

OPTIMIZATION IN FREQUENCY DOMAIN DESIGN OF CONTROL SYSTEMS

A DISSERTATION

submitted in partial fulfilment
of the requirements for the award of the degree
of

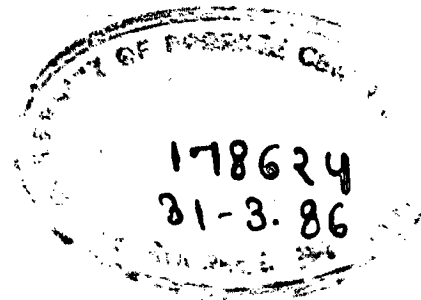
MASTER OF ENGINEERING

in

ELECTRICAL ENGINEERING
(System Engineering and Operations Research)

By

RAJEEV SHARMA



DEPARTMENT OF ELECTRICAL ENGINEERING
UNIVERSITY OF ROORKEE
ROORKEE, 247 667 (INDIA)

June, 1985

Gratis

CANDIDATE'S DECLARATION

I hereby certify that the work which is being presented in the dissertation entitled, "OPTIMIZATION IN FREQUENCY DOMAIN DESIGN OF CONTROL SYSTEMS" in partial fulfilment of the requirements for the award of the Degree of MASTER OF ENGINEERING IN ELECTRICAL ENGINEERING with specialisation in SYSTEM ENGINEERING AND OPERATIONS RESEARCH, submitted in the Department of Electrical Engineering, University of Roorkee is an authentic record of my own work carried out for a period of about eleven months, from July 1984 to June 1985, under the supervision of Dr. Jayant Pal, Reader, Department of Electrical Engineering, University of Roorkee, Roorkee, India.

The matter embodied in this dissertation has not been submitted by me for the award of any other degree or diploma.

ROORKEE :
JUNE , 1985.

Rajeev
(RAJEEV SHARMA)

This is to certify that the above statement made by the candidate is correct to the best of my knowledge.

ROORKEE :
JUNE , 1985.

Jayant Pal
06/07/85
(JAYANTAPAL)
READER

DEPARTMENT OF ELECTRICAL ENGINEERING
UNIVERSITY OF ROORKEE, ROORKEE INDIA

ACKNOWLEDGEMENT

I express my deep sense of gratitude to Dr. Jayant Pal, Reader, Department of Electrical Engineering, University of Roorkee, Roorkee for his constant encouragement, expert guidance and keen interest throughout the work.

I am also grateful to my friend, Mr. Sanjay Mathur for his constant and timely help.

Rajeev
(RAJEEV SHARMA)

Abstract

In this dissertation, we propose to use optimization techniques in the frequency domain design of control system. This is different from the optimal control techniques in which optimization is done in the time domain. The objective of this work is to test the suitability or otherwise of using optimization techniques to find the controller parameters so as to minimize the squared error of frequency response deviations of the controlled system and a specification model. The graphs have also been drawn for time response and frequency response of different cases. The results are attached at the end of each case.

C O N T E N T S

PAGE No.

CANDIDATE'S DECLARATION

ACKNOWLEDGEMENT

ABSTRACT

CHAPTER

1.	INTRODUCTION.	...	1
2.	REVIEW OF CONTROL SYSTEM DESIGN THEORY.	...	4
3.	FREQUENCY DOMAIN DESIGN USING OPTIMIZATION.	...	8
4.	EXAMPLES.	...	16
5.	CONCLUSIONS.	...	29
	REFERENCES	...	30

I. INTRODUCTION

Design of control systems represents an interesting and complex subject in control system studies. In a simplified manner the design problem of control systems can be described with the aid of the block diagram of Figure 1.

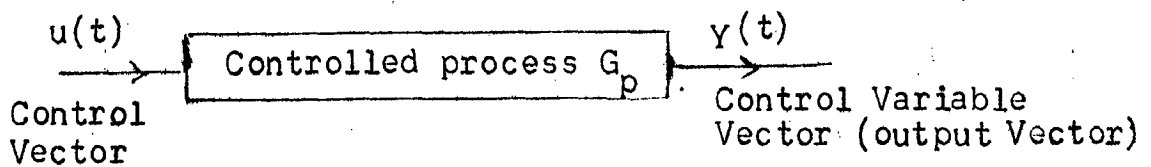


Fig.1: Block Diagram of a controlled Process.

The Figure 1 shows a controlled process whose output Vector $Y(t)$ represents q controlled variables and the control vector $u(t)$ represents p control signals. The problem is to find a set of 'appropriate' signals $u(t)$, so that the controlled variable vector $Y(t)$ behaves as desired. The description of the basic design problem is simplified by overlooking the possible existence of external disturbances.

Once the desired control vector $u(t)$ for satisfactory control is determined, a controller is usually needed to generate this control from the reference inputs and the state vector $x(t)$ or output $Y(t)$.

(2)

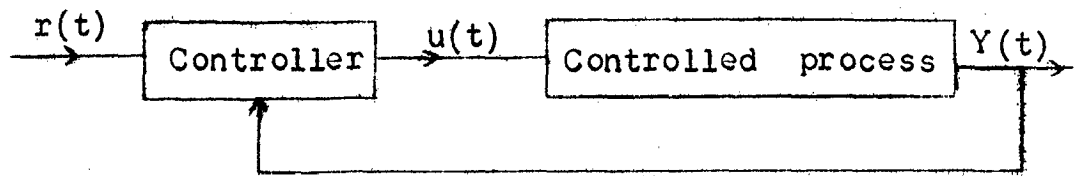


Fig.2: Block Diagram of a control system with output feedback.

Figure 2 illustrates the block diagram of a control system whose control vector is derived from the input vector, and the output vector. This type of system is referred to as an output feedback system. The block diagram is intended only for the purpose of illustrating the philosophy of designing control systems and no attempt is made to include all possible configurations.

The design and parameter adjustment of the open loop transfer function of the system for specified closed loop performance is carried out somewhat more easily in frequency domain (i.e. through frequency response) than in time domain (i.e. through time response). Further, the effects of noise disturbance and parameter variations are relatively easy to visualize and assess through frequency response. If necessary, the transient response of a system can be obtained from its frequency response through the Fourier integral.

The frequency response is easily evaluated from the sinusoidal transfer function which can be obtained

(3)

simply by replacing s with $j\omega$ in the system transfer function $T(s)$. The transfer function $T(j\omega)$ thus obtained, is a complex function of frequency and has both a magnitude and a phase angle. These characteristics are conveniently represented by graphical plots.

II. REVIEW OF CONTROL SYSTEM DESIGN THEORY

The early stage of the theoretical development of the design of control systems was characterized by the works of Nyquist, Nichols and Bode who developed such classical methods as the Nyquist plot, Bode diagram and Nichols Chart. A unique feature of these methods is that they are all graphical techniques which are conducted in the frequency domain. In the design of control systems, both the time and frequency responses are of importance. The use of the frequency domain techniques leads to graphical methods for the design of controllers.

The classical design of control systems involve a trial and error approach. The proper selection of the system configuration as well as the parameters of the controller depend to a great extent on the experience and judgement on the part of designer. In the frequency domain design, the design specifications usually are given in terms of such criteria as gain margin, phase margin, peak resonance and band width. These criteria, however, should be related to the time domain specifications such as rise time, overshoot and settling time which are more amenable to direct measurements. The distinct disadvantage of the classical design of control systems is that it does not indicate whether a solution actually exists for

the design problem at the outset. It is entirely possible that design requirements are so stringent or may be contradictory so that they can not be satisfied by any system configuration or controllers that are physically realizable. Even when a solution does exist, the classical design may yield a system that may not be the best one.

The introduction of the root locus technique by Evans in 1950 made possible the design of control systems to be carried out in the S-plane. The main advantage of the root locus method is that information on frequency domain as well as time domain characteristics can be derived directly from the pole-zero configuration in the S-plane. With the knowledge of the closed loop transfer function poles and zeros, the time domain response is determined readily by means of inverse Laplace transform and the frequency response is obtained from the Bode plot. However, the root locus design still is basically a trial and error procedure and it relies on the reshaping of the root loci to obtain a satisfactory pole-zero configuration for the closed loop system.

The work by Norbert Wiener in the late 1940s opened a new horizon to the design of control systems. Wiener introduced not only statistical considerations in control system design, but also the idea of a performance index. For the first time, the design engineer was able to start

(6)

from a set of design criteria and carry out the design by means of a completely analytical procedure. We are able to design a control system that is optimum or the best possible with respect to a given performance criterion. The principle of Wiener's optimization technique is demonstrated by the block diagram in Fig.1. The design objective is to determine the closed loop transfer function $Y(s)/U(s)$ of the system such that the error between the desired output and the actual output is minimized. In Wiener's statistical design technique, the mean-square value of the error $e(t)$ is used as the performance index J i.e.

$$J = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T e^2(t) dt \quad \dots (1)$$

The reason for using the mean square error as the performance index is that the minimization of this particular performance index induces an analytical design procedure.

State Variable approach is a direct time domain approach which provides a basis for the modern control theory using system optimization. It is a very powerful technique for the analysis and design of linear and non-linear, time-invariant or time-variant, multi-input multi output systems. The organisation of the state variable approach is such that it is easily amenable to solution through digital computers.

In the present work, we propose to use optimization techniques in the frequency domain design of control systems. This is different from the optimal control techniques in which optimization is done in the time domain. The objectives of this work is to test the suitability or otherwise of using optimization techniques to find the controller parameters so as to minimize the squared error of frequency response deviations of the controlled system and a specification model. The details of the proposed technique are given in the following chapter.

III. FREQUENCY DOMAIN DESIGN USING OPTIMIZATION

The design problem may be stated as follows. Given the plant transfer function $G(s)$ as

$$G(s) = \frac{\sum_{i=0}^m a_i s^i}{\sum_{i=0}^n b_i s^i} \quad \dots (2)$$

Where $m \leq n$

Let us choose a pre-compensator as

$$C(s) = \frac{\sum_{i=0}^{r-1} C_i s^i}{\sum_{i=0}^r d_i s^i} \quad \dots (3)$$

So that the closed loop system with unity feedback is given by

$$T(s) = \frac{G(s) C(s)}{1 + G(s)C(s)} \quad \dots (4)$$

approximates a given model transfer function $M(s)$

$$M(s) = \frac{\sum_{i=0}^q e_i s^i}{\sum_{i=0}^p f_i s^i} \quad \dots (5)$$

Where $q \leq p$

in some sense. In other words, we seek to design $C(s)$ so that $T(s)$ approaches $M(s)$ over a frequency range (ω_0, ω_1) . It may be noted that the function $T(s)$ involves the unknown parameters $C_i, d_i, i \in (0, r)$ of $C(s)$ while e_i, f_i of $M(s)$ are known. We define the unknown parameters of $C(s)$ as

(9)

$$p = [C_i, d_i; i \in (0, r)] \quad \dots (6)$$

Error Criteria :

We may choose any one of the several error criteria commonly used. The most popular one is the mean squared error function defined by

$$E = \frac{1}{2} \int_{\omega_0}^{\omega_1} |T(j\omega) - M(j\omega)|^2 d\omega \quad \dots (7)$$

or more generally the weighted mean squared error function defined by

$$E = \frac{1}{2} \int_{\omega_0}^{\omega_1} W(\omega) |T(j\omega) - M(j\omega)|^2 d\omega \quad \dots (8)$$

Where $| |$ represents the absolute value of a complex function and $W(\omega)$ is a real non-negative weighting function.

Iteration algorithm :

STEP-1: Make a reasonable guess of the controller parameters C_i, d_i . This initial guess need not be close to the optimal values. With this choice of parameters values $T(p, j\omega)$ can be computed.

STEP-2: Use the element values of Step-1 and an analysis programme to compute the error function $E(p)$. If $E(p) \leq \epsilon$, where ϵ is a small preassigned positive number, the problem is solved, the parameter values chosen in step-1 are satisfactory. Usually, we get $E(p) \gg \epsilon$, in this case we must proceed to step-3.

STEP-3 : Introduce a small perturbation on the parameter values. That is replace C_i by $C_i + \delta C_i$, d_i by $d_i + \delta d_i$, where δC_i and δd_i represent the small change on the element values C_i , d_i respectively. This means that parameters vector \underline{p} is replaced by $\underline{p} + \delta \underline{p}$. Using these adjusted parameter values, the corresponding transfer function $T(\underline{p} + \delta \underline{p}, j\omega)$ and the error function $E(\underline{p} + \delta \underline{p})$ can be computed. We then choose \underline{p} so that the following two conditions are satisfied :

1. $E(\underline{p} + \delta \underline{p}) < E(\underline{p})$
2. $|E(\underline{p} + \delta \underline{p}) - E(\underline{p})|$ is maximized.

The first condition guarantees that the adjustment of the parameter values is in the right direction in the sense that the new system is one step closer to the desired one. The second condition assures that \underline{p} is chosen in an optimal fashion in the sense that the difference between the original error function and the adjusted one is as large as possible.

STEP-4: Use the new parameter values $\underline{p} + \delta \underline{p}$ to compute $T(\underline{p} + \delta \underline{p}, j\omega)$ and $E(\underline{p} + \delta \underline{p})$. If $E(\underline{p} + \delta \underline{p}) \leq \epsilon$, stop the iterations; $\underline{p} + \delta \underline{p}$ is the optimal parameter vector. If $E(\underline{p} + \delta \underline{p}) > \epsilon$, use $\underline{p} + \delta \underline{p}$ as the new parameter values, go back to step-3 and continue the process until one of the following conditions is satisfied :

(11)

1. $E \leq \theta$ or
2. $|E_{i+1} - E_i| \leq \eta$

where η is a pre-assigned positive number and E_i denotes the error function at the i th iteration. The first condition implies that the error function has reached the desired limit and the iterations can be terminated. The second condition implies that the error function has reached a minimum point (or a saddle point) and further iterations will not reduce E appreciably. This minimum however, might be a local minimum rather than the global minimum. In the case where E has reached, a local minimum a new initial guess might be chosen and iterative process may be repeated until the global minimum is found and the optimum parameters values are obtained.

Mean Squared Error Optimization :

We use a perturbation technique to compute the optimum change δp on the parameter vector p that satisfies condition 1 and 2 of Step-3 of the previous algorithm.

Perturbation Analysis :

To introduce the basic idea behind the perturbation analysis, let us first consider the mean squared error function of equation (1). The generalization to any error criterion will then follow.

(12)

Changing the parameter vector \underline{p} by the 'small' vector $\delta\underline{p}$ will cause a change δT on the transfer function $T(\underline{p}, j\omega)$, which in turn will result in a perturbation δE on the error function $E(\underline{p})$. Using equation (7), the change in $E(\underline{p})$ is

$$E(\underline{p}+\delta\underline{p}) - E(\underline{p}) = \frac{1}{2} \int_{\omega_0}^{\omega_1} [|T(\underline{p}, j\omega) + \delta T(\underline{p}, j\omega) - M(j\omega)|^2 - |T(\underline{p}, j\omega) - M(\underline{p}, j\omega)|^2] d\omega \quad \dots (9)$$

Equation (9) can be written as

$$E(\underline{p}+\delta\underline{p}) - E(\underline{p}) = \frac{1}{2} \int_{\omega_0}^{\omega_1} [(T + \delta T - M)(\bar{T} + \delta\bar{T} - \bar{M}) - (T - M)(\bar{T} - \bar{M})] d\omega \quad \dots (10)$$

Where \bar{T} , $\delta\bar{T}$ and \bar{M} denote the complex conjugates of T , δT and M respectively.

Simplifying (10) yields :

$$E(\underline{p}+\delta\underline{p}) - E(\underline{p}) = \frac{1}{2} \int_{\omega_0}^{\omega_1} [(T - M)\delta\bar{T} + (\bar{T} - \bar{M})\delta T + |\delta T|^2] d\omega \quad \dots (11)$$

Since by assumption $\delta\underline{p}$ is small and $T(\underline{p}, j\omega)$ is considered to be a smooth continuous function of \underline{p} then δT is small. Consequently, $|\delta T|^2$ is a second order term in comparison with the other terms of the integrand, and hence can be neglected in this equation. We then have

(13)

$$E(\underline{p} + \delta \underline{p}) - E(\underline{p}) = \delta E(\underline{p}) = \frac{1}{2} \int_{w_0}^{w_1} [(T-M)\delta\bar{T} + (\bar{T}-\bar{M})\delta T] dw \dots (12)$$

Where $\delta E(\underline{p})$ is the approximate change in $E(\underline{p})$ after neglecting the second order term using the properties of complex functions, the equation simplifies to

$$\delta E(\underline{p}) = \int_{w_0}^{w_1} \text{Re} \left\{ [\bar{T}(\underline{p}, jw) - \bar{M}(jw)] \delta T(\underline{p}, jw) \right\} dw \dots (13)$$

$\delta T(\underline{p}, jw)$ can be expanded in terms of the perturbation on the parameter values as follows :

$$\delta T = \sum_{i=0}^{r-1} \frac{\delta T}{\delta C_i} \delta C_i + \sum_{i=0}^r \frac{\delta T}{\delta d_i} \delta d_i \dots (14)$$

Where the partial derivatives are taken with respect to adjustable parameters. If there are other parameters in the system that can be adjusted, the corresponding partial derivatives will be added to (13). Using a vector notation, this equation can be written as

$$\delta T(\underline{p}, jw) = g^T(\underline{p}, jw) \delta \underline{p} \dots (14)$$

Where we have used the following notations

$$g^T(\underline{p}, jw) = \left[\frac{\delta T}{\delta C_1}, \frac{\delta T}{\delta C_2}, \dots, \frac{\delta T}{\delta C_{r-1}}, \frac{\delta T}{\delta d_1}, \frac{\delta T}{\delta d_2}, \dots, \frac{\delta T}{\delta d_r} \right] \dots (15)$$

(14)

The function $g(\underline{p}, j\omega)$ as defined is commonly referred to as the gradient of T with respect to \underline{p} . Replacing $\delta T(\underline{p}, j\omega)$ from (14) into (12) and observing that $\delta \underline{p}$ is independent of w , we get

$$\delta E = \left(\int_{w_0}^{w_1} R_e \{ [\bar{T}(\underline{p}, j\omega) - \bar{M}(j\omega)] g^T(\underline{p}, j\omega) \} dw \right) \delta \underline{p} \quad \dots (16)$$

We now make the following important observation. Since $M(j\omega)$ is given at each iteration, the parameter vector is known (by choosing) then $\bar{T}(\underline{p}, j\omega)$ and $g^T(\underline{p}, j\omega)$ can be computed for each w . Consequently, the coefficient of $\delta \underline{p}$ in (16) can be computed in terms of the parameter values of the previous iterations. Let us, therefore rewrite (16) in compact form.

$$\delta E(\underline{p}) = \beta^T(\underline{p}) \delta \underline{p} \quad \dots (17)$$

Where $\beta(\underline{p})$ is a column vector called the gradient of $E(\underline{p})$ and is defined by

$$\beta^T(\underline{p}) = \int_{w_0}^{w_1} R_e \{ [T(\underline{p}, j\omega) - M(j\omega)] g^T(\underline{p}, j\omega) \} dw \quad \dots (18)$$

The optimization problem now is reduced to obtaining $\delta \underline{p}$ such that, for a given $\beta^T(\underline{p})$, the perturbation on the error function δE satisfies the following two conditions:-

(15)

1. $\delta E < 0$
2. $|\delta E|$ is maximized.

To obtain an efficient and rapidly convergent algorithm, it is necessary to satisfy condition 2.

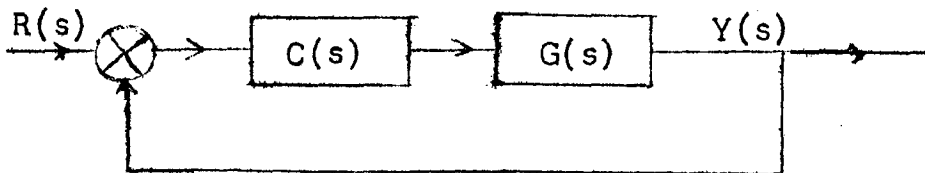
To find the solution to our optimization problem, we must make certain assumptions regarding the 'smallness' of the parameter perturbation.

