	CW pump house, Desalination plant	17.08

 TABLE 5.3: Plant components at different levels

8	Space for lay down and pre assembly and green belt (to east of switch	11.28
	yard)	
7	Desalination unit and water storage area	7.68
7	Desilting basin to the south of coal stock pile unit area	5.26
6	Space for lay down and pre assembly and green belt (to east of main plant)	52.19
Total	plant area	257.66

5.2.2 Location of Streams around Plant Boundary

There are five natural drains in vicinity of plant. These are Krishnapalem nala, upper Rambilli nala, lower Rambilli nala (Upper Rambilli nala is termed as lower Rambilli nala after confluence with Krishnapalem nala), Doraipalem nala (passing through plant area on east side) and Pudimadaka nala. Doraipalem nala joins Pudimadaka nala near south east boundary of plant area. The plant site is located on high ground between the drains on west and east sides. In general, all the drains flow in north to south directions following the slope of terrain the Green Ampt Method has been used for estimating infiltration. according to various land use/cover and soil conditions, Green Ampt parameters are shown in Table 5.6.

5.2.3 Bankful Discharge Calculations and Computation of Streams

In order to assess the flooding, bankful discharge capacity of natural drains have been estimated using slope area method. For estimation of cross section parameters, approximate ground levels on the left and right banks have been worked out with the help of recent contour map of the plant area. Eleven locations have been selected to assess the bankful discharge capacity. There are five natural drains in vicinity of plant. These are Krishnapalem Nala, upper Rambilli nala, lower Rambilli nala (after confluence of Krishnapalem nala), Doraipalem nala (passing through plant area on east side) and Pudimadaka nala. Doraipalem nala joins Pudimadaka nala near south east boundary of plant area. The plant site is located on high ground between the drains on west and east sides. In general, all the drains flow in north to south directions following the slope of terrain. To compute bankful capacity of these nala the cross sections has being taken near to the adjoining nala's and also section taken at the point where two nala's coincides each other. Using the below Empirical formulae the bankful discharge capacity is calculated:

Velocity (v) has been estimated by Manning's equation $V(m/s) = \frac{1}{n} \times R^{2/3} \times S^{1/2}$

 $Q(m^3/s) = A \times V$ where,

- n: Manning roughness coefficient assumed to be 0.0375 for small streams in plains with small boulders.
- \blacktriangleright R: hydraulic mean depth (=A/P)
- ➤ A (m²): Cross section area
- ➢ P (m): perimeter
- > S (m/m): surface water slope assumed to be same as river bed slope (0.00391)
- \triangleright Q: discharge (m³/s).

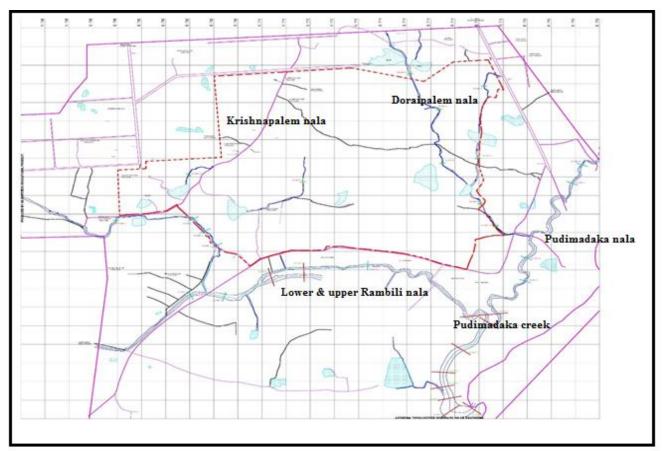


Fig 5.6: Nala sections at the plant boundary.

Sl.no.	Nala	Velocity (m/s)	Discharge (m	Discharge (m ³ /sec)		
		Maximum	Minimum	Maximum	Minimum		
1	Krishnapalem	2.31	1.71	127.86	44.59		
2	Doraipalem	1.82	1.78	50.59	45.20		
3	Lower & Upper Rambilli	3.31	2.09	1005.15	152.97		
4	Pudimadaka	3.21	3.00	520.37	363.23		
5	Pudimadaka creek	3.94	2.82	1841.73	386.52		

TABLE 5.4: Velocity and discharge of nala's in the plant area

5.3 FREQUENCY ANALYSIS OF 1-DAY ANNUAL MAXIMUM RAINFALL

Daily rainfall data for Vishakhapatnam from 2000-2011 in which data for 2003 and 2004 are missing and for Kakinada station from 1996-2014 (18 years) have been utilized for estimation of design storm. The maximum rainfall of Vishakhapatnam for missing data years of 2003 and 2004 has been taken the same as of Kakinada station, i.e. 120 mm on 15 July 2003 and 119.6 mm on 3 Aug. 2004, respectively. Thus, the 1-Day annual maximum rainfall series was constructed for Vishakhapatnam for 12 years (2000-2011) and EV Type I probability distribution was applied. Return period of 1-day annual maximum rainfall series at Vishakhapatnam is estimated in Table 5.5. Fig 5.7 shows graphical frequency analysis of 1-day annual maximum rainfall at Vishakhapatnam.

5.3.1 Regional Depth Duration Frequency Studies

The study area lies in Eastern Coastal Region Sub Zone 4a defined by CWC (1987). India Meteorological Department (IMD) has conducted detailed rainfall study for the Sub Zone 4(a, b, c) (CWC 1987) utilizing the data of 24 self-recording rain gauge stations and 376 ordinary rain gauge stations maintained by IMD/States and 43 self-recording rainguages of Indian Railways maintained in 10 bridge catchments in these subzones.

Sl.	Year	Date	Annual Max	Rainfall in	Rank	m/(n+1)	Return
No.			1-day	Descending	(m)		Period
			Rainfall	Order			(Years)
		25-Aug-					
1	2000	00	86	183	1	0.08	13.00
2	2001	30-Sep-01	114	153.2	2	0.15	6.50
3	2002	10-Jun-02	74	132	3	0.23	4.33
4	2003	15-Jul-03	120	129.4	4	0.31	3.25
5	2004	3-Aug-04	119.6	124.3	5	0.38	2.60
6	2005	20-Sep-05	153.2	120	6	0.46	2.17
7	2006	4-Aug-06	124.3	119.6	7	0.54	1.86
8	2007	5-Oct-07	115.1	115.1	8	0.62	1.63
9	2008	10-Feb-08	129.4	114	9	0.69	1.44
10	2009	30-Sep-09	84	86	10	0.77	1.30
11	2010	1-Nov-10	183	84	11	0.85	1.18
12	2011	7-Jul-11	132	74	12	0.92	1.08

TABLE 5.5: Frequency analysis of 24-hr Annual Maximum Rainfall at Vishakhapatnam

TABLE 5.5(a): 1-day rainfall (mm) of various return periods

Station	Return period (Years)							
	2	5	10	25	50	100	200	500
1-day rainfall at Vishakhapatnam(mm)	115	150	170	190	200	238	260	285
24-hr rainfall (mm)	132.25	172.5	195.5	218.5	230	273.7	299	327.75

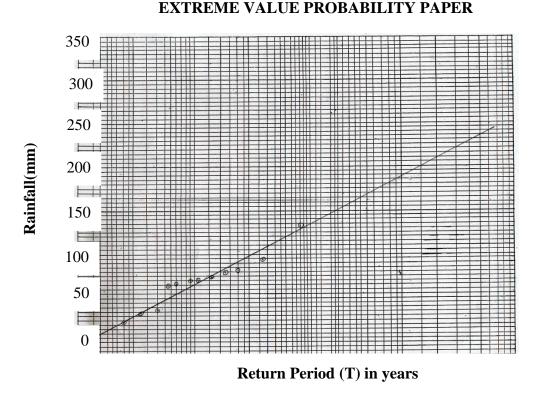


Figure 5.7: EV Type-I Probability distribution of annual maximum 1-day rainfall at Vishakhapatnam

5.3.3 Design Storm

In the absence of site specific hydro-meteorological data, regional approach has been adopted to arrive at the design storms of return periods corresponding to 25 years, 50 years and 100 years, the drainage network for this plant is designed for 25 year return period flood. Design storm duration is adopted as 6 hours considering the geomorphological characteristics of the area. The hourly distributions of rainfall for 25 year return period storm is given in Table 5.6.

WRD&M, IIT ROORKEE

Return Period	Rainfall (mm)	Hour					
(Year)		1 st	2 nd	3 rd	4 th	5 th	6th
25	Cumulative	77.76	106.56	123.84	132.48	141.12	144
	Incremental	77.76	28.8	17.28	8.64	8.64	2.88

TABLE 5.6: Time distribution of Cumulative and Incremental Rainfall of different Return Periods

5.4 DESIGN CONSIDERATIONS

The drainage layout has been planned based on the following considerations:

- Drainage channels should safely carry storm runoff caused by design storm of 25 year return period.
- Bed slope of drainage channels is to be kept such that flow is carried with sufficient velocity so that silting does not occur in channels and channel invert levels are not in deep cutting.
- > Concrete lined rectangular sections are provided throughout.
- Vertical drops are necessary to negotiate level differences in plant components as proposed.
- Based on engineering as well as economic considerations, several outfalls are proposed at suitable locations to follow the natural topography.
- Channel slope, length, bed width is determined such that the capacity utilization in each of the channel segments (ratio of discharge contributed by connecting subcatchments to the channel carrying capacity) is near 1.0. However, in few channel segments this requirement has to be compromised based on hydraulic and drainage layout considerations.
- > Green Ampt method has been used for modelling infiltration.
- ➢ Kinematic wave routing has been used for flow routing in channels.

5.5 DRAINAGE PLAN

Fig 5.8 and 5.9 shows the adopted drainage plan in the main plant area. Plant area, is having undulated topography and there is a significant difference in ground level. For the efficient and economic disposal of generated runoff, the plant area is divided into forty number of

subcatchments with four different drain network, namely A, B, C and D with individual outlets O1, O2, O3, O4. For the analysis the plant area is divided into two parts as shown in the Fig 5.8 and 5.9.

Natural drainage indicates that; the existing ground levels vary from 1m to 20.5 m in the project area. The north-west part of the area has elevations in the range of 1.6m to 20.5 m. The south-west part and eastern part of the project area have lower elevations in the range of 1 m to 6.0 m. Fig 5.8 and 5.9 shows the proposed layout of drainage channels (rectangular section) and runoff contributing subcatchments. Four lateral drains will collect the storm runoff in the main plant area. Water from the drains are collected in the outfall. The outfalls are in different elevation. Water from these outfalls shall be disposed of to the sea. In drainage plan D, three storage units are provided (T3, T4, T5) in order to retain the existing ponds in the plant area.

Soil	Saturated hydraulic	Soil suction head	porosity
	conductivity	(mm/hr.)	
	(mm/hr.)		
Silty Clay	1.0	292.2	0.092

TABLE 5.7: Green Ampt parameters used in storm rainfall - runoff study

Source: SWMM model manual 5.1

5.5.1 Shape and Size of the Channel Section

SWMM simulates runoff from subcatchments and flow through channels. Shape, size of channels sections and slope of channels (invert levels at upstream and downstream end of each channels) are to be specified for simulation study.

Peak discharge resulting from the subcatchments are computed by rational formula (Q=CIA), Runoff coefficient (C) is obtained from the SWMM module. Invert levels are decided such that excessive excavation is avoided and the same time and discharge capacities are adequate to carry storm runoff in channels without causing excessive surface flooding. It is proposed to provide concrete lined rectangular channel. The manning's roughness co-efficient is taken as n=0.016.

5.5.2 Preparation of Input Data File

Fig 5.8 and 5.9 shows sub-catchments, junction, conduits, outfalls along with user assigned identification names. The input data/parameters used in this SWMM study are given below.

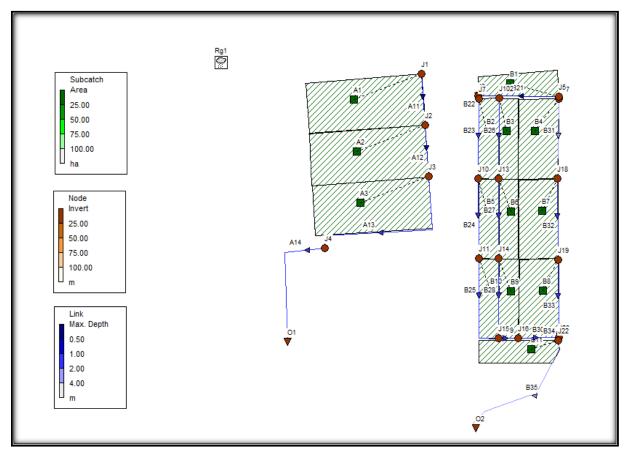


Figure 5.8: Pudimadaka internal drainage layout part 1

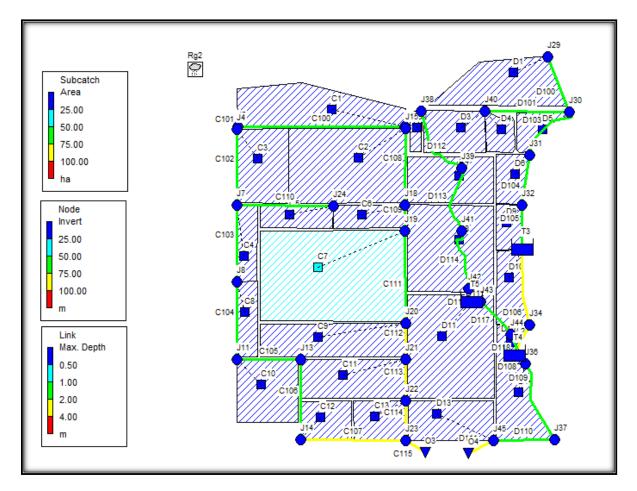


Figure 5.9: Pudimadaka internal drainage layout part 2

1. Raingauge- A raingauge provides rainfall data for one or more sub-catchments in the study area. In this study, drainage network is designed for 25 year of return period employing a distribution factor, this design storm is then distributed at 1-hour interval for the first six-hour duration, as follows.

