

COMPARISON BETWEEN CONVENTIONAL AND ANN-BASED FLOOD FORECASTING METHODS

A DISSERTATION

*Submitted in partial fulfillment of the
requirements for the award of the degree
of*

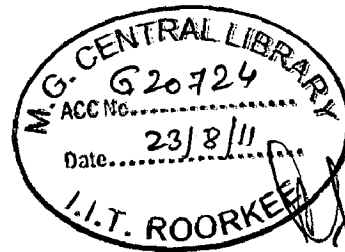
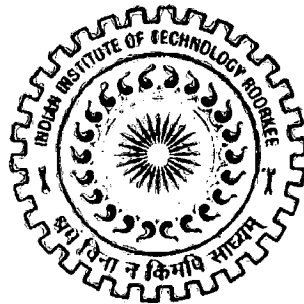
MASTER OF TECHNOLOGY

in

WATER RESOURCES DEVELOPMENT (CIVIL)

By

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JUNE, 2011**

CANDIDATE'S DECLARATION

I hereby certify that the work, which is being presented in this Dissertation entitled "**COMPARISON BETWEEN CONVENTIONAL AND ANN-BASED FLOOD FORECASTING METHODS**" in partial fulfillment of the requirements for the award of the degree of MASTER OF TECHNOLOGY in Water Resources Development (Civil) and submitted to the Department of Water Resources Development and Management, Indian Institute of Technology, Roorkee, is an authentic record of my own work carried out during the period from July 2010 to June 2011 under the supervision and guidance of Dr. S.K. Mishra, Associate Professor, Department of Water Resources Development and Management, Indian Institute of Technology, Roorkee, India.

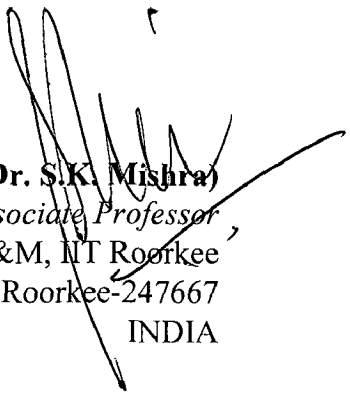
I have not submitted the matter embodied in this dissertation for the award of any other degree.

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CERTIFICATE

This is to certify that the above mentioned statement made by the candidate is correct to the best of my knowledge.


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Date: June, 2011

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ABSTRACT

Flood forecasting models have been developed for many different large rivers. Traditionally they are based on regressions of downstream with upstream gages. Recently, more physically based models have been used which consist of an input like areal averaged rainfall, gauge levels or discharges at upstream gauges measured in real time and transferred to the regional forecasting centre, where they are converted by means of suitable hydrological and hydraulic models into future water levels and discharges at some critical points. Basis of most models is a numerical model for the rainfall - runoff process, whose parameters are fitted to meet local conditions. In the hydrological context, as in many other fields, artificial neural networks (ANN) are increasingly used as black-box, simplified models. For hydrological applications, ANN models can take advantage of their capability to reproduce the unknown relationship existing between a set of input variables descriptive of the system, for example, rainfall and set of output variables, for example, river flow rate.

Mahanadi is a major river basin of eastern India comprising a catchment of 141569 sq. km. Its major part is occupied by Chhatisgarh and Odisha States. The basin lying in the South-West monsoon tract is exposed to myriad hydro-climatic variations. The reservoir Hirakud which drains nearly 83000 sq. km. is the prime flood moderation structure in the basin, and the catchment of about 50000 sq. km. remains unregulated. Both the Hirakud release and intercepted catchment cause the flood damage to about 9000 sq. km of delta. As such there is not a serious flooding problem existing in the upstream of Hirakud. However, the Mahanadi delta is threatened by floods every 2 or 3 years. Out of the 19 rainfall-generated floods observed during the post-Hirakud period, 13 were due to intercepted catchment contribution and 6 due to Hirakud dam releases. During these floods five coastal districts were affected and a great loss to life and property occurred. The option for another flood moderation structure is not justifiable due to several socio reasons. Presently, inflows to Hirakud are forecast by Central Water Commission, Govt. of India, using MIKE-11, NAM, and HD (Hydrodynamic) models. To this end, data from Automatic Weather Stations and satellite images are used. These

models however employ unit hydrograph and routing approaches, which may not be appropriate for deltaic regions, and therefore, may not be accurate.

In this study, three hourly stage data available for the monsoon period at the two gauge sites namely Khairmal and Naraj in Mahanadi basin have been used to develop an ANN-based forecasting model, and its performance evaluated. The performance criteria used are coefficient of determination (COD), Root Mean Square Error (RMSE), and Nash and Sutcliffe (1970) efficiency (NSE). Three cases were considered in model formulation. In Case-I which considers Khairmal stage only as input, ANN model is found to perform better than the conventional models. The former yielded NSE of 88%, RMSE = 0.47 m, and COD = 0.93 in calibration, and these values in validation are NSE=85%, RMSE = 0.46 m, and COD = 0.95. On the other hand, the latter exhibited NSE = 54%, RMSE = 0.94 m, and COD = 0.54 in calibration and NSE = 62%, RMSE = 0.76 m, and COD = 0.64 in validation. In Case-II which considers Naraj stage only as input, ANN model yielded NSE = 99%, RMSE = 0.11 m, and COD = 0.99 in calibration, and NSE= 99%, RMSE = 0.08 m, and COD = 0.99 in validation. The statistical model exhibited NSE = 99%, RMSE = 0.11 m, and COD = 0.99 in calibration and NSE = 99%, RMSE = 0.08 m, and COD = 0.99 in validation. In Case-III which considered both Khairmal and Naraj stages, the resulting ANN model yielded NSE = 99%, RMSE = 0.11 m, and COD = 0.99 in calibration, and NSE = 99%, RMSE = 0.08 m, and COD = 0.99 in validation. The counterpart statistical model exhibited NSE = 99%, RMSE = 0.12 m, and COD = 0.99 in calibration and NSE = 99%, RMSE = 0.09 m, and COD = 0.99 in validation. In Case-II and Case-III both ANN and statistical models have performed equally well, and therefore, statistical model can be opted instead of complex ANN model. In Case-I, the ANN model can be a better and more reliable option for forecasting the floods in deltaic situations.

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ABBREVIATIONS AND SYMBOLS

E	=	Efficiency
etc.	=	Et cetera
e.g.	=	exempli gratia (=for example)
et al.	=	et alia (=and others)
Fig.	=	Figure
i.e.	=	id est ("that is")
Km ²	=	Kilometer Square
m	=	metre
r	=	Correlation coefficient
σ	=	Standard deviation
ANN	=	Artificial Neural Network
ARIMA	=	Auto Regressive Moving Average
ARMA	=	autoregressive moving average
ARS	=	Agricultural Research Service
ATRG	=	Automatic Transmission Rain Gauge
BP	=	Back Propagation
CORR	=	Correlation coefficient
CWC	=	Central Water Commission
CWCFF	=	Central Water Commission Flood Forecast
DHI	=	Danish Hydraulic Institute
FF	=	Flood Forecasting

GIS	=	Geographical Information System
GUI	=	Graphical User Interface
HD	=	Hydrodynamic
HF	=	High Frequency
MLR	=	multiple- linear regression
MSE	=	Mean Square Error
NAM	=	Nedbor-Afstromnings-Model (<i>Rainfall-Runoff Model</i>)
NLP	=	Nonlinear Prediction
RMSE	=	Root Mean Square Error
SOFM	=	Self-Organizing Feature Map
SSARR	=	(Stream flow Synthesis and Reservoir Regulation
ST	=	Sediment Transport
SWAT	=	Soil and Water Assessment Tool
TD	=	Transport-Dispersion
USDA	=	United State Department of Agriculture
UK	=	United Kingdom
VHF	=	Very High Frequency
WFFS	=	Web-based flood forecasting system
WQ	=	Water Quality

Flooding has been a major concern for people inhabiting in the vicinity of rivers and water bodies since the dawn of civilization. Despite the fascinating developments achieved in many areas during the last three decades, the hazard of flooding has not yet been eradicated. In fact, recent floods seem to have been more abundant and more destructive in many regions of the globe than the earlier ones, and the projections for the future look gloomy. This calls for a need to re-think the strategy for flood preparedness. Traditionally, the strategy was to protect as far as was technically possible and affordable. However, since complete protection is never possible and an acceptable level of protection may be expensive, an alternative approach is to accommodate floods, i.e. to prepare to live with floods.

Floods are recurrent phenomena in India from time immemorial. Almost every year some or the other parts of the country are affected by floods of varying magnitudes. Different regions of the country have different climates and rainfall patterns and as such, it is also experienced that while some parts are suffering from devastating floods, another part is from droughts. With the increase in population and developmental activity, there has been a tendency to occupy the flood plains which has resulted in more and increasingly serious damages over the years. Because of the varying rainfall distribution, areas which are not traditionally prone to floods also often experience severe inundation. Thus, flood is the single most frequent disaster faced by the country.

A flood is an overflow of an expanse of water that submerges land. Flooding may result from the volume of water within a body of water, such as a river or lake, which overflows or breaks levees, with the result that some of the water escapes its usual boundaries. While the size of a lake or other body of water will vary with seasonal changes in precipitation and snow melt, it is not a significant flood unless such escapes of water endanger land areas used by man like a village, city or other inhabited area. Floods often cause damage to homes and businesses if they are placed in natural flood plains of rivers. While flood damage can be virtually eliminated by moving away from rivers and other bodies of water, since time out of mind, people have lived and worked by the water to seek sustenance and capitalize on the gains of

cheap and easy travel and commerce by being near water. That humans continue to inhabit areas threatened by flood damage is evidenced by the fact that the perceived value of living near the water exceeds the cost of (repeated) periodic flooding. Floods can also occur in rivers, when flow exceeds the capacity of the river channel, particularly at bends or meanders. In India, billions of rupees are spent every year in flood control and flood forecasting. The hydrograph of extreme floods and stages corresponding to flood peaks provide valuable data for hydrologic design. Further, of various characteristics of the flood hydrograph, probably the most important and widely used parameter is the flood peak. At a given location in a stream, flood peaks vary from year to year and their magnitude constitutes a hydrologic series which enables one to assign a frequency to a given flood-peak value. In the design of hydraulic structures, the peak flow that can be expected with an assigned frequency (say 1 in 100 years or so) is of primary importance to adequately proportion the structure to accommodate its effect. The design of bridges, culvert, waterways, and spillways for dams and estimation of scour at a hydraulic structure are some examples where flood-peak values are required.