EXAMPLE 1:

CASE I: Consider the design of a system whose model transfer function is given by

$$M(s) = \frac{25 + 4.242s}{25 + 7.07s + s^2}$$

and the actual topology of the system is given as



Where $G(s) = \frac{3}{s^2 + 4s + 3}$

and $C(s) = K_C \left[1 + \frac{1}{\tau_1 s} \right]$

$$\therefore T(s) = \frac{1}{1 + \frac{1}{G(s)C(s)}}$$

$$= \frac{1}{1 + \frac{\tau_1 s (s^2 + 4s + 3)}{K_C (1 + \tau_1 s) 3}}$$

$$T(s) = \frac{3K_C (1 + \tau_1 s)}{3K_C + 3\tau_1 s(1 + K_C) + 4\tau_1 s^2 + \tau_1 s^3}$$

$$T(p, j\omega) = \frac{3K_C (1 + \tau_1 j\omega)}{3K_C + j\omega 3\tau_1 (1 + K_C) - 4\omega^2 \tau_1 - j\tau_1 \omega^3}$$

(17)

$$\frac{\partial T(p, j\omega)}{\partial K_C} = \frac{-3\omega^2 \tau_1 (\omega^2 - 7) + j\omega(9\tau_1 - 15\omega^2 \tau_1)}{D^2}$$

$$\text{Where } D = 3K_C - 4\omega^2 \tau_1 + j\omega(3\tau_1 + 3K_C \tau_1 - \tau_1 \omega^2)$$

$$\frac{\partial T(p, j\omega)}{\partial C_1} = \frac{-3K_C[-\omega^2(7 - \omega^2 + 3K_C) + j\omega(3 + K_C - \omega^2)]}{D^2}$$

$$AKC = 5.0$$

$$\tau_1 = 1.0$$

On writing arithmetic expressions

```

D=CMLPX(3.0*AKC-4.0*w**2*T1,3.0*T1+3.0*AKC*T1-T1*w**2)
NA=CMLPX(-3.0*w**2*T1*(w**2-7.0),w*(9.0*T1-15.0*w**2*T1)
NB=CMLPX(-3.0*AKC*(-w**2*(7.0-w**2+3.0*AKC),
w*(3.0+AKC-5.0*w**2))

DH1 = CMLPX(25.0- w**2, 7.07*w)
DH2 = CMLPX(25.0, 4.242*w)
DH3 = CMLPX(3.0*AKC, 3.0*w*AKC)
H1 = DH2/DH1
H2 = DH3/D

```

(18)

CASE-II: Again, we consider the same model transfer function as in the Case-I and with the same plant transfer function

$$G(s) = \frac{3}{s^2 + 4s + 3}$$

$$\begin{aligned} \text{but } C(s) &= [K_P + \frac{K_I}{s} + K_D s] \\ &= [\frac{K_I + K_P s + K_D s^2}{s}] \end{aligned}$$

The closed loop transfer function is

$$\begin{aligned} T(s) &= \frac{C(s) G(s)}{1 + C(s) G(s)} \\ &= \frac{[\frac{K_I + sK_P + K_D s^2}{s}] [\frac{3}{s^2 + 4s + 3}]}{1 + [\frac{K_I + K_P s + K_D s^2}{s}] [\frac{3}{s^2 + 4s + 3}]} \end{aligned}$$

$$T(p, s) = \frac{3[K_I + K_P s + K_D s^2]}{s^3 + (4 + 3K_D)s^2 + 3(1 + K_P)s + 3K_I}$$

$$T(p, jw) = \frac{3[(K_I - K_D w^2) + jwK_P]}{3K_I - (4 + 3K_D)w^2 + jw(3 + 3K_P - w^2)}$$

(19)

$$\frac{\partial T}{\partial K_P} = \frac{-3w^2(3-w^2) - j3w(9K_D w^2 + 4w^2)}{D^2}$$

$$\frac{\partial T}{\partial K_I} = \frac{3[-4w^2 + jw(3-w^2)]}{D^2}$$

$$\frac{\partial T}{\partial K_D} = \frac{-3w^2[6K_I - 4w^2 - 15K_D w^2] - j3w^3[3 + 3K_P - w^2]}{D^2}$$

Arithmetic expressions will be

$$D = \text{CMPLX}(3.0*AKI - (4.0 + 3.0*AKD)*w^{**2}, w*(3.0 + 3.0*AKP - w^{**2}))$$

$$NB = \text{CMPLX}(3.0*(-4.0*w^{**2}), 3.0*w*(3.0 - w^{**2}))$$

$$NA = \text{CMPLX}(-3.0*w^{**2}*(3.0 - w^{**2}), 3.0*w*(9.0*AKD*w^{**2} - 4.0*w^{**2}))$$

$$NC = \text{CMPLX}(-3.0*w^{**2}(6.0*AKI - 4.0*w^{**2} - 15.0*AKD*w^{**2}), \\ -3.0*w^{**3}(3.0 + 3.0*AKP - w^{**2}))$$

$$T(jw) = \frac{25 + j4.242 w}{25 - w^2 + j7.07w}$$

$$DH2 = \text{CMPLX}(25.0, 4.242*w)$$

$$DH1 = \text{CMPLX}(25.0 - w^{**2}, 7.07*w)$$

$$H1 = DH2 / DH1$$

$$DH3 = \text{CMPLX}(3.0*(AKI - AKD*w^{**2}), 3.0*AKP*w)$$

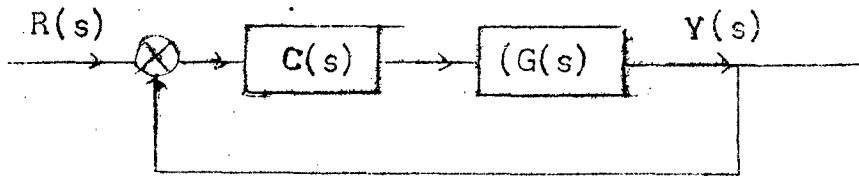
$$H2 = DH3 / D$$

(20)

CASE-III: Consider the design of a plant whose ^{model} transfer function is given by

$$H(s) = \frac{25 + 4.242s}{25 + 7.07s + s^2}$$

and the desired topology is shown below



Where $G(s) = \frac{3}{s^2 + 4s + 3}$

and $C(s) = \left[K_p + \frac{K_I}{s} \right] = \left[\frac{K_I + sK_p}{s} \right]$

Closed loop transfer function = $\frac{G(s) C(s)}{1 + G(s) C(s)}$

$$T(s) = \frac{[K_I + sK_p]/s [3/(s^2 + 4s + 3)]}{1 + \left[\frac{K_I + sK_p}{s} \right] \left[\frac{3}{s^2 + 4s + 3} \right]}$$

$$T(p,s) = \frac{3[K_I + sK_p]}{3K_I + 3K_p s + s^3 + 4s^2 + 3s}$$

(21)

$$T(p, jw) = \frac{3K_I + j3wK_P}{3K_I - 4w^2 + jw(3K_P + 3 - w^2)}$$

$$\frac{\partial T}{\partial K_P} = \frac{-3w^2(3 + 12K_P - w^2) - j12w^3}{D^2}$$

$$\frac{\partial T}{\partial K_I} = \frac{9 - 15w^2}{D^2}$$

Arithmetic expressions will be

$$D = \text{CMPLX}(3.0*AKI - 4.0*w**2, w*(3.0*AKP + 3.0 - w**2))$$

$$NA = \text{CMPLX}(-3.0*w**2*(3.0 + 12.0*AKP - w**2), -12.0*w**3)$$

$$NB = \text{CMPLX}(9.0 - 15.0*w**2, 0)$$

$$DH2 = \text{CMPLX}(25.0, 4.242*w)$$

$$DH1 = \text{CMPLX}(25.0 - w**2, 7.07*w)$$

$$H1 = DH2/DH1$$

$$DH3 = \text{CMPLX}(3.0*AKI, 3.0*w*AKP)$$

$$H2 = DH3/D$$

TO FIND CLOSED LOOP TRANSFER FUNCTIONS FROM THE TABLES
OBTAINED FROM THE COMPUTER RESULTS:

EXAMPLE-ICASE-I:

Sl. No.	Initial Guess		Final Values		w_0 to w_1	Error
	K_C	τ_1	K_C	τ_1		
1.	5.00	1.00	2.4174	2.1653	0 to 5	0.2158
2.	5.00	1.00	5.0082	0.9972	0 to 0.25	0.0431
3.	5.00	1.00	5.0272	1.0047	0 to 0.5	0.0523
4.	5.00	1.00	5.3016	1.3252	0 to 1	0.1142

Closed loop transfer function will be

$$T_1(s) = \frac{3K_C(1 + \tau_1 s)}{3K_C + 3\tau_1 s(1 + K_C) + 4\tau_1 s^2 + \tau_1 s^3}$$

$$T_1(s) = \frac{3.3492 + 7.2522s}{3.3492 + 10.2521s + 4s^2 + s^3}$$

$$T_2(s) = \frac{15.0667 + 15.0245s}{15.0667 + 18.0245s + 4s^2 + s^3}$$

$$T_3(s) = \frac{15.0110 + 15.0815s}{15.0110 + 18.0815s + 4s^2 + s^3}$$

$$T_4(s) = \frac{12.0018 + 15.9047s}{12.0018 + 18.9047 + 4s^2 + s^3}$$

CASE-II:

Initial guess :

$$K_P = 5.000$$

$$K_I = 1.000$$

$$K_D = 0.1000$$

Final values $K_P = 0.7470$, $K_I = 1.0514$, $K_D = 0.2338$

Error = 0.306

Closed loop transfer function will be

$$T(s) = \frac{3[K_I + K_P s + K_D s^2]}{s^3 + (4 + 3K_D)s^2 + 3(1 + K_P)s + 3K_I}$$

$$T(s) = \frac{3.1542 + 2.241s + 0.7014s^2}{3.1542 + 5.241s + 4.2338s^2 + s^3}$$

CASE-III:

Sl. No.	Initial guess		Final Values		w_0 to w_1	Error
	K_P	K_I	K_P	K_I		
A.	5.000	1.000	4.1844	0.9717	0 to 5	1.2417
B.	5.000	1.000	4.9991	1.0014	0 to .25	0.0014
C.	5.000	1.000	4.9942	1.0027	0 to .5	0.0138
D.	5.000	1.000	4.9739	1.0029	0 to 1	0.0938

Closed loop transfer function will be

$$T_A(s) = \frac{2.9151 + 12.5532s}{2.9151 + 15.5532s + 4s^2 + s^3}$$

$$T_B(s) = \frac{3.0042 + 14.9973s}{3.0042 + 17.9973s + 4s^2 + s^3}$$

$$T_C(s) = \frac{3.0081 + 14.9826s}{3.0081 + 17.9826s + 4s^2 + s^3}$$

$$T_D(s) = \frac{3.0087 + 14.9217s}{3.0087 + 17.9217s + 4s^2 + s^3}$$

From all these closed loop transfer functions, we shall determine the time and frequency responses of the systems.

```

DIMENSION S1(100),S2(100),S3(100),E(100),SE(100),DATA(21,3)
COMMON A,B,C,FE,H1,H2,H3,I,H2,H3,PH1,PH2
REAL I1,I2,I3
C
INITIAL GUESS
AKC=5.
I1=1.
I2=0.
I3=0.
H1=1./(-1)
PRINT *,AKC,I1
DO 2 ITER=1,3
  I1=I1+1
  C=C*PLX(3.,I1-4.,**2,.(3.*AKC+3.(-I1**2)))
  H1=H1+2
  A=C*PLX(-3.,I1**2*(3.0+12.*AKC-I1**2),-12.0*I1**3)
  B=C*PLX(9.,-15.0*I1**2,0.)
  PH1=C*PLX(3.,-I1**2,4.0*I1)
  PH2=C*PLX(3.,I1,3.0*AKC*I1)
  DESIRED TRANSFER FUNCTION IS #1, ACTUAL TRANSFER FUNCTION IS #2
  H1=3./PH1
  H2=PH2/D
  DATA(I,1)=H1
  DATA(I,2)=CABS(H1)
  DATA(I,3)=CABS(H2)
  H1=12-H1
  H2=C*LOG(H1)*(A/DD)/2.0
  H3=C*LOG(H1)*(B/DD)/2.0
  H3=C*LOG(H1)*(C/DD)/2.0
  S1(I)=REAL(H1)
  S2(I)=REAL(H2)
  S3(I)=REAL(H3)
  E(I)=(CABS(H1)**2)/2.0
  I1=I1+B
CONTINUE
CALL GRAPHX(DATA,N,1H,5H,I1,H2)
C
CHOOSE THE FOLLOWING STEP SIZES
H1=.1
H2=.1
H3=.1
C
USE THE SIMPSON'S RULE OF INTEGRATION TO COMPUTE THE GRADIENT
CALL SPS(S1,I1,H1,AKC)
AKC=-H1*AKC+AKC
CALL SPS(S2,H1,H1,AKC)
I1=-H2*AKC+I1
CALL SPS(S3,H1,H1,EP)
SE(ITER)=EP
PRINT *,AKC,I1,EP
FOR AT(1,5X,4F10.4)
C
STOP THE ITERATION IF THE ERROR EP IS LESS THAN 0.0001
IF(EP.LE..0001) GO TO 12
=
2
CONTINUE
DO 10 J=1,5
  DATA(I,1)=I
  DATA(I,2)=S1(J)
  DATA(I,3)=S2(J)
  CALL GRAPHX(DATA,5,1H,5H,ERROR)
  STOP
END
SUBROUTINE SPS(Y,H,A,AKC)
DIMENSION Y(1)
DOO=.
EVE=.
I=-3
DO 1 I=I,2
  EVE=EVE+Y(I)
  DOO=DOO+Y(I+1)
  A=(1/3.0)*(Y(I)+4.*(EVE+Y(I+1))+2.*DOO+Y(I+2))
  RETURN
END
CALL GRAPHX(DATA,5,1H,5H,VARDEP)
PRINT *,DATA(21,3),-(121)
PRINT *,I,ITER
FOR AT(1,5X,4F10.4)
PRINT *,VARDEP
FOR AT(1,5X,4F10.4)
PRINT *,THE INDEPENDENT VARIABLE IS ',2A1.1)
PRINT *,VARDEP
FOR AT(1,5X,4F10.4)
PRINT *,THE DEPENDENT VARIABLE IS ',2A1.1)
HIGEST=DATA(1,2)
SAL=DATA(1,2)
DO 1 I=2,
  IF(DATA(I,2).GT.HIGEST)HIGEST=DATA(I,2)

```

178624

LIBRARY UNIVERSITY OF UTAH
 KEMBLER

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40

```

1      C=(DATA(I,2).LT.S AL)S AL=DATA(I,2)
      I=1
      N=2
      C=(DATA(I,2).GT.3IGEST)/IGEST=DATA(I,3)
2      C=(DATA(I,3).LT.S AL)S AL=DATA(I,3)
      I=1
      N=2
      C=(DATA(I,2).LT.S AL)S AL=DATA(I,2)
      I=1
      N=2
3      C=(DATA(I,2).LT.S AL)S AL=DATA(I,2)
      I=1
      N=2
      DATA(I,2)=(DATA(I,2)-S AL)*.7/.7+S+.1
      DATA(I,3)=(DATA(I,3)-S AL)*.7/.7+S+.1
      IDEX=DATA(I,2)
      JDEX=DATA(I,3)
      S(I,DEX)=IH+
      S(J,DEX)=IH*
      PRINT I, DATA(I,1), (B(I,1), I=1,61)
      S(I,DEX)=IH
      S(J,DEX)=IH
4      FOR AT(9X,51.1,35X,1H,4X,211.4, /10X,61(1H*))
100    FOR AT(14L,73.2,1X,61A1)
      RETURN
      END

```


5.0000	1.0000	
5.0001	1.0000	0.0433
5.0002	0.9999	0.0433
5.0003	0.9999	0.0433
5.0004	0.9999	0.0433
5.0005	0.9998	0.0433
5.0005	0.9998	0.0433
5.0006	0.9998	0.0433
5.0007	0.9997	0.0433
5.0008	0.9997	0.0433
5.0009	0.9997	0.0433
5.0010	0.9997	0.0433
5.0011	0.9996	0.0433
5.0012	0.9996	0.0433
5.0013	0.9996	0.0433
5.0014	0.9995	0.0432
5.0015	0.9995	0.0432
5.0016	0.9995	0.0432
5.0016	0.9994	0.0432
5.0017	0.9994	0.0432
5.0018	0.9994	0.0432
5.0019	0.9993	0.0432
5.0020	0.9993	0.0432
5.0021	0.9993	0.0432
5.0022	0.9992	0.0432
5.0023	0.9992	0.0432
5.0024	0.9992	0.0432
5.0025	0.9991	0.0432
5.0026	0.9991	0.0432
5.0026	0.9991	0.0432
5.0027	0.9990	0.0432
5.0028	0.9990	0.0432
5.0029	0.9990	0.0432
5.0030	0.9990	0.0432
5.0031	0.9989	0.0432
5.0032	0.9989	0.0432
5.0033	0.9989	0.0432
5.0034	0.9989	0.0432
5.0035	0.9988	0.0432
5.0036	0.9988	0.0432
5.0037	0.9987	0.0432
5.0037	0.9987	0.0432
5.0038	0.9987	0.0432

5.0079	0.9972	0.0431
5.0080	0.9972	0.0431
5.0081	0.9972	0.0431
5.0082	0.9972	0.0431

5.	1	51
5.	2	51
5.	3	51
5.	4	51
5.	5	52
5.	6	52
5.	7	52
5.	8	52
5.	9	52
5.	10	52
5.	11	52
5.	12	52
5.	13	52
5.	14	52
5.	15	52
5.	16	52
5.	17	52
5.	18	52
5.	19	52
5.	20	52
5.	21	52
5.	22	52
5.	23	52
5.	24	52
5.	25	52
5.	26	52
5.	27	52
5.	28	52
5.	29	52
5.	30	52
5.	31	52

5.011	1.	23	. 521
5.012	1.	24	. 521
5.013	1.	24	. 521
5.014	1.	25	. 521
5.015	1.	26	. 521
5.016	1.	26	. 521
5.017	1.	27	. 521
5.018	1.	27	. 521
5.019	1.	28	. 521
5.020	1.	29	. 521
5.021	1.	29	. 521
5.022	1.	30	. 521
5.023	1.	30	. 521
5.024	1.	31	. 522
5.025	1.	31	. 522
5.026	1.	32	. 522
5.027	1.	32	. 522
5.028	1.	33	. 522
5.029	1.	33	. 522
5.030	1.	34	. 522
5.031	1.	34	. 522
5.032	1.	35	. 522
5.033	1.	35	. 522
5.034	1.	36	. 522
5.035	1.	37	. 522
5.036	1.	37	. 522
5.037	1.	38	. 522
5.038	1.	38	. 522
5.039	1.	39	. 522
5.040	1.	39	. 522
5.041	1.	40	. 522
5.042	1.	40	. 522
5.043	1.	41	. 522
5.044	1.	41	. 522
5.045	1.	42	. 522
5.046	1.	42	. 522
5.047	1.	43	. 522
5.048	1.	43	. 522
5.049	1.	44	. 522
5.050	1.	44	. 522

5.0000	1.0000	
5.0000	1.0000	0.0014
4.9999	1.0001	0.0014
4.9999	1.0001	0.0014
4.9999	1.0002	0.0014
4.9998	1.0002	0.0014
4.9998	1.0003	0.0014
4.9998	1.0003	0.0014
4.9998	1.0004	0.0014
4.9997	1.0004	0.0014
4.9997	1.0005	0.0014
4.9997	1.0005	0.0014
4.9996	1.0006	0.0014
4.9996	1.0006	0.0014
4.9996	1.0007	0.0014
4.9995	1.0007	0.0014
4.9995	1.0008	0.0014
4.9995	1.0008	0.0014
4.9995	1.0009	0.0014
4.9994	1.0009	0.0014
4.9994	1.0010	0.0014
4.9994	1.0010	0.0014
4.9993	1.0011	0.0014
4.9993	1.0011	0.0014
4.9993	1.0012	0.0014
4.9992	1.0012	0.0014
4.9992	1.0012	0.0014
4.9992	1.0013	0.0014
4.9992	1.0013	0.0014
4.9991	1.0014	0.0014
4.9991	1.0014	0.0014

7.1 7.4
77 7.4
7.2 7.4
7.10 7.4
8.0 7.4
8.1 7.4
6.7 7.4
8.2 7.4
8.5 7.4
8.6 7.4
8.7 7.4
8.8 7.4
8.9 7.4
9.0 7.4
9.1 7.4
9.2 7.4
9.3 7.4
9.4 7.4
9.5 7.4
9.6 7.4
9.7 7.4
9.8 7.4
9.9 7.4
10.0 7.4
10.1 7.4
10.2 7.4
10.3 7.4
10.4 7.4
10.5 7.4
10.6 7.4
10.7 7.4
10.8 7.4
10.9 7.4
11.0 7.4
11.1 7.4
11.2 7.4
11.3 7.4
11.4 7.4
11.5 7.4
11.6 7.4
11.7 7.4
11.8 7.4
11.9 7.4
12.0 7.4
12.1 7.4
12.2 7.4
12.3 7.4
12.4 7.4
12.5 7.4
12.6 7.4
12.7 7.4
12.8 7.4
12.9 7.4
13.0 7.4
13.1 7.4
13.2 7.4
13.3 7.4
13.4 7.4
13.5 7.4
13.6 7.4
13.7 7.4
13.8 7.4
13.9 7.4
14.0 7.4
14.1 7.4
14.2 7.4
14.3 7.4
14.4 7.4
14.5 7.4
14.6 7.4
14.7 7.4
14.8 7.4
14.9 7.4
15.0 7.4
15.1 7.4
15.2 7.4
15.3 7.4
15.4 7.4
15.5 7.4
15.6 7.4
15.7 7.4
15.8 7.4
15.9 7.4
16.0 7.4
16.1 7.4
16.2 7.4
16.3 7.4
16.4 7.4
16.5 7.4
16.6 7.4
16.7 7.4
16.8 7.4
16.9 7.4
17.0 7.4
17.1 7.4
17.2 7.4
17.3 7.4
17.4 7.4
17.5 7.4
17.6 7.4
17.7 7.4
17.8 7.4
17.9 7.4
18.0 7.4
18.1 7.4
18.2 7.4
18.3 7.4
18.4 7.4
18.5 7.4
18.6 7.4
18.7 7.4
18.8 7.4
18.9 7.4
19.0 7.4
19.1 7.4
19.2 7.4
19.3 7.4
19.4 7.4
19.5 7.4
19.6 7.4
19.7 7.4
19.8 7.4
19.9 7.4
20.0 7.4