Time (hour)	1 st	2 nd	3 rd	4 th	5 th	6 th
Incremental Rainfall (mm)	77.78	28.8	17.28	8.64	8.64	2.88

2. Subcatchment- Subcatchments are hydrologic units of land whose topography and drainage system elements direct surface runoff to a single discharge point. The whole study area is divided into 40 sub-catchments. These sub-catchments differ in their topography, land use, soil and finally discharge their runoff into single outlet point as shown in fig 5.8 and 5.9. Discharge outlet points can be either nodes of the drainage system or other subcatchments.

User-assigned sub-catchment			
Name of the rain gauge associated with the sub-catchment.			
Name of one single outlet of sub-catchment that receives runoff from it.			
Area of sub-catchment in hectares			
Characteristic width of overland flow path for sheet flow runoff in meters.			
Characteristic width is given by the subcatchment area divided by the			
average maximum overland flow length. The maximum overland flow is the			
length of the flow path from the inlet to the furthest drainage point of the			
subcatchment.			
Average percent slope of the sub-catchment is assumed to be 1in 1000 for all subcatchments			
Percent of land area which is impervious. It ranges from 5% to 100%			
Manning's n for overland flow over the impervious portion of sub-			
catchment. It is taken as 0.012			
Manning's n for overland flow over the previous portion of sub-catchment.			
It is taken as 0.05.			
Depth of depression storage on the impervious portion of the sub-catchment.			
It is taken as zero.			
Depth of depression storage on the pervious portion of the sub-catchment. It			
is taken as 2.54mm.			
Percent of the impervious area with no depression storage. Assumed to be			
100%			
Outlet: runoff from both area flows directly to outlet.			
The option controls how infiltration of rainfall into the upper zone of			
subcatchment is modeled. Green Ampt parameters such as suction			
head(mm), hydraulic conductivity (mm/hr), initial moisture deficient (equal			
to difference of porosity and field capacity) corresponding to sandy loam			
to anticipate of Porosity and their experies, corresponding to same round			
with relatively higher/lower percent of sand and silty loam soils found in			

TABLE 5.8: Sub-catchment properties

3. Junction – In a drainage network, junctions are the nodes which join links. A Junction also shows an outlet of any sub-catchment which receives runoff from that sub-catchment. Fig 5.7 and 5.8 shows how a node is attached with each sub-catchment and it joins the links up to outfall of the area to route the runoff.

Name	User assigned junction name
Inflows	Assign time series, dry weather to the junction. Assumed to be zero.
Invert El.	Invert elevation of the junction in meters.
Max. Depth	Max. Depth of junction (i.e. from ground surface to invert) in meters.
Initial depth	Depth of water at the junction at the start of the simulation in meters. Assumed to be zero.
Surcharge Depth	Additional depth of water beyond Max. Depth that is allowed before the junction floods in meters. This parameter can be used to simulate bolted manhole covers. Assumed to be zero as no flooding is allowed.
Ponded Area	Area occupied by ponded water atop the junction after flooding occurs in sq. Meters. It is taken as zero.

4. Conduit- Conduits are pipes or channels that move water from one node to another in the conveyance system. Conduits are used to convey the water to the outfall, it can be an open channel or closed conduit. Conduits are joined with nodes to divert the water and it is provided with an adequate slope so that the water flows by gravity.

Name	User assigned conduit name
Inlet Node	Name of the node on the inlet end of the conduit. (which is normally the end at higher elevation)
Outlet node	Name of the node on the outlet end of the conduit. (which is normally the end at lower elevation)

TABLE 5.10: Conduit Properties

Shape	Geometric properties of the conduit's. An open channel is provided for this study. The geometric properties of the conduit's cross-section. Rectangular channel section is taken.
Length	Length of conduit in meters.
Roughness	Manning's Roughness coefficients. It is taken as 0.016 for concrete lined open channel.
Inlet offset	Height of the conduit invert above the node invert at the upstream end of the conduit in meters.
Outlet offset	Height of the conduit invert above the node invert at the downstream end of the conduit in meters.
Initial Flow	Initial flow in conduit. It is zero.
Maximum	Maximum flow allowed in the conduit under dynamic wave routing. Use
Flow	zero if not applicable.

5. Outfall- Outlets are flow control devices that are typically used to control outflows from storage units. Outfall is the final output obtained in any catchment area. Further, it is a combination for all sub-catchments which in turn contribute to total runoff in the whole catchment area. Conveyance system routes the runoff and discharges into the river or any storage unit

TABLE 5.11: Outfall Node Properties.

Name	User-assigned outfall name
Inflows	Assign time series, dry weather to the outfall
Invert El.	Invert elevation of the outfall in meters.
Tide Gate	NO- no tide gate is provided.
Туре	Type of outfall boundary condition: Free: outfall stage determined by minimum or critical flow depth and normal flow depth in the connecting conduit.

6. Storage Units-Storage Units are drainage system nodes that provide storage volume.

Name	User-assigned storage unit name.		
Tag	Optional label used to categorize or classify the storage unit.		
Inflows	Click the ellipsis button (or press Enter) to assign external direct, dry weather, or RDII inflows to the storage unit.		
Invert El.	Elevation of the bottom of the storage unit (feet or meters).		
Max. Depth	Maximum depth of the storage unit (feet or meters).		
Initial Depth	Initial depth of water in the storage unit at the start of the simulation (feet or meters).		
Storage Curve	 Method of describing how the surface area of the storage unit varies with water depth: FUNCTIONAL uses the function: Area = A×(Depth)^B + C to describe how surface area varies with depth; TABULAR uses a tabulated area versus depth curve. In either case, depth is measured in feet (or meters) above the bottom and surface area in sq. feet (or sq. meters). 		
TABULAR	The tabulated data is given for T3, T4, T5.		
Curve Name	Name of the Storage Curve containing the relationship between surface area and storage depth (double-click to edit the curve). The curve will be extrapolated outwards to meet the unit's Max. Depth if need be.		

5.6 RESULTS OF SWMM STUDY

ANNEXURE 1 and ANNEXURE 2 provides summary information on analysis options, runoff quantity continuity, flow routing continuity and routing time step summary. Total storm rainfall in 6-hour duration is 144 mm (25 year return period) using Green Ampt model. The summary of Runoff quantity and Flow routing results are shown is the Table 5.13 & 5.14.

Runoff Quantity	Part 1	Part 2	Total Volume
Continuity			(hectare-m)
Total Precipitation	19.812	31.788	51.6
Evaporation Loss	0.000	0.000	0.000
Infiltration Loss	4.597	6.840	11.437
Surface Runoff	14.396	24.474	38.87
Final Storage	0.824	0.506	1.33
Continuity Error (%)	-0.031	-0.102	-0.133

 TABLE 5.13: Runoff Quantity Continuity Summary

 TABLE 5.14: Flow Routing Continuity Summary

Flow Routing Continuity	Part 1	Part 2	Volume
			(ha-m)
Dry Weather Inflow	0.000	0.000	0.000
Groundwater Inflow	0.000	0.000	0.000
External Inflow	0.000	0.000	0.000
Final Stored Volume	0.102	0.085	0.187
Wet Weather Inflow	14.394	24.473	38.867
RDII Inflow	0.000	0.000	0.000

5.7 CONCLUSION

The proposed plant layout of different components is at different F.G.L, this will be more economical than levelling the entire plant area. From SWMM study it is evident that the channels are hydraulically efficient to drain out the generated storm (Annexure part 1 and Annexure part 2 shows the entire results of SWMM). Shape and size of the channels can be further reduced depending upon the sub catchment runoff.

CHAPTER – 6 FLOOD CONTROL IN COASTAL AREA

6.1 INRODUCTION

This chapter, focuses on external flooding and its vulnerability in coastal regions that occurs due to the natural disaster such as tsunami, tides, storm surges due to heavy rainfall. Due to which sea water penetrates the coast with high speed causing excessive inundation which is called run-up. Fig.6.1 shows the different aspects of inundation. Run-up is used for determine extent of vulnerability, human settlement in coastal area it is useful in coastal land use planning. The run-up level data available for the study area i.e., (Andaman and Nicobar Islands) indicates 4 m in Port Blair (1868), 0.76 m in Car Nicobar (1881) and 1.22 m in Port Blair (1881) (Zhao, 2006). Due to developmental activities human encroachment takes place in coastal area for settlement or for agriculture purpose in the flood plain, is the place where all flood damages occur. This flood plain can be defined as relatively flat area bordering the stream (source: current science, 2005). Flood inundate valuable properties, endanger lives, due to high rate of flow or run-off from the catchment area causing large scale of erosion and results in deposition of sediments, floods also cause damage for drainage channels, bridges, and other structures and also results in loss of lives, economic losses etc.,

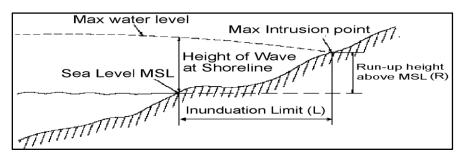


Figure 6.1: - Schematic diagram showing measurement of run-up height.

Flood control i.e., measures taken to reduce the effects of flood. The flood control is primarily aimed for the control of flood damage, there are many programs associated with flood control that determines on the basis of constructing various types of works, and to estimate the amount of damage. Many Literature is available on different methods of flood control. The methods are classified as below (Dube, 2008).

- Construction of detention and storage tanks in the catchment areas for flood moderation.
- Construction of ring bunds around imported towns properties etc., to prevent flooding.
- > Construction of bye-pass channels on the rivers and divert the flood water.
- ➢ Flood plain zoning.
- Providing suitable drainage arrangement
- > Conversion of soils by catchment area treatment plan ad prevent soil erosion
- Flood relief works, construction of embankment during flooding and emergency measures.
- > Flood prediction warning system to keep alert in advance.
- Construction of dykes in sea shores to prevent flooding due to tsunami and sea level rise.

6.2 EFFECT OF TSUNAMI IN ANDAMAN AND NICOBAR

Tectonics, gas-hydrate destabilization and submarine landslides are possible sources for generation of tsunamis (Narayana, 2010). The description of tsunami is discussed in chapter 2 briefly. The great Sumatra tsunami of 2004 is a significant reminder of understanding seismic and tsunami hazards, the average slip of this earthquake was 12-15 m and the propagation was about 2.5 km/s over a distance of 1200 km, this earthquake produced vertical displacements approaching 5 m above the sundra trench southwest of Nicobar Islands creating a largest tsunami record in Indian Ocean. As per the data available in national U.S. Geophysical data centre of National oceanic and Administration (http://www.ngdc.noaa.gov) 16 tsunami events was recorded in regions of Indian ocean from past 1700-2016. The details are shown in table 6.1.

Year	Tsunami Earthquake magnitude	cause Volcano	Location	Max.water ht. height
1737	-	-	Calcutta	-
1819	7.7	-	Kutch	-
1845	6.3	-	Rann of Kutch	-

TABLE 6.1 showing tsunami events, location and cause from the year 1700 - 2016

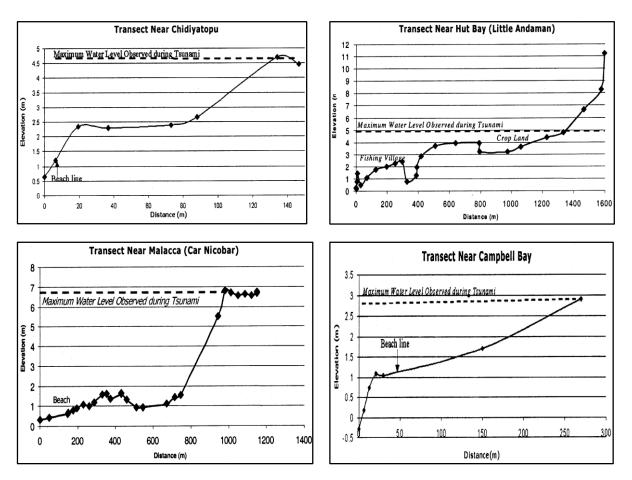
1847	-	-	Little Nicobar Island	
1868	-	-	Andaman Island	4
1876	-	-	Bay of Bengal	-
1881	7.9	-	Car Nicobar	1.22
1897	8.7	-	Assam	-
1905	7.8	-	Kangra, India	-
1941	7.6	-	Andaman sea, east coast of India	1.50
1950	8.6	-	India-China	0.50
1955	7.3	_	Little Nicobar Island	-
1978	-	-	India	-
2002	6.5	-	A&N, India	-
2009	7.5	-	A&N	0.01
2010	7.5	-	Little A&N	0.03

(Source: http://www.ngdc.noaa.gov)

The Andaman and Nicobar Islands (A&N) located in the subduction zone of Burma Plate are classified as seismic zone 5, indicating high level of risk due to earthquakes (Zhao, 2006). A tsunami was generated on 26 December 2004 by an earthquake of magnitude M 9.0 that occurred off Sumatra Island of Indonesia with the epicentre located on the shallow depths of seabed, and the Acoustic Tide Gauge (ATG) of the National Institute of Ocean Technology (NIOT), located inside the Port Blair bay (Chattam Island), which was set only for normal tidal variations, could record the sea water level up to 3.5 m on the day of tsunami. This is about 1.5 m more than normal tide level (Ilayaraja, 2009). Table 6.2 shows the run-up level at different sites of Andaman and Nicobar coast which were taken using Real-time Kinematic Global Positioning System and Fig.6.2 shows coastal land profile during the 2004 tsunami.