Total control of flood is not practicable from economic considerations and therefore flood management is essential. The flood management rationally refers a provision of reasonable degree of protection against floods by structural/non-structural measures to mitigate the recurring havoc caused by floods. Non-structural measures like flood forecasting and warning of incoming floods have also played a significant role in reducing the loss of life and movable property apart from alerting the civil and engineering authorities, in-charge of various works to take appropriate advance action to fight the onslaught of floods.

Flood forecasting for a river basically means estimating future discharges or water levels in the river at selected places along the river during the flood season. The aim is to forecast river stage and its time of occurrence at a place along the river. For formulating flood forecasts, it is necessary to have relevant hydrological data, such as physical and geographical characteristics of the river catchment and flood plains, such as current levels of water and flow in the river; and hydro-meteorological data, such as rainfall in the catchment and weather forecast. Forecasting river flow or stage after heavy rain is important for public safety, environment, and water management. An early warning system is a set of procedures designed to protect human lives and

minimize damages to be expected from a flood which exceeds a certain critical level. It consists of a number of related and connected parts: forecasting, transformation of forecast into a warning, transmission of warning to local decision makers, conversion of warning into remedial action.

A forecasting model can be a black-box or a physically based, or a conceptual model. The black-box models are based on transfer functions which relate inputs with outputs. These models, as the name suggests, generally do not have any physical basis. Some commonly used black-box models include the unit hydrograph approaches, regression analysis, and time series models. The physically based models use the physical laws of various processes to model the catchments response. These laws are expressed through partial differential equations solved using numerical methods. The conceptual models fall intermediate to the physical and black-box models. Generally, the term 'conceptual' is used to describe models which rely on simple arrangement of a relatively small number of interlinked conceptual elements (such as storages), each representing a segment of land phase of hydrologic cycle.

1.1 Objective of the study

1. To propose an ANN-based flood forecasting method for deltaic region of Mahanadi basin.
2. To compare the forecasting results with those due to available conventional methods.

1.2 Organization of Work

The present thesis has been divided into six chapters including the present one. **Chapter 2** presents a review of the literature. **Chapter 3** contains methodology. **Chapter 4** presents the study area, data availability, and data processing. **Chapter 5** discusses the results, and finally, **Chapter 6** concludes the study.

The word "flood" comes from the Old English *flod*, a word common to Germanic languages (compare German *Flut*, Dutch *vloed* from the same root as is seen in *flow*, *float*; also compare with Latin *fluctus*, *flumen*). Deluge myths are mythical stories of a great flood sent by a deity or deities to destroy civilization as an act of divine retribution, and are featured in the mythology of many cultures. Flood forecasting is the use of real-time precipitation and stream flow data in rainfall-runoff and stream flow routing models to forecast flow rates and water levels for periods ranging from a few hours to days ahead, depending on the size of the watershed or river basin. Flood forecasting can also make use of forecasts of precipitation in an attempt to extend the lead-time available. It is an important component of flood warning distinguished in that the outcome of flood forecasting is a set of forecast time-profiles of channel flows or river levels at various locations, while "flood warning" is the task of making use of these forecasts to make decisions about whether flood warning should be issued to the general public or whether previous warnings should be rescinded or retracted.

2.1 DEFINITION OF FLOOD

General definition of flood in hydrology is "temporary covering by water of lands that are not normally covered by water". It is also defined as "an unusually high stage in a river – normally the level at which the river overflows its banks and inundates the adjoining area". Some definitions available on web in the context of water flow are quoted below:

- ✓ The rising of a body of water and its overflowing onto normally dry land; "plains fertilized by annual inundations" (wordnet.princeton.edu/perl/webwn).
- ✓ The temporary inundation of normally dry land areas resulting from the overflowing of the natural or artificial confines of a river or other body of water (www.grid.unep.ch/product/publication/freshwater_europe/glos.php).
- ✓ The inundation of a normally dry area caused by high flow, or overflow of water in an established watercourse, such as a river, stream, or drainage ditch; or ponding of water at or near the point where the rain fell. This is a duration

type event with a slower onset than flash flooding, normally greater than 6 hours (www.srh.noaa.gov/jetstream/append/glossary_f.htm).

- ✓ High flow, overflow or inundation of a normally dry area which causes or threatens damage. (ggweather.com/glossary.htm).
- ✓ Stream flow greater than the channel capacity (www.pskf.ca/publications/glossary.html).
- ✓ An event during which the volume of water in a stream becomes so great that it covers areas outside the stream's normal channel (www2.wwnorton.com/college/geo/earth2/glossary/f.htm).
- ✓ An overflowing of water beyond the channel's capacity (www.oas.org/cdmp/document/mitiplan/mitgloss.doc).
- ✓ Where a river overflows its banks and spreads out on the valley floor (www.swgfl.org.uk/rivers/waterwheel.htm).
- ✓ Any flow that exceeds the bank full capacity of a stream or channel and flows out of the floodplain; greater than bank full discharge (Buttecreekwatershed.org/ecr/new/glossary.htm).

2.2 CHARACTERISTICS OF FLOOD

The rise and fall of water level in river is called flood wave. Its highest point, or crest, travels progressively downstream. In the upstream portions of a river the flood crest passes quickly. Further downstream the greater volume of water causes slower passage of the flood crest, resulting in floods of longer duration. In many regions, annual floods follow the thaws and rains of spring: flooding may also occur because of thawing ice jamming narrower and shallower parts of a river. Less predictable are floods resulting from ocean waves, called storm surges, pushed onshore by an advancing hurricane, and from sudden torrential flows, called flash floods, following a brief, intense rainstorm or the bursting of a natural or man-made dam or levee. In addition to the duration and quantity of rainfall, the nature of the soil (permeability; state of saturation) of an area affects the frequency of floods. The following terms are frequently used to describe flood characteristics:

Intensity of floods is characterized by two methods (i) depth of inundation and (ii) area of inundation.

Frequency of floods represents the number of times an area is inundated during a particular time interval.

Durations of flood represent the length of time interval during which a particular area is inundated.

Meandering is due to changes its river because of siltation and erosion.

Severity of flood depends on damages caused by floods.

Flood typology also depends on types and magnitudes of damages caused.

River streams having velocity less than critical velocity have less silt carrying capacity and drops silts and sands and height of river bed is raised and surrounding areas are inundated. Such river stages are known as aggrading stage.

Degrading river (Erosions): River having velocity more than critical velocity erodes the river bed and known as eroding river.

2.3 CAUSES OF FLOOD

The major causes of flood are:

1. Due to heavy rainfall including cyclonic precipitation.
2. Inadequate capacity within banks of a river to contain high flows.
3. Poor natural drainage in an area or drainage congestion.
4. Synchronisation of high flows in main river and tributaries
5. Retardation of flow due to tidal and backwater effects, resulting in water stagnation and inundation, tsunamis.
6. Snowmelt and glacial outburst.
8. Heavy rainstorms/cloud-burst.

Apart from the overflow of rivers, the floods may also be caused by the failure of dams with sudden release of huge amount of water causing considerable damage to life and property.

2.4 FLOOD CONTROL MEASURES

The term 'flood control' is used to denote all efforts exercised to reduce damage to life and property caused by floods. From an extremely large flood occurring in a river the complete and strict control of the flood of negligible loss is neither physically possible nor economically feasible. However, there are ways by which to mitigate or minimize to some extent the impact of flood damage on people and property by adopting the following protective methods:

2.4.1 Structural measures

The structural measures comprise reservoirs and retarding structures which store peaks, channel improvements which increase flood carrying capacity, embankments and levees which keep the water away from flood prone areas, detention basins which absorb some flood water, flood ways which divert flood flows from one channel to another and overall improvement in the drainage system. In effect, the structural measures reduce the flood damage by restricting the movement of flood water in to the flood plains.

2.4.1.1 Storage Reservoirs

Flood control storage reservoirs have been built on many streams and rivers to store flood waters. A storage reservoir holds a portion of the flood waters when the flood is rising and releases it later when the flood is receding.

2.4.1.2 Detention Reservoirs

A detention reservoir stores excess water during floods and releases it after the flood. It is similar to a storage reservoir but it is provided with large gated spillways and sluiceways to release the stored water in a controlled way. In the earlier stages of a flood, the gates are left open and the water is released, subjected to the safe carrying capacity of the channel downstream. In the later stages of the flood, when the discharge downstream exceeds the maximum capacity of the downstream channel, the gates are kept partially closed. There is basically no difference between the detention reservoir and a storage reservoir, except that the former has a larger spillway capacity and sluiceway capacity to permit rapid downstream flow just before or after a flood. The reservoir is quickly emptied and thus the full reservoir capacity is made available again for moderating a subsequent flood after a short interval. In this manner, the available capacity is more effectively utilized.

2.4.1.3 Levees

Levees, also called dikes, are earthen walls which are constructed parallel to the river flow at some suitable distance from the river. Such walls or embankments may be raised either on both sides of the river or only on one side for some suitable distance, where the river is passing through towns and cities or other places of importance. These embankments retain and confine the flood water in between them, thereby preventing them from spreading into adjoining lands and towns. The levees being earthen walls require much care and maintenance. Although levees provide

protection from some floods, they can, being earthen, be eroded by large floods and cause enormous damage.

2.4.1.4 Flood Walls

Flood walls are used in a developed area where it is rather difficult to obtain enough land for the construction of levees. Because of flat slopes, levees require a very large base width. If the land is limited, it is more economical to construct flood walls. A flood wall is a reinforced concrete and cement (RCC) or masonry wall.

2.4.1.5 Channel Improvement

The improvement of river channels involves straightening, widening or deepening of channels to increase their discharge carrying capacity.

2.4.1.6 Flood ways

Flood ways are bypass and diversion channels into which part of the flood would be diverted during high floods. A floodway can be a natural or manmade channel and its location is controlled essentially by topography. Generally, wherever they are feasible, flood ways offer an economical alternative to other structural flood control works.

2.4.2 Non-structural measures

The non-structural measures include flood plain management, flood forecasting and warning, flood plain zoning, flood proofing, flood insurance etc., which play significant role in reducing flood damages.

2.4.2.1 Flood Plain Management

The structural measures have been emphasizing on the attempts to modify the floods. The non-structural measures on the other hand lay stress on attempts to modify the susceptibility to flood damage and attempts to modify the loss burden. They strive to keep the people away from flood waters, bearing in mind the stark reality that the flood plains in fact, belong to the river and that the floods are not only a curse but also a blessing in disguise in some ways. It contemplates use of flood plains judiciously, simultaneously permitting vacating of the same for use of the river whenever the situation calls for. This technique allows the use of flood plains reducing the hazard, while retaining its beneficial effects. Flood plain management which would comprise of flood forecasting and warning, flood plain zoning and flood proofing.