163 1111+1
164 1111+1
165 1111+1
166 1111+1
167 1111+1
168 1111+1
169 1111+1
170 1111+1
171 1111+1
172 1111+1
173 1111+1
174 1111+1
175 1111+1
176 1111+1
177 1111+1
178 1111+1
179 1111+1
180 1111+1
181 1111+1
182 1111+1
183 1111+1
184 1111+1
185 1111+1
186 1111+1
187 1111+1
188 1111+1
189 1111+1
190 1111+1
191 1111+1
192 1111+1
193 1111+1
194 1111+1
195 1111+1
196 1111+1
197 1111+1
198 1111+1
199 1111+1

101 1111+1
102 1111+1
103 1111+1
104 1111+1
105 1111+1
106 1111+1
107 1111+1
108 1111+1
109 1111+1
110 1111+1
111 1111+1
112 1111+1
113 1111+1
114 1111+1
115 1111+1
116 1111+1
117 1111+1
118 1111+1
119 1111+1
120 1111+1
121 1111+1
122 1111+1
123 1111+1
124 1111+1
125 1111+1
126 1111+1
127 1111+1
128 1111+1
129 1111+1
130 1111+1
131 1111+1
132 1111+1
133 1111+1
134 1111+1
135 1111+1
136 1111+1
137 1111+1
138 1111+1
139 1111+1
140 1111+1
141 1111+1
142 1111+1
143 1111+1
144 1111+1
145 1111+1
146 1111+1
147 1111+1
148 1111+1
149 1111+1

1003 1111+1
1004 1111+1
1005 1111+1
1006 1111+1
1007 1111+1
1008 1111+1
1009 1111+1
1010 1111+1
1011 1111+1
1012 1111+1
1013 1111+1
1014 1111+1
1015 1111+1
1016 1111+1
1017 1111+1
1018 1111+1
1019 1111+1
1020 1111+1
1021 1111+1
1022 1111+1
1023 1111+1
1024 1111+1
1025 1111+1
1026 1111+1
1027 1111+1
1028 1111+1
1029 1111+1
1030 1111+1
1031 1111+1
1032 1111+1
1033 1111+1
1034 1111+1
1035 1111+1
1036 1111+1
1037 1111+1
1038 1111+1
1039 1111+1
1040 1111+1
1041 1111+1
1042 1111+1
1043 1111+1
1044 1111+1
1045 1111+1
1046 1111+1
1047 1111+1
1048 1111+1
1049 1111+1

11031 1111+1
11032 1111+1
11033 1111+1
11034 1111+1
11035 1111+1
11036 1111+1
11037 1111+1
11038 1111+1
11039 1111+1
11040 1111+1
11041 1111+1
11042 1111+1
11043 1111+1
11044 1111+1
11045 1111+1
11046 1111+1
11047 1111+1
11048 1111+1
11049 1111+1
11050 1111+1
11051 1111+1
11052 1111+1
11053 1111+1
11054 1111+1
11055 1111+1
11056 1111+1
11057 1111+1
11058 1111+1
11059 1111+1
11060 1111+1
11061 1111+1
11062 1111+1
11063 1111+1
11064 1111+1
11065 1111+1
11066 1111+1
11067 1111+1
11068 1111+1
11069 1111+1
11070 1111+1
11071 1111+1
11072 1111+1
11073 1111+1
11074 1111+1
11075 1111+1
11076 1111+1
11077 1111+1
11078 1111+1
11079 1111+1
11080 1111+1

11081 1111+1
11082 1111+1
11083 1111+1
11084 1111+1
11085 1111+1
11086 1111+1
11087 1111+1
11088 1111+1
11089 1111+1
11090 1111+1
11091 1111+1
11092 1111+1
11093 1111+1
11094 1111+1
11095 1111+1
11096 1111+1
11097 1111+1
11098 1111+1
11099 1111+1
11100 1111+1
11101 1111+1
11102 1111+1
11103 1111+1
11104 1111+1
11105 1111+1
11106 1111+1
11107 1111+1
11108 1111+1
11109 1111+1
11110 1111+1
11111 1111+1
11112 1111+1
11113 1111+1
11114 1111+1
11115 1111+1
11116 1111+1
11117 1111+1
11118 1111+1
11119 1111+1
11120 1111+1
11121 1111+1
11122 1111+1
11123 1111+1
11124 1111+1
11125 1111+1
11126 1111+1
11127 1111+1
11128 1111+1
11129 1111+1
11130 1111+1
11131 1111+1
11132 1111+1
11133 1111+1
11134 1111+1
11135 1111+1
11136 1111+1
11137 1111+1
11138 1111+1
11139 1111+1
11140 1111+1
11141 1111+1
11142 1111+1
11143 1111+1
11144 1111+1
11145 1111+1
11146 1111+1
11147 1111+1
11148 1111+1
11149 1111+1
11150 1111+1

0.1000E+01, 1
DER OF DENOMINATOR POLYNOMIAL IS =, 1

DER OF DENOMINATOR POLYNOMIAL IS =, 2

MINIMUM VALUE OF FREQUENCY IS = 0.1000E+01

MAXIMUM VALUE OF FREQUENCY IS = 0.1000E+04

NUMERATOR COEFFICIENTS ARE

.2500E+02 .4242E+01 E+01
DENOMINATOR COEFFICIENTS ARE

.2500E+02 .7071E+01 0.1000E+01

S.NO	FREQUENCY	PHASE ANGLE	GROUP	AG-1 CODE	PHASE ANGLE
0	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
1	0.100000E+01	0.100000E+01	0.11312068E+02	0.10000014E+01	-0.64813317E+01
2	0.200000E+01	0.100000E+01	0.22624543E+02	0.10000058E+01	-0.12962849E+00
3	0.300000E+01	0.100000E+01	0.33937834E+02	0.10000130E+01	-0.19447388E+00
4	0.400000E+01	0.100000E+01	0.45252346E+02	0.10000231E+01	-0.25927184E+00
5	0.500000E+01	0.100000E+01	0.56566487E+02	0.10000361E+01	-0.32410372E+00
6	0.600000E+01	0.100000E+01	0.67880662E+02	0.10000519E+01	-0.38894488E+00
7	0.700000E+01	0.100000E+01	0.79207286E+02	0.10000706E+01	-0.45379721E+00
8	0.800000E+01	0.100000E+01	0.90530762E+02	0.10000922E+01	-0.51866251E+00
9	0.900000E+01	0.100000E+01	0.10185749E+03	0.10001166E+01	-0.58354264E+00
10	0.100000E+02	0.100000E+01	0.11318788E+03	0.10001440E+01	-0.64843949E+00
11	0.110000E+02	0.100000E+01	0.12452234E+03	0.10001742E+01	-0.71335469E+00
12	0.120000E+02	0.100000E+01	0.13586129E+03	0.10002073E+01	-0.77829071E+00
13	0.130000E+02	0.100000E+01	0.14720511E+03	0.10002432E+01	-0.84324881E+00
14	0.140000E+02	0.100000E+01	0.15855422E+03	0.10002820E+01	-0.90823095E+00
15	0.150000E+02	0.100000E+01	0.16990902E+03	0.10003237E+01	-0.97323906E+00
16	0.160000E+02	0.100000E+01	0.18126993E+03	0.10003682E+01	-0.10382750E+01
17	0.170000E+02	0.100000E+01	0.19263733E+03	0.10004156E+01	-0.11033406E+01
18	0.180000E+02	0.100000E+01	0.20401164E+03	0.10004659E+01	-0.11684377E+01
19	0.190000E+02	0.100000E+01	0.21539327E+03	0.10005189E+01	-0.12335681E+01
20	0.200000E+02	0.100000E+01	0.22678261E+03	0.10005749E+01	-0.12987338E+01
21	0.210000E+02	0.100000E+01	0.23818007E+03	0.10006336E+01	-0.13639364E+01
22	0.220000E+02	0.100000E+01	0.24958606E+03	0.10006952E+01	-0.14291780E+01
23	0.230000E+02	0.100000E+01	0.26100096E+03	0.10007596E+01	-0.14944602E+01
24	0.240000E+02	0.100000E+01	0.27242520E+03	0.10008269E+01	-0.15597850E+01
25	0.250000E+02	0.100000E+01	0.28385915E+03	0.10008970E+01	-0.16251541E+01
26	0.260000E+02	0.100000E+01	0.29530325E+03	0.10009698E+01	-0.16905695E+01
27	0.270000E+02	0.100000E+01	0.30675786E+03	0.10010455E+01	-0.17560329E+01
28	0.280000E+02	0.100000E+01	0.31822340E+03	0.10011240E+01	-0.18215462E+01
29	0.290000E+02	0.100000E+01	0.32970028E+03	0.10012053E+01	-0.18871111E+01
30	0.300000E+02	0.100000E+01	0.34118887E+03	0.10012894E+01	-0.19527296E+01
31	0.310000E+02	0.100000E+01	0.35268960E+03	0.10013762E+01	-0.20184035E+01
32	0.320000E+02	0.100000E+01	0.36420264E+03	0.10014659E+01	-0.20841344E+01
33	0.330000E+02	0.100000E+01	0.37572898E+03	0.10015583E+01	-0.21499243E+01
34	0.340000E+02	0.100000E+01	0.38726846E+03	0.10016534E+01	-0.22157751E+01
35	0.350000E+02	0.100000E+01	0.39882163E+03	0.10017514E+01	-0.22816884E+01
36	0.360000E+02	0.100000E+01	0.41038992E+03	0.10018521E+01	-0.23476662E+01
37	0.370000E+02	0.100000E+01	0.42197068E+03	0.10019556E+01	-0.24137101E+01
38	0.380000E+02	0.100000E+01	0.43356735E+03	0.10020616E+01	-0.24798221E+01
39	0.390000E+02	0.100000E+01	0.44517929E+03	0.100217.52E+01	-0.2546039E+01
40	0.400000E+02	0.100000E+01	0.45680690E+03	0.10022821E+01	-0.26122572E+01
41	0.410000E+02	0.100000E+01	0.46845056E+03	0.10023950E+01	-0.26785842E+01
42	0.420000E+02	0.100000E+01	0.48011067E+03	0.10025133E+01	-0.27449860E+01
43	0.430000E+02	0.100000E+01	0.49178763E+03	0.10026330E+01	-0.28114549E+01

44	0.4400	3E+00	0.101190E+01	- .5318178E-01	0.1002755E+01	-0.20750225E+01
45	0.4500	3E+00	0.1015503E+01	- .5151939E-01	0.1002860E+01	-0.20740008E+01
46	0.4600	3E+00	0.1016231E+01	- .5209233E-01	0.1003081E+01	-0.20711381E+01
47	0.4700	3E+00	0.1016911E+01	- .53867155E-01	0.1003138E+01	-0.20781601E+01
48	0.4800	3E+00	0.1017603E+01	- .55003845E-01	0.10032715E+01	-0.21450765E+01
49	0.4900	3E+00	0.1018370E+01	- .50222153E-01	0.10034071E+01	-0.21210516E+01
50	0.5000	3E+00	0.1019179E+01	- .11318788E-01	0.1003441E+01	-0.206134391E+00
51	0.2000	3E+00	0.1000378E+01	- .22070261E-01	0.10005749E+01	-0.12987338E+01
52	0.3000	3E+00	0.1000779E+01	- .31118886E-01	0.10012894E+01	-0.19527295E+01
53	0.4000	3E+00	0.1001240E+01	- .45680687E-01	0.10022821E+01	-0.26122571E+01
54	0.5000	3E+00	0.1001922E+01	- .57403707E-01	0.10035453E+01	-0.32791218E+01
55	0.6000	3E+00	0.1002675E+01	- .69324262E-01	0.10050692E+01	-0.39550959E+01
56	0.7000	3E+00	0.1003539E+01	- .81481074E-01	0.10068418E+01	-0.46419059E+01
57	0.8000	3E+00	0.1004468E+01	- .93910955E-01	0.10088434E+01	-0.53412429E+01
58	0.9000	3E+00	0.1005432E+01	- .10664600E+00	0.10111720E+01	-0.60547138E+01
59	0.1000	3E+01	0.1006399E+01	- .11971854E+00	0.10134953E+01	-0.67838725E+01
60	0.1100	3E+01	0.1007332E+01	- .13315773E+00	0.10161950E+01	-0.75301877E+01
61	0.1200	3E+01	0.1008189E+01	- .14698972E+00	0.10188482E+01	-0.82950398E+01
62	0.1300	3E+01	0.1008926E+01	- .16123724E+00	0.10217286E+01	-0.90797071E+01
63	0.1400	3E+01	0.1009494E+01	- .17591911E+00	0.10247081E+01	-0.98853583E+01
64	0.1500	3E+01	0.1009820E+01	- .19104908E+00	0.10277558E+01	-0.10713039E+02
65	0.1600	3E+01	0.1010091E+01	- .20663839E+00	0.10308639E+01	-0.11563000E+02
66	0.1700	3E+01	0.1010305E+01	- .22268918E+00	0.10339227E+01	-0.12437992E+02
67	0.1800	3E+01	0.1010469E+01	- .23920002E+00	0.10369701E+01	-0.13330640E+02
68	0.18999999E+01	3E+01	0.10107399E+01	- .25616240E+00	0.10399426E+01	-0.14260073E+02
69	0.19999999E+01	3E+01	0.10106279E+01	- .27350087E+00	0.10428001E+01	-0.15208544E+02
70	0.20999999E+01	3E+01	0.10104791E+01	- .29137260E+00	0.10455013E+01	-0.16182150E+02
71	0.21999999E+01	3E+01	0.10102395E+01	- .30950741E+00	0.10480004E+01	-0.17180787E+02
72	0.22999999E+01	3E+01	0.99704929E+00	- .32810694E+00	0.10502007E+01	-0.18204158E+02
73	0.23999999E+01	3E+01	0.9934089E+00	- .34694522E+00	0.10522435E+01	-0.19251759E+02
74	0.24999999E+01	3E+01	0.9882949E+00	- .36602847E+00	0.10539951E+01	-0.20322887E+02
75	0.25999999E+01	3E+01	0.9823190E+00	- .38529542E+00	0.10551793E+01	-0.21416630E+02
76	0.26999999E+01	3E+01	0.9754362E+00	- .40467774E+00	0.10556000E+01	-0.22531875E+02
77	0.27999999E+01	3E+01	0.9676282E+00	- .42410075E+00	0.10564875E+01	-0.23667315E+02
78	0.28999999E+01	3E+01	0.9588152E+00	- .44348422E+00	0.10564386E+01	-0.24821451E+02
79	0.29999999E+01	3E+01	0.94907571E+00	- .46270344E+00	0.10555770E+01	-0.25992610E+02
80	0.30999999E+01	3E+01	0.9383162E+00	- .48179035E+00	0.10537743E+01	-0.27178954E+02
81	0.31999999E+01	3E+01	0.9265129E+00	- .50053494E+00	0.10510616E+01	-0.28378499E+02
82	0.32999999E+01	3E+01	0.9138096E+00	- .51888672E+00	0.10474527E+01	-0.29589135E+02
83	0.33999999E+01	3E+01	0.9001831E+00	- .53675614E+00	0.10429910E+01	-0.30808647E+02
84	0.34999999E+01	3E+01	0.8854901E+00	- .55405625E+00	0.10376531E+01	-0.32034739E+02

88	0.38999999E+01	0.671324E+01	-0.61544379E+00	0.10235681E+01	-0.3695755E+02
89	0.39999999E+01	0.6724197E+01	-0.6293333E+00	0.1018093E+01	-0.3816102E+02
90	0.40999999E+01	0.6733754E+01	-0.6417101E+00	0.10110521E+01	-0.39397107E+02
91	0.41999999E+01	0.67417386E+01	-0.65318171E+00	0.10034777E+01	-0.40603335E+02
92	0.42999999E+01	0.67478686E+01	-0.6633609E+00	0.99539526E+00	-0.41797978E+02
93	0.43999999E+01	0.675197314E+01	-0.67275529E+00	0.98668358E+00	-0.42979972E+02
94	0.44999999E+01	0.675467851E+01	-0.68131822E+00	0.97783234E+00	-0.44140536E+02
95	0.46000000E+01	0.681266893E+01	-0.68827156E+00	0.96882182E+00	-0.45293023E+02
96	0.47000000E+01	0.68181884E+01	-0.69448426E+00	0.95883961E+00	-0.46422939E+02
97	0.48000000E+01	0.68191132E+01	-0.69969337E+00	0.94852383E+00	-0.47532952E+02
98	0.49000000E+01	0.68211621E+01	-0.70392533E+00	0.93611245E+00	-0.48621892E+02
99	0.50000000E+01	0.682063996E+01	-0.70719718E+00	0.92134953E+00	-0.49733972E+01
100	0.52000000E+01	0.68162785E+01	-0.72735618E+00	0.90428771E+00	-0.51208545E+02
101	0.53000000E+01	0.68497569E+01	-0.76274346E+00	0.88556770E+00	-0.525992612E+02
102	0.54000000E+01	0.68028196E+01	-0.76293303E+00	0.86180903E+00	-0.538181021E+02
103	0.55000000E+01	0.67077111E+01	-0.76721358E+00	0.92744329E+00	-0.49688745E+02
104	0.60000000E+01	0.64901136E+01	-0.69799658E+00	0.81410156E+00	-0.59023990E+02
105	0.70000000E+01	0.28743184E+01	-0.64454161E+00	0.70572726E+00	-0.65965652E+02
106	0.80000000E+01	0.2008759E+00	-0.57997553E+00	0.61351969E+00	-0.70965942E+02
107	0.90000000E+01	0.14325652E+00	-0.51897477E+00	0.53838392E+00	-0.74568523E+02
108	0.10000000E+02	0.10581212E+00	-0.46585444E+00	0.47772017E+00	-0.77213235E+02
109	0.11000000E+02	0.8590226E-01	-0.42024106E+00	0.42847348E+00	-0.79109929E+02
110	0.12000000E+02	0.6291516E-01	-0.38291319E+00	0.3884671E+00	-0.80609997E+02
111	0.13000000E+02	0.50318553E-01	-0.35084182E+00	0.35403165E+00	-0.81938195E+02
112	0.14000000E+02	0.4168256E-01	-0.32352669E+00	0.32012266E+00	-0.82765035E+02
113	0.15000000E+02	0.3418827E-01	-0.30006379E+00	0.30199615E+00	-0.83511946E+02
114	0.16000000E+02	0.2876021E-01	-0.27973448E+00	0.2812993E+00	-0.84129971E+02
115	0.17000000E+02	0.24570257E-01	-0.26197311E+00	0.2631228E+00	-0.84641977E+02
116	0.18000000E+02	0.21232055E-01	-0.24633431E+00	0.24724767E+00	-0.85073574E+02
117	0.19000000E+02	0.18533061E-01	-0.23246564E+00	0.23320323E+00	-0.85441631E+02
118	0.20000000E+02	0.1632461E-01	-0.2200661E+00	0.220069039E+00	-0.85759030E+02
119	0.21000000E+02	0.14484951E-01	-0.20896976E+00	0.20947118E+00	-0.86034659E+02
120	0.22000000E+02	0.12945744E-01	-0.19693337E+00	0.19935416E+00	-0.86276714E+02
121	0.23000000E+02	0.1164241E-01	-0.18982704E+00	0.19016373E+00	-0.86490382E+02
122	0.24000000E+02	0.1052909E-01	-0.18152709E+00	0.18183219E+00	-0.86680439E+02
123	0.25000000E+02	0.9570223E-02	-0.17303071E+00	0.17419382E+00	-0.86850546E+02
124	0.26000000E+02	0.87389771E-02	-0.16695177E+00	0.16716033E+00	-0.87003658E+02
125	0.27000000E+02	0.8013721E-02	-0.16095175E+00	0.16071747E+00	-0.87142187E+02
126	0.28000000E+02	0.73751653E-02	-0.15456647E+00	0.15471231E+00	-0.87263115E+02
127	0.29000000E+02	0.68122957E-02	-0.1490556E+00	0.14920126E+00	-0.87363105E+02
128	0.30000000E+02	0.63123290E-02	-0.1439069E+00	0.14400026E+00	-0.87448074E+02
129	0.31000000E+02	0.58663656E-02	-0.1391199E+00	0.13920357E+00	-0.87585032E+02
130	0.32000000E+02	0.54668333E-02	-0.1346403E+00	0.13475277E+00	-0.87700911E+02
131	0.33000000E+02	0.5107000E-02	-0.1304555E+00	0.1305053E+00	-0.87757033E+02