Location	Maximum run-up level (m)	Distance of sea water			
		inundation inland (m)			
Andaman and Nicobar Islands, South Andaman (Port Blair)					
JNRM college, 2.9 130					
Aberdeen					
Bamboo Flat	3.5	250			
New Wandoor	3.7	215			
Wandoor	3.9	215			
Chidiyatopu	4.5	130			
Sippyghat	2.0	2000			
(Creek)					
North Andaman					
Digilipur	1.5	100			
Rangat	1.5	200			
Little Andaman	<u> </u>	<u> </u>			
Hut Bay	5.0	1200			
Car Nicobar					
Malacca	7.0	1000			
Great Nicobar					
Campbell bay	3.0	300			
(Central)					
Campbell bay	6.0	50			
(North)					

TABLE 6.2: The Run-up level of sea water during tsunami in A&N (Murthy et al, 2006).



(Source: current science, June 2005)

Figure 6.2: shows Coastal land profile at Chidiyatopu (South Andaman), Hut Bay (Little Andaman), Malacca (Car Nicobar) and Campbell Bay (Great Nicobar).



(Source: Current science, may 2005)

Figure 6.3: Inundation of land and waterlogging up to 1.0 m in low-lying areas around Sippyghat near Port Blair.

Further, from the aerial as well as field surveys along the North, Middle and South Andaman Islands exhibits land subsidence and Inundation of land due to rise in water level and water-logging up to 1.0 m were common in the low-lying areas of Port Blair area., the (source: current science., may 2005). Fig 6.3 shows Inundation of land and waterlogging up to 1.0 m in low-lying areas near Port Blair.

6.3 STUDY OF TIDAL DATA AT PORT BLAIR

Frequency study of the water level during monsoon at Port Blair using Gumbel's probability method for different return period, of 5 yrs., 10 yrs., 25 yrs., 50 yrs., and 100 yrs. has been made as shown in Annexure-6A

It is apparent from the study that maximum predicted water level of 2.52 m is of the frequency of 100 yrs. return period and the A.H.W.L of 2.48 m. during the month of July to October is of the frequency of 5-yrs return period.

However, to provide a balance between the economy and safety up to a dependable degree of confidence commensurate with requirement under different situation, it is proposed to fix up the high water level at 2.52 m. having a frequency of 100-yrs return period for the design of undersluice at different places of Andaman and Nicobar Islands under Water Shed Development Projects.

6.3.1 Analysis of Daily High and Low Tide Table for Period from 2005 to 2015

The daily tide water levels at Port Blair (Andaman Islands) for the year 2005 to 2015 have been downloaded from **website tides.mobilegeographics.com**. Data corresponding to new moon day & full moon day are shown in Annexure 6B. Average of the H.W.L is 2.4m (i.e. in the month of August & October), Similarly, average of L.W.L is 0.1m (in the month of March).

In the Annexure 6B, figure 6B-1 shows graphical depiction of New Moon Tidal events in each month from the year 2005 to 2015 and figure 6B-2 shows graphical depiction of Full Moon Tidal events in each month from the year 2005 to 2015.

Entire daily data were analyzed to find highest and lowest tidal level in each month of the years 2005 to 2015 as shown in table 6.3. The highest and lowest tidal level in each month of the years 2005 to 2015 are graphically depicted in figure 6.4

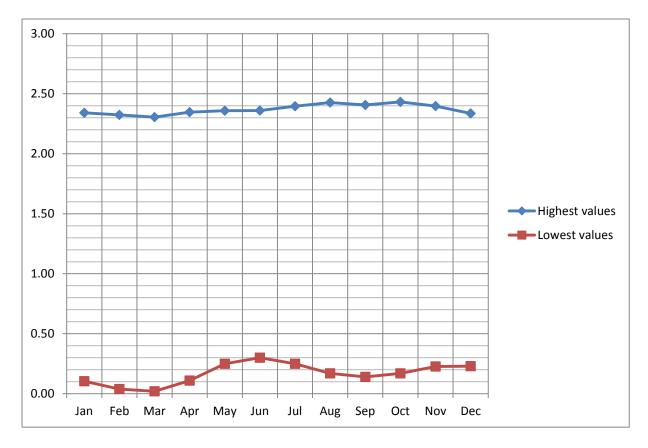


Figure 6.4: Highest and lowest tidal level in each month of the years 2005 to 2015

TABLE 6.	3: 2005	5-2015 N	IONTH	LY HIG	HEST A	ND LOV	VEST T	IDAL V	ALUE															
Months	Ja	nuary tic	le level ((m)	Fel	bruary ti	de level	(m)	Μ	larch tid	le level (m)	A	April tide	e level (n	n)	I	May tide	level (m)	J	une tide	level (m)
Years	Date	High	Date	Low	Date	High	Date	Low	Date	High	Date	Low	Date	High	Date	Low	Date	High	Date	Low	Date	High	Date	Low
2005	11	2.36	12	0.14	9	2.34	11	0.06	10	2.28	12	0.05	26	2.3	9	0.14	25	2.35	8	0.3	23	2.38	23	0.31
2006	31	2.36	31	0.06	28	2.35	1	0.05	1	2.34	2	-0.02	29	2.34	1	0.12	27	2.28	14	0.34	13	2.28	13	0.39
2007	20	2.29	22	0.13	18	2.33	20	0.01	21	2.34	20	-0.01	18	2.4	18	0.07	17	2.38	17	0.23	16	2.32	16	0.37
2008	23	2.26	24	0.18	8	2.23	10	0.11	10	2.26	9	0.04	8	2.36	7	0.07	6	2.4	6	0.17	5	2.39	4	0.28
2009	12	2.36	13	0.1	10	2.32	11	0.05	29	2.25	12	0.09	26	2.33	26	0.19	26	2.37	25	0.27	24	2.41	24	0.26
2010	31	2.39	31	0.05	1	2.34	1	0.01	1	2.33	2	-0.01	1	2.3	1	0.11	15	2.27	15	0.32	14	2.34	14	0.3
2011	21	2.35	22	0.06	19	2.35	20	-0.02	21	2.35	21	-0.01	19	2.39	19	0.1	18	2.36	18	0.25	17	2.3	16	0.36
2012	11	2.24	12	0.19	9	2.28	10	0.06	10	2.29	10	0.01	8	2.39	8	0.05	7	2.43	7	0.15	5	2.41	5	0.24
2013	12	2.36	13	0.11	10	2.28	12	0.09	29	2.29	29	0.09	27	2.38	27	0.14	26	2.43	26	0.19	24	2.44	25	0.21
2014	2	2.41	3	0.08	1	2.37	2	0.02	1	2.31	2	0.03	1	2.27	1	0.11	16	2.34	16	0.24	14	2.4	15	0.23
2015	21	2.38	23	0.05	19	2.37	21	-0.02	22	2.32	21	0.01	20	2.36	19	0.1	19	2.34	18	0.25	4	2.29	4	0.32
Avg.		2.34		0.10		2.32		0.04		2.31		0.02		2.35		0.11		2.36		0.25		2.36		0.30
Months	J	luly tide	level (m)	A	ugust tid	e level (1	m)	Sept	ember t	ide level	(m)	Oc	tober tid	le level (m)	Nov	ember ti	de level	(m)	Dec	ember ti	de level	(m)
Years	Date	High	Date	Low	Date	High	Date	Low	Date	High	Date	Low	Date	High	Date	Low	Date	High	Date	Low	Date	High	Date	Low
2005	23	2.44	23	0.23	21	2.46	21	0.16	18	2.38	19	0.14	18	2.38	17	0.19	3	2.33	3	0.28	2	2.31	2	0.31
2006	13	2.37	13	0.29	11	2.45	11	0.17	9	2.44	9	0.1	8	2.47	7	0.11	6	2.43	5	0.18	5	2.31	6	0.31
2007	31	2.32	31	0.3	30	2.4	30	0.15	20	2.46	28	0.11	27	2.49	26	0.14	25	2.42	25	0.23	25	2.31	25	0.25
2008	4	2.39	4	0.3	2	2.37	19	0.26	17	2.36	17	0.19	16	2.44	15	0.18	4	2.43	14	0.22	13	2.38	15	0.21
2009	23	2.45	24	0.2	21	2.43	21	0.17	20	2.36	19	0.18	19	2.34	18	0.26	4	2.36	3	0.28	3	2.35	4	0.26
2010	14	2.42	14	0.21	11	2.47	12	0.14	9	2.42	9	0.11	8	2.45	8	0.15	6	2.39	6	0.24	22	2.28	24	0.23
2011	4	2.31	31	0.28	30	2.42	30	0.13	29	2.47	20	0.11	21	2.48	27	0.15	25	2.4	27	0.22	25	2.31	26	0.23
2012	5	2.38	5	0.28	3	2.35	19	0.23	18	2.39	17	0.17	16	2.46	16	0.15	14	2.46	15	0.17	14	2.41	15	0.15
2013	24	2.45	24	0.2	22	2.4	22	0.2	20	2.31	20	0.23	6	2.36	6	0.23	4	2.41	4	0.21	4	2.41	5	0.17
2014	14	2.46	14	0.18	12	2.48	12	0.14	10	2.42	10	0.13	9	2.41	9	0.17	7	2.35	7	0.25	23	2.35	24	0.16
2015	4	2.37	4	0.27	31	2.46	31	0.12	29	2.46	29	0.1	28	2.47	28	0.14	26	2.39	27	0.21	25	2.28	27	0.24
Avg.		2.40		0.25		2.43		0.17		2.41		0.14		2.43		0.17		2.40		0.23		2.34		0.23

6.4 STORM RAINFALL & RUNOFF

Design storm and flood scenarios are required for (i) planning of storm water drainage in the plant area and the area in vicinity and (ii) for protecting the plant area from external flooding. This covers estimation of storm rainfall of various return periods for draining of storm water from the solar plant area to avoid flooding.

6.4.1 Frequency Analysis of Annual maximum 1-day rainfall at Port Blair

26years (1989 to 2014) data series of annual maximum 1-day rainfall at Port Blair has been analyzed as shown in Table 6.4 and Figure 6.5. Data from the period 1989 to 1999 has been taken from unpublished report. Daily rainfall data for the period from 2000 to 2014 has been procured from IMD. The 1-day rainfall and 1-hr rainfall of various return periods are given in Table 6.5 below.

Year	Max. 1day rainfall	rank m	series in descendi ng order	Plotting position m/n+1 = m/27	Return period 27/m
1989	129.88	1	237.6	0.0370	27.00
1990	84.3	2	212.9	0.0741	13.50
1991	145.6	3	206.8	0.1111	9.00
1992	126.7	4	204.9	0.1481	6.75
1993	128.4	5	197.3	0.1852	5.40
1994	195.6	6	195.6	0.2222	4.50
1995	237.6	7	192.2	0.2593	3.86
1996	119	8	179.1	0.2963	3.38
1997	192.2	9	163.5	0.3333	3.00
1998	107.9	10	156.5	0.3704	2.70
1999	66	11	145.6	0.4074	2.45
2000	112.5	12	138.3	0.4444	2.25
2001	138.3	13	129.88	0.4815	2.08
2002	124.4	14	128.4	0.5185	1.93
2003	107.8	15	126.7	0.5556	1.80
2004	108.2	16	125.2	0.5926	1.69

TABLE 6.4: Frequency Analysis of Annual Maximum 1-Day Rainfall at Port Blair

2005	197.3	17	124.4	0.6296	1.59
2006	156.5	18	119	0.6667	1.50
2007	114.7	19	114.7	0.7037	1.42
2008	206.8	20	112.5	0.7407	1.35
2009	125.2	21	108.2	0.7778	1.29
2010	95.3	22	107.9	0.8148	1.23
2011	163.5	23	107.8	0.8519	1.17
2012	179.1	24	95.3	0.8889	1.13
2013	212.9	25	84.3	0.9259	1.08
2014	204.9	26	66	0.9630	1.04

TABLE 6.5: ONE-Day Rainfall and 1-hr Rainfall of Various Return Periods

Return Period (year)	20	25	50	75	100	1000
1-day rainfall (mm)	218	228	247	260	268	335
1-hr rainfall (mm)	113.5	118.7	128.6	135.4	139.6	174.5

The largest 1-day storm rainfall value is 335 corresponding to a return period of 1000 years, storm water drains are not designed for unusual occurrences of rare storms on account of high cost of large size drains/pipes as well as non-utilization of their full capacity for most of the years, besides having risk of siltation and clogging of drains/pipes due to non-generation of self-cleansing velocity in partly flowing condition.

It is suggested that 247 mm rainfall of 1-day duration corresponding to 50 year return period as obtained from frequency analysis of 26 years' annual maximum 1-Day rainfall data series may be adopted for design purposes.