2.4.2.2 Flood Forecasting

Flood forecasting for a river basically means estimating future stages or water levels in the river at selected places along the river during the flood season. The aim is to forecast river stage and its time of occurrence at a place along the river. For formulating flood forecasts, it is necessary to have relevant hydrological data, such as physical and geographical characteristics of the river catchment and flood plains, such as current levels of water and flow in the river; and hydro-meteorological data, such as rainfall in the catchment and weather forecast. These data are then the basic input to flood forecasting techniques, which may include graphical techniques, rainfall runoff models, unit hydrograph and computer models.

2.4.2.3 Flood Plain Zoning

Flood plain zoning means restricting any human activity in the flood plains of a river. The areas affected by floods are divided into different zones in flood plain zoning. The area affected by flood increases as the flood discharge increases. The flood discharge depends upon the recurrence interval. Therefore, the flood plain zoning can be done according to the recurrence interval. For example, flood zones can be demarcated as zones of 1, 2, 5, 10, 15, or 100 year floods. Evidently, the area under a 100-year flood will be much more than under a 5-year flood. The basic objective of flood plain zoning is to restrict encroachment of the zone which frequently comes under the influence of flood. The areas which are prone to yearly flood may be put to agricultural uses. However, crops and vegetables grown in these zones should be of such types that they are harvested well before the start of the next rainy season.

From the past experience it is learnt that, the structural measures can not altogether eliminate the residual hazard from rare flood events primarily due to high cost and topographical constraints. Therefore, along with the structural measures, adequate attention is needed for planning and implementation of non-structural measures, the urgent among these being flood forecasting and warning, so also flood plain zoning and management.

2.4.2.4 Flood Proofing

Any combination of structural and non-structural additions, changes, or adjustments to structures which reduce or eliminate flood damage to real estate or improved real property, water and sanitary facilities, structures and their contents. Flood Proofing is the provision of long term, non structural or minor structural measures to mitigate the effects of floods.

Non Structural Flood Proofing Measures are

- Institutional measures to coordinate development activities related to flood control and drainage;
- Planning developments in flood-prone areas to take account of prevailing hydrological conditions; and
- Ensuring hydrological data and analysis are available to those involved with design.

2.4.2.5 Flood Insurance

Though flood risk has been included in the list of items covered by General Insurance Companies, it is popular in urban areas only. The insurance companies have also not been able to arrive at different rates of insurance premiums for different areas. Therefore, there is a need to evaluate the risk associated with flooding of different areas and to modify the insurance schemes based on it.

2.5 WHAT IS FLOOD FORECASTING

Flood forecasting may be defined as "the process of estimating the future stages or flows and its time sequence at selected points along the river during floods". Flood forecasts are prediction of (i) the crest and its time of occurrence; and (ii) the stages expected at various points of time during the period of rising and falling stages of the river above or specified water level called the "Warning Level".

Some other relevant definitions are as follows:

- § *Forecasting*: estimation of some variable at a specific future time or over a specified future time interval.
- § *Prediction*: estimation of future conditions, without reference to a specific time.
- § *Real-time forecasting*: forecasts are made based on the current conditions.
- § *Lead time*: time (interval) over which a forecast is made.

Utility of the forecast depends on accuracy and timeliness. At the time of the event, the value of the forecast is zero. Hence, the entire operation of the flood forecasting service has to be planned around a time-factor keeping in view that the operational data being generally poor and incomplete; a compromise between the theoretically desirable complications and computational details becomes necessary. This calls for use of appropriate techniques or methods to meet the requirements of

accuracy and period of warning to different locations, and then there should be efficient arrangement for dissemination of forecasts/information. Attempts should be to convey the forecasts/warnings to the authorities concerned such that they get adequate time to organize necessary measures, if required in light of the forecasts issued.

2.6 WHY FLOOD FORECASTING

Most emergency measures during floods require prediction of incoming flood with the help of hydrological and hydro-meteorological analysis, rapid warning to flood plain inhabitants and advance preparation involving provision of flood-fighting materials and a plan of action for intense activity immediately prior to, during and immediately following flooding. Once the flood forecasts are received by the Civil and Engineering authorities, the chain of activities start- warnings are issued, people and property are evacuated immediately prior to flood, patrolling of the affected area is organised, protection works including sealing off inlet points are affected and rescue operations are done during the flood and, after the flood recedes, rapid drainage, clean-up and rehabilitation follow.

Experience has shown that damage to movable property as well as loss of human and cattle lives etc., can be reduced to a considerable extent by forecasting flood with adequate warning time. On receipt of such advance warnings, the people can move to safer places in an organised manner with their movable property and cattle. Conversely, this may also, by providing appropriate reassurance, avoid costly and unnecessary evacuation. In the long-range plan of flood protection and prevention of flood damages, the flood forecasting services assumes considerable significance not only in the unprotected flood prone areas for organising rescue and relief operation but also in the area already protected by giving advance warning to the engineering authorities, for keeping desired vigil and safeguarding various structures. Short-term forecasts or flood forecasts of several hours and days provide flood warnings which can be used to operate reservoirs and emergency flood ways. It has now been universally recognised as an important component of flood-fighting and flood damage mitigation measures. As a matter of fact, in numerous situations when topographic (lack of potential dam sites) and or economic factors make the control of flood impractical and/or unjustifiable on economic consideration and in other cases

until such times as the flood control measures to provide positive protection against flood damage are implemented, flood forecasting provides an alternative means of reducing flood damage including loss of life.

Flood forecasting also plays a very important role in reducing flood damages by helping in proper regulation of reservoirs because an ideal operating procedure requires perfect fore knowledge of the inflow and the hydrograph shape. A properly planned hydrologic forecasting system not only helps in moderation of floods but also in overall management of the available water resources for various purposes.

2.7 METHOD FOR DETERMINING THE PEAK FLOOD

The hydrograph of extreme floods and stages corresponding to flood peaks provide valuable data for purposes of hydrologic design. Further, of the various characteristics of the flood hydrograph, probably the most important and widely used parameter is the flood peak. At a given location in a stream, flood peaks vary from year to year and their magnitude constitutes a hydrologic series which enable one to assign a frequency to a given flood-peak value. In the design of practically all hydraulic structures the peak flow that can be expected with an assigned frequency (say 1 in 100 years) is of primary importance to adequately proportion the structure to accommodate its effect. The design of bridges, culvert waterways and spillways for dams and estimation of scour at a hydraulic structure are some examples wherein flood-peak values are required.

To estimate the magnitude of a flood peak the following alternative methods are available:

1. Rational method,
2. Empirical method,
3. Unit-hydrograph technique, and
4. Statistical or Frequency method.

The use of particular methods depends on (i) the desired objective, (ii) the available data, and (iii) the importance of the project. Further, the rational formula is only applicable to small size (<50 km²) catchments and the unit hydrograph method is normally restricted to moderate-size catchments with areas less than 5000 km².

2.8 STEPS OF FLOOD FORECASTING

Flood forecasting for a river basically means estimating future stages or water levels in the river at selected places along the river during the flood season. The aim is to forecast river stage and its time of occurrence at a place along the river. For formulating flood forecasts, it is necessary to have relevant hydrological data, such as physical and geographical characteristics of the river catchment and flood plains, such as current levels of water and flow in the river; and hydro-meteorological data, such as rainfall in the catchment and weather forecast. These data are then the basic input to flood forecasting techniques, which may include graphical techniques, rainfall runoff models, unit hydrograph and computer models.

A flood forecasting system basically involves five steps. It begins from data collection to warning received by end user. The steps are (CWC, 1980),

- (i) Data collection
- (ii) Data dissemination
- (iii) Data processing and Formulation of forecasting
- (iv) Verification of forecast
- (v) Dissemination of forecast

The above steps are shown in flow chart given in Fig. 2.1

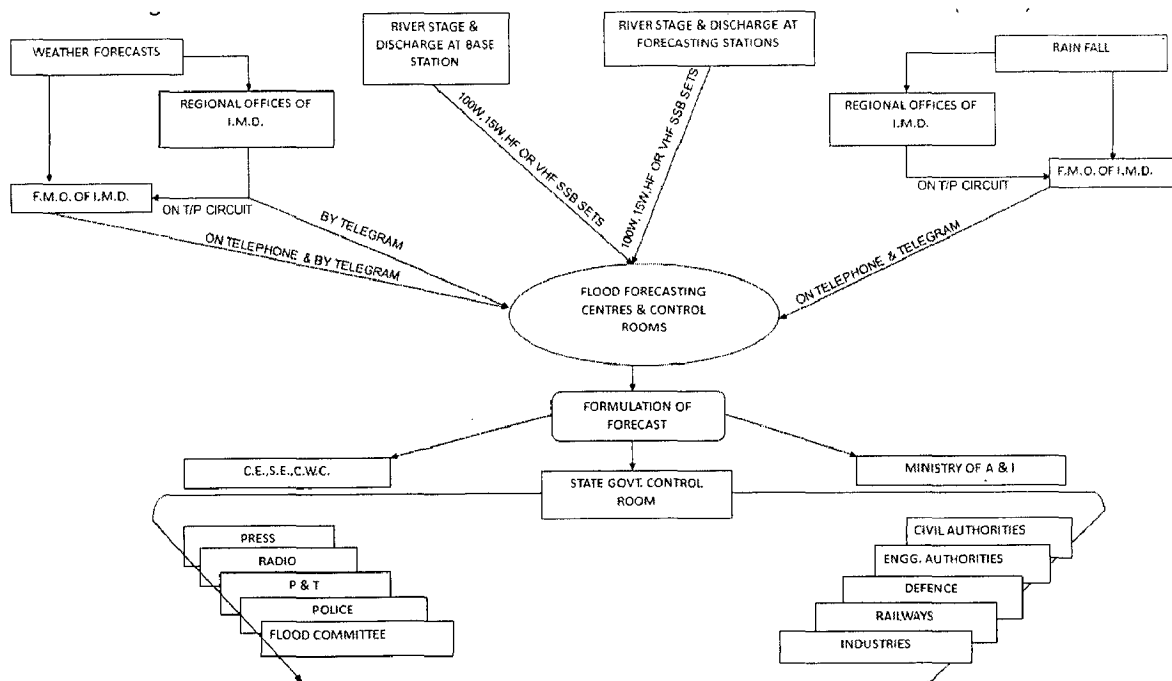


Fig 2.1: Schematic diagram of existing flood forecasting system in India.

2.8.1 Data Collection

A large number of hydrological and hydro-meteorological data are required for development of a river forecasting model and for operational forecast formulation. At the development stage of a flood forecasting model, all the available historical data can be utilised for identification of the various parameters of the model where as at the time of actual forecast formulation, only limited number of data may be available in time. Hence the term "Data Collection" in a broader sense means;

- (a) Collection of all possible historical data from various sources for development of flood forecasting model; and
- (b) Identification of representative or key data network where real time data transmission can be ensured with available resources.