132	0.3400000E+02	0.4767444E-02	0.1200000E+00	0.2000000E+00
133	0.3500000E+02	0.446891555E-02	0.12279035E+00	0.12280137E+00
134	0.3600000E+02	0.4216211E-02	0.11930507E+00	0.11938031E+00
135	0.3700000E+02	0.39778827E-02	0.11600701E+00	0.11607519E+00
136	0.3800000E+02	0.37504638E-02	0.11265736E+00	0.11294981E+00
137	0.3900000E+02	0.35505907E-02	0.10993204E+00	0.10998981E+00
138	0.4000000E+02	0.33626680E-02	0.10712954E+00	0.10718231E+00
139	0.4100000E+02	0.31895327E-02	0.10446070E+00	0.10445157E+00
140	0.4200000E+02	0.30296034E-02	0.10193467E+00	0.10197968E+00
141	0.4300000E+02	0.28915737E-02	0.99523011E-01	0.99561719E-01
142	0.4400000E+02	0.27442798E-02	0.97223604E-01	0.97262326E-01
143	0.4500000E+02	0.26166983E-02	0.95028749E-01	0.95064769E-01
144	0.4600000E+02	0.24979280E-02	0.92931432E-01	0.92964998E-01
145	0.4700000E+02	0.23871589E-02	0.90925261E-01	0.90956593E-01
146	0.4800000E+02	0.22836903E-02	0.88900439E-01	0.88933684E-01
147	0.4900000E+02	0.21863855E-02	0.87163467E-01	0.87197897E-01
148	0.1000000E+02	0.10581212E+00	0.46585444E+00	0.47772017E+00
149	0.2000000E+02	0.1632464E-01	0.22008610E+00	0.22069039E+00
150	0.3000000E+02	0.63123290E-02	0.14390989E+00	0.14404826E+00
151	0.4000000E+02	0.33626888E-02	0.10712954E+00	0.10718231E+00
152	0.5000000E+02	0.20951790E-02	0.85397576E-01	0.85423299E-01
153	0.6000000E+02	0.14345344E-02	0.71024187E-01	0.71038673E-01
154	0.7000000E+02	0.100445660E-02	0.60804727E-01	0.60813699E-01
155	0.8000000E+02	0.74508289E-03	0.53162105E-01	0.53168345E-01
156	0.9000000E+02	0.62568665E-03	0.47229954E-01	0.47234098E-01
157	0.1000000E+03	0.50531159E-03	0.42400499E-01	0.42493504E-01
158	0.1100000E+03	0.41674193E-03	0.38616637E-01	0.38618866E-01
159	0.1200000E+03	0.34960645E-03	0.35390845E-01	0.35392571E-01
160	0.1300000E+03	0.29750980E-03	0.32662908E-01	0.32664263E-01
161	0.1400000E+03	0.25626650E-03	0.30325739E-01	0.30326822E-01
162	0.1500000E+03	0.22305100E-03	0.28300932E-01	0.28301811E-01
163	0.1600000E+03	0.19591219E-03	0.26529751E-01	0.26530474E-01
164	0.1700000E+03	0.17344516E-03	0.24967326E-01	0.24967929E-01
165	0.1800000E+03	0.15463672E-03	0.23578786E-01	0.23579293E-01
166	0.1900000E+03	0.13873276E-03	0.22336622E-01	0.22337053E-01
167	0.2000000E+03	0.12516412E-03	0.21218837E-01	0.21219207E-01
168	0.2100000E+03	0.11349461E-03	0.20207634E-01	0.20207953E-01
169	0.2200000E+03	0.10338540E-03	0.19238459E-01	0.19244736E-01
170	0.2300000E+03	0.94570300E-04	0.18419290E-01	0.18449533E-01
171	0.2400000E+03	0.86356649E-04	0.17680115E-01	0.17680329E-01
172	0.2500000E+03	0.79015046E-04	0.16972526E-01	0.16972715E-01
173	0.2600000E+03	0.73967245E-04	0.16319409E-01	0.16319570E-01
174	0.2700000E+03	0.6956432E-04	0.15710715E-01	0.15710854E-01

176	0.2900	E+03	0.59133672E-04	-0.1163186E-01	0.14631607E-01	-0.89767261E+02
177	0.3000	E+03	0.55532154E-04	-0.11142620E-01	0.14142729E-01	-0.89775058E+02
178	0.3100	E+03	0.52012537E-04	-0.10650245E-01	0.13646344E-01	-0.89782332E+02
179	0.3200	E+03	0.48799257E-04	-0.10258119E-01	0.13253499E-01	-0.89789119E+02
180	0.3300	E+03	0.45883193E-04	-0.12356514E-01	0.12855596E-01	-0.89795553E+02
181	0.3400	E+03	0.43221994E-04	-0.12478270E-01	0.12478345E-01	-0.89801578E+02
182	0.3500	E+03	0.40781021E-04	-0.12121650E-01	0.12121719E-01	-0.89807259E+02
183	0.3600	E+03	0.38547655E-04	-0.11741850E-01	0.11744913E-01	-0.89812622E+02
184	0.3700	E+03	0.3649179E-04	-0.11466262E-01	0.11466320E-01	-0.89817696E+02
185	0.3800	E+03	0.34593274E-04	-0.11164447E-01	0.11164511E-01	-0.89822501E+02
186	0.3900	E+03	0.32841561E-04	-0.10876116E-01	0.10878165E-01	-0.89827060E+02
187	0.4000	E+03	0.31217790E-04	-0.10606105E-01	0.10606151E-01	-0.89831389E+02
188	0.4100	E+03	0.29712123E-04	-0.10347368E-01	0.10347411E-01	-0.89835508E+02
189	0.4200	E+03	0.28313398E-04	-0.10100955E-01	0.10100995E-01	-0.89839431E+02
190	0.4300	E+03	0.27011926E-04	-0.98660062E-02	0.98660432E-02	-0.89843170E+02
191	0.4400	E+03	0.25796324E-04	-0.96417345E-02	0.96417740E-02	-0.89846739E+02
192	0.4500	E+03	0.24661859E-04	-0.94274431E-02	0.94274755E-02	-0.89850149E+02
193	0.4600	E+03	0.23601631E-04	-0.92224659E-02	0.92224962E-02	-0.89853412E+02
194	0.4700	E+03	0.22615471E-04	-0.90262133E-02	0.90262417E-02	-0.89856534E+02
195	0.4800	E+03	0.21673941E-04	-0.88381397E-02	0.88381664E-02	-0.89859526E+02
196	0.4900	E+03	0.20779764E-04	-0.86577443E-02	0.86577693E-02	-0.89862396E+02
197	0.5000	E+03	0.51534159E-03	-0.42490499E-01	0.42493504E-01	-0.89318644E+02
198	0.2000	E+03	0.12516412E-03	-0.21218837E-01	0.21219207E-01	-0.89662065E+02
199	0.3000	E+03	0.55532154E-04	-0.14142620E-01	0.14142729E-01	-0.89775058E+02
200	0.4000	E+03	0.31217790E-04	-0.10606105E-01	0.10606151E-01	-0.89831389E+02
201	0.5000	E+03	0.19973761E-04	-0.84845660E-02	0.84845895E-02	-0.89865151E+02
202	0.6000	E+03	0.13956545E-04	-0.70703275E-02	0.70703411E-02	-0.89887647E+02
203	0.7000	E+03	0.1189195E-04	-0.60602063E-02	0.60602148E-02	-0.89903709E+02
204	0.8000	E+03	0.77998695E-05	-0.53026382E-02	0.53026439E-02	-0.89915754E+02
205	0.9000	E+03	0.61525068E-05	-0.47134304E-02	0.47134345E-02	-0.89925121E+02
206	0.1000	E+04	0.49915650E-05	-0.42420707E-02	0.42420737E-02	-0.89932614E+02
207	0.1100	E+04	0.41251708E-05	-0.38564168E-02	0.38564190E-02	-0.89938745E+02

89	0.39994180E+1	0.39994180E+1	0.12144211E+11	0.12150977E+11	0.380877E+12
90	0.41994180E+1	0.41994180E+1	0.11855311E+11	0.11862885E+11	0.91591215E+12
91	0.43994180E+1	0.43994180E+1	0.11496711E+11	0.11542676E+11	0.95122554E+12
92	0.45994180E+1	0.45994180E+1	0.11084980E+11	0.11212163E+11	0.96501495E+12
93	0.47994180E+1	0.47994180E+1	0.10624055E+11	0.10852154E+11	0.10148516E+13
94	0.49994180E+1	0.49994180E+1	0.10114221E+11	0.10477182E+11	0.10453367E+13
95	0.51994180E+1	0.51994180E+1	0.95394862E+10	0.10114119E+11	0.10744431E+13
96	0.53994180E+1	0.53994180E+1	0.91315178E+10	0.97297924E+10	0.11021416E+13
97	0.55994180E+1	0.55994180E+1	0.86243764E+10	0.93583044E+10	0.11264265E+13
98	0.57994180E+1	0.57994180E+1	0.81231775E+10	0.89926758E+10	0.11533179E+13
99	0.59994180E+1	0.59994180E+1	0.72782316E+10	0.10159668E+11	0.12955080E+12
100	0.62004180E+1	0.62004180E+1	0.53698102E+10	0.11303988E+11	0.28311913E+12
101	0.63004180E+1	0.63004180E+1	0.11293615E+11	0.12861443E+11	0.53104664E+12
102	0.64004180E+1	0.64004180E+1	0.12142108E+11	0.12150977E+11	0.880678E+12
103	0.65004180E+1	0.65004180E+1	0.75473356E+10	0.86360241E+10	0.11764499E+13
104	0.66004180E+1	0.66004180E+1	0.46719956E+10	0.57535571E+10	0.13501859E+13
105	0.67004180E+1	0.67004180E+1	0.22951937E+10	0.40034023E+10	0.14501863E+13
106	0.68004180E+1	0.68004180E+1	0.14064402E+10	0.29344242E+10	0.15131651E+13
107	0.69004180E+1	0.69004180E+1	0.92643015E+09	0.22442686E+10	0.15561914E+13
108	0.70004180E+1	0.70004180E+1	0.61313125E+09	0.17741995E+10	0.15874631E+13
109	0.71004180E+1	0.71004180E+1	0.46561568E+09	0.14395204E+10	0.16112825E+13
110	0.72004180E+1	0.72004180E+1	0.34533262E+09	0.11925271E+10	0.16300619E+13
111	0.73004180E+1	0.73004180E+1	0.26874275E+09	0.10048365E+10	0.16452894E+13
112	0.74004180E+1	0.74004180E+1	0.21075577E+09	0.85872545E+09	0.16579016E+13
113	0.75004180E+1	0.75004180E+1	0.16851194E+09	0.74266054E+09	0.16685356E+13
114	0.76004180E+1	0.76004180E+1	0.13752128E+09	0.64886634E+09	0.16776356E+13
115	0.77004180E+1	0.77004180E+1	0.11352708E+09	0.57195023E+09	0.16855132E+13
116	0.78004180E+1	0.78004180E+1	0.91844798E+08	0.50805672E+09	0.16924052E+13
117	0.79004180E+1	0.79004180E+1	0.71076714E+08	0.45438972E+09	0.16984950E+13
118	0.80004180E+1	0.80004180E+1	0.56224979E+08	0.40885919E+09	0.17039151E+13
119	0.81004180E+1	0.81004180E+1	0.46665114E+08	0.36969072E+09	0.17087744E+13
120	0.82004180E+1	0.82004180E+1	0.37764035E+08	0.33627433E+09	0.17131526E+13
121	0.83004180E+1	0.83004180E+1	0.31263194E+08	0.30706762E+09	0.17171212E+13
122	0.84004180E+1	0.84004180E+1	0.27182777E+08	0.28152783E+09	0.17217360E+13
123	0.85004180E+1	0.85004180E+1	0.24379768E+08	0.25916245E+09	0.17249429E+13
124	0.86004180E+1	0.86004180E+1	0.21330131E+08	0.23919628E+09	0.17278850E+13
125	0.87004180E+1	0.87004180E+1	0.17715136E+08	0.22154038E+09	0.17296860E+13
126	0.88004180E+1	0.88004180E+1	0.14474438E+08	0.20577769E+09	0.17321750E+13
127	0.89004180E+1	0.89004180E+1	0.11737171E+08	0.19103591E+09	0.17344752E+13
128	0.90004180E+1	0.90004180E+1	0.94501717E+07	0.17892678E+09	0.17371050E+13
129	0.91004180E+1	0.91004180E+1	0.77300070E+07	0.16743717E+09	0.17391956E+13
130	0.92004180E+1	0.92004180E+1	0.61001400E+07	0.15723892E+09	0.17411456E+13
131	0.93004180E+1	0.93004180E+1	0.46001000E+07	0.14755533E+09	0.17429700E+13

131	0.350	0.000	-0.1317134	-1	-0.13391770	-2	0.1339277E+1	-1	-0.1746870	+3
132	0.350	0.000	-0.1317134	-1	-0.13281752	-2	0.13112453E+1	-1	-0.1746516	+3
133	0.350	0.000	-0.1317134	-1	-0.11250451	-2	0.12378465E+1	-1	-0.17471239	+3
134	0.370	0.000	-0.1167101	-1	-0.11390940	-2	0.11713017E+1	-01	-0.17492615	+3
135	0.380	0.000	-0.1157111	-1	-0.96548200	-3	0.11099948E+1	-1	-0.17506213	+3
137	0.390	0.000	-0.1094171	-1	-0.83121670	-3	0.10533891E+1	-01	-0.17519156	+3
138	0.410	0.000	-0.9470171	-2	-0.11793181	-3	0.10111431E+1	-01	-0.17531310	+3
139	0.410	0.000	-0.9440173	-2	-0.75911150	-3	0.96240930E+02	-02	-0.17542930	+3
141	0.420	0.000	-0.9162730	-2	-0.75038970	-3	0.94736109E+02	-02	-0.17553876	+3
141	0.430	0.000	-0.8819772	-2	-0.55715020	-3	0.86539050E+02	-02	-0.17564498	+3
142	0.440	0.000	-0.8501537	-2	-0.41321570	-3	0.82621280E+02	-02	-0.17574532	+3
143	0.450	0.000	-0.7876712	-2	-0.57276970	-3	0.78976083E+02	-02	-0.17584110	+3
144	0.450	0.000	-0.7537270	-2	-0.53130077E+03	-03	0.75502298E+02	-02	-0.17593205	+3
145	0.470	0.000	-0.7219130	-2	-0.5225125	-3	0.72304590E+02	-02	-0.17602023	+3
146	0.480	0.000	-0.6921110	-2	-0.47131137	-3	0.69300719E+02	-02	-0.17610419	+3
147	0.490	0.000	-0.6641351	-2	-0.44200711E+03	-03	0.66551260E+02	-02	-0.17618081	+3
148	0.100	0.000	-0.1651531	-1	-0.54313125E+01	-1	0.17741945E+01	-01	-0.15674661	+3
149	0.200	0.000	-0.1311311	-1	-0.60242979E+02	-12	0.14885909E+01	-01	-0.17639151	+3
150	0.300	0.000	-0.1770493	-1	-0.19010780	-2	0.17692070E+01	-01	-0.17371100	+3
151	0.400	0.000	-0.9970570	-2	-0.81733291E+03	-13	0.10010149E+01	-01	-0.17531310	+3
152	0.500	0.000	-0.5376072	-2	-0.11600070E+03	-13	0.63914055E+02	-02	-0.17620100	+3
153	0.600	0.000	-0.1251920	-2	-0.24300003E+03	-13	0.44317212E+02	-02	-0.17680900	+3
154	0.700	0.000	-0.3249701	-2	-0.15117450E+03	-13	0.32532751E+02	-02	-0.17733657	+3
155	0.800	0.000	-0.2447108	-2	-0.11109510E+03	-13	0.24894573E+02	-02	-0.17767157	+3
156	0.900	0.000	-0.1904783	-2	-0.71722020E+04	-14	-0.19002572E+02	-02	-0.17793005	+3
157	1.000	0.000	-0.1511000	-2	-0.51733102E+04	-14	0.15922504E+02	-02	-0.17813810	+3
158	0.110	0.000	-0.1315402	-2	-0.30860110E+02	-12	0.13156540E+02	-02	-0.17830701	+3
159	0.120	0.000	-0.1110740	-2	-0.29917670E+02	-12	0.11153510E+02	-02	-0.17840990	+3
160	0.130	0.000	-0.9410519	-3	-0.25520010E+01	-11	0.94172970E+00	-00	-0.17650809	+3
161	0.140	0.000	-0.6117901	-3	-0.10832070E+01	-10	0.81192700E+00	-00	-0.17867100	+3
162	0.150	0.000	-0.7170415	-3	-0.15309030E+01	-10	0.70722710E+00	-00	-0.17870970	+3
163	0.160	0.000	-0.6210250	-3	-0.12612090E+01	-10	0.62154095E+00	-00	-0.17683730	+3
164	0.170	0.000	-0.5510600	-3	-0.10510390E+01	-10	0.55054670E+00	-00	-0.17690570	+3
165	0.180	0.000	-0.4997509	-3	-0.35500120E+01	-15	0.49105530E+00	-00	-0.17895660	+3
166	0.190	0.000	-0.4560805	-3	-0.7531330E+00	-15	0.44070990E+00	-00	-0.17902100	+3
167	0.200	0.000	-0.3797000	-3	-0.5537000E+00	-15	0.39772070E+00	-00	-0.17907020	+3
168	0.210	0.000	-0.3000000	-3	-0.5570000E+00	-15	0.36074230E+00	-00	-0.17911030	+3
169	0.220	0.000	-0.3200970	-3	-0.48100017E+00	-15	0.34200050E+00	-00	-0.17915000	+3
170	0.230	0.000	-0.3160000	-3	-0.3200000E+00	-15	0.3071950E+00	-00	-0.17919100	+3
171	0.240	0.000	-0.2710000	-3	-0.3735300E+00	-15	0.27617091E+00	-00	-0.17922511	+3
172	0.250	0.000	-0.2500000	-3	-0.3300000E+00	-15	0.25005207E+00	-00	-0.17925612	+3
173	0.260	0.000	-0.2300000	-3	-0.2377000E+00	-15	0.23551557E+00	-00	-0.17929074	+3
174	0.270	0.000	-0.2100000	-3	-0.2320000E+00	-15	0.21820490E+00	-00	-0.17931125	+3

176	0.29	-	-	0.1891495E-3	-	0.2116171E-3	0.1191110E-3	-	0.1753547E+3
177	0.30	+	+	0.1707352E-3	-	0.1912218E-3	0.1767018E-3	-	0.1793615E+3
178	0.31	+	+	0.1551176E-3	-	0.1731032E-3	0.1655263E-3	-	0.1794015E+3
179	0.32	+	+	0.1553652E-3	-	0.1575592E-3	0.1553363E-3	-	0.1794101E+3
180	0.33	+	+	0.1410661E-3	-	0.1436616E-3	0.1267056E-3	-	0.1794365E+3
181	0.34	+	+	0.1375915E-3	-	0.1313531E-3	0.1375972E-3	-	0.1794531E+3
182	0.35	+	+	0.1298195E-3	-	0.1201162E-3	0.1296461E-3	-	0.1794697E+3
183	0.36	+	+	0.1227276E-3	-	0.1119523E-3	0.1227321E-3	-	0.1794834E+3
184	0.37	+	+	0.1151625E-3	-	0.1119159E-3	0.1161671E-3	-	0.1794974E+3
185	0.38	+	+	0.1111771E-3	-	0.9002671E-3	0.1111516E-3	-	0.1795106E+3
186	0.39	+	+	0.1057161E-3	-	0.8712864E-3	0.1045759E-3	-	0.1795232E+3
187	0.40	+	+	0.9941615E-3	-	0.8056297E-3	0.9941132E-3	-	0.1795351E+3
188	0.41	+	+	0.9451769E-3	-	0.7491302E-3	0.9462161E-3	-	0.1795465E+3
189	0.42	+	+	0.9165725E-3	-	0.6967742E-3	0.9016647E-3	-	0.1795575E+3
190	0.43	+	+	0.8612162E-3	-	0.6092423E-3	0.8602315E-3	-	0.1795670E+3
191	0.44	+	+	0.8215488E-3	-	0.6051175E-3	0.8215712E-3	-	0.1795774E+3
192	0.45	+	+	0.7954426E-3	-	0.5665167E-3	0.7954671E-3	-	0.1795868E+3
193	0.46	+	+	0.7516094E-3	-	0.5305353E-3	0.7516796E-3	-	0.1795950E+3
194	0.47	+	+	0.7014791E-3	-	0.4472111E-3	0.7013195E-3	-	0.1796041E+3
195	0.48	+	+	0.6032591E-3	-	0.4667716E-3	0.6034169E-3	-	0.1796126E+3
196	0.49	+	+	0.5614361E-3	-	0.4337739E-3	0.5624517E-3	-	0.1796216E+3
197	0.50	+	+	0.4511946E-3	-	0.5171329E-3	0.4592251E-3	-	0.1796301E+3
198	0.51	+	+	0.3475763E-3	-	0.6455756E-3	0.3577267E-3	-	0.1796392E+3
199	0.52	+	+	0.1717352E-3	-	0.1911208E-3	0.1767608E-3	-	0.1796490E+3
200	0.53	+	+	0.9911051E-3	-	0.6064267E-3	0.9911327E-3	-	0.1796581E+3
201	0.54	+	+	0.6352139E-3	-	0.1247315E-3	0.6362106E-3	-	0.1796675E+3
202	0.55	+	+	0.4113451E-3	-	0.2333225E-3	0.4161097E-3	-	0.1796774E+3
203	0.56	+	+	0.3215495E-3	-	0.1506939E-3	0.3245931E-3	-	0.1796877E+3
204	0.57	+	+	0.2151324E-3	-	0.1008166E-3	0.2165152E-3	-	0.1796983E+3
205	0.58	+	+	0.1963557E-3	-	0.7081718E-3	0.1963576E-3	-	0.1797092E+3
206	0.59	+	+	0.1591790E-3	-	0.5161816E-3	0.1591467E-3	-	0.1797202E+3
207	0.60	+	+	0.1314455E-3	-	0.3473113E-3	0.1314450E-3	-	0.1797312E+3