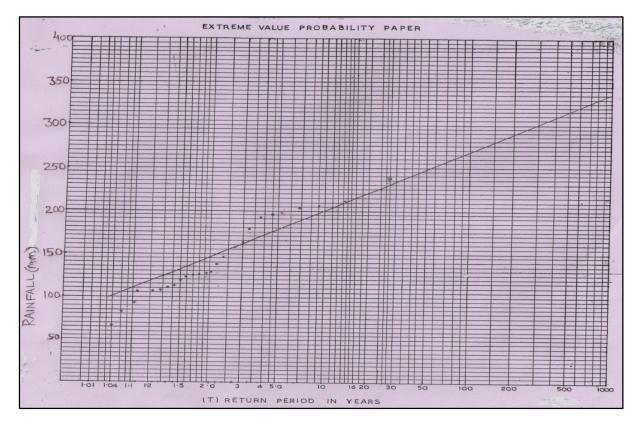


Figure 6.5: Frequency analysis of 1-day annual maximum rainfall at Port Blair.

In the present study, the main aim is to understand the flooding situation in the Port Blair referring to previous literature. In Port Blair it is evident that the major destruction was caused due to the great Sumatra tsunami and earthquake (Mw 9.2) of December 2004 inundating the coast land which includes agriculture land, townships and properties, low-lying coastal zone is more prone to coastal hazards, hence, any projects taken up in low-lying area, one should have proper knowledge regarding coastal hazard behavioral characteristics and possible remedial measures that can be adopted to control the intensity of coastal flooding. An attempt is made in this present study considering a case study in Port Blair to protect the plant area from this flooding and last the project for long-term, and suggest the structural/non-structural measures to divert the excess flooded water safely out of the plant area. The plant characteristics locations have been described in chapter-3 briefly. Fig 6.6 shows the components parts of plant distributed area wise.

The total plant area is about 126.21 ha as mentioned in the Fig.6.6, the solar plant area is about 40.65 ha, and remaining area is about 85.56 ha, the watershed boundary divides the plant area into two parts and the area of divided at watershed location of Mithakhari nala is about 31.57 ha as shown in fig.6.6 and remaining portion is about 94.64 ha. The volume of

run-off that can be generated considering 1-day storm runoff. Depth of rainfall is 247 mm corresponding to 50 year return period. It is assumed that all rainfall shall be converted into runoff due to ground level being very near to mean sea level and very shallow water table.

The storm runoff is computed for the worst possible condition as below: Runoff volume from catchment area of Mithakharinala (considering no loss)

= 247 mm x
$$10^{-3}$$
 m rain x 31.57 ha
= 77977.9 m³

Runoff volume from the remaining catchment area (considering no loss)

$$= 247 \times 10^{-3}$$
 m rain x (126.21 - 31.57 - 40.65) ha

$$= 133354.8 \text{ m}^3$$

Runoff volume from the Solar Plant area (considering no loss)

$$= 247 \times 10^{-3}$$
 m rain x 40.65 ha Solar Plant area x 10^4 m²

$$= 100406 \text{ m}^3$$

Total runoff volume = $77977.9 + 133354.8 + 100406 = 311738.7 \text{ m}^3$

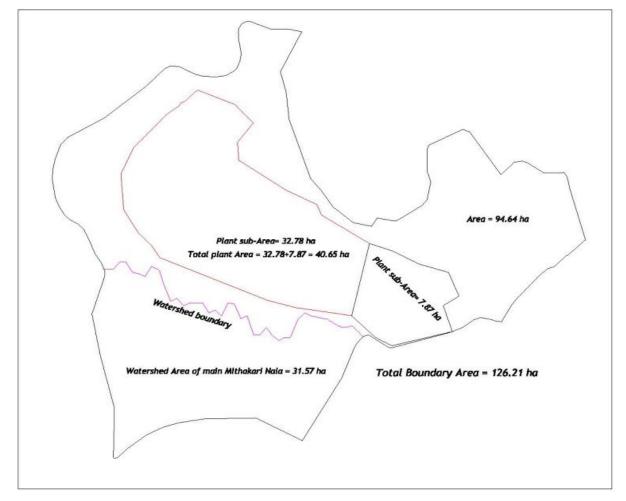


Figure 6.6: Mithakhari solar power plant area details

The solar plant area is entirely flat (referring. Mithakharinala which joins the sea through an undersluice and entire plant area storm water is drained through the undersluice which is already existing in the plant. The details of existing structure taken from unpublished report are as follows.

Crest level of undersluice = (+) 0.30 m

Slope of channel = 0.1 / 1000, Length of channel = 2.1 km (approx.)

Drop in water level = $(0.1 / 1000) \times 2.1 \times 1000 \text{ m} = 0.21 \text{ m}$

Water level at off-take of canal = (+) 0.30 + 0.21 = (+) 0.51 m

From the topographic survey data area of spread at (+) 0.51 m = 28.59 ha

Thus, the area of 28.59 ha (up to R.L (+) 0.51m) remains under perpetual flooding and it cannot be drained through the existing undersluice, maximum of this area lies at solar plant and also causing waterlogging. The undersluice is operated manually such that the entry of sea water to the proposed plant area is restricted. Its gates are closed when there is a high tide so that the sea water does not enter the plant area and these gates are opened during low tide. Referring to previous literature it is seen, Inundation of land and waterlogging up to 1.0 m in low-lying areas to Sumatra tsunami of 2004 (figure 6.3). Therefore, it can be recommended that the solar plant area may be kept the level of 1.0 m, provided with proper sluice gate in order to divert the excess flood water.

6.5 CONCLUSION.

In planning for the flood protection scheme for the solar plant site, the following options can be visualized. These options are not mutually exclusive and an appropriate combination can be considered:

- Raising the level of land at solar plant site by earth filling. Earth filling up to (+) 0.5 m necessary to avoid perpetual waterlogging. Earth filling above (+) 0.5m level would help in reducing depth and duration of temporary flooding in the plant area.
- > Peripheral embankment around the plant site coupled with pumping.
- Diversion of Mithakharinala to sea on right side. The diversion can be done at a location just below road culvert or at a location further downstream which will require sluice for control of flooding due to high tide inflow.
- Draining of Mithakhari watershed runoff through the existing undersluice and that of the remaining area (including solar plant) runoff through a separate storm water channel and undersluice to sea.

CHAPTER-7

SUMMARY AND CONCLUSION

The main objective of this dissertation work is to illustrate use of modern analytical tools in planning and design of i) internal drainage and ii) measures for controlling external flooding of industrial area located in coastal region.

To take up any industrial project in the coastal region the problem of flooding has put a question mark on sustainability of prestigious project. Depending upon the terrain/topography and type of project taken up requires proper understanding and knowledge about the area and its vulnerability towards flooding in in order to make the project sustainable. For this study, depending upon the terrain/topography two case studies were considered.

i. The first case study pertains to planning and design of internal drainage of a thermal power plant proposed near village Pudimadaka, Vishakhapatnam, Andra Pradesh(study area-I).

50 year return period total water levels(TWLs) along the coast of Vishakhapatnam district range from 4.5 m to 4.8m. The total water level is projected on to the adjacent coastal area and plant site by using topography to demarcate the horizontal extent of inundation. This conservative approach may slightly overestimate the extension of 105 inundations, but it is desirable for hazard mitigation as well as coastal zone management and is widely used around the world (Jain et al. 2010).

SRTM data based DEM study of the study area has been carried out, and topographic contours generated., elevations ranges were from 0 m to 173 m. Contours of 5m,10m, 15m, 20m and above elevations on north and west side of the plant indicates that the area is safe considering cyclone surges (4.5m to 4.8m) of 50 year return period. Contours ranging from 1m to 5 m on south side of plant up to sea coast. It is seen that area adjacent to southern boundary and eastern boundary of the plant have elevations lower than 4m (1m to 4m). The cyclone surges may travel up along Pudimadaka creek and inundate the low-lying areas. These low lying areas are susceptible to flooding and inundation for several days when flood water in streams is unable to discharge to sea due to high tides and cyclone surges.

The finished grade levels (FGL) of various parts in the plant are in the range of 6.0m on east side to 14.0 m in coal yard area. Thus, there is no danger of cyclonic flooding in the plant area. The green belt on east side will have FGL of 6.0 m and hence safe against flooding but it is not so in the green belt on south side. Greenbelt in south east part has natural ground level between 2m to 4m. The ground level outside southern boundary is in the range of 1.5m

to 2.5m. Therefore, this part is prone to flooding when sea water level is high and there is heavy rainfall in vicinity of the plant area.

Rambilli nala flows along southern boundary of the plant in east west direction. that flooding occurs mainly because flood water cannot flow towards sea due to high water level in sea. Land remains submerged for several days. Thus, a protection wall can be built along south side boundary to avoid submergence of the green belt.

Based on the 25 year return period flood generated using SWMM model. Various channels/conduits were designed. The maximum velocity attained in each channel is generally below or near to 2 m/s. In this study, trial values of channel dimensions were employed such that no channel/node exhibits surcharge or flooding or overflow, the analysis showed infiltration loss 11.437 ha-m and surface runoff is 38.87 ha-m. Evaporation loss during the flood event is assumed to be negligible.51.6 ha-m is accounted as total precipitation, as per the SWMM results it is found that layout of drainage channels is hydraulically satisfactory.

ii. The second case study pertains to planning and design of measures for controlling external flooding in Mithakhari solar plant, at Port Blair, Andaman and Nicobar.

A number of alternatives/options were explored for safe disposal of storm runoff to sea starting from the simplest of water-proofing of the area to the isolation of the plant area with diversion of Mithakhari nala, a separate arrangement for storm runoff channels and undersluice, increase in the frame-work of solar panels, and so on. These were evaluated in terms of availability of earth-work; involvement of cost in construction of the associated structures, O&M, and R&R issues. Finally, a flood control scheme without diversion Mithakhari nala as given below is recommended:

- > Raise the ground level of Solar Plant area by 0.70 m requiring 74700 m³ of earth fill.
- Raise the solar panels by 0.44 m (=1.14 0.70) = 0.45 m (say) from the raised ground level of the Solar Plant area to avoid flooding due to 1 in 50-year flood. Normally, a clearance of 0.5 m above ground level is provided for the tilted panel. Here, to avoid flooding, additional 20 cm clearance for free board is desirable. Thus, height of solar panel = 0.65 m.
- The existing approach road dividing the Solar Plant area into two parts may be strengthened and retained for inspection purpose.
- The above scheme is economical and robust, it requires earth filling and peripheral drains without involvement of any additional flood control structure and without affecting the design of solar panels/frame-work, and thus, may be preferred.

ANNEXURE – 6A

FREQUENCY ANALYSIS OF ANNUAL MAX TIDAL LEVELS 2005 to 2015

Annual maximum tidal levels for the years 2005 to 2015 are shown in table. Graphical frequency analysis on Gumble probability paper has been carried out. Highest water level of different return period is as given below.

Wp (5) = 2.48

Wp (10) = 2.49

$$Wp(25) = 2.5$$

Wp (50) = 2.51

Wp (100) = 2.52.

				No. of			
				times the		Chance	
				maximum	Reoccurrence	percentage	
			Maximum	W.L. is	internal i.e.	or	
			Water	equaled	frequency	exceedance	
			level in	or	nequency	Probability	
			meter	exceeded	Y+1		
			arranged	i.e.	$a = \frac{Y+1}{b}$	100	
		Maximum	in	ranking		a	
S1.	Date of	Water	ascending	of W.L			
No	Reoccurrence	level in m	order(Wp)	(b)			Wp^2
1	2	3	4	5	6	7	8
1	21-08-2005	2.46	2.49	1	12	8.33	6.20
2	08-10-2006	2.47	2.48	2	6	16.67	6.15
3	27-10-2007	2.49	2.48	3	4	25.00	6.15
4	16-10-2008	2.44	2.47	4	3	33.33	6.10
5	23-07-2009	2.45	2.47	5	2.4	41.67	6.10
6	12-08-2010	2.47	2.47	6	2	50.00	6.10
7	27-10-2011	2.48	2.46	7	1.71	58.33	6.05
8	14-11-2012	2.46	2.46	8	1.5	66.67	6.05
9	24-07-2013	2.45	2.45	9	1.33	75.00	6.00
10	12-08-2014	2.48	2.45	10	1.2	83.33	6.00
11	28-10-2015	2.47	2.44	11	1.09	91.67	5.95
Y=11		27.12	27.12				66.87

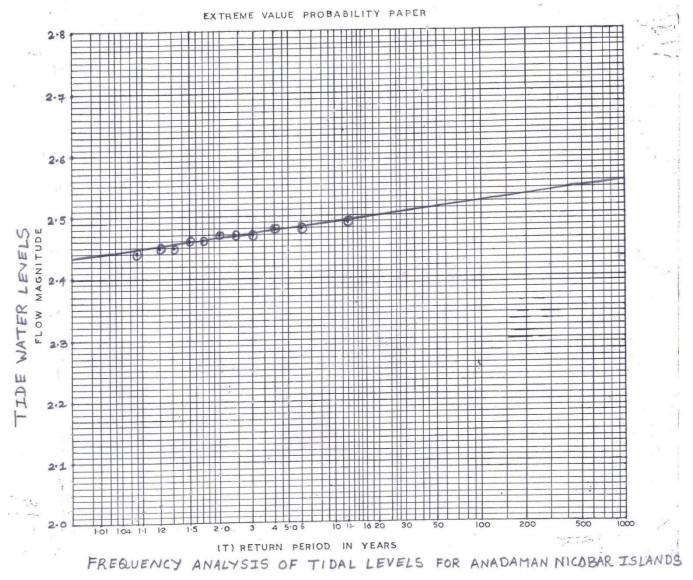


Figure .. Frequency analysis of annual maximum tidal levels (2005 to 2015).