Data Required:

- i. Gauge/discharge and/or rainfall data are required for flood forecasting
- ii. Interception, evaporation, evapo-transpiration, interflow, infiltration, ground water and percolation are also used as inputs to several conceptual models
- iii. Number of reporting stations depend upon hydrologic need, availability of observers and communication;
- iv. Density of rain gauge station required vary with basin topography and meteorological factors
- v. 8 to 10 years of basic hydrological and meteorological data to develop a workable forecasting method.

2.8.2 Data Transmission

Transmission of data from the field stations to the flood forecasting centres plays a very vital role in flood forecasting. Transmission of data essentially refers to the transmission of limited number of data to be used for operational forecast formulation through a quickest possible channel. If a good deal of time is wasted in transmission of hydrological and hydro-meteorological data from the field stations, there will be hardly any sufficient time left for formulation of forecast and subsequent warning. Transmission of the observed data on real time basis is therefore, extremely necessary for efficient flood forecasting.

The essential requirements of a good transmission system are that it should be reliable, quick, and capable of transmitting data at desired frequency, expandable, cheap and computer compatible.

Various systems of Data Transmission:

Some of the most commonly used data transmission systems all over the world are:

- a) Land line communication, i.e. telephone and telegraph
- b) HF and VHF wireless network; and
- c) Telemetry system including ATRG (Automatic Transmission Rain Gauge), satellite radar, mobiles, internet and FAX.

2.8.3 Data Processing and Formulation of Forecasting

The analysis of data and formulation of forecast is the most important stage in the process of flood forecast. Some model is used to estimate the forecast from the available hydrological and hydro-meteorological data. The model may be a simple gauge to gauge relation between upstream and downstream gauges or a very comprehensive catchment model like Stanford Watershed Model Mark IV incorporating a large number of hydrological, hydro-meteorological, and basin parameters. The use of appropriate model depends on the availability of data, forecast requirement, computational facilities, and the degree of accuracy desired etc.

The methods for formulating the real time flood forecast may be categorized under two groups: Statistical and deterministic methods.

2.8.3.1 Statistical Methods

Methods based on statistical approach making use of statistical techniques can be presented either in the form of graphical relations or mathematical equations. A large number of data covering a wide range of conditions are analysed to derive the relationship which are inter-alia include gauge to gauge relationship with or without additional parameter and rainfall peak stage relationships. These methods are more commonly used by the Central Water Commission to issue real time forecast in India.

Method based on statistical approach makes use of the statistical techniques to analyse the historical data with an objective to develop methods for the formulation of flood forecasts. The methods thus developed can be presented either in the form of

graphical relations or mathematical equations. A large number of data, covering a wide range conditions are analysed to derive the relationships which inter-alia include gauge to gauge relationship with or without additional parameter and rainfall peak stage relationship.

In the technique of gauge/discharge correlation the various variables which affect the stage at the forecasting point are:

- i. Stage and discharge of the base station;
- ii. Stage and discharge of the forecasting station;
- iii. Change in stage and discharge of the base station;
- iv. Travel time at various stages;
- v. The rainfall (amount, intensity and duration) in the intercepting catchment;
- vi. Topography, nature of vegetation, type of soil, land use, density of population, depth of ground water table, soil moisture efficiency etc. of the intercepted catchment;
- vii. The atmospheric and climatic conditions; and
- viii. Stage and discharge of any important tributary joining the main stream between the base station and forecasting station.

Factor (i) to (iv) are basic parameters used in developing the correlation curve. Factor (v) and (vi) are taken in to account by introducing the rainfall and API. Factor (vii) is a minor one and can be considered by introducing an additional parameter. The factor (viii) is very important and can be neglected if the contribution of the tributary is very small. In many hydrologic studies, regression methods like multiple-linear regression (MLR), autoregressive moving averaging (ARMA) and autoregressive integrated moving average (ARIMA) have been used extensively by various researchers for river flow and stage forecasting (Tingsanchali and Gautam 2000); Bruen and Yang, 2005).

(a) Direct correlation between gauge and discharge at U/S and D/S

In such case, only gauge and discharge data of the base stations and forecasting stations are utilised in different forms. The simplest of all is the correlations between the N^{th} hour stage of base station and $(N+T)^{\text{th}}$ hour stage of forecasting stations; where T is the travel time of flood wave between the base station and the forecasting station.

This type of relations can be developed and used for a reach of the river where there is no major tributary with considerable discharge, catchment between the two

stations is small so that the effect of rain is negligible and the travel time from base station to the forecasting stations is fairly constant for various stages.

However, in most of the cases the travel time is not constant and varies with water level. Apart from this such relations give considerable errors under different conditions. These relations can be considerably improved if the following aspects are taken into account:

- The variation in travel time- This can be taken into account by appropriately drawing a travel time-curve (U/S stage Vs travel time).
- Varying conditions during rising and falling stages of the flood- It is always desirable to draw separate curves for rising and falling conditions.
- Downstream boundary condition- This is also a very important factor, especially for the forecasting in the lower reaches of the river which falls in the sea or a larger river. When the outfall channel is in high stage or there is high tide in the sea, it will definitely have back water effect and the water level in the falling stream will be different than that normal conditions. Hence it is always desirable to take into account the tidal effect or the water level of outfall channel.
- Characteristic of flood wave- Generally the forecast at downstream stations are quite reliable when the storm results in the formation of single peak. But with one flood wave immediately followed by another there is considerable effect in the water level at the downstream station in different conditions. For example when a smaller flood wave is followed by a comparatively larger flood wave with high peak, the two flood waves may overlap resulting in slight increase in the level at downstream station than the normal case. On the contrary, if a larger flood wave is followed by a smaller flood wave, the same flood wave may not have any effect by the time it reaches the downstream station.

Finding correlation between stage and discharges between upstream and downstream gauging stations is one of the simplest methods. This gives better result when there is less influence of tributaries joining the main stream in between or the intercepted catchment is not influenced by heavy rainfall. Here correlation between upstream gauge and downstream gauge has been derived by simple mathematical equation with corresponding travel time.

Vieira et al. (1993) used the statistical model, which is based on a multiple regression technique, extends the forecasting range of the model from 3 hrs up to 24 hrs, and presents good accuracy (estimated mean absolute errors smaller than 10 cm) for short-term forecasts up to 9 hrs. Historically, researchers have relied on conventional modelling techniques, either deterministic, which consider the physics of the underlying process, or systems theoretic/black box (Jain et al., 2003). Jain et al., (2003) further investigated the suitability of some deterministic and statistical techniques along with the artificial neural networks (ANNs) technique to model an event-based rainfall-runoff process. Specifically, two unit hydrograph models, four regression models, and two ANN models were developed.

Abudu et al. (2010) used the application of partial least-squares regression (PLSR) in seasonal stream flow forecasting was investigated using snow water equivalent, precipitation, temperature from automatic Snow Telemetry sites, and previous flow conditions as input variables. The forecast performance of PLSR models was compared to principal components regression (PCR) models as well as to the Natural Resources Conservation Service (NRCS) official forecasts in three basins. The results indicated that using a correlation-weighted precipitation index is a relatively effective method in both improving forecast accuracy and developing relatively parsimonious regression models.

2.8.3.2 Deterministic methods

SSARR (Stream flow Synthesis and Reservoir Regulation) model, Sacramento Model, NAM-System 11 FF model (MIKE-11), HEC-1D, CWCFF1 and SWAT are some of the conceptual watershed models for formulating the real time flood forecast.

(i) SSARR (Stream flow Synthesis And Reservoir Regulation) Model

The Stream flow Synthesis and Reservoir Regulation (SSARR) Model was developed to provide mathematical hydrologic simulations for systems analysis as required for the planning, design, and operation of water control works. The SSARR Model has been further developed for operational river forecasting and river management activities. As a general purpose mathematical model of a river system, the SSARR Model is a useful tool for stream flow and runoff forecasting, as well as for long term studies of the hydrology of a river system.

(ii) The Rainfall-Runoff Model, NAM

NAM is a deterministic rainfall-runoff model of the lumped conceptual type. NAM is an abbreviation of the Danish: "Nedbor-Afstromnings-Model", meaning precipitation-runoff-model. This model was originally developed by the Hydrologic Section of the Institute of Hydrodynamics and Hydraulic Engineering at the Technical University of Denmark (Nielsen and Hansen 1973). The NAM model has been further developed and extensively applied by DHI (Jonch-Clausen and Refsgaard 1984). NAM simulates the rainfall-runoff process in rural catchments. It operates by accounting continuously for the moisture content in five different and mutually interrelated storages representing physical elements in the catchment.

The data input requirements are precipitation, potential evapo-transpiration and (only if snow occurs) temperature data. The sampling interval of the input data can be given arbitrarily. Thus, typically, for flood modelling six-hourly or three hourly rainfall data would be appropriate, while daily rainfall data would be sufficient for most other purposes.

For the purpose of flood forecasting a hydrological model of the NAM-type and complexity is believed to be appropriate. It has been documented both by Kitandinis and Bras (1978) and by Jorgensen (1981), that conceptual models are superior to black box models (as e.g. the ARIMA type of models) for flood forecasting. A more complex conceptual model will probably not yield better stream flow simulations because the main uncertainty in the rainfall-runoff modelling of the flood situations usually pertains to the assessment of the rainfall input.

The NAM model is a well proven engineering tool which has been applied successfully to more than 50 catchments in different climatic regions throughout the World. Hence, in addition to numerous applications in Denmark, it has been applied for water supply studies in Borneo, Tanzania and Sri Lanka, irrigation and flood control studies in Thailand, flood forecasting and flood control studies in India, and for hydropower studies in Greenland and Tanzania.

(iii) MIKE-11

MIKE-11 is a menu-driven software package for the simulation of flows, sediment transport and water quality in rivers, estuaries, irrigation systems and similar

water bodies. The simulation system is comprised of 4 modules:-(i)A hydrodynamic module(HD) which computes discharges and water level variations in rivers and flood plains, (ii) A sediment transport module(ST),(iii) A transport-dispersion module(TD), and (iv) A water quality module(WQ).

The MIKE-11 system also includes a rainfall-runoff model (NAM) which stimulates catchment runoff to the river composed of overland flow, interflow and base flow. For forecasting of discharge and water levels in real-time a special flood forecasting module has been added (FF). It streamlines and facilitates the data management, model simulations and updating required for operational flood forecasting in real-time.

The HD basis module has three options for solving the governing hydrodynamic equations (Saint Venant equations), namely fully dynamic wave, diffusive wave and kinematic wave approximation. Selection of wave approximation type depends on river topography and flow conditions.