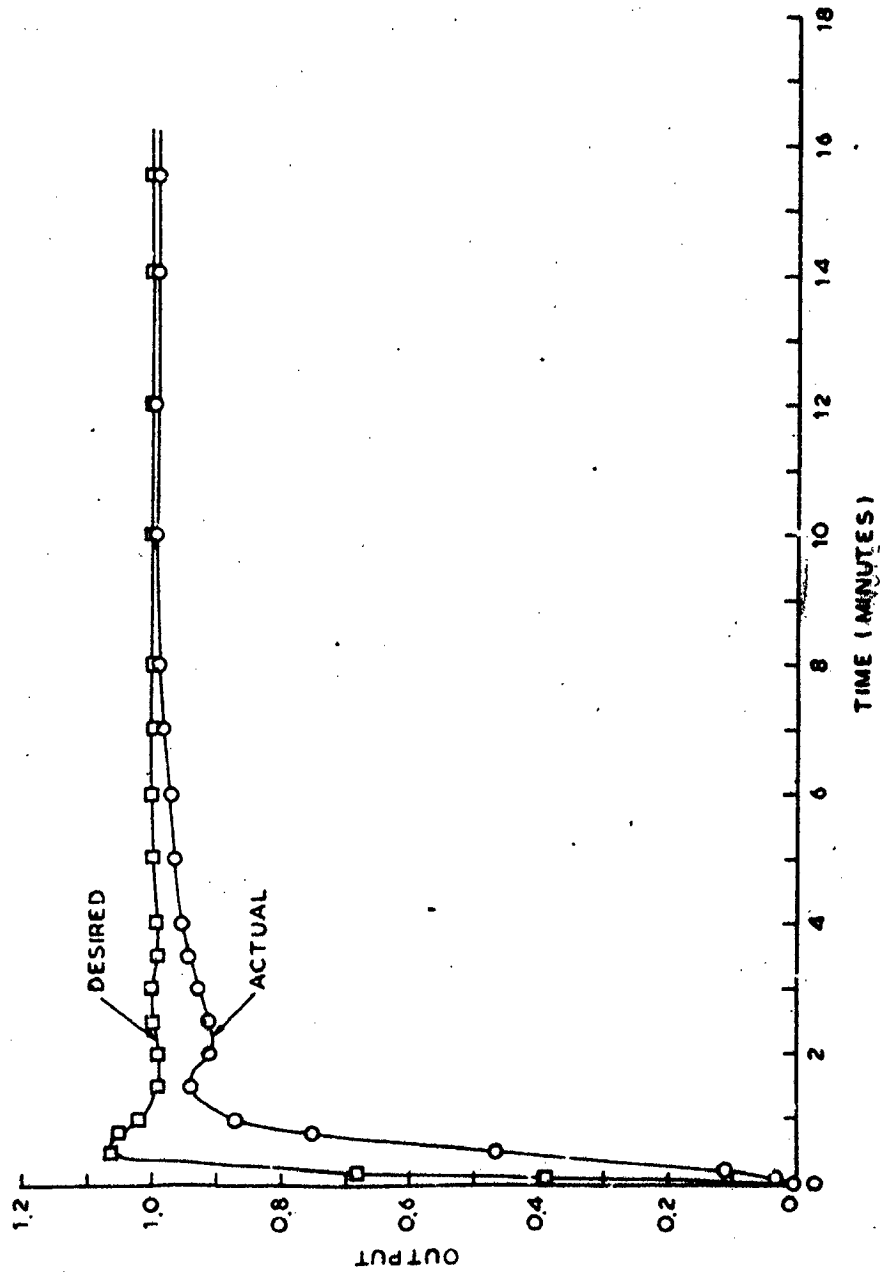


FIG TIME RESPONSE FOR EXAMPLE 1 (CASE 1 ($\omega = 0$ TO 5))

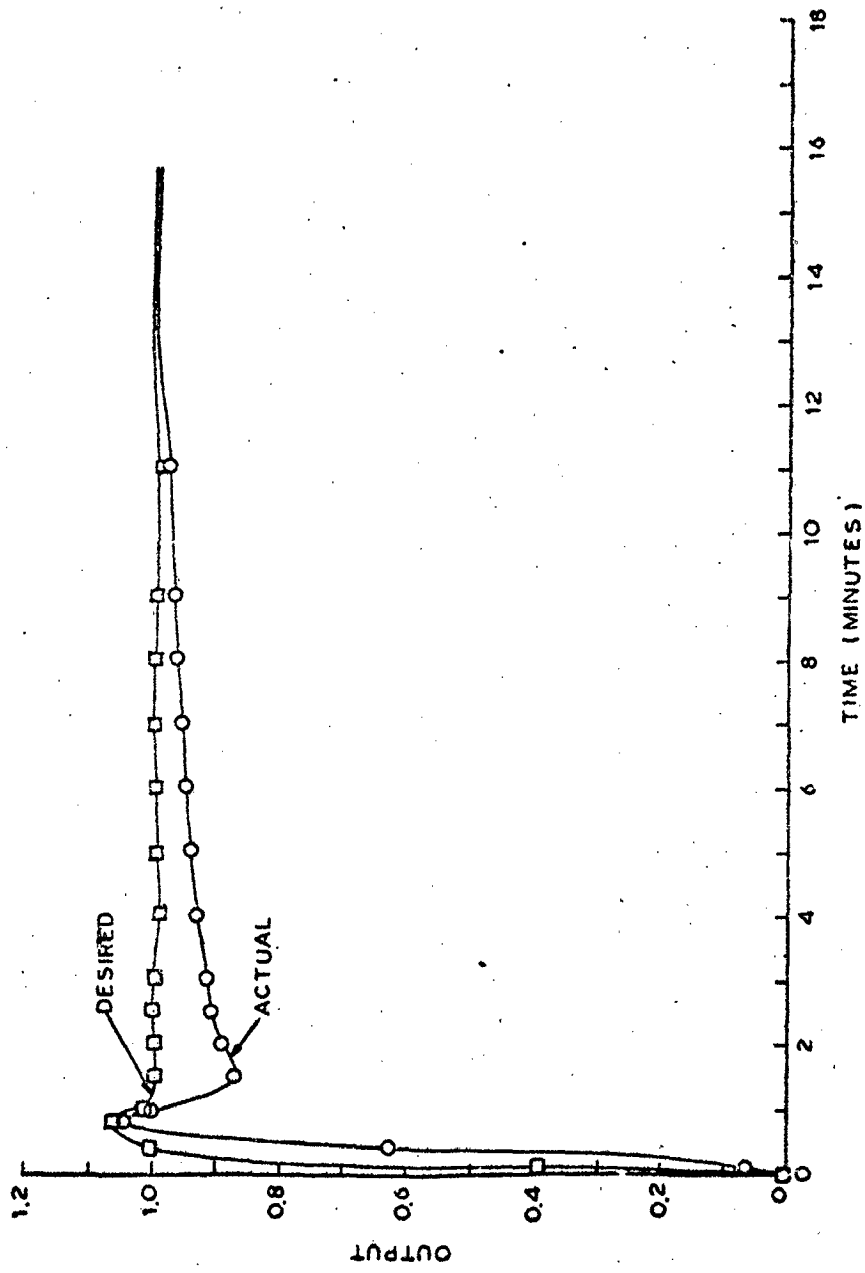


FIG. TIME RESPONSE FOR EXAMPLE 1 CASE III ($\omega = 0$ TO 0.25)

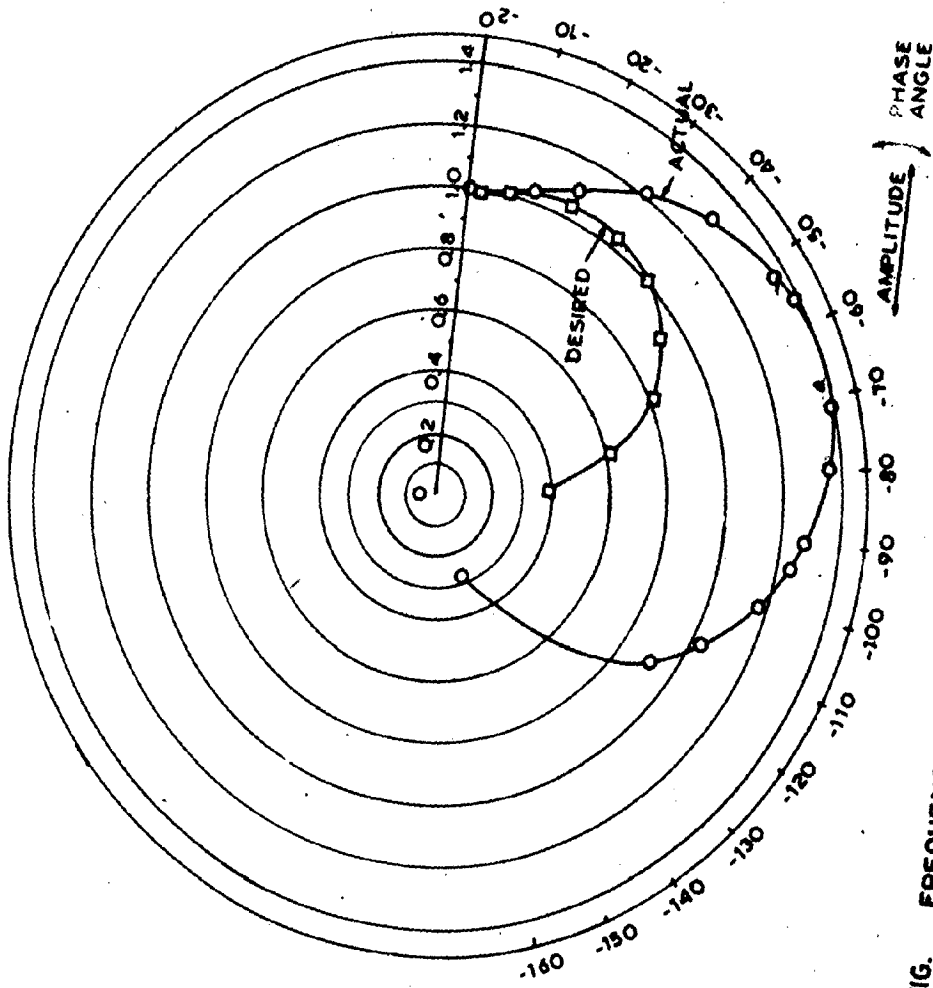


FIG. FREQUENCY RESPONSE FOR EXAMPLE 1 CASE 1 ($\omega=0$ TO 0.25)

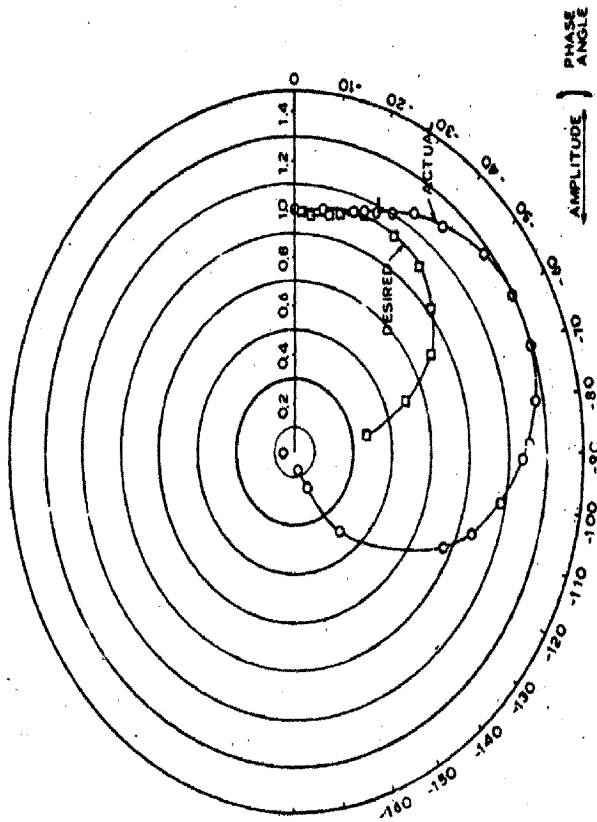


FIG FREQUENCY RESPONSE FOR EXAMPLE 1 CASE 1 ($\omega = 0$ TO 1)

EXAMPLE 2:

Consider the control problem of a plant with time delay as given below : -

The Plant Transfer function $G(s) = \frac{2.08 e^{-3.4s}}{13.2s + 1}$ and $C(s) = [K_p + K_I/s]$

Model transfer function $M(s) = e^{-3.4s} \left[\frac{4.04265 + 8.009}{s^2 + 4.4431s + 8.009} \right]$

The closed loop transfer function

$$T(s) = \frac{G(s) C(s)}{1 + G(s) C(s)}$$

$$T(p, s) = \frac{2.08 e^{-3.4s} [K_I + K_p s]}{13.2s^2 + s + 2.08 e^{-3.4s} [K_I + sK_p]}$$

$$T(p, s) = \frac{2.08 [\cos 3.4w - s \sin 3.4w] [K_I + sK_p]}{-13.2w^2 + sw + 2.08 (\cos 3.4w - s \sin 3.4w) (K_I + sK_p)}$$

$$T(p, jw) = \frac{2.08 [K_I \cos 3.4w + wK_p \sin 3.4w + j(wK_p \cos 3.4w - K_I \sin 3.4w)]}{-13.2w^2 + 2.08 [K_I \cos 3.4w + wK_p \sin 3.4w] + j[w + 2.08 (wK_p \cos 3.4w - K_I \sin 3.4w)]}$$

$$\frac{\partial T(p, jw)}{\partial K_p} = \frac{2.08w}{D^2} [-13.2w^2 \sin 3.4w - w \cos 3.4w + jw (\sin 3.4w - 13.2w \cos 3.4w)]$$

$$\text{Where } D = -13.2w^2 + 2.08 [K_I \cos 3.4w + wK_p \sin 3.4w] + j[w + 2.08 (wK_p \cos 3.4w - K_I \sin 3.4w)]$$

$$\frac{\partial T(p, jw)}{\partial K_I} = \frac{2.08}{D^2} [-13.2 w^2 \cos 3.4w + w \sin 3.4w + jw (\cos 3.4w + 13.2 w \sin 3.4w)]$$

On writing arithmetic expressions:

(26)

$$D = \text{CMPLX}(-13.2*w**2 + 2.08*(AKI*\text{COS}(3.4*w) + w*AKP*\text{SIN}(3.4*w)), \\ w + 2.08*(w*AKP*\text{COS}(3.4*w) - AKI*\text{SIN}(3.4*w)))$$

$$NA = \text{CMPLX}(2.08*w*(-13.2*w**2*\text{SIN}(3.4*w) - w*\text{COS}(3.4*w)), \\ 2.08*w**2*(\text{SIN}(3.4*w) - 13.2*w*\text{COS}(3.4*w)))$$

$$NB = \text{CMPLX}(2.08*(-13.2*w**2*\text{COS}(3.4*w) + w*\text{SIN}(3.4*w)), \\ 2.08*w*\text{COS}(3.4*w) + 13.2*w*\text{SIN}(3.4*w))$$

$$DH1 = \text{CMPLX}(-w**2 + 8.009, 4.443*w)$$

$$DH2 = \text{CMPLX}(8.009*\text{COS}(3.4*w) + 4.04265*w*\text{SIN}(3.4*w), \\ 4.04265*w*\text{COS}(3.4*w) - 8.009*\text{SIN}(3.4*w))$$

$$H1 = DH2 / DH1$$

$$DH3 = \text{CMPLX}(2.08*(AKI*\text{COS}(3.4*w) + w*AKP*\text{SIN}(3.4*w)), \\ 2.08*(w*AKP*\text{COS}(3.4*w) - AKI*\text{SIN}(3.4*w)))$$

TO FIND CLOSED LOOP TRANSFER FUNCTIONS FOR THE SYSTEM

Sl. No.	Guess Values		Final Values		w_0 to w_1	Error
	K_P	K_I	K_P	K_I		
A1	2.0	0.1	2.0004	0.1135	0 to 0.5	0.0002
A2	2.0	0.1	2.0512	0.0744	0 to 0.2	0.0084
A3	2.0	0.1	2.0046	0.1349	0 to 0.1	0.0009

Closed loop transfer functions will be

$$T_{A1}(s) = \frac{0.0185 + 0.2956s - 0.5385s^2 + 0.3152s^3}{0.0185 + 0.3744s + 0.6334s^2 + 2.1558s^3 + s^4}$$

In this example $e^{-3.4s}$ has been approximated as

$$e^{-3.4s} = \left[\frac{1 - 3.4s/2 + (3.4s)^2/12}{1 + 3.4s/2 + (3.4s)^2/12} \right]$$

$$e^{-3.4s} = \frac{1 - 1.7s + 0.9633s^2}{1 + 1.7s + 0.9633s^2}$$

$$T_{A2}(s) = \frac{0.0126 + 0.3148s + 0.5587s^2 + 0.3232s^3}{0.0126 + 0.3935s + 0.6131s^2 + 2.163s^3 + s^4}$$

$$T_{A3}(s) = \frac{0.0220 + 0.2903s + 0.5362s^2 + 0.1522s^3}{0.0220 + 0.3690s + 0.6356s^2 + 1.9928s^3 + s^4}$$

The model transfer functions can also be simplified as

$$M(s) = e^{-3.4s} \left[\frac{4.04265s + 8.009}{s^2 + 4.4431s + 8.009} \right]$$

(28)

$$\text{Approximating } e^{-3.4s} = \frac{1 - 1.7s + 0.9633s^2}{1 + 1.7s + 0.9633s^2}$$

$$\therefore M(s) = \frac{8.3141 - 9.9265s + 0.8745s^2 + 4.0425s^3}{8.3141 + 18.7463s + 16.8879s^2 + 6.2078s^3 + s^4}$$

With the help of all these closed loop transfer functions and the model transfer function, time and frequency responses have been determined.

1.	1	1	1
2.	2	2	2
3.	3	3	3
4.	4	4	4
5.	5	5	5
6.	6	6	6
7.	7	7	7
8.	8	8	8
9.	9	9	9
10.	10	10	10
11.	11	11	11
12.	12	12	12
13.	13	13	13
14.	14	14	14
15.	15	15	15
16.	16	16	16
17.	17	17	17
18.	18	18	18
19.	19	19	19
20.	20	20	20
21.	21	21	21
22.	22	22	22
23.	23	23	23
24.	24	24	24
25.	25	25	25
26.	26	26	26
27.	27	27	27
28.	28	28	28
29.	29	29	29
30.	30	30	30
31.	31	31	31
32.	32	32	32
33.	33	33	33
34.	34	34	34
35.	35	35	35
36.	36	36	36
37.	37	37	37
38.	38	38	38
39.	39	39	39
40.	40	40	40
41.	41	41	41
42.	42	42	42
43.	43	43	43
44.	44	44	44
45.	45	45	45
46.	46	46	46
47.	47	47	47
48.	48	48	48
49.	49	49	49
50.	50	50	50
51.	51	51	51
52.	52	52	52
53.	53	53	53
54.	54	54	54
55.	55	55	55
56.	56	56	56
57.	57	57	57
58.	58	58	58
59.	59	59	59
60.	60	60	60
61.	61	61	61
62.	62	62	62
63.	63	63	63
64.	64	64	64
65.	65	65	65
66.	66	66	66
67.	67	67	67
68.	68	68	68
69.	69	69	69
70.	70	70	70
71.	71	71	71
72.	72	72	72
73.	73	73	73
74.	74	74	74
75.	75	75	75
76.	76	76	76
77.	77	77	77
78.	78	78	78
79.	79	79	79
80.	80	80	80
81.	81	81	81
82.	82	82	82
83.	83	83	83
84.	84	84	84
85.	85	85	85
86.	86	86	86
87.	87	87	87
88.	88	88	88
89.	89	89	89
90.	90	90	90
91.	91	91	91
92.	92	92	92
93.	93	93	93
94.	94	94	94
95.	95	95	95
96.	96	96	96
97.	97	97	97
98.	98	98	98
99.	99	99	99
100.	100	100	100