<u>ANNEXURE – 6B</u>

ANALYSIS OF DAILY TIDE LEVEL FROM 2005 TO 2015

Two tides called "Semi-diurnal tides are found to differ from each other. Another interesting feature of tides lies in the fact that the tidal range at any location fluctuates steadily and gradually from day to day in accordance with the lunar phase. The tidal range at the full and new moon is found to be the maximum. This phase is called the "Spring Tide". After the occurrence of the Neap Tide at the middle of moon cycle when the tidal range is the minimum.

The tidal curve at the sea face of a tidal estuary in Bay of Bengal is found to have a symmetrical harmonic shape, the periods of both flow and Ebb tide being practically equal. As it goes upwards, the period of Ebb tide increases more than flow tides. Thus the flow velocities are more than the subsequent Ebb velocities along the tidal channel as proceeded upward. There is another interesting point in this connection viz. the tidal range starts increasing steadily and gradually upwards from the sea face, attains maximum value at the certain point and starts diminishing thereafter till at the terminal point of tidal propagation it becomes practically nil.

STUDY OF TIDAL DATA AT PORT BLAIR

The daily tide water levels at port Blair (Andaman Islands) for the year 2005 to 2015 have been downloaded from tides.mobilegeographics.com. Ongoing through readings it would be apparent that there are two consecutive values (i.e. new moon & full moon) in each month during which H.W.L (High water level) is high compared to other days of the same month.

Data corresponding to new moon day & full moon day are shown in table 6B-1. Average of the H.W.L is 2.4m (i.e. in the month of August & October), Similarly, average of L.W.L is 0.1m (in the month of March).

Figure 6B-1 shows graphical depiction of New Moon Tidal events in each month from the year 2005 to 2015. Figure 6B-2 shows graphical depiction of Full Moon Tidal events in each month from the year 2005 to 2015.

Voor	Month	Dov	Low						Low	-				•	Moon
Year		Day	1	434	0.20	High	434	1.0		DM	0.22	High	DM	0.01	
2005	January	Mon 10	2:55	AM	0.29	8:45	AM	1.8	2:45	PM	0.32	9:05	PM	2.31	New Moon
2006	January	Sun 29	3:02	AM	0.27	8:54	AM	1.82	2:55	PM	0.3	9:09	PM	2.29	New Moon
2007	January	Fri 19	3:20	AM	0.32	9:10	AM	1.77	3:10	PM	0.35	9:24	PM	2.23	New Moon
2008	January	Tue 8	3:09	AM	0.46	9:00	AM	1.65	2:53	PM	0.47	9:12	PM	2.09	New Moon
2009	January	Mon 26	3:22	AM	0.4	9:20	AM	1.71	3:11	PM	0.43	9:27	PM	2.08	New Moon
2010	January	Fri 15	3:18	AM	0.43	9:16	AM	1.68	3:02	PM	0.47	9:25	PM	2.08	New Moon
2011	January	Tue 4	3:06	AM	0.39	9:01	AM	1.74	2:51	PM	0.44	9:13	PM	2.16	New Moon
2012	January	Mon 23	3:11	AM	0.28	9:07	AM	1.85	3:04	PM	0.34	9:20	PM	2.22	New Moon
2013	January	Sat 12	3:20	AM	0.16	9:17	AM	1.97	3:18	PM	0.22	9:33	PM	2.36	New Moon
2014	January	Wed 1	2:47	AM	0.24	8:40	AM	1.94	2:44	PM	0.22	9:00	PM	2.37	New Moon
2014	January	Fri 31	3:19	AM	0.1	9:17	AM	2.05	3:22	PM	0.15	9:33	PM	2.38	New Moon
2015	January	Tue 20	2:52	AM	0.2	8:45	AM	1.9	2:51	PM	0.2	9:04	PM	2.3	New Moon
						-						_			
Year	Month	Day	Low	-		High	-	-	Low	_		High	_	1	Moon
2005	February	Wed 9	3:31	AM	0.14	9:28	AM	1.95	3:28	PM	0.23	9:41	PM	2.34	New Moon
2006	February	Tue 28	3:22	AM	0.06	9:23	AM	2.1	3:28	PM	0.14	9:35	PM	2.35	New Moon
2007	February	Sat 17	3:02	AM	0.23	8:59	AM	1.9	3:01	PM	0.27	9:10	PM	2.26	New Moon
2008	February	Thu 7	3:25	AM	0.28	9:21	AM	1.84	3:21	PM	0.33	9:29	PM	2.18	New Moon
2009	February	Wed 25	3:24	AM	0.25	9:25	AM	1.93	3:28	PM	0.3	9:31	PM	2.12	New Moon
2010	February	Sun 14	3:25	AM	0.32	9:29	AM	1.83	3:23	PM	0.37	9:34	PM	2.07	New Moon
2011	February	Thu 3	3:25	AM	0.33	9:26	AM	1.81	3:17	PM	0.39	9:33	PM	2.12	New Moon
2012	February	Wed 22	3:24	AM	0.23	9:28	AM	1.96	3:26	PM	0.3	9:36	PM	2.15	New Moon
2013	February	Sun 10	3:08	AM	0.17	9:07	AM	1.99	3:10	PM	0.23	9:21	PM	2.28	New Moon
2015	February	Thu19	3:16	AM	0.1	9:16	AM	2.1	3:24	PM	0.1	9:31	PM	2.4	New Moon
Year	Month	Day	Low			High			Low			High			Moon
2005	March	Thu 10	3:11	AM	0.12	9:12	AM	2.06	3:17	PM	0.2	9:24	PM	2.28	New Moon
2006	March	Wed 29	2:54	AM	0.07	9:00	AM	2.22	3:11	PM	0.14	9:13	PM	2.26	New Moon
2007	March	Mon 19	3:08	AM	0.05	9:13	AM	2.21	3:23	PM	0.11	9:25	PM	2.29	New Moon
2008	March	Fri 7	2:57	AM	0.22	8:57	AM	1.99	3:04	PM	0.26	9:07	PM	2.18	New Moon
2009	March	Thu 26	2:49	AM	0.24	8:55	AM	2.06	3:05	PM	0.28	9:03	PM	2.07	New Moon
2010	March	Tue 16	3:18	AM	0.25	9:25	AM	2.02	3:31	PM	0.29	9:32	PM	2.04	New Moon
2011	March	Sat 5	3:23	AM	0.27	9:31	AM	1.96	3:29	PM	0.32	9:37	PM	2.06	New Moon
2012	March	Thu 22	2:53	AM	0.29	9:04	AM	2.01	3:06	PM	0.33	9:13	PM	2.03	New Moon
2013	March	Tue 12	3:18	AM	0.16	9:25	AM	2.11	3:30	PM	0.22	9:37	PM	2.17	New Moon
2014	March	Sat 1	3:01	AM	0.1	9:03	AM	2.11	3:11	PM	0.15	9:18	PM	2.31	New Moon
2014	March	Mon 31	3:12	AM	0.11	9:21	AM	2.24	3:32	PM	0.16	9:36	PM	2.18	New Moon
2015	March	Fri 20	2:53	AM	0.10	8:58	AM	2.2	3:09	PM	0.10	9:14	PM	2.3	New Moon
v												TT' 1			
Year	Month	Day	Low		0.1	High			Low	D) (0.0	High		0.1	Moon
2005	April	Sat 9	3:10			9:21			3:31	PM	0.2	9:33	PM	2.1	New Moon
2006	April	Fri 28	2:55	AM		9:11	AM		3:29	PM	0.2	9:26	PM	2.1	New Moon
2007	April	Tue 17	2:35	AM		8:46			3:03	PM	0.1	9:01	PM	2.2	New Moon
2008	April	Sun 6	2:53			9:02			3:18	PM	0.2	9:15	PM	2.2	New Moon
2009	April	Sat 25	2:43	AM		8:55			3:17	PM	0.2	9:10	PM	2.0	New Moon
2010	April	Wed 14	2:42	AM	0.3	8:53	AM	2.1	3:08	PM	0.3	9:03	PM	2.0	New Moon

Table 6B-1 Low and High Tide Levels on full moon day and new moon day

2011	April	Sun 3	2:4	8 AN	1 0.3	9:0)2 A	M	2.0	3:07	7 PN	1 0.4	9:10) PM	1 2.0	New Moon
2012	April	Sat 21	2:4						2.1	3:13			9:13			New Moon
2013	April	Wed 10) 2:4	8 AN	1 0.3	3 9:0)1 A	M	2.1	3:10			9:13	3 PM	1 2.0	New Moon
2014	April	Tue 29	2:4		1 0.3	8 8:5	58 A	M	2.2	3:14	4 PM	1 0.3	9:14	4 PM	1 2.0	New Moon
2015	April	Sun 19	3:0	4 AN	1 0.1	0 9:1	6 A	M	2.3	3:33	3 PN	1 0.1	0 9:24	4 PM	1 2.2	New Moon
Year	Month	Day	Low	•		High				Low			High		-	Moon
2005	May	Sun 8	2:36	AM	0.3	8:54	AM	2.2	22	3:10	PM	0.34		PM	1.94	New Moon
2006	May	Sat 27	2:26	AM	0.36	8:49	AM			3:14	PM		9:08	PM	1.87	New Moon
2007	May	Thu 17	2:43	AM	0.23	9:03	AM			3:28	PM			PM	1.98	New Moon
2008	May	Mon 5	2:20	AM	0.2	8:36	AM			2:59	PM	0.22	8:53	PM	2.05	New Moon
2009	May	Sun 24	2:14	AM	0.33	8:32	AM	2.3	3	3:01	PM	0.32	8:52	PM	1.93	New Moon
2010	May	Fri 14	2:40	AM	0.35	8:56	AM	2.2	22	3:22	PM	0.35	9:11	PM	1.89	New Moon
2011	May	Tue 3	2:40	AM	0.37	8:57	AM	2.1	12	3:15	PM	0.39	9:08	PM	1.85	New Moon
2012	May	Mon 21	2:43	AM	0.45	9:05	AM	2.1	3	3:25	PM	0.44	9:19	PM	1.8	New Moon
2013	May	Fri 10	2:45	AM	0.38	9:06	AM	2.1	6	3:21	PM	0.39	9:21	PM	1.87	New Moon
2014	May	Thu 29	2:50	AM	0.41	9:12	AM	2.2	22	3:32	PM	0.39	9:31	PM	1.87	New Moon
2015	May	Mon 18	2:39	AM	0.3	8:56	AM	2.3	3	3:17	PM	0.3	9:15	PM	2.0	New Moon
Year	Month	Day	Low			High				Low			High			Moon
2005	June	Tue 7	2:37	AM	0.49	9:05	AM	2.17	r	3:28	PM	0.48	9:22	PM	1.75	New Moon
2006	June	Sun 25	2:07	AM	0.56	8:37	AM	2.18	;	3:08	PM	0.51	9:00	PM	1.74	New Moon
2007	June	Fri 15	2:24	AM	0.42	8:50	AM	2.31		3:22	PM	0.38	9:15	PM	1.85	New Moon
2008	June	Wed 4	2:39	AM	0.32	9:01	AM	2.39)	3:33	PM	0.28	9:26	PM	1.93	New Moon
2009	June	Tue 23	2:44	AM	0.39	9:04	AM	2.38	;	3:39	PM	0.30	9:32	PM	1.94	New Moon
2010	June	Sat 12	2:18	AM	0.44	8:38	AM	2.24		3:10	PM	0.40	8:59	PM	1.86	New Moon
2011	June	Thu 2	2:46	AM	0.45	9:04	AM	2.18	;	3:33	PM	0.43	9:21	PM	1.82	New Moon
2012	June	Tue 19	2:23	AM	0.55	8:47	AM	2.11		3:12	PM	0.51	9:04	PM	1.76	New Moon
2013	June	Sat 8	2:19	AM	0.52	8:46	AM	2.12	2	3:06	PM	0.50	9:03	PM	1.77	New Moon
2014	June	Fri 27	2:31	AM	0.54	8:57	AM	2.16	i	3:19	PM	0.49	9:17	PM	1.81	New Moon
2015	June	Tue 16	2:18	AM	0.4	8:40	AM	2.3		3:06	PM	0.4	9:02	PM	1.9	New Moon
Year	Month	Day	Low			High				Low			High			Moon
2005	July	Wed 6	2:22	AM	0.64	8:54	AM	2.11		3:21	PM	0.58	9:16	PM	1.69	New Moon
2006	July	Tue 25	2:44	AM	0.64	9:09	AM	2.16	5	3:37	PM	0.52	9:34	PM	1.79	New Moon
2007	July	Sat 14	2:20	AM	0.57	8:44	AM	2.24	ŀ	3:20	PM	0.46	9:13	PM	1.82	New Moon
2008	July	Thu 3	2:31	AM	0.45	8:54	AM	2.35	5	3:30	PM	0.34	9:23	PM	1.91	New Moon
2009	July	Wed 22	2:39	AM	0.42	8:56	AM	2.39)	3:30	PM	0.27	9:25	PM	2.03	New Moon
2010	July	Mon 12	2:53	AM	0.42	9:08	AM	2.37	,	3:42	PM	0.29	9:35	PM	2.01	New Moon
2011	July	Fri 1	2:31	AM	0.52	8:49	AM	2.2		3:21	PM	0.44	9:10	PM	1.85	New Moon
2011	July	Sun 31	3:01	AM	0.42	9:11	AM	2.34		3:40	PM	0.28	9:36	PM	2.09	New Moon
2012	July	Thu 19	2:47	AM	0.54	9:02	AM	2.18	3	3:29	PM	0.44	9:23	PM	1.9	New Moon
2013	July	Mon 8	2:38	AM	0.57	9:02	AM	2.13	3	3:24	PM	0.5	9:21	PM	1.81	New Moon
2014	July	Sun 27	2:53	AM	0.55	9:14	AM	2.16	5	3:33	PM	0.47	9:34	PM	1.89	New Moon
2015	July	Thu 16	2:44	AM	0.5	9:06	AM	2.2		3:29	PM	0.4	9:29	PM	1.9	New Moon
Vaar	Mart	Dari	τ			TT:	h			Т -			11:	h		Moon
Year 2005	Month	Day Fri 5	Lov 2:54		0.63	Hig 2 0.16	1	1 2	.14	Lov 3:39		1 0.5	Hig 1 9:38	-	I 1.82	Moon
2003	August	rn 3	2:54	+ AW	0.03	3 9:16		1 2	.14	5:55		1 0.5	9:30	B PM	1.84	2 New Moon