(iv) Unit Hydrograph based models:

In India, the applications of unit hydrograph technique are restricted to the catchments of sizes less than 5000 Sq. Km. However, for the catchments of size more than 5000 sq. km., a network model is developed. In this model the catchment is divided in to sub-catchments and the main river is divided in to sub-reaches, considering the two consecutive nodes. The nodes are the points where the tributary of the sub-catchments join the main river. The principle of unit hydrograph is applied for converting the excess rainfall to direct surface runoff for each sub-catchment parameters as additional rainfall runoff data are reported and using these updated parameters the future flows are estimated for forecasting. Gosain (1984) has used a Unit Hydrograph based real-time flood forecast model on River Yamuna.

(v) HEC-RAS

It is an integrated package of hydraulic analysis programs, in which the user interacts with the system through the use of a Graphical User Interface (GUI). The system is capable of performing Steady and Unsteady Flow water surface profile calculations, and will include Sediment Transport and several hydraulic design computations in the

future.

HEC-RAS has the ability to import three-dimensional (3D) river schematic and cross section data created in a GIS or CADD system. While the HEC-RAS software only utilizes two-dimensional data during the computations, the three-dimensional information is used in the program for display purposes. After the user has completed a hydraulic analysis, the computed water surface profiles can be exported back to the GIS or CADD system for development and display of a flood inundation map. The HEC has developed an Arc View GIS extension called GeoRAS that was specifically designed to process geospatial data for use with HEC-RAS. The Geo-RAS software allows a user to write geometric data to a file in the required format for HEC-RAS. HEC-RAS contains five optional methods for specifying floodplain encroachments. This is again a public domain model and shall be used for assessing flood inundation areas.

(vi) CWCF1 (Central Water Commission Flood Forecast 1)

The fundamental of concept of the CWCF1 (Central Water Commission Flood Forecast 1) model is based on the fact that fluid tends to maintain uniform levels under free conditions. When fluids of two different chambers with different levels are allowed to mix freely, their new levels after a certain time interval will depend on their levels at the beginning of the time interval and the time lapse.

In this model a river channel is visualized as comprising of a number of parallel slices. As water flows through these slices various processes take place simultaneously between each two adjoining slices; major processes are identified as follows:

1. Water flows from higher elevation to lower elevation;
2. Some of the water is absorbed and retained in the dry river banks;
3. Some of the water evaporates;
4. Some of the water spreads away from the river bank and returns to the main stream when the river stage falls;
5. Some of the spilled water crosses the river bank and is held up in pits and low-lying areas, never returning to the main stream;
6. At some places water takes a separate course and joins the river downstream.

The above processes are dependent on the following physical processes:

- a) Process 1 depends on the difference of levels of water in the two adjoining slices and slope of the river bed;
- b) process 2 depends on the dryness of river banks, which in turn depends on the previous maximum water level and the lapse of time since its occurrence;
- c) process 3 depends on the dryness of the air and the air temperature;
- d) Process 4, 5 and 6 depend on the slope of the river, bank conditions and river characteristics.

In this model, processes 1, 4, 5 and 6 are combined together as characteristics of a river channel at a particular location which remain almost unchanged.

(vii) SWAT (Soil and Water Assessment Tool)

SWAT is the acronym for Soil and Water Assessment Tool, a river basin, or watershed, scale model developed by Dr. Jeff Arnold for the USDA Agricultural Research Service (ARS). SWAT was developed to predict the water and sediment yield in large complex watersheds with varying soils, land use and management conditions. SWAT is a continuous time model. The model has a real-time flood forecasting component also. The present version of the model has a interface on ArcGIS. The model is a public domain model.

(viii) Artificial Neural Network (ANN)

ANN is a computational method inspired by the studies of the brain and nervous system in biological organisms (Schalkoff, 1997). One of the characteristics of the neural network is their ability to learn. A neural network is not programmed like a conventional computer program, but is presented with examples of the pattern, observations and concepts, or any type of data which it is supposed to learn. Through the process of learning (also called training) the neural network organizes itself to develop an internal set of features that it uses to classify information or data. Due to this massively parallel processing architecture the ANN is capable of efficiently handling complex computations, thus making it the most preferred technique today for high speed processing of huge data. ANN has been in existence since the 1940s, but since current algorithms have overcome the limitations of those early networks

great interest in the practical applications of ANN has arisen in recent decades. ANN have been proven to provide better solution when applied to (1) complex system that may be poorly described or understood; (2) problem that deals with noise or involve pattern recognition, diagnosis, abstraction, and generalization; and (3) situations where input is incomplete or ambiguous by nature. It has been reported that an ANN has the ability to extract patterns in phenomena, which avoids the selection of a model form such as linear, power, or polynomial. ANN Model is another class of Black Box models introduced for modelling real time problems where the nonlinear relationship between the rainfall and runoff process exists. The use of ANN in real time flood forecasting is of very recent origin (Lekkas et al., 2004).

Artificial neural networks are a type of parallel computer structure, within which a number of processing units are linked together so that the computer's memory is distributed and information is passed in a parallel manner. A large number of ANN architectures and algorithms have been developed so far, multilayer feedforward networks (Rumelhart *et al.*, 1986), self-organising feature maps (Kohonen, 1982), Hopfield networks (Hopfield, 1987), counter propagation networks (Hecht-Nielsen, 1987), radial basis function networks (Powell, 1987) and recurrent ANNs (Elman network; Elman, 1988). Of these networks, the most commonly used are feed forward networks and radial basis function networks (Karunanithi, *et al.*, 1994; Bishop, 1995). Multi-layer feed forward networks have been found to perform best when used in hydrological applications (Hsu *et al.*, 1995; Dawson and Wilby, 1999) and as such they are by far the most commonly used (Maier and Dandy, 2000). The attempt to choose between different methods and define which is the superior, is likely to fail as in most cases the choice should be "application oriented". It is preferable for every new application to test different types of ANNs rather than use a pre-selected one.

Training: To train an ANN, the following procedure is generally applied. Training data patterns are fed sequentially into the input layer, and this information is propagated through the network. The resulting output predictions $y_j(t)$ are compared with a corresponding desired or actual output, $d_j(t)$. The mean squared error at any time t , $E(t)$, may be calculated over the entire data set using Equation (2.1). The

intermediate weights are adjusted using an appropriate learning rule until $E(t)$ has decayed sufficiently.

$$MSE(t) = \frac{1}{2} \sum_{j=1}^n (y_j(t) - d_j(t))^2 \quad (2.1)$$

A wide range of training algorithms has been developed to achieve optimum model performance. For feed forward ANNs, the error back propagation algorithm with the gradient descent update rule (Rumelhart *et al.*, 1986) is most commonly employed. However, there are a number of inconvenient drawbacks associated with the use of this algorithm. For example, prior to ANN training it is necessary to specify the network architecture, that is, the number and configuration of its hidden units. The learning ability and performance of an ANN model depends on the suitability of its architecture. If the network is too small, it may have insufficient degrees of freedom to fully capture all the underlying relationships in the data. Conversely, if the network is too large, it may fail to generalise, memorising events in the training data that are not necessarily representative of the system under consideration.

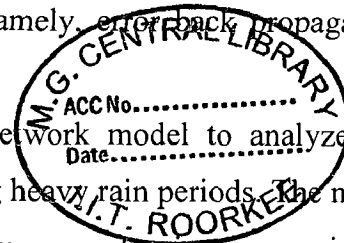
For hydrological applications, ANN models can take advantage of their capability to reproduce the unknown relationship existing between a set of input variables descriptive of the system, for example, rainfall, and a set of output variables, for example, river flow rate (Chakraborty *et al.*, 1992; Bishop, 1994). Cottrell and Girard (1995) and Yang (1996) stated that due to the ability of filling in gaps where information is missing, ANN provides a way of unravelling correlation complex systems. Therefore, we are encouraged further to examine its forecasting ability for non-ideal time series data. Using real hydrometric data, Dawson and Wilby (1998) used an ANN to forecast flow rates for 6-h lead time in two flood-prone catchments in the U.K. They also did forecasting at a gauging station for longer periods of time (about 6 months) using rainfall and flow discharge data measured at the same gauging station.

Methods to continuously forecast water levels at a site along a river are generally model based (Thirumalaiah *et al.*, 1998). Physical processes influencing occurrence of a river stage are, however, highly complex and uncertain, which makes it difficult to capture them in some form of deterministic or statistical model. Neural networks provide model-free solutions and hence can be expected to be appropriate in these conditions. Built-in dynamism in forecasting, data-error tolerance, and lack of

requirements of any exogenous input are additional attractive features of neural networks. Author highlights their use in real-time forecasting of water levels at a given site continuously throughout the year based on the same levels at some upstream gauging station and/or using the stage time history recorded at the same site. The network is trained by using three algorithms, namely, error back propagation, cascade correlation, and conjugate gradient.

Campolo et al (1999) developed a neural network model to analyze and forecast the behaviour of the river Tagliamento, during heavy rain periods. The makes use of distributed rainfall information coming from several rain gauges in the mountain district and predicts the water level of the river at the section closing the mountain district. The water level at the closing section in the hours preceding the event was used to characterize the behaviour of the river system subject to the rainfall perturbation.

ASCE (2000a) described the role of ANNs in hydrology. Apart from description of various aspects of ANN and some guidelines on their uses a brief comparison of ANNs and other modelling philosophies in hydrology were also presented. A discussion on the strengths and limitations of ANN brought out the similarities they have with other modelling approaches, such as physical model. ASCE (2000b) examined the role of ANN in various branches of hydrology presented an excellent critical review of published work. With identification of merits and demerits, it was found that ANNs are tools for modelling many of the non-linear hydrologic processes such as rainfall-runoff, stream flow, ground water management, water quality simulation and precipitation. A good physical understanding of the hydrologic process being modelled can help in selecting the input vectors and designing a more efficient neural network. However, artificial neural networks were found to be data intensive, and there appears to be no established methodology for their design and successful implementation. The merits and limitations of ANN applications were discussed and potential research avenues were explored. In brief, most of the ANN studies available are on training and testing of ANN rainfall-runoff studies provide enough evidences that ANN are highly capable in learning and extracting the behaviour of a system, when sufficient data is available for training of ANN model. The performance of the developed ANN has frequently been compared with other empirical, conceptual and statistical models. The comparison is normally input dependent and the ANNs resulted in superior performance. The use of artificial



neural network for runoff and sediment yield simulation and forecasting is an area that is yet to be fully explored.

Wei et al. (2002) described a new approach to the flood disaster prediction problems. The results proved that the use of ANN with the capacity of mapping or function approximating on the flood disaster prediction problem is a valid approach, which is not only simple but also reliable. Since its mapping approximation process is independent of the types of variable relationships. Obviously, this method could also be extended to a wide variety of flood disaster problems such as danger forecasting. However, many further works are needed for the wide applications on flood disaster prediction problems such as the choice of proper ANN topology structures, and the improvement of its algorithm.