2.0000	.1180	.11
2.0001	.1181	.11
2.0002	.1182	.11
2.0003	.1183	.11
2.0004	.1184	.11
2.0005	.1185	.11
2.0006	.1186	.11
2.0007	.1187	.11
2.0008	.1188	.11
2.0009	.1189	.11
2.0010	.1190	.11
2.0011	.1191	.11
2.0012	.1192	.11
2.0013	.1193	.11
2.0014	.1194	.11
2.0015	.1195	.11
2.0016	.1196	.11
2.0017	.1197	.11
2.0018	.1198	.11
2.0019	.1199	.11
2.0020	.1200	.12
2.0021	.1201	.12
2.0022	.1202	.12
2.0023	.1203	.12
2.0024	.1204	.12
2.0025	.1205	.12
2.0026	.1206	.12
2.0027	.1207	.12
2.0028	.1208	.12
2.0029	.1209	.12
2.0030	.1210	.12
2.0031	.1211	.12
2.0032	.1212	.12
2.0033	.1213	.12
2.0034	.1214	.12
2.0035	.1215	.12
2.0036	.1216	.12
2.0037	.1217	.12
2.0038	.1218	.12
2.0039	.1219	.12
2.0040	.1220	.12
2.0041	.1221	.12
2.0042	.1222	.12
2.0043	.1223	.12
2.0044	.1224	.12
2.0045	.1225	.12
2.0046	.1226	.12
2.0047	.1227	.12
2.0048	.1228	.12
2.0049	.1229	.12
2.0050	.1230	.12
2.0051	.1231	.12
2.0052	.1232	.12
2.0053	.1233	.12
2.0054	.1234	.12
2.0055	.1235	.12
2.0056	.1236	.12
2.0057	.1237	.12
2.0058	.1238	.12
2.0059	.1239	.12
2.0060	.1240	.12
2.0061	.1241	.12
2.0062	.1242	.12
2.0063	.1243	.12
2.0064	.1244	.12
2.0065	.1245	.12
2.0066	.1246	.12
2.0067	.1247	.12
2.0068	.1248	.12
2.0069	.1249	.12
2.0070	.1250	.12
2.0071	.1251	.12
2.0072	.1252	.12
2.0073	.1253	.12
2.0074	.1254	.12
2.0075	.1255	.12
2.0076	.1256	.12
2.0077	.1257	.12
2.0078	.1258	.12
2.0079	.1259	.12
2.0080	.1260	.12
2.0081	.1261	.12
2.0082	.1262	.12
2.0083	.1263	.12
2.0084	.1264	.12
2.0085	.1265	.12
2.0086	.1266	.12
2.0087	.1267	.12
2.0088	.1268	.12
2.0089	.1269	.12
2.0090	.1270	.12
2.0091	.1271	.12
2.0092	.1272	.12
2.0093	.1273	.12
2.0094	.1274	.12
2.0095	.1275	.12
2.0096	.1276	.12
2.0097	.1277	.12
2.0098	.1278	.12
2.0099	.1279	.12
2.0100	.1280	.12
2.0101	.1281	.12
2.0102	.1282	.12
2.0103	.1283	.12
2.0104	.1284	.12
2.0105	.1285	.12
2.0106	.1286	.12
2.0107	.1287	.12
2.0108	.1288	.12
2.0109	.1289	.12
2.0110	.1290	.12
2.0111	.1291	.12
2.0112	.1292	.12
2.0113	.1293	.12
2.0114	.1294	.12
2.0115	.1295	.12
2.0116	.1296	.12
2.0117	.1297	.12
2.0118	.1298	.12
2.0119	.1299	.12
2.0120	.1300	.13
2.0121	.1301	.13
2.0122	.1302	.13
2.0123	.1303	.13
2.0124	.1304	.13
2.0125	.1305	.13
2.0126	.1306	.13
2.0127	.1307	.13
2.0128	.1308	.13
2.0129	.1309	.13
2.0130	.1310	.13
2.0131	.1311	.13
2.0132	.1312	.13
2.0133	.1313	.13
2.0134	.1314	.13
2.0135	.1315	.13
2.0136	.1316	.13
2.0137	.1317	.13
2.0138	.1318	.13
2.0139	.1319	.13
2.0140	.1320	.13
2.0141	.1321	.13
2.0142	.1322	.13
2.0143	.1323	.13
2.0144	.1324	.13
2.0145	.1325	.13
2.0146	.1326	.13
2.0147	.1327	.13
2.0148	.1328	.13
2.0149	.1329	.13
2.0150	.1330	.13
2.0151	.1331	.13
2.0152	.1332	.13
2.0153	.1333	.13
2.0154	.1334	.13
2.0155	.1335	.13
2.0156	.1336	.13
2.0157	.1337	.13
2.0158	.1338	.13
2.0159	.1339	.13
2.0160	.1340	.13
2.0161	.1341	.13
2.0162	.1342	.13
2.0163	.1343	.13
2.0164	.1344	.13
2.0165	.1345	.13
2.0166	.1346	.13
2.0167	.1347	.13
2.0168	.1348	.13
2.0169	.1349	.13
2.0170	.1350	.13
2.0171	.1351	.13
2.0172	.1352	.13
2.0173	.1353	.13
2.0174	.1354	.13
2.0175	.1355	.13
2.0176	.1356	.13
2.0177	.1357	.13
2.0178	.1358	.13
2.0179	.1359	.13
2.0180	.1360	.13
2.0181	.1361	.13
2.0182	.1362	.13
2.0183	.1363	.13
2.0184	.1364	.13
2.0185	.1365	.13
2.0186	.1366	.13
2.0187	.1367	.13
2.0188	.1368	.13
2.0189	.1369	.13
2.0190	.1370	.13
2.0191	.1371	.13
2.0192	.1372	.13
2.0193	.1373	.13
2.0194	.1374	.13
2.0195	.1375	.13
2.0196	.1376	.13
2.0197	.1377	.13
2.0198	.1378	.13
2.0199	.1379	.13
2.0200	.1380	.13

1.

2.

3.

4.

44	0.14	+	-	0.1470308000	-	0.1470308000	0.2200000000	-	0.2200000000
45	0.15	+	-	0.1512050000	-	0.1512050000	0.2250000000	-	0.2250000000
46	0.16	+	-	0.1617000000	-	0.1617000000	0.2300000000	-	0.2300000000
47	0.17	+	-	0.1719300000	-	0.1719300000	0.2350000000	-	0.2350000000
48	0.18	+	-	0.1819000000	-	0.1819000000	0.2400000000	-	0.2400000000
49	0.19	+	-	0.1907000000	-	0.1907000000	0.2450000000	-	0.2450000000
50	0.20	+	-	0.1920000000	-	0.1920000000	0.2500000000	-	0.2500000000
51	0.21	+	-	0.2003340000	-	0.2003340000	0.2550000000	-	0.2550000000
52	0.22	+	-	0.2133000000	-	0.2133000000	0.2600000000	-	0.2600000000
53	0.23	+	-	0.2192000000	-	0.2192000000	0.2650000000	-	0.2650000000
54	0.24	+	-	0.2219200000	-	0.2219200000	0.2700000000	-	0.2700000000
55	0.25	+	-	0.2277900000	-	0.2277900000	0.2750000000	-	0.2750000000
56	0.26	+	-	0.2335770000	-	0.2335770000	0.2800000000	-	0.2800000000
57	0.27	+	-	0.2391730000	-	0.2391730000	0.2850000000	-	0.2850000000
58	0.28	+	-	0.2445680000	-	0.2445680000	0.2900000000	-	0.2900000000
59	0.29	+	-	0.2497630000	-	0.2497630000	0.2950000000	-	0.2950000000
60	0.30	+	-	0.2547580000	-	0.2547580000	0.3000000000	-	0.3000000000
61	0.31	+	-	0.2595530000	-	0.2595530000	0.3050000000	-	0.3050000000
62	0.32	+	-	0.2641480000	-	0.2641480000	0.3100000000	-	0.3100000000
63	0.33	+	-	0.2685430000	-	0.2685430000	0.3150000000	-	0.3150000000
64	0.34	+	-	0.2727380000	-	0.2727380000	0.3200000000	-	0.3200000000
65	0.35	+	-	0.2767330000	-	0.2767330000	0.3250000000	-	0.3250000000
66	0.36	+	-	0.2805280000	-	0.2805280000	0.3300000000	-	0.3300000000
67	0.37	+	-	0.2841230000	-	0.2841230000	0.3350000000	-	0.3350000000
68	0.38	+	-	0.2875180000	-	0.2875180000	0.3400000000	-	0.3400000000
69	0.39	+	-	0.2907130000	-	0.2907130000	0.3450000000	-	0.3450000000
70	0.40	+	-	0.2937080000	-	0.2937080000	0.3500000000	-	0.3500000000
71	0.41	+	-	0.2965030000	-	0.2965030000	0.3550000000	-	0.3550000000
72	0.42	+	-	0.2991980000	-	0.2991980000	0.3600000000	-	0.3600000000
73	0.43	+	-	0.3017930000	-	0.3017930000	0.3650000000	-	0.3650000000
74	0.44	+	-	0.3042880000	-	0.3042880000	0.3700000000	-	0.3700000000
75	0.45	+	-	0.3066830000	-	0.3066830000	0.3750000000	-	0.3750000000
76	0.46	+	-	0.3089780000	-	0.3089780000	0.3800000000	-	0.3800000000
77	0.47	+	-	0.3111730000	-	0.3111730000	0.3850000000	-	0.3850000000
78	0.48	+	-	0.3132680000	-	0.3132680000	0.3900000000	-	0.3900000000
79	0.49	+	-	0.3152630000	-	0.3152630000	0.3950000000	-	0.3950000000
80	0.50	+	-	0.3171580000	-	0.3171580000	0.4000000000	-	0.4000000000
81	0.51	+	-	0.3189530000	-	0.3189530000	0.4050000000	-	0.4050000000
82	0.52	+	-	0.3206480000	-	0.3206480000	0.4100000000	-	0.4100000000
83	0.53	+	-	0.3222430000	-	0.3222430000	0.4150000000	-	0.4150000000
84	0.54	+	-	0.3237380000	-	0.3237380000	0.4200000000	-	0.4200000000
85	0.55	+	-	0.3251330000	-	0.3251330000	0.4250000000	-	0.4250000000
86	0.56	+	-	0.3264280000	-	0.3264280000	0.4300000000	-	0.4300000000
87	0.57	+	-	0.3276230000	-	0.3276230000	0.4350000000	-	0.4350000000
88	0.58	+	-	0.3287180000	-	0.3287180000	0.4400000000	-	0.4400000000
89	0.59	+	-	0.3297130000	-	0.3297130000	0.4450000000	-	0.4450000000
90	0.60	+	-	0.3306080000	-	0.3306080000	0.4500000000	-	0.4500000000
91	0.61	+	-	0.3314030000	-	0.3314030000	0.4550000000	-	0.4550000000
92	0.62	+	-	0.3321980000	-	0.3321980000	0.4600000000	-	0.4600000000
93	0.63	+	-	0.3329930000	-	0.3329930000	0.4650000000	-	0.4650000000
94	0.64	+	-	0.3336880000	-	0.3336880000	0.4700000000	-	0.4700000000
95	0.65	+	-	0.3343830000	-	0.3343830000	0.4750000000	-	0.4750000000
96	0.66	+	-	0.3350780000	-	0.3350780000	0.4800000000	-	0.4800000000
97	0.67	+	-	0.3357730000	-	0.3357730000	0.4850000000	-	0.4850000000
98	0.68	+	-	0.3364680000	-	0.3364680000	0.4900000000	-	0.4900000000
99	0.69	+	-	0.3371630000	-	0.3371630000	0.4950000000	-	0.4950000000
100	0.70	+	-	0.3378580000	-	0.3378580000	0.5000000000	-	0.5000000000

86	0.324500	+	0.277500	=	0.602000	0.775771	=	0.599130	+2
89	0.394500	+	0.122500	=	0.517000	0.759324	=	0.361300	+2
90	0.404500	+	0.507000	=	0.911500	0.742553	=	0.372210	+2
92	0.414500	+	0.557500	=	0.972000	0.740000	=	0.359400	+2
93	0.424500	+	0.517500	=	0.942000	0.711197	=	0.397255	+2
95	0.434500	+	0.677500	=	1.112000	0.690591	=	0.357380	+2
96	0.444500	+	0.504500	=	0.949000	0.682713	=	0.346052	+2
98	0.464500	+	0.495000	=	0.959500	0.666922	=	0.321300	+2
96	0.474500	+	0.731500	=	1.206000	0.655630	=	0.331023	+2
97	0.484500	+	0.572500	=	1.057000	0.643257	=	0.347590	+2
98	0.494500	+	0.446000	=	0.940500	0.631110	=	0.359752	+2
99	0.504500	+	0.737000	=	1.241500	0.619009	=	0.363523	+2
100	0.514500	+	0.137000	=	0.651500	0.613917	=	0.955121	+1
101	0.524500	+	0.923000	=	1.447500	0.572791	=	0.197032	+2
102	0.534500	+	0.612000	=	1.146500	0.759324	=	0.301910	+2
103	0.544500	+	0.420000	=	0.964500	0.649171	=	0.335590	+2
104	0.554500	+	0.311000	=	0.865500	0.522590	=	0.330651	+2
105	0.564500	+	0.235000	=	0.799500	0.451180	=	0.333702	+2
106	0.574500	+	0.163000	=	0.737500	0.366218	=	0.323933	+2
107	0.584500	+	0.117000	=	0.701500	0.356379	=	0.351182	+2
108	0.594500	+	0.120000	=	0.714500	0.319447	=	0.373932	+2
109	0.604500	+	0.100000	=	0.704500	0.290980	=	0.363279	+2
110	0.614500	+	0.867700	=	1.482200	0.267130	=	0.119740	+2
111	0.624500	+	0.725000	=	1.349500	0.249000	=	0.728117	+2
112	0.634500	+	0.627700	=	1.262200	0.229539	=	0.742561	+2
113	0.644500	+	0.543000	=	1.187500	0.214331	=	0.751763	+2
114	0.654500	+	0.463000	=	1.117500	0.201025	=	0.759752	+2
115	0.664500	+	0.420000	=	1.084500	0.189340	=	0.761200	+2
116	0.674500	+	0.363000	=	1.037500	0.176890	=	0.773635	+2
117	0.684500	+	0.312500	=	0.997500	0.163829	=	0.782753	+2
118	0.694500	+	0.311000	=	1.002000	0.151173	=	0.790009	+2
119	0.704500	+	0.262100	=	0.966600	0.138474	=	0.795716	+2
120	0.714500	+	0.257500	=	0.972000	0.146500	=	0.796700	+2
121	0.724500	+	0.235000	=	0.959500	0.132000	=	0.801095	+2
122	0.734500	+	0.216000	=	0.950500	0.126275	=	0.807197	+2
123	0.744500	+	0.199500	=	0.944000	0.129320	=	0.818950	+2
124	0.754500	+	0.189750	=	0.944250	0.126471	=	0.813195	+2
125	0.764500	+	0.179000	=	0.943000	0.118000	=	0.810771	+2
126	0.774500	+	0.155000	=	0.929500	0.115250	=	0.820001	+2
127	0.784500	+	0.147000	=	0.931500	0.102000	=	0.821000	+2
128	0.794500	+	0.139750	=	0.934250	0.107500	=	0.820700	+2
129	0.804500	+	0.130000	=	0.934500	0.102770	=	0.821000	+2
130	0.814500	+	0.120000	=	0.934500	0.100000	=	0.833000	+2

176	0.29	0.04	0.1055112	=	0.1114088	=	0.1114088	=	0.1031000	+ 4
177	0.3	0.04	0.1077375	=	0.1772625	=	0.1773184	=	0.1250701	+ 2
178	0.31	0.04	0.1107695	=	0.1042305	=	0.1042370	=	0.0420703	+ 2
179	0.32	0.04	0.1148250	=	0.1199130	=	0.1199118	=	0.0433200	+ 2
180	0.33	0.04	0.1199415	=	0.0993149	=	0.0993330	=	0.1032134	+ 4
181	0.34	0.04	0.1261890	=	0.0855100	=	0.0855703	=	0.043227	+ 2
182	0.35	0.04	0.1336720	=	0.0834623	=	0.0834105	=	0.0433295	+ 2
183	0.36	0.04	0.1424775	=	0.0771697	=	0.0770424	=	0.0434000	+ 2
184	0.37	0.04	0.1527315	=	0.0735750	=	0.0735033	=	0.0434700	+ 2
185	0.38	0.04	0.1645130	=	0.0697100	=	0.0696192	=	0.0435400	+ 2
186	0.39	0.04	0.1779215	=	0.0660710	=	0.0660713	=	0.0436100	+ 2
187	0.4	0.04	0.1930210	=	0.0627950	=	0.0627950	=	0.0436800	+ 2
188	0.41	0.04	0.2098730	=	0.0598250	=	0.0598257	=	0.0437500	+ 2
189	0.42	0.04	0.2285150	=	0.0571000	=	0.0570508	=	0.0438200	+ 2
190	0.43	0.04	0.2489820	=	0.0545900	=	0.0545230	=	0.0438900	+ 2
191	0.44	0.04	0.2713050	=	0.0523100	=	0.0523008	=	0.0439600	+ 2
192	0.45	0.04	0.2955130	=	0.0501900	=	0.0501794	=	0.0440300	+ 2
193	0.46	0.04	0.3216250	=	0.0482000	=	0.0481609	=	0.0441000	+ 2
194	0.47	0.04	0.3496730	=	0.0463300	=	0.0462854	=	0.0441700	+ 2
195	0.48	0.04	0.3796930	=	0.0445600	=	0.0445220	=	0.0442400	+ 2
196	0.49	0.04	0.4117150	=	0.0429500	=	0.0429077	=	0.0443100	+ 2
197	0.5	0.04	0.4457700	=	0.0414600	=	0.0414161	=	0.0443800	+ 2
198	0.51	0.04	0.4818800	=	0.0400700	=	0.0400255	=	0.0444500	+ 2
199	0.52	0.04	0.5199700	=	0.0387700	=	0.0387257	=	0.0445200	+ 2
200	0.53	0.04	0.5599700	=	0.0375500	=	0.0375050	=	0.0445900	+ 2
201	0.54	0.04	0.6018100	=	0.0364000	=	0.0363503	=	0.0446600	+ 2
202	0.55	0.04	0.6454300	=	0.0353100	=	0.0352606	=	0.0447300	+ 2
203	0.56	0.04	0.6908700	=	0.0342700	=	0.0342209	=	0.0448000	+ 2
204	0.57	0.04	0.7380700	=	0.0332800	=	0.0332312	=	0.0448700	+ 2
205	0.58	0.04	0.7869700	=	0.0323400	=	0.0322915	=	0.0449400	+ 2
206	0.59	0.04	0.8375100	=	0.0314500	=	0.0314018	=	0.0450100	+ 2
207	0.6	0.04	0.8896400	=	0.0306100	=	0.0305621	=	0.0450800	+ 2

DER OF NUMERATOR POLYNOMIAL IS =, 3

DER OF DENOMINATOR POLYNOMIAL IS =, 4

MINIMUM VALUE OF FREQUENCY IS = .1E-01

MINIMUM VALUE OF FREQUENCY IS = .1E-01

NUMERATOR COEFFICIENTS ARE

.83141000E+01 -1.99265000E+01 .87050000E+00 0.40425000E+1

DENOMINATOR COEFFICIENTS ARE

.83141000E+01 0.18746300E+02 .16987000E+02 0.62078000E+01 0.10000000E+00

S.No	FREQUENCY	REAL PART	IMAGINARY PART	REAL PART	IMAGINARY PART
1	0.10000000E+01	0.99911535E+00	-0.31671312E-01	0.10000000E+01	0.00000000E+00
2	0.20000000E+01	0.99766185E+00	-0.60922335E-01	0.19000000E+01	-0.33951000E+01
3	0.30000000E+01	0.99473922E+00	-0.10328691E+00	0.10000000E+01	-0.59270000E+01
4	0.40000000E+01	0.99065319E+00	-0.13753556E+00	0.10000000E+01	-0.79043536E+01
5	0.50000000E+01	0.98547117E+00	-0.17162083E+00	0.10000000E+01	-0.99071035E+01
6	0.60000000E+01	0.97906127E+00	-0.20553136E+00	0.10000000E+01	-0.11050420E+02
7	0.70000000E+01	0.97148846E+00	-0.23920190E+00	0.10000000E+01	-0.13032704E+02
8	0.80000000E+01	0.96276915E+00	-0.27260340E+00	0.10000000E+01	-0.15004207E+02
9	0.90000000E+01	0.95295100E+00	-0.30569516E+00	0.10000000E+01	-0.17007756E+02
10	0.10000000E+02	0.94204211E+00	-0.33844915E+00	0.10000000E+01	-0.19062405E+02
11	0.11000000E+02	0.92995442E+00	-0.37091647E+00	0.11001109E+01	-0.21073927E+02
12	0.12000000E+02	0.91682215E+00	-0.40276000E+00	0.10013907E+01	-0.23071620E+02
13	0.13000000E+02	0.90289427E+00	-0.43420006E+00	0.10010310E+01	-0.25069321E+02
14	0.14000000E+02	0.88873087E+00	-0.46526291E+00	0.10018911E+01	-0.27067033E+02
15	0.15000000E+02	0.87497113E+00	-0.49573720E+00	0.10021093E+01	-0.29064750E+02
16	0.16000000E+02	0.86136558E+00	-0.52564911E+00	0.10024074E+01	-0.31062465E+02
17	0.17000000E+02	0.84852192E+00	-0.55496331E+00	0.10027038E+01	-0.33060213E+02
18	0.18000000E+02	0.83581659E+00	-0.58364553E+00	0.10031190E+01	-0.35057926E+02
19	0.19000000E+02	0.82355442E+00	-0.61166216E+00	0.10034729E+01	-0.37055603E+02
20	0.20000000E+02	0.81162157E+00	-0.63898022E+00	0.10031506E+01	-0.39053375E+02
21	0.21000000E+02	0.80004693E+00	-0.66556706E+00	0.10042365E+01	-0.41051147E+02
22	0.22000000E+02	0.78889535E+00	-0.69139240E+00	0.10040060E+01	-0.43048741E+02
23	0.23000000E+02	0.77819817E+00	-0.71642441E+00	0.10050739E+01	-0.45046353E+02
24	0.24000000E+02	0.76799731E+00	-0.74063372E+00	0.10055201E+01	-0.47043967E+02
25	0.25000000E+02	0.75814629E+00	-0.76399123E+00	0.10059844E+01	-0.49041585E+02
26	0.26000000E+02	0.74869510E+00	-0.78660706E+00	0.10065069E+01	-0.51039197E+02
27	0.27000000E+02	0.73968524E+00	-0.80860217E+00	0.10069973E+01	-0.53036809E+02
28	0.28000000E+02	0.73109552E+00	-0.82980200E+00	0.10074656E+01	-0.55034428E+02
29	0.29000000E+02	0.72289537E+00	-0.85033607E+00	0.10078217E+01	-0.57032046E+02
30	0.30000000E+02	0.71519119E+00	-0.86711306E+00	0.10085758E+01	-0.59028283E+02
31	0.31000000E+02	0.70793631E+00	-0.88047739E+00	0.10091467E+01	-0.61023858E+02
32	0.32000000E+02	0.70109100E+00	-0.89105519E+00	0.10097356E+01	-0.63018815E+02
33	0.33000000E+02	0.69469425E+00	-0.90179051E+00	0.10103413E+01	-0.65013160E+02
34	0.34000000E+02	0.68869587E+00	-0.91167516E+00	0.10109644E+01	-0.67006903E+02
35	0.35000000E+02	0.68305283E+00	-0.92051789E+00	0.10116066E+01	-0.69000121E+02
36	0.36000000E+02	0.67781694E+00	-0.92835928E+00	0.10122616E+01	-0.71000877E+02
37	0.37000000E+02	0.67295610E+00	-0.93529312E+00	0.10129354E+01	-0.73000135E+02
38	0.38000000E+02	0.66852049E+00	-0.94135810E+00	0.10136257E+01	-0.75000000E+02
39	0.39000000E+02	0.66446952E+00	-0.94659000E+00	0.10143325E+01	-0.77000000E+02
40	0.40000000E+02	0.66075500E+00	-0.95101000E+00	0.10150550E+01	-0.79000000E+02
41	0.41000000E+02	0.65733500E+00	-0.95462000E+00	0.10157950E+01	-0.81000000E+02
42	0.42000000E+02	0.65427000E+00	-0.95752000E+00	0.10165500E+01	-0.83000000E+02