2005		T I 0.1	2.00	43.6	0.55	0.04		0.10		10	D1 (0.4		0.44	DIA	1.00	
2006	August	Thu 24	3:08	AM	0.55	9:24	AM	2.18	_	3:40	PM	0.4			PM	1.98	New Moon
2007	August	Mon 13	2:59	AM	0.54	9:15	AM	2.25	_	3:39	PM	0.4			PM	1.97	New Moon
2008	August	Fri 1	2:31	AM	0.51	8:48	AM	2.32	_	3:21	PM	0.3			PM	1.98	New Moon
2008	August	Sun 31	3:03	AM	0.41	9:11	AM	2.32	_	3:30	PM	0.2			PM	2.17	New Moon
2009	August	Thu 20	2:33	AM	0.41	8:44	AM	2.37	_	3:11	PM	0.2			PM	2.16	New Moon
2010	August	Tue 10	2:44	AM	0.38	8:55	AM	2.4	-	3:23	PM	0.2			PM	2.16	New Moon
2011	August	Mon 29	2:46	AM	0.35	8:51	AM	2.36	-	3:14	PM	0.2			PM	2.26	New Moon
2012	August	Fri 17	2:31	AM	0.51	8:41	AM	2.2	_	3:04	PM	0.3			PM	2.04	New Moon
2013	August	Wed 7	3:00	AM	0.52	9:12	AM	2.18	_	3:33	PM	0.4			PM	1.97	New Moon
2014	August	Mon 25	2:39	AM	0.55	8:54	AM	2.13	_	3:08	PM	0.4			PM	1.98	New Moon
2015	August	Fri 14	2:34	AM	0.6	8:52	AM	2.2	3	3:10	PM	0.5	5	9:13	PM	1.9	New Moon
Year	Month	Day	Low			High	1		Ι	Low				High			Moon
2005	September	-	3:11	AM	0.5	-	AM	2.17	7 3	3:36	PM	0.3		9:39	PM	2.05	New Moon
2006	September	Fri 22	2:48	AM	0.5	8:57	AM	2.11	1 3	3:05	PM	0.3	39	9:15	PM	2.09	New Moon
2007	September		2:45	AM			AM	2.18	3 3	3:09	PM	0.3	38	9:15	PM	2.07	New Moon
2008	September	Mon 29	2:44	AM	0.4	8:48	AM	2.18	3 2	2:57	PM	0.3	3	9:08	PM	2.23	New Moon
2009	September	Sat 19	2:59	AM	0.3	9:03	AM	2.33	3 3	3:17	PM	0.1	18	9:26	PM	2.34	New Moon
2010	September	Wed 8	2:30	AM	0.3	8 8:36	AM	2.37	7 2	2:58	PM	0.1	17	9:02	PM	2.31	New Moon
2011	September	Tue 27	2:27	AM	0.3	8 8:28	AM	2.3	2	2:45	PM	0.1	16	8:53	PM	2.39	New Moon
2012	September	Sun 16	2:48	AM	0.3	8 8:48	AM	2.27	7 3	3:06	PM	0.2	22	9:11	PM	2.31	New Moon
2013	September	Thu 5	2:41	AM	0.5	5 8:47	AM	2.16	5 3	3:04	PM	0.3	37	9:06	PM	2.1	New Moon
2014	September	Wed 24	2:50	AM	0.5	5 8:54	AM	2.1	~	3:03	PM	0.3	36	9:11	PM	2.15	New Moon
2015	September	Sun 13	2:49	AM	0.5	5 9:00	AM	2.1	~ .	3:09	PM	0.4	4	9:18	PM	2.1	New Moon
Year	Month	Day	Low			High			Lo				Hig	rh		м	loon
2005	October	Mon 3	2:49	AM	0.5	8:50	AM	2.1	3:0		РМ	0.3	9:0	- -	1 2.2		ew Moon
2005	October	Sun 22	2:51	AM	0.3	8:49	AM	2.0	2:5		PM	0.3	9:0		_		ew Moon
2000	October	Thu 11	2:50	AM	0.4	8:53	AM	2.0	2:5		PM	0.4	9:1				ew Moon
		Wed															
2008	October	29	2:53	AM	0.4	8:52	AM	2.0	2:4		PM	0.4	9:0				ew Moon
2009	October	Sun 18	2:41	AM	0.3	8:40	AM	2.1	2:4		PM	0.3	9:0				ew Moon
2010	October	Fri 8	2:54	AM	0.2	8:54	AM	2.3	3:0		PM	0.2	9:1				ew Moon
2011	October	Thu 27 Mon	2:51	AM	0.2	8:48	AM	2.2	2:5	55	PM	0.2	9:1	0 PN	1 2.5		ew Moon
2012	October	Mon 15	2:27	AM	0.3	8:24	AM	2.2	2:3	36]	PM	0.2	8:4	7 PN	1 2.4	4 N	ew Moon
2013	October	Sat 5	2:52	AM	0.4	8:49	AM	2.2	3:0	02	PM	0.3	9:0	9 PN	1 2.3	3 N	ew Moon
2014	October	Fri 24	2:58	AM	0.4	8:53	AM	2.0	3:0	01	PM	0.3	9:1	1 PN	1 2.3	3 N	ew Moon
2015	October	Tue 13	2:57	AM	0.4	9:00	AM	2.00	3:0	04	PM	0.4	9:1	6 PN	1 2.2	2 N	ew Moon
Year	Month	Day	Low			Hig	h			Low				High			Moon
2005	November	Wed 2	2:54	AM	0.3	8:4	5 AN	1 2.0)1	2:52	PN	1 0	.28	9:05	PM	2.3	New Moon
2006	November	Tue 21	3:00	AM	0.4	3 8:4	9 AN	1 1.8	3	2:50	PN	1 0	.38	9:07	PM	2.21	New Moon
2007	November	Sat 10	2:56	AM	0.4	5 8:5	1 AN	1 1.8	6	2:47	PN	1 0.	.4	9:07	PM	2.18	New Moon
2008	November	Thu 27	2:37	AM	0.5	8:3	2 AN	1 1.7	'4	2:21	PN	1 0.	.46	8:48	PM	2.13	New Moon
2009	November	Tue 17	2:59	AM	0.3	9 8:5	5 AN	1 1.8	88	2:48	PN	1 0.	.38	9:12	PM	2.25	New Moon
2010	November	Sat 6	2:38	AM	0.2	.9 8:3	5 AN	1 2.0)6	2:38	PN	1 0.	.24	8:56	PM	2.39	New Moon
2011	November	Fri 25	2:39	AM	0.2	8:3	3 AN	1 1.9	9	2:35	PN	1 0.	.24	8:55	PM	2.4	New Moon
2012	November	Wed 14	2:51	AM	0.2	2 8:4	6 AN	1 2.0	19	2:51	PM	4 0.	.18	9:08	PM	2.46	New Moon

									-			r	-				r		
2013	November	Sun 3	;	2:31	AM	0.3	4	8:24	AM	1 2.0	05	2:33	B PN	I 0.2	5 8:	46	PM	2.3	New Moon
2014	November	Sat 2	2	2:39	AM	0.3	8	8:30	AM	1 1.	92	2:36	5 PM	1 0.3	1 8:	50	PM	2.2	27 New Moon
2015	November	Wed	11	2:36	AM	0.4	. :	8:33	AM	1 1.9	9	2:35	5 PM	1 0.4	8:	50	PM	2.2	New Moon
	•																		
Year	Month	Day		Low				High	l			Low			Hig	h			Moon
2005	Decembe	r Thu	1	2:34	A	M 0	.4	8:22	AN	1 1.	9	2:26	PM	0.3	8:44]	PM	2.3	New Moon
2006	Decembe	er Wee	20	2:50	A	M 0	.5	8:35	AM	1 1.	7	2:34	PM	0.4	8:55	5]	PM	2.2	New Moon
2007	Decembe	er Sun	9	2:43	A	M 0	.5	8:34	AN	1 1.	7	2:25	PM	0.5	8:50)]	PM	2.1	New Moon
2008	Decembe	er Sat	27	3:03	A	M 0	.5	8:57	AN	1 1.	6	2:42	PM	0.5	9:09)]	PM	2.1	New Moon
2009	Decembe	er Wed	16	2:53	A	M 0	.5	8:46	AN	1 1.	7	2:32	PM	0.5	9:01	.]	PM	2.1	New Moon
2010	Decembe	er Sun	5	2:30	A	M 0	.4	8:22	AN	1 1.	8	2:18	PM	0.4	8:42	2 1	PM	2.3	New Moon
2011	Decembe	er Sat	24	2:35	A	M 0	.3	8:27	AN	1 1.	8	2:25	PM	0.4	8:47	']	PM	2.3	New Moon
2012	Decembe	r Thu	13	2:42	A	M 0	.3	8:35	AN	1 1.	9	2:38	PM	0.2	8:57	']	PM	2.4	New Moon
2013	Decembe	r Tue	3	2:56	A	M 0	.3	8:48	AN	1 2		2:53	PM	0.2	9:09)]	PM	2.4	New Moon
2014	Decembe	er Mor	22	3:04	A	M 0	.3	8:54	AN	1 1.	9	2:59	PM	0.3	9:14]	PM	2.3	New Moon
2015	Decembe	er Fri I	1	2:52	A	M 0	.4	8:42	AN	1 1.	8	2:45	PM	0.4	9:00)]	PM	2.2	New Moon
							1												
Year	Month	Day	Lo	w			Hi	gh			I	Low			High	1			Moon
2005	January	Tue 25	3:2	23 A	М	0.45	9:2	20	AM	1.64	3	3:06	PM	0.48	9:27	F	PM	2.05	Full Moon
								T											

2005	January	Tue 25	3:23	AM	0.45	9:20	AM	1.64	3:06	PM	0.48	9:27	PM	2.05	Full Moon
2006	January	Sat 14	3:18	AM	0.47	9:12	AM	1.63	2:55	PM	0.51	9:22	PM	2.07	Full Moon
2007	January	Wed 3	2:57	AM	0.42	8:48	AM	1.69	2:39	PM	0.46	9:03	PM	2.17	Full Moon
2008	January	Tue 22	3:05	AM	0.31	8:58	AM	1.77	2:53	PM	0.38	9:11	PM	2.23	Full Moon
2009	January	Sun 11	3:10	AM	0.22	9:03	AM	1.87	3:03	PM	0.28	9:20	PM	2.34	Full Moon
2010	January	Fri 1	3:20	AM	0.24	9:11	AM	1.9	3:13	PM	0.26	9:29	PM	2.36	Full Moon
2010	January	Sat 30	3:08	AM	0.16	9:05	AM	1.96	3:07	PM	0.21	9:19	PM	2.36	Full Moon
2011	January	Thu 20	3:23	AM	0.2	9:17	AM	1.93	3:20	PM	0.24	9:31	PM	2.32	Full Moon
2012	January	Mon 9	3:09	AM	0.37	9:01	AM	1.77	3:00	PM	0.38	9:13	PM	2.17	Full Moon
2013	January	Sun 27	3:19	AM	0.34	9:16	AM	1.8	3:14	PM	0.36	9:25	PM	2.12	Full Moon
2014	January	Thu 16	3:16	AM	0.4	9:16	AM	1.74	3:06	PM	0.42	9:26	PM	2.09	Full Moon
2015	January	Mon 5	3:10	AM	0.4	9:08	AM	1.8	2:58	PM	0.4	9:20	PM	2.1	Full Moon