Chang and Chen (2003) presented a hybrid ANN including the fuzzy clustering scheme along with Radial Basis Functions for water stage forecasting in an estuary under high flood effects. They showed that ANN could be a powerful tool for solving such a poorly defined and complex problem. The primary goal of this paper was to investigate the applicability of hybrid structure of Artificial Neural Networks, Self Organizing Radial Basis (SORB), in streamflow forecasting. The architecture employed consists of Self-Organizing Feature Map (SOFM) as an unsupervised training scheme for data clustering, which correspondingly provides the parameters required for the Gaussian functions in RBF neural network. Spread of the Gaussian functions extracted from SOFM seemed to be tunable, and tuning was done in parallel to training the RBF network.

Laio et al (2003) compared performances of ANN and NLP (nonlinear prediction) for lead times of 1-, 3-, 6-, 12- and 24-hours using rainfall data in the input vector and the flow stage at a gauging station on Tanaro River in Alba in north-western Italy. According to Sudheer and Jain (2004), ANN model has various mathematical compositions capable of modelling extremely complex physical systems. It has the potential to be more flexible and less assumption-dependant approach to act as a simulation model for the hydrologic systems.

Moradkhani et al. (2004) improved stream flow forecasting using the self-organizing radial basis function ANN. Dawson et al. (2006) explored the potential of ANN in flood estimation in ungauged catchments and evaluated possible spatial biases in ANN model output error. Based on information at stations upstream of a river, a back-propagation neural network model was employed by Kerh (2006) to

forecast flood discharge at station downstream of the river which lacks measurement. The performance of the neural network model was evaluated from the indices of root mean square error, coefficient of efficiency, error of peak discharge, and error of time to peak. The verification results showed that the neural network model is preferable, which performs relatively better than that of the conventional Muskingum method. Furthermore, the developed model with different input parameters was trained to check the sensitivity of physiographical factors. The results exhibited that flood discharge and water stage, are two factors to dominate the accuracy of estimation. Meanwhile, the physiographical factors had a slight and positive influence on the accuracy of the prediction. The time varied flood discharge forecasting at an unmeasured station might provide a valuable reference for designing an engineering project in the vicinity of the investigation region.

Li et al. (2006) introduced a Web-based flood forecasting system (WFFS), which includes five main modules: real-time rainfall data conversion, model-driven hydrologic forecasting, model calibration, precipitation forecasting, and flood analysis, is presented in this paper. The WFFS brings significant convenience to personnel engaged in flood forecasting and control and allows real-time contribution of a wide range of experts at other spatial locations in times of emergency. The conceptual framework and detailed components of the proposed WFFS, which employs a multi-tiered architecture, are illustrated. Multi-tiered architecture offers great flexibility, portability, reusability and reliability. The prototype WFFS has been developed in Java programming language and applied in Shuangpai region with a satisfactory result.

Yu et al. (2006) proposed the use of support vector machine, a novel artificial intelligence-based method derived from statistical learning theory, for real-time stage forecasting model. The lags associated with the input variables are determined by applying the hydrological concept of the time of response, and a two-step grid search method is applied to find the optimal parameters, and thus overcome the difficulties in constructing the learning machine. Two structures of models used to perform multiple-hour-ahead stage forecasts are developed.

Ren (2010) presented a new classified real-time flood forecasting framework by integrating a fuzzy clustering model and neural network with a conceptual hydrological model. A fuzzy clustering model was used to classify historical floods in

terms of flood peak and runoff depth, and the conceptual hydrological model was calibrated for each class of floods. A back-propagation (BP) neural network was trained by using real-time rainfall data and outputs from the fuzzy clustering model. BP neural network provided a rapid on-line classification for real-time flood events. Based on the on-line classification, an appropriate parameter set of hydrological model was automatically chosen to produce real-time flood forecasting. Different parameter sets was continuously used in the flood forecasting process because of the changes of real-time rainfall data and on-line classification results. Chen et al. (2010) introduced a decision group Back-Propagation Neural Network for flood forecasting.

According to Panda (2010), simulation of water levels at different sections of a river using physically based flood routing models is quite cumbersome, because it requires many types of data such as hydrologic time series, river geometry, hydraulics of existing control structures and channel roughness coefficients. Normally in developing countries like India it is not easy to collect these data because of poor monitoring and record keeping. Therefore, ANN technique is used as an effective alternative in hydrologic simulation studies. The present study aims at comparing the performance of the ANN technique with a widely used physically based hydrodynamic model in the MIKE 11 environment. The MIKE 11 hydrodynamic model was calibrated and validated for the monsoon periods (June–September) of the years 2006 and 2001, respectively. Feed forward neural network architecture with Levenberg–Marquardt (LM) back propagation training algorithm was used to train the neural network model using hourly water level data of the period June–September 2006. The trained ANN model was tested using data for the same period of the year 2001. Simulated water levels by the MIKE 11HD were compared with the corresponding water levels predicted by the ANN model. The results obtained from the ANN model were found to be much better than that of the MIKE 11HD results as indicated by the values of the goodness of fit indices used in the study.

Kar et.al (2010) in their study described that downstream of Mahanadi basin is devoid of a sound flood forecasting system. They have compared both ANN and statistical methods using peak discharges in downstream catchment of Hirakud for flood forecasting at delta head.

2.8.4 Verification of forecasting

The following are the main purpose of forecast verification:

- (i) To find the degree of accuracy and inaccuracy of the forecast;
- (ii) To find out the possible reason for error and to suggest the possible improvement in the existing system;
- (iii) To select the appropriate model parameter.

An accurate forecast means that the difference between the forecast level and the corresponding observed level is not considerable. In an ideal situation, the forecast and the corresponding observed values of water stage should be one and the same. However for all practical purposes, it has been assumed that a forecast may be called sufficiently correct if the difference between the forecast and the corresponding observed values of water stage is within +/- 15 cm and peak discharge of +/- 20% is accepted. Level forecast and Inflow forecast reliable to an extent of 95% (WMO, 1994).

2.8.5 Dissemination of forecast

The utility of flood forecast is dependent on both accuracy and timeliness. Under-prediction can lead to dangerous situation resulting in damage of life and property in the areas, victim of mistaken and misplaced confidence. On the other hand, over-prediction will result in avoidable and unnecessary evacuation, flood fighting measures including costly engineering and panic among the people. Timeliness is also equally important. It should be borne in mind that the value of the forecast is zero at the time of the event. Hence, longer the warning time, greater will be its utility. But here there is need for caution. The forecast of almost zero warning time will be hundred percent accurate while there is chance of the error increasing progressively upon various factors. Hence, there is need for some sort of a compromise between the accuracy and the warning time keeping in view that a warning period of less than 10 to 12 hours in our country will not mean much of a help in organizing flood fighting measures.

The organisations responsible for flood warning and flood fighting should be informed about the incoming flood as early as possible so that the required action is planned and activities set into operation with least possible delay. They should also be kept informed of the propagation of a flood wave and of any change in the present as

well as anticipated flood situation with respect of time, these information which are supplied by the forecasting units in the form of Flood forecast Bulletin must be clear and include necessary details so that a very realistic picture of the incoming danger is depicted. There should be arrangement for double check with well defined responsibility in every office authorised to issue flood forecasts in order to avoid dissemination of wrong forecasts including even inadvertent mistakes because hardly any time is left for review between receipt of forecasts and start of chain of activities.

The present thesis work proposes an ANN-based flood forecasting model and compares its application results with those due to conventional techniques. Among the conventional techniques, simple regression approaches are used. These techniques are employed largely due to inapplicability of physically based models to the complex deltaic system.

3.1 STATISTICAL APPROACH

3.1.1 Multiple Linear Regression

The general purpose of multiple regression is to learn more about the relationship between several independent or predictor variables as a dependent or criterion variable. In general, multiple regression allows the researcher to ask (and hopefully answer) the general question “what is the best predictor of” The general computational problem that needs to be solved in multiple regression analysis is to fit a straight line to a number of points. In the simplest case- one dependent and one independent variable one- can be visualized in scatter plot.

3.1.1.1 Method of Least Squares

In the scatter plot, we have an independent or X variable, and a dependent or Y variable. The goal of linear regression procedures is to fit a straight line through the points. Specifically, a line is computed so that the squared deviations of the observed points from that line are minimized. Thus, this general procedure is sometimes also referred to as least squares estimation.

3.1.1.2 Regression Equation

A line in a two dimensional or two variable space is defined by the equation $Y = a + b \cdot X_j$, the Y variable can be expressed in terms of a constant ‘a’ and a slope ‘b’ times the X variable. The constant is also referred to as the intercept, and the slope ‘b’ as the regression coefficient or b-coefficient. In the multivariate case, when there are more than one independent variable, the regression line cannot be visualized in the two dimensional space, that can be computed just as easily. In general, multiple regression procedures estimate a linear equation of the form:

$$Y = a + b_1 \cdot X_1 + b_2 \cdot X_2 + \dots + b_n \cdot X_n \quad (3.1)$$

3.1.1.3 Unique prediction and partial correlation

It may be noted from the above equation that the regression coefficients (or b-coefficients) represent the independent contributions of each independent variable to the prediction of the dependent variable. Another way to express this fact is to say that, for example, variable X_1 is correlated with the Y variable, after controlling for all other independent variables. This type of correlation is also referred to as a partial correlation.

3.1.1.4 Predicted and residual scores

The regression line expresses the best prediction of the dependent variable (Y), given the independent variables (X). However, the nature is rarely (if ever) perfectly predictable, and usually there is substantial variation of the observed points around the fitted regression line. The deviation of a particular point from the regression line (its predicted value) is called the residual value. Residuals are calculated by working out 'expected' value of Y by applying the regression equation to the actual values of X and then subtracting each expected Y value from its corresponding actual Y value. Where the value of Y predicted by the equation is less than the actual value of Y, the residual is positive. Negative residuals result from cases where Y is predicted higher than it actually is.

3.1.1.5 Assumptions, limitations, and practical considerations

(a) Assumption of linearity

First of all, as is evident in the name multiple linear regression, it is assumed that the relationship between variables is linear. In practice this assumption can virtually never be confirmed. Fortunately, multiple regression procedures are not greatly affected by minor deviations from this assumption. However, as a rule it is prudent to always look at bivariate scatter plot of the variables of interest. If curvature in the relationships is evident, one may consider either transforming the variables, or explicitly allowing for non-linear components.

(b) Limitations

The major conceptual limitation of all regression techniques is that one only ascertains relationships, but never be sure about underlying causal mechanism.

(c) Choice of the number of variables

Multiple regression is a seductive technique: "Plug in" as many predictor variables as one can think of and usually at least a few of them will come out significant. This is because one is capitalizing on chance when simply including as

many variables as one can think of as predictors of some other variables of interest. This problem is compounded when, in addition, the number of observations is relatively low. Most researchers recommend that there should be at least 10 to 20 times as many observations as one has variables, otherwise the estimates of the regression line are probably very unstable and unlikely to replicate if one were to do the study over.