44	0.44900000E+01	0.58775239E+01	0.11163110E+01	0.11189175E+01	0.11189175E+01	0.11189175E+01
45	0.45000000E+01	0.58802665E+01	0.11185183E+01	0.11189175E+01	0.11189175E+01	0.11189175E+01
46	0.46000000E+01	0.59689557E+01	0.11196706E+01	0.11197775E+01	0.11197775E+01	0.11197775E+01
47	0.47000000E+01	0.60331380E+01	0.11195907E+01	0.11205018E+01	0.11205018E+01	0.11205018E+01
48	0.48000000E+01	0.60861251E+01	0.11183709E+01	0.11216770E+01	0.11216770E+01	0.11216770E+01
49	0.49000000E+01	0.61275810E+01	0.11160323E+01	0.11222710E+01	0.11222710E+01	0.11222710E+01
50	0.50000000E+01	0.61421218E+01	0.11338449E+01	0.11209003E+01	0.11209003E+01	0.11209003E+01
51	0.52000000E+01	0.67742156E+01	0.11639960E+01	0.11203005E+01	0.11203005E+01	0.11203005E+01
52	0.53000000E+01	0.68516141E+01	0.11807171E+01	0.11205755E+01	0.11205755E+01	0.11205755E+01
53	0.54000000E+01	0.69522761E+01	0.11996104E+01	0.11215055E+01	0.11215055E+01	0.11215055E+01
54	0.55000000E+01	0.70467082E+01	0.12125665E+01	0.11231398E+01	0.11231398E+01	0.11231398E+01
55	0.60000000E+01	0.76929138E+01	0.12919574E+01	0.11326732E+01	0.11326732E+01	0.11326732E+01
56	0.70000000E+01	0.93952171E+01	0.17369732E+01	0.11434231E+01	0.11434231E+01	0.11434231E+01
57	0.80000000E+01	0.93372534E+01	0.14914292E+01	0.11551515E+01	0.11551515E+01	0.11551515E+01
58	0.90000000E+01	0.11452198E+02	0.21738019E+02	0.11675854E+01	0.11675854E+01	0.11675854E+01
59	0.10000000E+02	0.10788527E+02	0.58333070E+02	0.11688428E+01	0.11688428E+01	0.11688428E+01
60	0.11000000E+02	0.10468514E+02	0.31553241E+02	0.11693370E+01	0.11693370E+01	0.11693370E+01
61	0.12000000E+02	0.96423325E+01	0.54193853E+02	0.11660936E+01	0.11660936E+01	0.11660936E+01
62	0.13000000E+02	0.84563959E+01	0.73174752E+02	0.11182847E+01	0.11182847E+01	0.11182847E+01
63	0.14000000E+02	0.79372782E+01	0.28366612E+03	0.11296115E+01	0.11296115E+01	0.11296115E+01
64	0.15000000E+02	0.54865541E+01	0.93915445E+02	0.11398626E+01	0.11398626E+01	0.11398626E+01
65	0.16000000E+02	0.38825393E+01	0.11811563E+02	0.11487559E+01	0.11487559E+01	0.11487559E+01
66	0.17000000E+02	0.22835016E+01	0.11332686E+02	0.11561456E+01	0.11561456E+01	0.11561456E+01
67	0.18000000E+02	0.73211848E+01	0.11592692E+02	0.11618701E+01	0.11618701E+01	0.11618701E+01
68	0.18999999E+02	0.74154130E+01	0.11629641E+02	0.11652259E+01	0.11652259E+01	0.11652259E+01
69	0.19999999E+02	0.21161001E+02	0.11475627E+02	0.11669118E+01	0.11669118E+01	0.11669118E+01
70	0.20999999E+02	0.33778802E+02	0.11166257E+02	0.11665991E+01	0.11665991E+01	0.11665991E+01
71	0.21999999E+02	0.45180020E+02	0.11173141E+02	0.11643180E+01	0.11643180E+01	0.11643180E+01
72	0.22999999E+02	0.55352800E+02	0.11195192E+02	0.11601921E+01	0.11601921E+01	0.11601921E+01
73	0.23999999E+02	0.64274451E+02	0.93848721E+02	0.11500421E+01	0.11500421E+01	0.11500421E+01
74	0.24999999E+02	0.71980716E+02	0.89219370E+02	0.11402702E+01	0.11402702E+01	0.11402702E+01
75	0.25999999E+02	0.78524221E+02	0.92221160E+02	0.11369421E+01	0.11369421E+01	0.11369421E+01
76	0.26999999E+02	0.83972319E+02	0.75044640E+02	0.11201915E+01	0.11201915E+01	0.11201915E+01
77	0.27999999E+02	0.88414159E+02	0.67814651E+02	0.11141001E+01	0.11141001E+01	0.11141001E+01
78	0.28999999E+02	0.91805859E+02	0.66429118E+02	0.11011210E+01	0.11011210E+01	0.11011210E+01
79	0.29999999E+02	0.94560946E+02	0.53618053E+02	0.10071972E+01	0.10071972E+01	0.10071972E+01
80	0.30999999E+02	0.90476979E+02	0.46819769E+02	0.10723321E+01	0.10723321E+01	0.10723321E+01
81	0.31999999E+02	0.97723402E+02	0.42702030E+02	0.10509562E+01	0.10509562E+01	0.10509562E+01
82	0.32999999E+02	0.98389857E+02	0.36030507E+02	0.10411075E+01	0.10411075E+01	0.10411075E+01
83	0.33999999E+02	0.98573071E+02	0.28133170E+02	0.10201108E+01	0.10201108E+01	0.10201108E+01
84	0.34999999E+02	0.98209207E+02	0.22574122E+02	0.10080210E+01	0.10080210E+01	0.10080210E+01
85	0.35999999E+02	0.97361021E+02	0.17305027E+02	0.99121035E+00	0.99121035E+00	0.99121035E+00
86	0.36999999E+02	0.96725877E+02	0.12504045E+02	0.97531797E+00	0.97531797E+00	0.97531797E+00
87	0.37999999E+02	0.96300075E+02	0.79850601E+01	0.95072001E+00	0.95072001E+00	0.95072001E+00

88	0.389999982E+01	0.84127249E+01	0.37942312E+01	0.94223475E+01	0.23100000E+01
89	0.399999995E+01	0.92589860E+01	0.26940046E+03	0.92589860E+01	0.22601230E+01
90	0.409999998E+01	0.91002630E+01	0.36330200E+01	0.91975220E+01	0.22000000E+01
91	0.419999990E+01	0.89410000E+01	0.69110017E+01	0.89303022E+01	0.21450000E+01
92	0.429999994E+01	0.87825019E+01	0.99132145E+01	0.87010000E+01	0.20800000E+01
93	0.439999998E+01	0.85345323E+01	0.12672042E+00	0.86200000E+01	0.20400000E+01
94	0.449999990E+01	0.83002237E+01	0.15189455E+00	0.84774128E+01	0.19821700E+02
95	0.460000000E+01	0.81442725E+01	0.17486911E+00	0.83296927E+01	0.12110232E+02
96	0.470000000E+01	0.79460000E+01	0.19500027E+00	0.81850327E+01	0.13034500E+02
97	0.480000000E+01	0.77527950E+01	0.21484702E+00	0.80400000E+01	0.15000000E+02
98	0.490000000E+01	0.75586572E+01	0.23214530E+00	0.79071137E+01	0.17070000E+02
99	0.100000000E+01	0.10784527E+01	0.50333670E+01	0.10042650E+01	0.17090500E+03
100	0.200000000E+01	0.21161040E+01	0.11475027E+01	0.11669100E+01	0.79550050E+02
101	0.300000000E+01	0.90566946E+01	0.53610040E+00	0.10870972E+01	0.29552590E+02
102	0.400000000E+01	0.92589865E+01	0.61947119E+03	0.92589881E+01	0.42065301E+01
103	0.500000000E+01	0.73072132E+01	0.24703307E+00	0.77726980E+01	0.18042947E+02
104	0.600000000E+01	0.56655686E+01	0.34002541E+00	0.66076013E+01	0.30370500E+02
105	0.700000000E+01	0.43956221E+01	0.36527530E+00	0.57152519E+01	0.39726534E+02
106	0.800000000E+01	0.34754439E+01	0.36271363E+00	0.50234279E+01	0.46223517E+02
107	0.900000000E+01	0.28020677E+01	0.39897710E+00	0.44760117E+01	0.51229550E+02
108	0.100000000E+02	0.23013811E+01	0.33125631E+00	0.40330000E+01	0.55203039E+02
109	0.110000000E+02	0.19211750E+01	0.31271030E+00	0.36700000E+01	0.58035000E+02
110	0.120000000E+02	0.16259545E+01	0.29470527E+00	0.33659230E+01	0.61110000E+02
111	0.130000000E+02	0.13929691E+01	0.27783341E+00	0.31079741E+01	0.63372200E+02
112	0.140000000E+02	0.12001427E+01	0.26224677E+00	0.28865500E+01	0.65301229E+02
113	0.150000000E+02	0.10541802E+01	0.24797000E+00	0.26941809E+01	0.66908400E+02
114	0.160000000E+02	0.92901649E+00	0.23492025E+00	0.25263000E+01	0.68423090E+02
115	0.170000000E+02	0.82473913E+00	0.22302299E+00	0.23770390E+01	0.69705022E+02
116	0.180000000E+02	0.73090311E+00	0.21214633E+00	0.22450296E+01	0.70443119E+02
117	0.190000000E+02	0.66245379E+00	0.20219321E+00	0.21276070E+01	0.71059100E+02
118	0.200000000E+02	0.59863446E+00	0.19306025E+00	0.20213414E+01	0.72773000E+02
119	0.210000000E+02	0.54357630E+00	0.18467751E+00	0.19251113E+01	0.73596000E+02
120	0.220000000E+02	0.49575256E+00	0.17694861E+00	0.18376212E+01	0.74340000E+02
121	0.230000000E+02	0.45395350E+00	0.16961028E+00	0.17577331E+01	0.75033144E+02
122	0.240000000E+02	0.41721129E+00	0.16320104E+00	0.16844920E+01	0.75659951E+02
123	0.250000000E+02	0.38574429E+00	0.15716855E+00	0.16171212E+01	0.76236200E+02
124	0.260000000E+02	0.35591579E+00	0.15136425E+00	0.15549243E+01	0.76701952E+02
125	0.270000000E+02	0.33020300E+00	0.14604703E+00	0.14973335E+01	0.77260000E+02
126	0.280000000E+02	0.30717360E+00	0.14100022E+00	0.14438555E+01	0.77716700E+02
127	0.290000000E+02	0.28806570E+00	0.13643120E+00	0.13940650E+01	0.78141700E+02
128	0.300000000E+02	0.26770310E+00	0.13207190E+00	0.13475037E+01	0.78530374E+02
129	0.310000000E+02	0.24600650E+00	0.12797610E+00	0.13041200E+01	0.78900000E+02
130	0.320000000E+02	0.23350150E+00	0.12412210E+00	0.12633030E+01	0.79250000E+02

132	0.3420000E+02	0.20871439E-1	0.11758918E+01	0.11650431E+01	0.75920000E+02
133	0.3500000E+02	0.19700159E-1	0.11381442E+01	0.11550679E+01	0.80170000E+02
134	0.3600000E+02	0.18620055E-1	0.11074281E+01	0.11229603E+01	0.80453000E+02
135	0.3700000E+02	0.17630786E-1	0.10783023E+01	0.10920273E+01	0.80711000E+02
136	0.3800000E+02	0.16721720E-1	0.10515664E+01	0.10636710E+01	0.80956000E+02
137	0.3900000E+02	0.15877672E-1	0.10263588E+01	0.10365911E+01	0.81188237E+02
138	0.4000000E+02	0.15095948E-1	0.09993368E+01	0.10106744E+01	0.81400917E+02
139	0.4100000E+02	0.14374410E-1	0.09754939E+01	0.98602203E+01	0.81619804E+02
140	0.4200000E+02	0.13695997E-1	0.09527498E+01	0.96250370E+01	0.81819672E+02
141	0.4300000E+02	0.13067940E-1	0.09310311E+01	0.94015743E+01	0.82010221E+02
142	0.4400000E+02	0.12482014E-1	0.09102707E+01	0.91870879E+01	0.82192067E+02
143	0.4500000E+02	0.11930631E-1	0.08904071E+01	0.89836990E+01	0.82365853E+02
144	0.4600000E+02	0.11422457E-1	0.08713842E+01	0.87903893E+01	0.82532048E+02
145	0.4700000E+02	0.10942538E-1	0.08531501E+01	0.86061390E+01	0.82691156E+02
146	0.4800000E+02	0.10492219E-1	0.08356574E+01	0.84271634E+01	0.82843672E+02
147	0.4900000E+02	0.10069122E-1	0.08188610E+01	0.82502919E+01	0.82989653E+02
148	0.1000000E+02	0.23019811E+01	0.33125631E+01	0.40338604E+01	0.55203600E+02
149	0.2000000E+02	0.59863446E-01	0.19306625E+01	0.20213414E+01	0.72773098E+02
150	0.3000000E+02	0.26778316E-01	0.13207196E+01	0.13075937E+01	0.78536372E+02
151	0.4000000E+02	0.15095909E-01	0.09993368E+01	0.10106744E+01	0.81400917E+02
152	0.5000000E+02	0.9671944E-02	0.06027228E+01	0.30652766E+01	0.63130225E+02
153	0.6000000E+02	0.67196802E-02	0.06714075E+01	0.67376675E+01	0.82762300E+02
154	0.7000000E+02	0.49385218E-02	0.05753953E+01	0.57751083E+01	0.85094053E+02
155	0.8000000E+02	0.37618509E-02	0.05039027E+01	0.50531986E+01	0.85707955E+02
156	0.9000000E+02	0.29685606E-02	0.04481765E+01	0.44917190E+01	0.86165000E+02
157	0.1000000E+03	0.24209878E-02	0.04035282E+01	0.40425386E+01	0.86666668E+02
158	0.1100000E+03	0.2009693E-02	0.03669577E+01	0.36750291E+01	0.86678699E+02
159	0.1200000E+03	0.16814678E-02	0.03364573E+01	0.33687726E+01	0.87139019E+02
160	0.1300000E+03	0.14327948E-02	0.03106330E+01	0.31098332E+01	0.87359137E+02
161	0.1400000E+03	0.12354613E-02	0.02884870E+01	0.28675143E+01	0.87547802E+02
162	0.1500000E+03	0.10762578E-02	0.02692861E+01	0.26950116E+01	0.87711397E+02
163	0.1600000E+03	0.94595210E-03	0.02524800E+01	0.25265721E+01	0.87851369E+02
164	0.1700000E+03	0.83795324E-03	0.02376472E+01	0.23774970E+01	0.87980507E+02
165	0.1800000E+03	0.74744507E-03	0.02244596E+01	0.22450001E+01	0.88092799E+02
166	0.1900000E+03	0.67184716E-03	0.02126579E+01	0.21270373E+01	0.88193198E+02
167	0.2000000E+03	0.60544677E-03	0.02020347E+01	0.20212549E+01	0.88283538E+02
168	0.2100000E+03	0.54916367E-03	0.01924220E+01	0.19250043E+01	0.88365200E+02
169	0.2200000E+03	0.50037676E-03	0.01836822E+01	0.18375037E+01	0.88439520E+02
170	0.2300000E+03	0.4578170E-03	0.01757015E+01	0.17570120E+01	0.88507029E+02
171	0.2400000E+03	0.42066326E-03	0.01683853E+01	0.16843778E+01	0.88569830E+02
172	0.2500000E+03	0.38750126E-03	0.01616536E+01	0.16170025E+01	0.88628553E+02
173	0.2600000E+03	0.35726059E-03	0.01554397E+01	0.15548090E+01	0.88679072E+02
174	0.2700000E+03	0.33222320E-03	0.01496655E+01	0.14972242E+01	0.88724570E+02

176	0.2900000E+03	0.28798177E-3	-0.13936690E-01	0.15530672E-01	-0.83718205E+02
177	0.3500000E+03	0.2891380E-3	-0.133872327E-01	0.13475015E-01	-0.86855726E+02
178	0.3100000E+03	0.25212310E-3	-0.13137900E-01	0.13501350E-01	-0.83892618E+02
179	0.3200000E+03	0.23651848E-3	-0.12639610E-01	0.12632125E-01	-0.89527249E+02
180	0.3300000E+03	0.22240179E-3	-0.12247992E-01	0.12250110E-01	-0.86159756E+02
181	0.3400000E+03	0.20951221E-3	-0.11887870E-01	0.11684710E-01	-0.86890355E+02
182	0.3500000E+03	0.19771153E-3	-0.11548317E-01	0.11550099E-01	-0.89019213E+02
183	0.3600000E+03	0.18688048E-3	-0.11227620E-01	0.11229175E-01	-0.89046419E+02
184	0.3700000E+03	0.17691566E-3	-0.10924251E-01	0.10925684E-01	-0.89672222E+02
185	0.3800000E+03	0.16772711E-3	-0.10636843E-01	0.10636165E-01	-0.89096639E+02
186	0.3900000E+03	0.15923624E-3	-0.10364168E-01	0.10365392E-01	-0.89119603E+02
187	0.4000000E+03	0.15137417E-3	-0.101085123E-01	0.10106256E-01	-0.89141809E+02
188	0.4100000E+03	0.14418130E-3	-0.98537091E-02	0.98597018E-02	-0.89162713E+02
189	0.4200000E+03	0.13731181E-3	-0.96240261E-02	0.96250054E-02	-0.89182678E+02
190	0.4300000E+03	0.13098949E-3	-0.94012557E-02	0.94011680E-02	-0.89201686E+02
191	0.4400000E+03	0.12511321E-3	-0.91866530E-02	0.91875046E-02	-0.89219831E+02
192	0.4500000E+03	0.1196497E-3	-0.89825410E-02	0.89833379E-02	-0.89237169E+02
193	0.4600000E+03	0.11446138E-3	-0.87873021E-02	0.87861475E-02	-0.89253753E+02
194	0.4700000E+03	0.10964260E-3	-0.86013689E-02	0.86010677E-02	-0.89269631E+02
195	0.4800000E+03	0.10512183E-3	-0.84212227E-02	0.84218787E-02	-0.89287848E+02
196	0.4900000E+03	0.10087510E-3	-0.82493668E-02	0.82500136E-02	-0.89299468E+02
197	0.5000000E+03	0.24209878E-2	-0.40352826E-01	0.40425386E-01	-0.86566638E+02
198	0.2500000E+03	0.60544677E-3	-0.12203473E-01	0.20212549E-01	-0.88263538E+02
199	0.3000000E+03	0.26311388E-3	-0.13472327E-01	0.13475015E-01	-0.88155726E+02
200	0.4000000E+03	0.15137417E-3	-0.101085123E-01	0.10106256E-01	-0.89141809E+02
201	0.5000000E+03	0.96881420E-4	-0.80844228E-02	0.80850032E-02	-0.89313457E+02
202	0.6000000E+03	0.67278433E-4	-0.67371659E-02	0.67375918E-02	-0.89427017E+02
203	0.7000000E+03	0.49320212E-4	-0.57717895E-02	0.57750011E-02	-0.89509023E+02
204	0.8000000E+03	0.37043211E-4	-0.50529841E-02	0.50531258E-02	-0.89578921E+02
205	0.9000000E+03	0.2971779E-4	-0.44915078E-02	0.44916673E-02	-0.89618038E+02
206	0.1000000E+04	0.24221426E-4	-0.40424279E-02	0.40425015E-02	-0.89656176E+02
207	0.1100000E+04	0.2016895E-4	-0.36749456E-02	0.36750013E-02	-0.89687954E+02

NO OF P... = 2... =, 4

PR OF COND... = 0... =, 1

J... VALU OF P... = ...