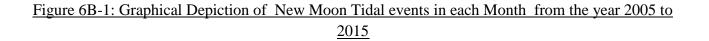
Year	Month	Day	Low			High			Low			High			Moon
2005	February	Thu 24	3:30	AM	0.3	9:31	AM	1.84	3:28	PM	0.36	9:36	PM	2.09	Full Moon
2006	February	Mon 13	3:32	AM	0.4	9:34	AM	1.76	3:23	PM	0.42	9:39	PM	2.07	Full Moon
2007	February	Fri 2	3:29	AM	0.4	9:26	AM	1.75	3:15	PM	0.43	9:33	PM	2.13	Full Moon
2008	February	Thu 21	3:25	AM	0.2	9:25	AM	1.93	3:23	PM	0.3	9:34	PM	2.19	Full Moon
2009	February	Mon 9	3:00	AM	0.2	8:57	AM	1.91	2:58	PM	0.27	9:10	PM	2.29	Full Moon
2010	February	Sun 28	2:49	AM	0.1	8:50	AM	2.06	2:57	PM	0.18	9:03	PM	2.3	Full Moon
2011	February	Fri 18	3:03	AM	0.1	9:02	AM	2.04	3:09	PM	0.17	9:16	PM	2.32	Full Moon
2012	February	Wed 8	3:24	AM	0.2	9:21	AM	1.97	3:26	PM	0.23	9:32	PM	2.25	Full Moon
2013	February	Tue 26	3:24	AM	0.2	9:24	AM	2.01	3:32	PM	0.24	9:34	PM	2.17	Full Moon
2014	February	Sat 15	3:25	AM	0.3	9:27	AM	1.87	3:25	PM	0.34	9:35	PM	2.09	Full Moon
2015	February	Wed 4	3:26	AM	0.3	9:28	AM	1.8	3:20	PM	0.4	9:37	PM	2.1	Full Moon

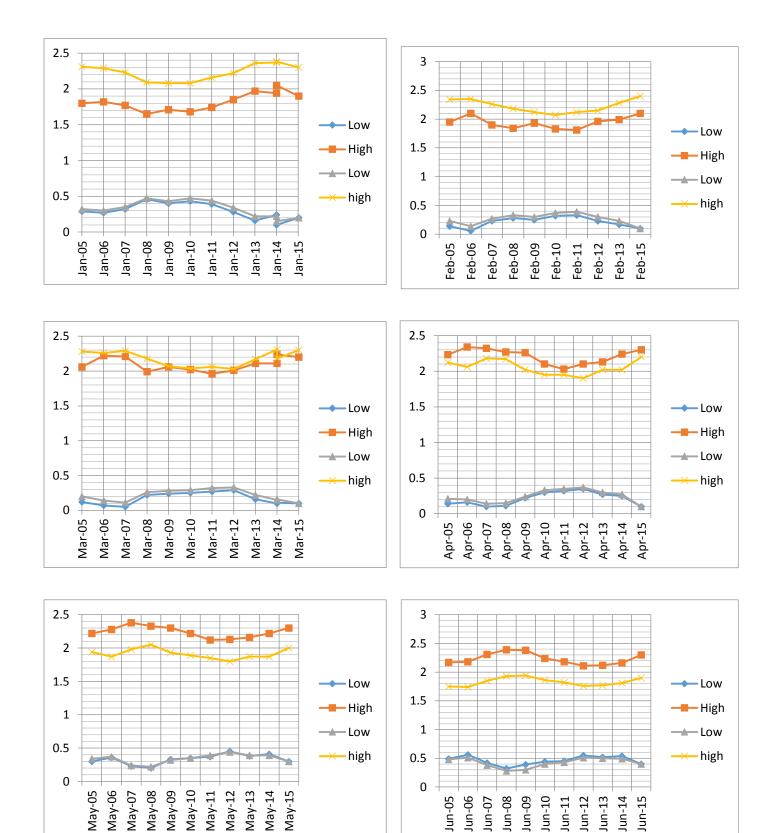
Year	Month	Day	Low			High			Low			High			Moon
2005	March	Sat 26	3:22	AM	0.20	9:26	AM	2.1	3:36	PM	0.3	9:34	PM	2.1	Full Moon
2006	March	Wed 15	3:25	AM	0.3	9:32	AM	2	3:33	PM	0.3	9:37	PM	2.1	Full Moon

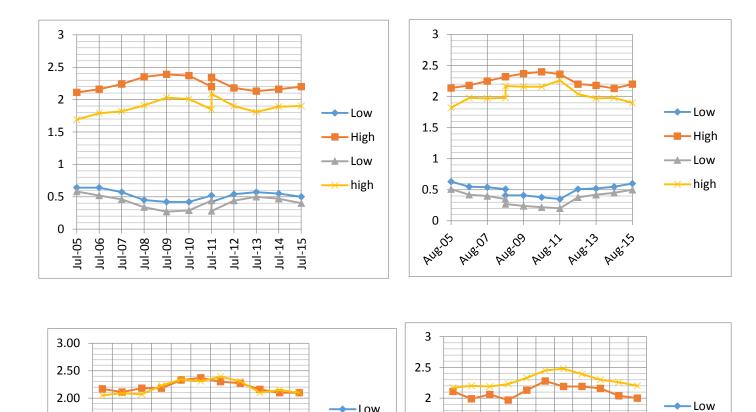
2007	March	Sun 4	3:29	AM	0.3	9:35	AM	1.9	3:31	PM	0.3	9:40	PM	2.1	Eull Moon	
2007	March	Sull 4 Sat 22	3:19	AM	0.5	9:33	AM	2.1	3:33	PM PM	0.3	9:40	PM PM	2.1Full Moon2.1Full Moon		
		Wed						+ +								
2009	March	11	3:12	AM	0.1	9:17	AM	2.1	3:22	PM	0.2	9:28	PM	2.2 Full Moon		
2010	March	Tue 30	2:57	AM	0.1	9:06	AM	2.3	3:19	PM	0.1	9:20	PM	2.2		
2011	March	Sat 19	2:36	AM	0.1	8:41	AM	2.2	2:53	PM	0.2	8:55	PM	2.3	Full Moon	
2012	March	Thu 8	2:57	AM	0.1	8:59	AM	2.1	3:10	PM	0.2	9:12	PM	2.2	Full Moon	
2013	March	Wed 27	2:53	AM	0.2	8:58	AM	2.1	3:12	PM	0.2	9:10	PM	2.1	Full Moon	
2014	March	Sun 16	2:56	AM	0.3	9:02	AM	2	3:07	PM	0.3	9:10	PM	2	Full Moon	
2015	March	Thu 5	3:02	AM	0.3	9.1	AM	1.9	3:05	PM	0.4	9:17	PM	2.0	Full Moon	
Vaar	Month	Dev	Low			High			Low			ILia	h		Maan	
Year			Low			High	1		Low				High		Moon	
2005	April	Sun 24	2:44	AM			AM	2.2	3:12						02 Full Moor	
2006	April	Thu 13	2:47	AM		8:59	AM	2.06	3:08						96 Full Moor	
2007	April	Mon 2	2:53	AM		9:05	AM	2.01	3:07	PM					99 Full Moor	
2008	April	Sun 20	2:42	AM			AM	2.11	3:09						92 Full Moor	
2009	April	Thu 9	2:40	AM		8:51	AM	2.16	3:02	PM					05 Full Moor	
2010	April	Wed 28	2:26	AM			AM	2.26	3:01	PM						
2011	April	Mon 18	2:44	AM		8:57	AM	2.35	3:16						15 Full Moor	
2012	April	Sat 7	3:02	AM		9:12	AM	2.34	3:30			9:2				
2013	April	Fri 26	2:56	AM	0.16		AM	2.34	3:30							
2014	April	Tue 15	2:51	AM	0.25		AM	2.15	3:16						03 Full Moor	
2015	April	Sat 4	2:56	AM	0.3	9:07	AM	2.0	3:14	PM	0.3	9:10	6 PN	1 2.	0 Full Moor	n
Year	Month	Day	Low			High			Low			High			Moon	
2005	May	Tue 24	2:45	AM	0.3	9:03	AM	2.32	3:31	PM	0.31	9:21	PM	1.94	4 Full Moon	
2006	May	Sat 13	2:37	AM	0.36	8:52	AM	2.18	3:15	PM	0.39	9:04	PM	1.8	7 Full Moon	
2007	May	Wed 2	2:38	AM	0.37	8:56	AM	2.11	3:11	PM	0.4	9:05	PM	1.8	5 Full Moon	
2008	May	Tue 20	2:34	AM	0.46	8:59	AM	2.12	3:19	PM	0.47	9:13	PM	1.70	5 Full Moon	
2009	May	Sat 9	2:35	AM	0.37	8:57	AM	2.18	3:14	PM	0.39	9:11	PM	1.8	5 Full Moon	
2010	May	Fri 28	2:35	AM	0.42	9:00	AM	2.23	3:24	PM	0.4	9:20	PM	1.8	3 Full Moon	
2011	May	Tue 17	2:18	AM	0.27	8:37	AM	2.33	3:02	PM	0.27	8:57	PM	1.9	9 Full Moon	
2012	May	Sun 6	2:35	AM	0.17	8:51	AM	2.39	3:15	PM	0.17	9:11	PM	2.0	Full Moon	
2013	May	Sat 25	2:32	AM	0.25	8:49	AM	2.38	3:17	PM	0.23	9:11	PM	2.04	4 Full Moon	
2014	May	Thu 15	2:55	AM	0.27	9:08	AM	2.3	3:34	PM	0.26	9:26	PM	2.0	1 Full Moon	
2015	May	Mon 4	2:52	AM	0.3	9:04	AM	2.1	3:23	PM	0.3	9:16	PM	1.9	Full Moon	
Year	Month	Day	Low			High			Low			High			Moon	
2005	June	Wed 22	2:27	AM	0.41	8:49	AM	2.33	3:24	PM	0.36	9:14	PM	1.8		
2006	June	Sun 11	2:08	AM	0.48	8:29	AM	2.18	3:01	PM	0.47	8:46	PM	1.7	9 Full Moon	
2007	June	Fri 1	2:37	AM	0.48	8:59	AM	2.14	3:26	PM	0.48	9:13	PM	1.7		
2007	June	Sat 30	2:21	AM	0.59	8:44	AM	2.12	3:17	PM	0.54	9:04	PM	1.7	3 Full Moon	
2008	June	Wed 18	2:12	AM	0.6	8:43	AM	2.08	3:09	PM	0.57	9:00	PM	1.6		
2009	June	Sun 7	2:07	AM	0.55	8:37	AM	2.11	3:01	PM	0.53	8:55	PM	1.7		
2010	June	Sat 26	2:20	AM	0.58	8:48	AM	2.16	3:17	PM	0.51	9:12	PM	1.7		
2011	June	Thu 16	2:42	AM	0.43	9:05	AM	2.30	3:35	PM	0.36	9:30	PM	1.8		
2012	June	Mon 4	2:14	AM	0.43	8:34	AM	2.37	3:04	PM	0.27	8:58	PM	1.9		
2013	June	Sun 23	2:16	AM	0.35	8:35	AM	2.38	3:06	PM	0.28	9:00	PM	2.0		
				1 1111	0.55					I - · -		2.00		1		