(d) Multi-co linearity and matrix III-conditioning

This is a common problem in many correlation analyses. When there are many variables involved, it is often not immediately apparent that this problem exists, and it may only manifest itself after several variables have already been entered in to the regression equation. Nevertheless, when this problem occurs it means that at least one of the predictor variables is (practically) completely redundant with other predictors. There are many statistical indicators of this type of redundancy as well as some remedies (e.g., Ridge regression).

(e) The importance of residual analysis

Even though most assumptions of multiple regressions cannot be tested explicitly, gross violations can be detected and should be dealt with appropriately. In particular outliers (i.e., extreme cases) can seriously bias the results by “pulling” or “pushing” the regression line in a particular direction thereby leading to biased regression coefficients. Often, excluding just a single extreme case can yield a completely different set of results.

3.1.2 Formulation of Models

The general representation of statistical models may be given by

$$Y_i = \sum_{j=0}^k \beta_j X_{ij} + \varepsilon \quad (3.2)$$

With $X_{i0}=1$. Here, X_{ij} is the independent variable for the i^{th} observation (various water stages in the present study), Y_i is the dependent variable for the i^{th} observation, β_j is unknown coefficients to be estimate, k is the number of coefficient (to be estimated) in the model, and ε is the error in the determination of Y_i which is generally assumed as having zero mean and constant standard deviation σ .

The unknown coefficients (β) are estimated by least squares method because here no assumption is necessary on the probability distribution data due to its

simplicity. Initially preliminary analysis of data was carried out before starting actual statistical regression analysis.

3.1.2.1 Preliminary analysis of data

The preliminary analysis consists of

- i. Initial filtration of data
- ii. Partial visual inspection of the data files
- iii. Creation of scatter plots

The outliers detected in the scatter plot were removed.

3.1.2.2 Secondary analysis

The filtered data for the data sets obtained after preliminary analysis is used to find correlation matrices predicting correlation of each flood forecasting parameters constituent stage at forecasting points. To enhance the visualization of the correlation matrix the square of correlation coefficient (COD) or coefficient of determination is calculated to indicate the contribution of individual flood forecasting parameters in explaining the variation in the dependent variable.

3.1.2.3 Selection of independent variables for regression analysis

If more number of independent variables as possible is used, the reliable fitted values can be determined and model prediction will be more accurate. Moreover, since COD gives the proportion of the variation in the dependent variables that is explained by the fitted regression model, one obviously wants COD to be large. But on the other hand, because of the costs involved in obtaining information on a large number of independent variables and subsequently monitoring them, there is interest in including as few independent variables as possible. Thus, one has to make compromise between these extremes, i.e. for selecting the best regression variables and thereby the best model. There is no unique statistical procedure for doing this (Draper and Smith, 1981). Different researchers suggested different statistical procedures namely: backward elimination, all possible regression, ridge regression, forward elimination in stepwise regression, principal component regression, and stage wise regression which may help information of optimum model. In the present study, the best subset regression approach has been used to select the best set of independent variables for dependent stage at forecasting points.

3.1.2.4 Best subset regression

Using the coefficient of determination (COD) i.e., the proportion of variation explained in the dependent variable, different best subsets of independent variables could be selected. The regression was assessed for each subset according to

- The value of COD achieved,
- The number of observations used in developing the model.

The model obtained from large dataset and achieving high COD is preferred.

3.2 ARTIFICIAL NEURAL NETWORK

An artificial neural network (ANN) is a computing paradigm designed to mimic the human brain and nervous system. Neural network (NN) has a big role to play in the field of water sector where complex natural processes dominate. The high degree of empiricism and approximation in the analysis of water quality systems make the use of neural network highly suitable. In other words, when the possibility of representing the complex relationships between various aspects of the processes in terms of physical or conceptual modelling is very remote, the neural network plays an important role.

ANN is an information processing system that uses an approach entirely different from conventional algorithmic programming and roughly replicates the behaviour of a human brain by emulating the operations and connectivity of biological neurons. From a mathematical point of view, it is a complex non-linear function with many parameters that are trained in such a way that the ANN output becomes similar to the measured output on a known data set. ANNs are highly distributed interconnections of adaptive nonlinear processing-elements (PEs) (Figure 3.1). When implemented in digital hardware, the processing-element is a simple sum of products followed by non-linearity. The connection strengths, also called the network weights, can be adapted such that the network's output matches the desired response.

In multi-layered perception, hidden layer means third layer of processing elements or units in between the input and output layers that increases computational power. In principle, the hidden layer can be more than one layer. In practice, the number of neurons in this layer is evaluated by trial and error. Hornik et al (1989) proved that a single hidden layer containing a sufficient number of neurons could be used to approximate any measurable functional relationship between the input data

and the output variable to any desired accuracy, in addition, De Viliars and Barnard (1993) showed that an ANN comprising of two hidden layers tends to be less accurate than its single hidden layer counterpart.

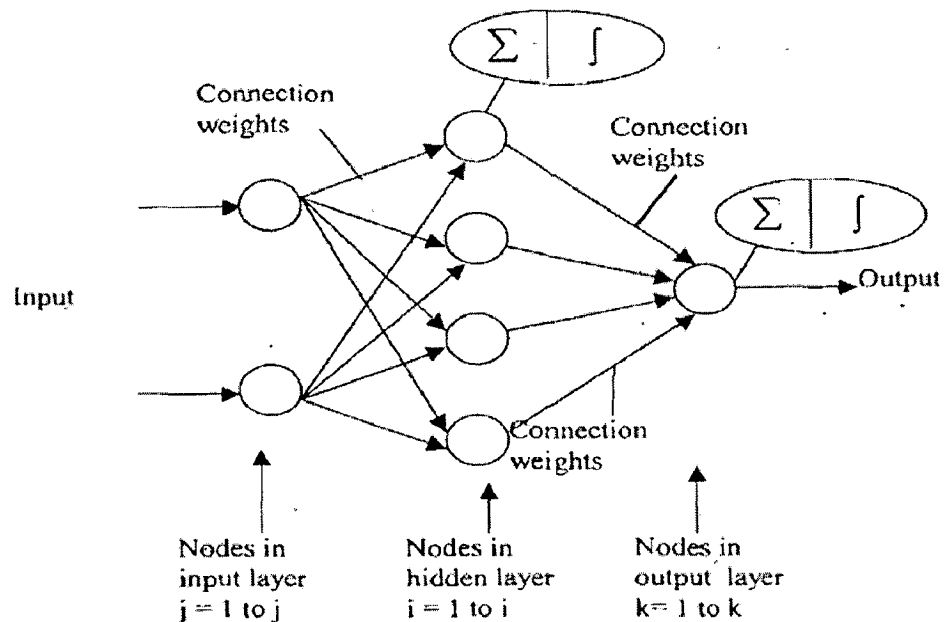


Fig. 3.1 The Building Blocks of ANN

The ANNs are not exactly the substitute of regression. General regression cannot solve the problems where the input dimension space is high and there is restriction on the number of input data. Regression imposes a priori variable selection, with all the inherent pitfalls, where one is limited to a few inputs among hundreds available. Regressions are performed using simple dependency functions that are not very realistic. In regression there is only one dependency function over the whole data set, instead of many distinct niches, which is taken care of by ANNs. Where dependency between the input variables and the output are not well-defined, ANNs solve it better. The most important difference between ANN and regression is that the former maps the output by generalization whereas the later by memorization. Generalization refers to the neural network producing reasonable outputs for inputs not encountered during learning. To over-simplify, if an object is represented in a network as a pattern of activation of several units, and if a unit or two responds incorrectly, the overall patterns remain pretty well the same, and the network will still respond correctly to stimuli.

ANNs have been developed as a generalization of mathematical models of neural biology and are based on following rules:

- (i) Information processing occurs at many single elements called nodes, also referred to as units of neurons.
- (ii) Signals are passed between nodes through connection links.
- (iii) Each connection link has an associated weight that represents its connection strength
- (iv) Each node typically applies a nonlinear transformation called activation function to its net input to determine its output signal.

3.2.1 ANN Structure

3.2.1.1 Biological neuron

A typical biological neuron comprises of Dendrites, Soma, Axon, and Synaptic Buttons, is shown in Figure (3.2). The dendrites form a very fine filamentary brush surrounding the body of the neuron. The information is picked up at the Dendrite. The Soma is cell body whereas the Axon is long transmission line like structure and the tail end of the Axon is called Synaptic Buttons. These neurons are so powerful in processing the information, that even a small earthworm with only 302 neuron has a computing power around one thousand times the power of Pentium-II Processor. Thus the computation power of parallel processing in neuro biological system is very high.

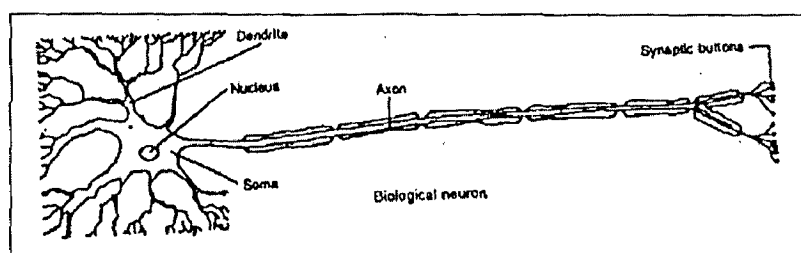


Fig. 3.2: Anatomy of Biological Neuron

3.2.1.2 Artificial neuron

Let neuron has a set of n inputs $x_1, x_2, x_3, \dots, x_n$ and $w_1, w_2, w_3, \dots, w_n$ are weights attached to the input link. The inputs to the neuron may come from the environment in which it is embedded or outputs to the other neuron are located in. The signals are passed to the cell body through the synapse, which may accelerate or retard. This acceleration or retardation of the input signal is modelled by the weights.