I... VALU OF P... = ...

OPERATOR CORRECT...

.27... = 1... = .1522... + 1

.2... = 1... = .1997... + 1

0.1	0.1	0.1	0.1	0.1	0.1
0.11	0.11	0.11	0.11	0.11	0.11
0.12	0.12	0.12	0.12	0.12	0.12
0.13	0.13	0.13	0.13	0.13	0.13
0.14	0.14	0.14	0.14	0.14	0.14
0.15	0.15	0.15	0.15	0.15	0.15
0.16	0.16	0.16	0.16	0.16	0.16
0.17	0.17	0.17	0.17	0.17	0.17
0.18	0.18	0.18	0.18	0.18	0.18
0.19	0.19	0.19	0.19	0.19	0.19
0.2	0.2	0.2	0.2	0.2	0.2
0.21	0.21	0.21	0.21	0.21	0.21
0.22	0.22	0.22	0.22	0.22	0.22
0.23	0.23	0.23	0.23	0.23	0.23
0.24	0.24	0.24	0.24	0.24	0.24
0.25	0.25	0.25	0.25	0.25	0.25
0.26	0.26	0.26	0.26	0.26	0.26
0.27	0.27	0.27	0.27	0.27	0.27
0.28	0.28	0.28	0.28	0.28	0.28
0.29	0.29	0.29	0.29	0.29	0.29
0.3	0.3	0.3	0.3	0.3	0.3
0.31	0.31	0.31	0.31	0.31	0.31
0.32	0.32	0.32	0.32	0.32	0.32
0.33	0.33	0.33	0.33	0.33	0.33
0.34	0.34	0.34	0.34	0.34	0.34
0.35	0.35	0.35	0.35	0.35	0.35
0.36	0.36	0.36	0.36	0.36	0.36
0.37	0.37	0.37	0.37	0.37	0.37
0.38	0.38	0.38	0.38	0.38	0.38
0.39	0.39	0.39	0.39	0.39	0.39
0.4	0.4	0.4	0.4	0.4	0.4
0.41	0.41	0.41	0.41	0.41	0.41
0.42	0.42	0.42	0.42	0.42	0.42

1.1	1	2.1	1	1.1	1	1.1	1
1.2	1	2.2	1	1.2	1	1.2	1
1.3	1	2.3	1	1.3	1	1.3	1
1.4	1	2.4	1	1.4	1	1.4	1
1.5	1	2.5	1	1.5	1	1.5	1
1.6	1	2.6	1	1.6	1	1.6	1
1.7	1	2.7	1	1.7	1	1.7	1
1.8	1	2.8	1	1.8	1	1.8	1
1.9	1	2.9	1	1.9	1	1.9	1
1.10	1	2.10	1	1.10	1	1.10	1
1.11	1	2.11	1	1.11	1	1.11	1
1.12	1	2.12	1	1.12	1	1.12	1
1.13	1	2.13	1	1.13	1	1.13	1
1.14	1	2.14	1	1.14	1	1.14	1
1.15	1	2.15	1	1.15	1	1.15	1
1.16	1	2.16	1	1.16	1	1.16	1
1.17	1	2.17	1	1.17	1	1.17	1
1.18	1	2.18	1	1.18	1	1.18	1
1.19	1	2.19	1	1.19	1	1.19	1
1.20	1	2.20	1	1.20	1	1.20	1
1.21	1	2.21	1	1.21	1	1.21	1
1.22	1	2.22	1	1.22	1	1.22	1
1.23	1	2.23	1	1.23	1	1.23	1
1.24	1	2.24	1	1.24	1	1.24	1
1.25	1	2.25	1	1.25	1	1.25	1
1.26	1	2.26	1	1.26	1	1.26	1
1.27	1	2.27	1	1.27	1	1.27	1
1.28	1	2.28	1	1.28	1	1.28	1
1.29	1	2.29	1	1.29	1	1.29	1
1.30	1	2.30	1	1.30	1	1.30	1
1.31	1	2.31	1	1.31	1	1.31	1
1.32	1	2.32	1	1.32	1	1.32	1

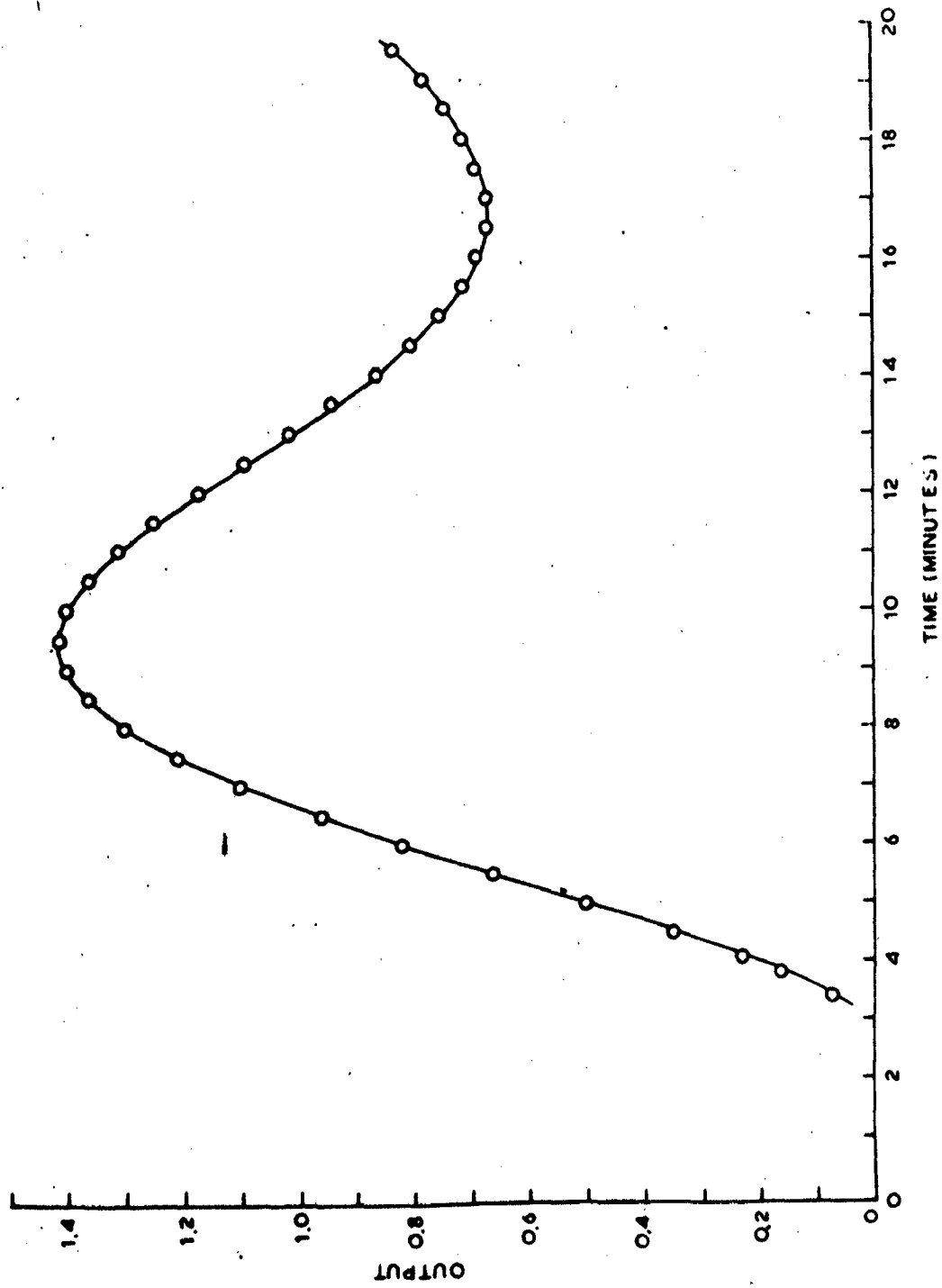


FIG TIME RESPONSE FOR EXAMPLE 2 CASE A2 ($\omega = 0$ TO 0.2)

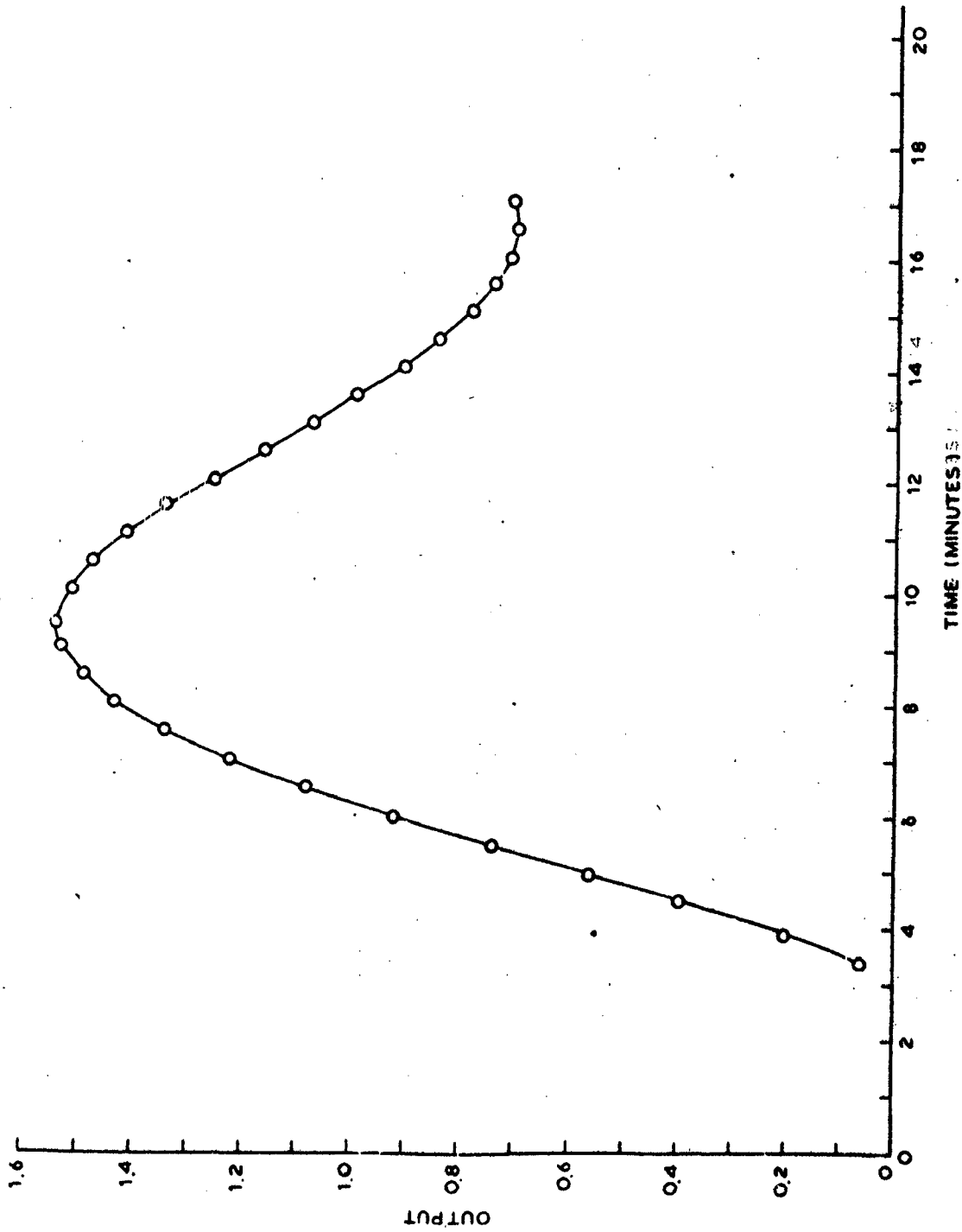


FIG TIME RESPONSE FOR EXAMPLE 2 CASE A3 ($\omega = 0$ TO 0.1)

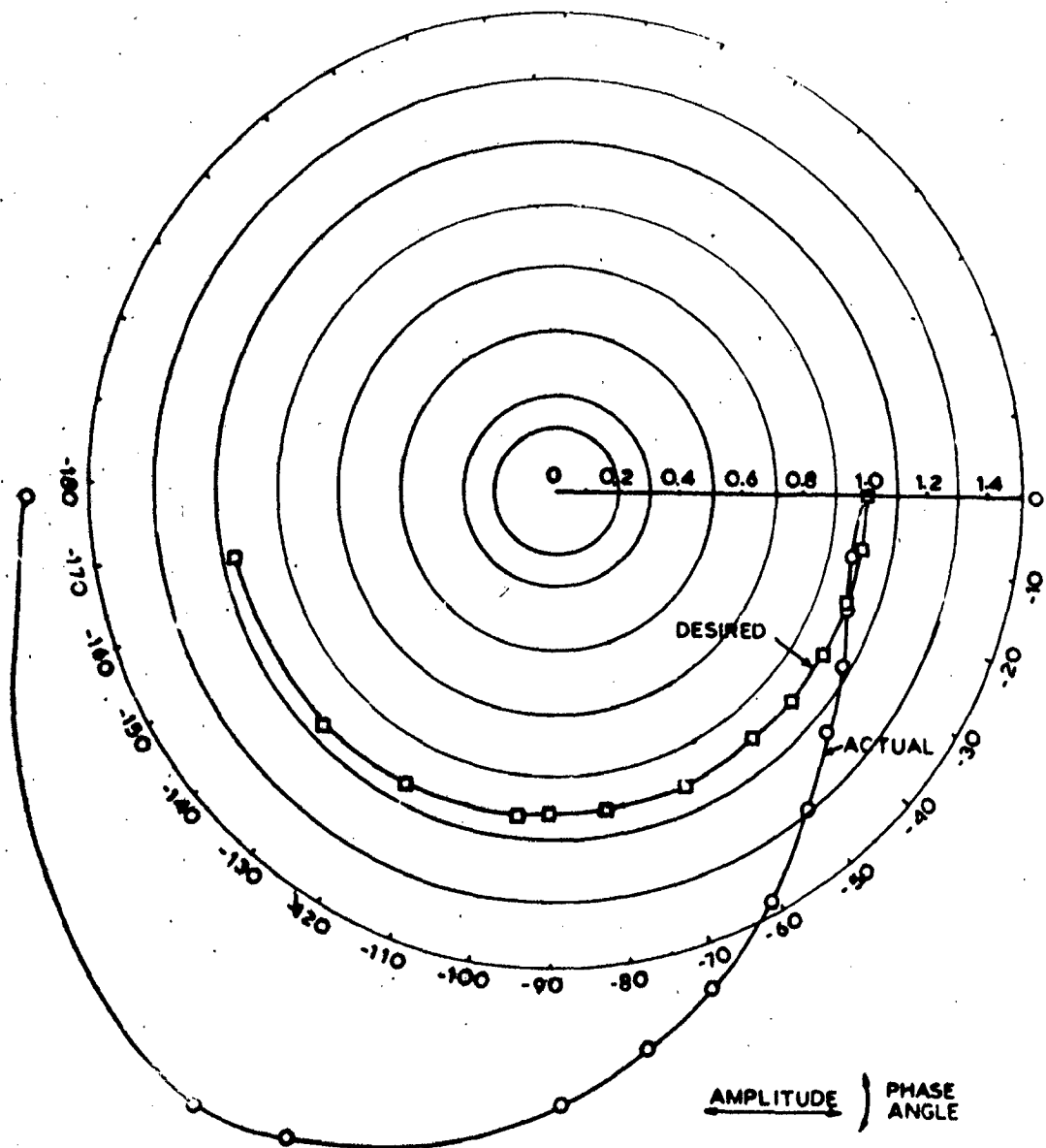


FIG FREQUENCY RESPONSE FOR EXAMPLE 2 CASE A1 ($\omega = 0$ TO 0.5)

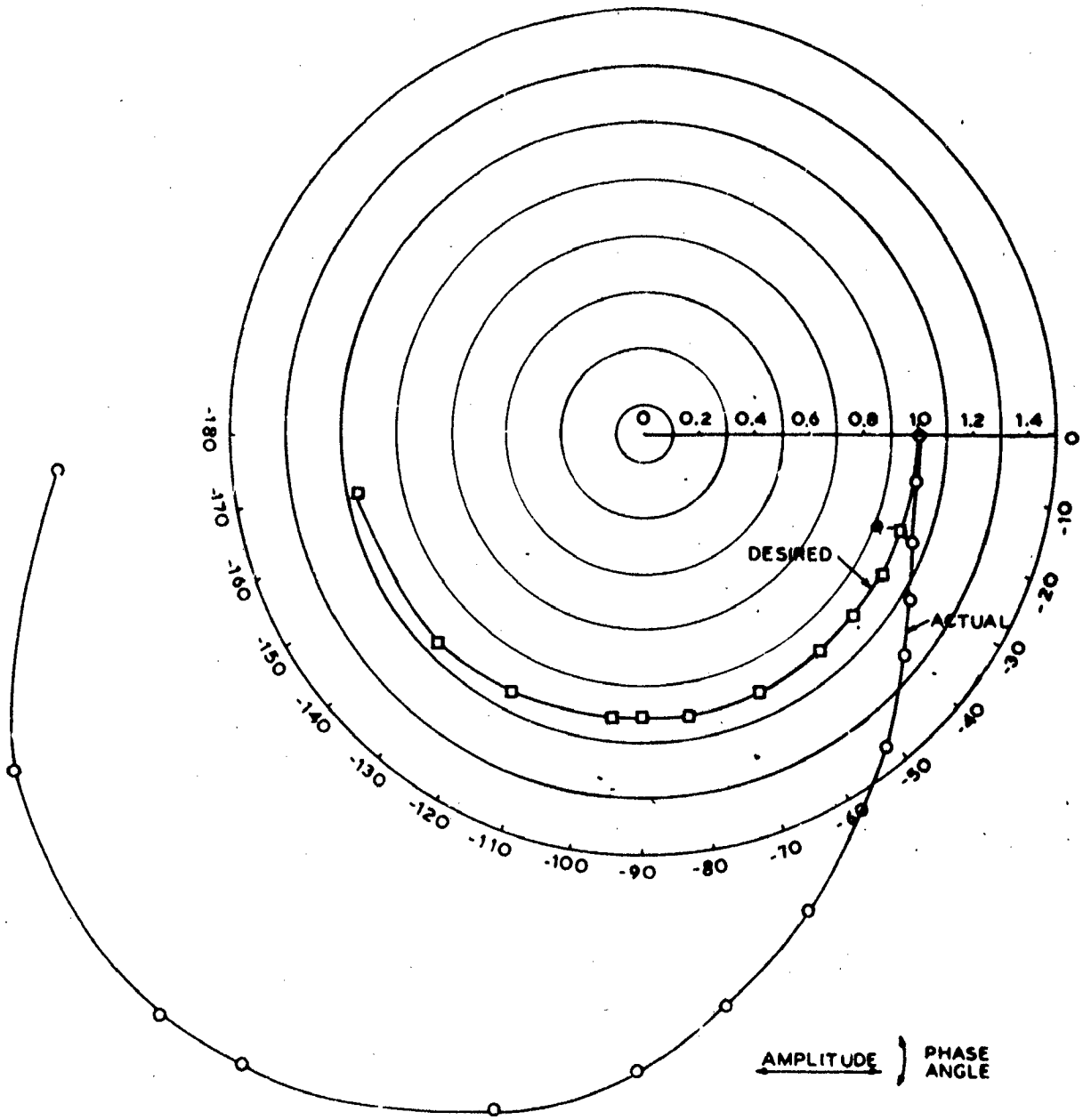


FIG FREQUENCY RESPONSE FOR EXAMPLE 2 CASE A3 ($\omega = 0$ TO 0.1)

V. CONCLUSIONS

In this work, optimization techniques have been used in the frequency domain design of single-input-single-output control systems. The suitability of using gradient methods for optimization to get the unknown controller parameters have been tested in this work. It is felt that other powerful parameter optimization techniques may be used to get better and quicker convergence.

It has been shown that this is a viable method for control system design for processes with/without time delay. The convergence of the results are dependent on a prior good choice of the controller parameters as well as on the range of frequency-interval (w_0, w_1) chosen in the performance index. It is found that a small value of w_1 (say 1 radian/sec.) normally leads to a good controller with quick convergence.

The ultimate effectiveness of this method may be found by testing on a range of real life process models and this work is relegated to future workers. It is felt that this is a new addition to the several methods of control system design available in the literature.

VI. REFERENCES

- [1] H.W. BODE, Network Analysis and Feedback Amplifier Design, D. Van Nostrand Reinhold Company, New York, 1945.
- [2] H.M. JAMES, N.B. NICHOLS and R.S. PHILLIPS, Theory of Servomechanisms, McGraw Hill Book Company.
- [3] W.R. EVANS, Control System Synthesis by Root Locus Method, Trans. AIEE, Vol. 69, 1950.
- [4] J.G. JRUXAL, Automatic Control System Synthesis, McGraw Hill Book Company, New York, 1955.
- [5] I.J. NAGRATH, M.GOPAL, Control Systems Engineering.
- [6] BENJAMIN, C.KUO, Automatic Control Systems.