2014	T	Б	• 12	0.25				0.51	434	0.24	2.01	DM	0.00	0.12	DM	2.00	E II M
2014	June		ri 13	2:35	A		0.34	8:51	AM	2.34	3:21	PM	0.29	9:13	PM	2.00	Full Moon
2015	June	Τι	ue 2	2:23	A	М	0.4	8:39	AM	2.2	3:04	PM	0.4	8:54	PM	1.9	Full Moon
Year	Month	D	ay	Low	,			High			Low			High			Moon
2005	July		Thu 21		A	AM 0.48		8:42 AM		2.33	3:18	PM	PM 0.35		9:10 PM		Full Moon
2006	July	Τι	ue 11	2:38	A	М	0.50	8:58	AM	2.27	3:34	PM	0.40	9:23	PM	1.88	Full Moon
2007	July	М	Ion 30	2:54		М	0.53	9:08	AM	2.25	3:39	PM	0.39	9:32	PM	1.94	Full Moon
2008	July		ri 18	2:41		М	0.62	9:03	AM	2.12	3:31	PM	0.52	9:25	PM	1.78	Full Moon
2009	July	Τι	ue 7	2:31	A	М	0.64	9:00	AM	2.10	3:26	PM	0.56	9:22	PM	1.73	Full Moon
2010	July	М	lon 26	2:50	А	М	0.60	9:12	AM	2.16	3:34	PM	0.48	9:35	PM	1.85	Full Moon
2011	July	Fı	ri 15			М	0.54	8:56	AM	2.24	3:25	PM	0.43	9:22	PM	1.88	Full Moon
2012	July	W	ved 4	2:50	А	М	0.40	9:09	AM	2.37	3:40	PM	0.30	9:36	PM	1.99	Full Moon
2013	July	М	[on 22	2:07	A	AM 0.43		8:25	AM	2.35	2:56	PM	0.31	8:52	PM	2.04	Full Moon
2014	July	Sa	at 12			М	0.39	8:37	AM	2.36	3:09	PM	0.29	9:03	PM	2.04	Full Moon
2015	July	Tl	hu 2	2:42	AM		0.40	8:57	AM	2.30	3:28	PM	0.4	9:19	PM	2.0	Full Moon
2015	July	Fı	ri 31	2:29	Α	М	0.40	8:42	AM	2.30	3:11	PM	0.3	9:06	PM	2.1	Full Moon
		P															
Year	Month	Da		Low		M	0.49	High	414	2.24	Low	DM	0.2	High	DM	2.06	Moon
2005	August		i 19	2:19	Al		0.48	8:33	AM	2.34	3:05	PM	0.3	9:02	PM	2.06	Full Moon
2006	August		ed 9	2:33	Al		0.48	8:47	AM	2.32	3:19	PM	0.32	9:14	PM	2.02	Full Moon
2007	August		ie 28	2:41	Al		0.45	8:48	AM	2.29	3:13	PM	0.28	9:13	PM	2.13	Full Moon
2008	August		in 17	3:05			0.49	9:13	AM	2.23	3:37	PM	0.35	9:35	PM	2.04	Full Moon
2009	August		iu 6	2:58			0.58	9:15	AM	2.15	3:35	PM	0.46	9:35	PM	1.9	Full Moon
2010	August		ie 24		2:38 AM		0.59	8:53	AM	2.13	3:08	PM	0.46	9:14	PM	1.96	Full Moon
2011	August		in 14	3:02	Al		0.51	9:17	AM	2.23	3:35	PM	0.39	9:39	PM	2.01	Full Moon
2012	August		nu 2	2:43	Al		0.45	8:58	AM	2.32	3:25	PM	0.33	9:24	PM	2.04	Full Moon
2012	August		i 31	2:34	Al		0.47	8:43	AM	2.24	3:02	PM	0.35	9:06	PM	2.11	Full Moon
2013	August		ed 21	2:46	Al		0.36	8:56	AM	2.38	3:19	PM	0.23	9:21	PM	2.21	Full Moon
2014	August		in 10	2:11	-	AM 0.40		8:24	AM	2.36	2:53	PM	0.27	8:51	PM	2.13	Full Moon
2015	August	Su	in 30	2:59	Al	М	0.30	9:06	AM	2.4	3:29	PM	0.2	9:31	PM	2.3	Full Moon
Year	Month		Day	L	ow			High	l		Low			High	1		Moon
2005	Septemb	er	Sun 18	2:	52	AN	1 0.3	8:57	AM	2.38	3:17	1	0.16	9:22	PM	2.3	Full Moon
2006	Septemb		Fri 8		03	AM		9:09	AM		3:30	-	0.13	9:34	PM	-	Full Moon
2007	Septemb		Thu 27		58	AN		8:59	AM		3:15	-		9:22	PM	-	Full Moon
2008	Septemb		Mon 1		44	AM		8:46	AM		3:04	-	0.27	9:07	PM	-	Full Moon
2009	Septemb		Fri 4		40	AN		8:50	-	-	3:04	-		9:09	PM		Full Moon
2010	Septemb		Thu 23			AM		8:51	AM	2.09	2:58	-	0.38	9:08	PM	-	Full Moon
2011	Septemb		Mon 1					8:54		-	3:03	-		9:13	PM	-	Full Moon
2012	Septemb		Sun 30		2:49 AN			8:53		-	2:58			9:12	PM		Full Moon
2013	Septemb		Thu 19		2:33 Al		-	8:38	AM	-	2:54		0.25	9:01	PM		Full Moon
2014	-		Tue 9			AM		8:51	AM	-	3:11	PM	-	9:16	PM	-	Full Moon
2015	Septemb		Mon 2			AM	-	2:46	AM	-	3:03	PM	0.1	9:10	PM	-	Full Moon
										<u> </u>							
Year	Month	onth Day		Low				High			Low	Π		High	1		Moon
2005	October	Μ	fon 17	2:34	A	М	0.32	8:34	AM	2.22	2:45	PM	0.19	8:57	PM	2.35	Full Moon
2006	October	S	at 7	2:45	A	М	0.24	8:46	AM	2.33	3:00	PM	0.11	9:10	PM	2.43	Full Moon
2007	October	F	ri 26	2:38	A	М	0.23	8:34	AM	2.20	2:44	PM	0.14	8:58	PM	2.46	Full Moon

2008 October Wed 15 2:55 AM 0.28 8:50 AM 2.19 3:01 PM 0.18 9:12 PM 2.4 2009 October Sun 4 2:46 AM 0.41 8:44 AM 2.10 2:55 PM 0.30 9:03 PM 2.2 2010 October Sat 23 2:51 AM 0.42 8:46 AM 1.97 2:50 PM 0.35 9:03 PM 2.2 2011 October Wed 12 2:50 AM 0.44 8:53 AM 2.02 2:54 PM 0.37 9:09 PM 2.1 2012 October Tue 30 2:58 AM 0.42 8:58 AM 1.94 2:54 PM 0.38 9:13 PM 2.2 2013 October Sat 19 2:52 AM 0.35 8:53 AM 2.10 2:56 PM 0.30 9:11 PM	4 Full Moon 2 Full Moon											
2010 October Sat 23 2:51 AM 0.42 8:46 AM 1.97 2:50 PM 0.35 9:03 PM 2.2 2011 October Wed 12 2:50 AM 0.44 8:53 AM 2.02 2:54 PM 0.37 9:09 PM 2.1 2012 October Tue 30 2:58 AM 0.42 8:58 AM 1.94 2:54 PM 0.38 9:13 PM 2.2	2 Full Moon											
2011 October Wed 12 2:50 AM 0.44 8:53 AM 2.02 2:54 PM 0.37 9:09 PM 2.1 2012 October Tue 30 2:58 AM 0.42 8:58 AM 1.94 2:54 PM 0.38 9:13 PM 2.2												
2012 October Tue 30 2:58 AM 0.42 8:58 AM 1.94 2:54 PM 0.38 9:13 PM 2.2	0 Full Moon											
2013 October Sat 19 2:52 AM 0.35 8:53 AM 2.10 2:56 PM 0.30 9:11 PM 2.2	1 Full Moon											
	9 Full Moon											
2014 October Wed 8 2:30 AM 0.29 8:32 AM 2.26 2:45 PM 0.19 8:55 PM 2.3	7 Full Moon											
2015 October Tue 27 2:28 AM 0.2 8:27 AM 2.2 2:38 PM 0.1 8:50 PM 2.4	Full Moon											
Year Month Day Low High Low High	Moon											
2005 November Wed 16 2:52 AM 0.34 8:48 AM 1.97 2:46 PM 0.3 9:07 PM 2	.31 Full Moon											
2006 November Sun 5 2:27 AM 0.28 8:23 AM 2.13 2:30 PM 0.18 8:46 PM 2	.41 Full Moon											
2007 November Sat 24 2:23 AM 0.29 8:15 AM 1.99 2:19 PM 0.23 8:39 PM 2	.4 Full Moon											
2008 November Thu 13 2:36 AM 0.29 8:28 AM 2.03 2:34 PM 0.22 8:52 PM 2	.41 Full Moon											
2009 November Tue 3 2:57 AM 0.34 8:48 AM 2.01 2:54 PM 0.28 9:08 PM 2	.34 Full Moon											
2010 November Sun 21 2:32 AM 0.46 8:21 AM 1.81 2:23 PM 0.39 8:40 PM 2	.19 Full Moon											
2011 November Fri 11 3:00 AM 0.44 8:54 AM 1.85 2:53 PM 0.4 9:10 PM 2	.19 Full Moon											
2012 November Wed 28 2:42 AM 0.48 8:39 AM 1.77 2:30 PM 0.45 8:55 PM 2	.13 Full Moon											
2013 November Sun 17 2:36 AM 0.43 8:33 AM 1.89 2:29 PM 0.39 8:51 PM 2	.21 Full Moon											
2014 November Fri 7 2:54 AM 0.28 8:52 AM 2.08 2:55 PM 0.25 9:12 PM 2	.35 Full Moon											
2015 November Thu 26 2:56 AM 0.20 8:53 AM 2.1 2:55 PM 0.2 9:14 PM 2	.40 Full Moon											
Year Month Day Low High Low High	Moon											
2005 December Thu 15 2:43 AM 0.45 8:35 AM 1.73 2:25 PM 0.44 8:53 PM 2.												
2006 December Tue 5 2:56 AM 0.32 8:49 AM 1.87 2:44 PM 0.33 9:08 PM 2.	31 Full Moon											
2007 December Mon 24 3:04 AM 0.3 8:55 AM 1.82 2:51 PM 0.34 9:14 PM 2.51	31 Full Moon											
2008 December Fri 12 2:26 AM 0.34 8:15 AM 1.85 2:17 PM 0.3 8:39 PM 2.17	34 Full Moon											
2009 December Wed 2 2:43 AM 0.36 8:31 AM 1.87 2:34 PM 0.31 8:53 PM 2.11	31 Full Moon											
2010 December Tue 21 2:57 AM 0.39 8:44 AM 1.77 2:46 PM 0.38 9:03 PM 2.4	22 Full Moon											
2011 December Sat 10 2:48 AM 0.48 8:39 AM 1.72 2:34 PM 0.45 8:54 PM 2.	13 Full Moon											
2012 December Fri 28 3:04 AM 0.45 9:00 AM 1.7 2:50 PM 0.45 9:11 PM 2.4	09 Full Moon											
2013 December Tue 17 2:57 AM 0.45 8:55 AM 1.74 2:43 PM 0.45 9:08 PM 2.	13 Full Moon											
2014 December Sat 6 2:44 AM 0.37 8:39 AM 1.87 2:35 PM 0.36 8:57 PM 2.11	24 Full Moon											
2015 December Fri 25 2:49 AM 0.3 8:44 AM 1.9 2:42 PM 0.3 9:02 PM 2.43	3 Full Moon											







-Low

🗕 High

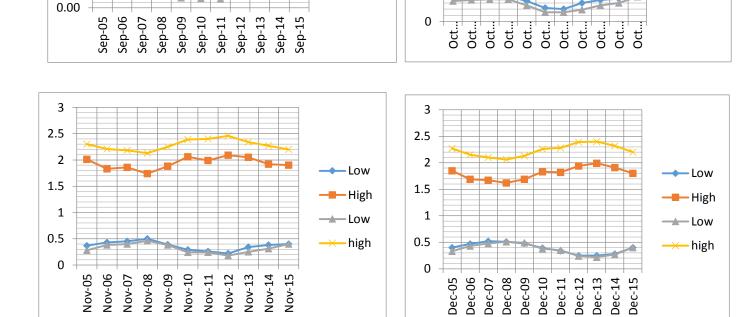
-Low

-high

1.5

1

0.5



1.50

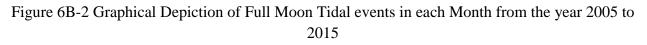
1.00

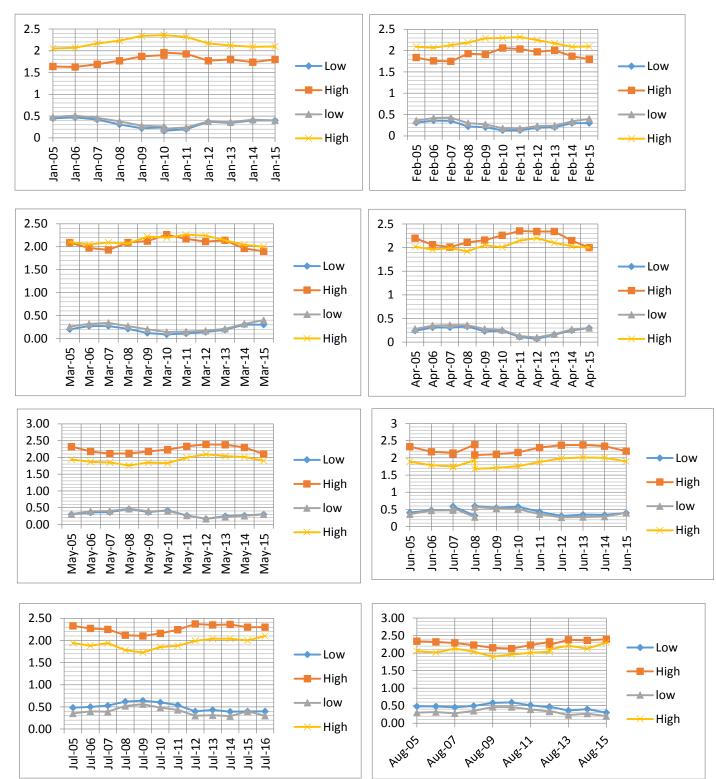
0.50

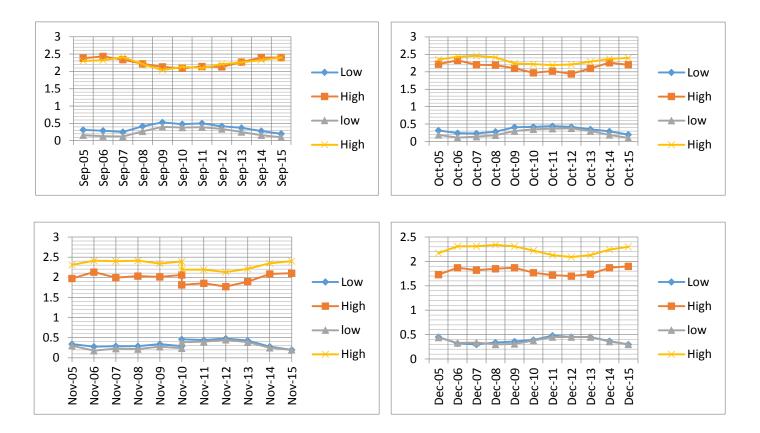
🗕 High

-Low

× – high







As discussed above, considering the spring tide (full moon tide & new moon tide), It has been graphically replicated as above. Monthly highest and lowest tide values of Port Blair, Andaman Islands from website tides.mobilegeographics.com from the period 2005 to 2015 was considered shown in table 6.3 and found highest tide ranging from 2.4 to 2.1 and lowest tide range from 0.1 to 0.5, the average highest tide was in the month of August & October i.e., 2.4 and lowest was in the month of month of march i.e., 0.1.

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