Weights are multiplicative factors of the inputs to account for the strength of the synapse. The total output is

$$I = W_1X_1 + W_2X_2 + W_3X_3 + \dots + W_nX_n$$

Or,
$$I = \sum w_i x_i \tag{3.4}$$

To generate the final output y , the sum is passed through a non-linear fitter Φ called activation function or transfer function, which releases the output y as

$$Y = \Phi(I) \tag{3.5}$$

The error (E) is calculated at the output as

$$E = \frac{1}{2} \sum [(y_{obs} - y_{est})^2] \tag{3.6}$$

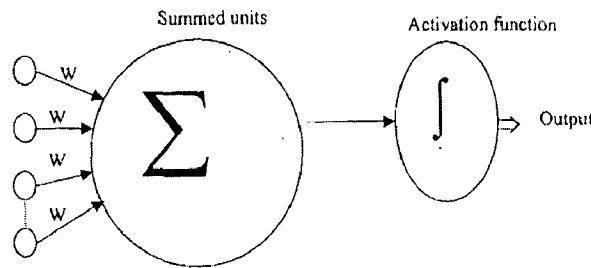


Fig. 3.3 Anatomy of artificial neuron

3.2.2 Gradient Descent Learning Algorithm

Gradient descent learning is the mostly used principle of ANN training. The reason is that trial computation is required to implement this method, and the fact that the gradient can be computed with local information. The principle of gradient descent learning is very simple. The weights are moved in a direction opposite to the direction of the gradient. The gradient of a surface indicates to the direction of the maximum rate of change. Therefore, if the weights are moved in the opposite direction of the gradient, the system state will approach points where the surface is flatter.

3.2.3 Neural Network Topology

The arrangement of the processing units, connections and pattern input / output in an ANN is referred to as topology. The processing units are arranged in three layers that are input, hidden and output. The units of a layer are similar in the sense that they all have the same activation dynamics and output function. The

number of input and the number of output are problem specific. There are no fixed rules as to the how many units should be included in the hidden layer. If there are too less units in the hidden layer, the network may have difficulty in generalizing the problem. On the other hand, if there are too many units in the hidden layer, the network may take an unacceptably long time to learn. On the basis of direction of information flow and processing the ANNs are classified as feed forward and feed backward network.

3.2.3.1 Feed forward network

The nodes are generally arranged in layers, starting from first input layer and ending at the final output layer. There can be several hidden layers with each layer having one or more nodes Information passes from the input to the output side. The neurons in one layer are connected to those in the next, but not to those in the same layer. Thus the output of a node in the one layer is only a dependent on the input it receives from previous layers and the corresponding weights.

3.2.3.2 Feed backward network

Information flows through the nodes in both directions from the input to the output side and vice-versa. This is generally achieved by recycling previous network outputs as current inputs, thus allowing for feedback.

3.2.4 Activation Function

This function is the mostly used function for solving ANN problems.

3.2.4.1 Sigmoid function

This function is a continuous function that varies gradually between asymptotic values 0 and 1 or -1 and +1 and is given by

$$\Phi(x) = \frac{1}{1 + e^{-\beta x}} \quad (3.7)$$

Where, β is the slope parameter, which adjusts the abruptness of the function as it changes between the two asymptotic values. Sigmoid functions are differentiable, which is an important feature of neural network theory. Experimental observations of biological neurons demonstrate that the firing is roughly sigmoid, when plotted(Fig.3.4).

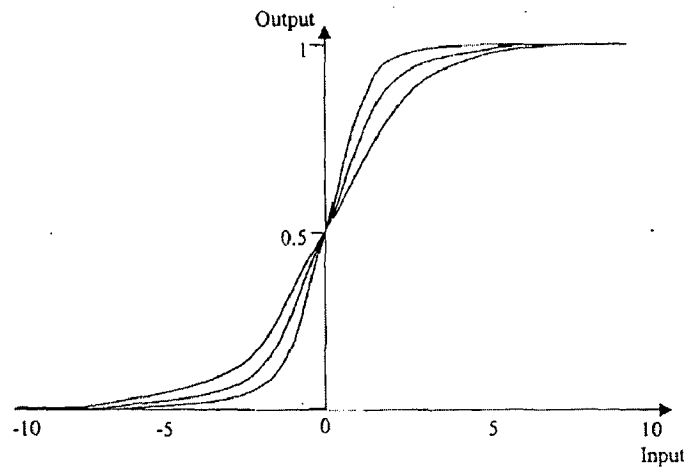


Fig 3.4: The Sigmoid Function

3.2.5 Architecture of ANN

The manner in which the neurons of a neural network are structurally and intimately linked with learning algorithm ceased to train the network. The optimal architecture is one, which yields the best performance in terms of error minimization, while training simple and compact structure. The numbers of input and output nodes are problem dependent. The flexibility lies in selecting number of hidden layers and in assigning the number of nodes to each of these layers.

3.2.6 Training of Artificial Neural Network

Once a network has been structured for a particular application, that network is ready to be trained. To start this process the initial weights are chosen randomly. Then, the training, or learning begins. Supervised and unsupervised are two methods used to train neural network.

3.2.6.1 Supervised training

In supervised training, both the inputs and the outputs are provided, the networks then process the inputs and compare its resulting outputs against the desired outputs. Errors are then propagated back through the system, causing the system to adjust the weights, which control the network. This process occurs over and over as the weights are continually tweaked. The set of data, which enables the training, is called the 'training set'. During the training of a network the same set of data is processed many times as the connection weights are ever refined. Sometimes, some networks never learn because the input data does not contain the specific information.

If a network simply cannot solve the problem, the designer then has to review the input and outputs, the number of layers, the number of elements per layer, the connections between the layers, the summation, transfer and training functions, and even the initial weight themselves, those changes create a successful network.

3.2.6.2 Unsupervised training

In unsupervised training, the network is provided with input but not with desired outputs. The system itself must then decide what features it will use to group the input data. At the present time, unsupervised learning is not well understood. Currently this field remains one that is still in the laboratory.

3.2.7 Back Propagation Algorithm

Back propagation is a system of method of training multi layer artificial neural networks. Scientist and Engineering community to the modelling has used it and processing of many quantitative phenomena using neural network has used it. This learning algorithm is applied to multi layer feed forwarded network consisting of neurons with continuous differentiate activation functions. Such networks associated with the back propagation-learning algorithm are called back propagation networks (Fig.3.5). The back propagation algorithm is a generalization of the least mean square algorithm that modifies network weights to minimize the mean squared error between the desired and actual outputs of the network. Back propagation uses supervised learning in which the network is trained using data for which inputs as well as desired outputs are known. Once trained, the network weights are frozen and can be used to compute output values for new input samples.

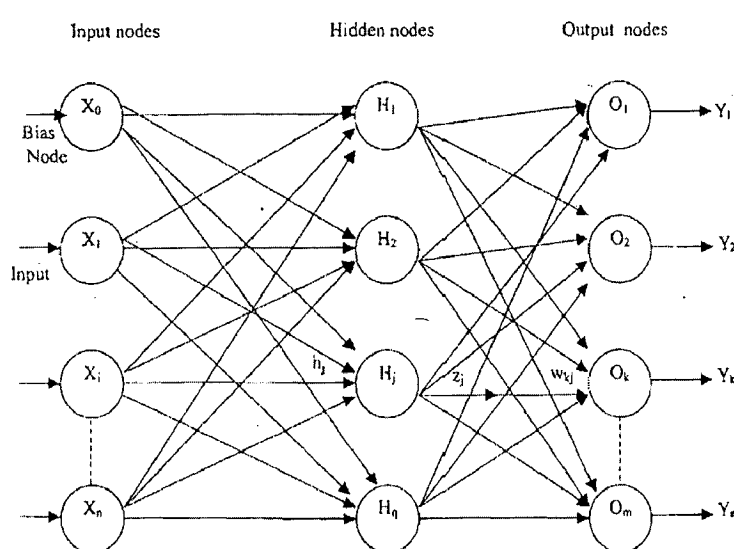


Fig 3.5 A typical three layered back propagation feed forward neural network

3.2.8 Learning Factors of Back Propagation

One of the major issues concerning back propagation algorithm is its convergence. The convergence of back propagation is based on some important learning factors such as the initial weights, the learning rate, the nature of training set and the architecture of the network.

3.2.8.1 Initial weights

The initial weights of a multi layer feed forward network strongly affect the ultimate solution. They are typically initialized by small random values (between -1.0 and 1.0 or -0.5 to +0.5). Equal weights values cannot train the network properly if the solution requires unequal weights to be developed. The initial weights cannot be large, otherwise the sigmoid will saturate, from the beginning and the system will stuck at a local minimum. The saturation is avoided by choosing the initial values of the synoptic weights to be uniformly distributed inside a small range of values. The range should not be too small as it can cause the learning to be very small.

3.2.8.2 Learning rate (η)

Weight vector change in back propagation are proportional to the negative gradient of the error, this guideline determines the relative changes that must occur in different weights when a training sample (or a set of samples) is presented, but does not fix the exact magnitudes of the desired weight changes. The magnitude change depends on the appropriate choice of the learning rate η . A large value of η will lead to rapid learning but the weight may then oscillate, while low values imply slow learning. This is typical of all gradient descent methods. The right value of η will depend on the application. Values between 0.1 and 0.9 have been used in many applications. The most efficient approach is to vary the learning rate as the training progresses, the effectiveness of learning rate may be checked as the training progresses and the value of the learning rate can be changed based on that.

3.2.8.3 Momentum factor (α)

Back propagation leads the weights in a neural network to a local minimum of the MSE, possibly substantially different from the global minimum that corresponds to the best choice of weights. This problem can be particularly bothersome if the "error surface" (plotting MSE against network weights) is highly uneven or jagged, with a large number of local minima.

We may prevent the network from getting stuck in some local minimum by making the weight changes depend on the average gradient of MSE in a small region

rather than the precise gradient at a point average $\frac{\partial E}{\partial W}$ in a small neighbourhood can allow the network weights to be modified in the general direction of MSE decrease, without getting stuck in some local minima.

Calculating averages can be an expensive task. A shortcut, suggested by Rumelhart et. al (1986) is to make weight changes in the i^{th} iteration of the back propagation algorithm depend on immediately preceding weight changes, made in the $(i-1)^{\text{th}}$ iteration. This has an averaging effect, and diminishes the drastic fluctuations in weight changes over consecutive iterations. The implementation of this method is straight-forward, and is accomplished by adding a momentum term to the weight update rule,

$$\Delta W_{kj}(t - 1) = \eta \delta_k X_j + \alpha \Delta W_{kj}(t) \quad (3.8)$$

Where, $\Delta W_{kj}(t)$ is the weight required at time t , and

α is an additional parameter known as momentum factor.

Values for the momentum coefficient α can be obtained adaptively, as in the case of the learning rate parameter η . A well-chosen value of α can significantly reduce the number of iterations for convergence. A value close to 0 implies that the past history does not have much effect on the weight change, while a value closer to 1 suggests that the current error has little effect on the weight change.

3.2.8.4 Data normalization

The variables fall in the range of 0 to 1, because it smoothen the solution space and averages out some of the noise effects. Such process is called normalization or standardization.

3.2.8.5 Training data and generalization

The training data submitted to the network for it to learn and generalize the relation between input and output should be sufficient and proper. Networks with too many trainable parameters for a given amount of training data learn well but do not generalize well. This phenomenon is called over fitting with too few trainable parameters; the network fails to learn the training data. In estimation of parameter of a water quality model, the available data are divided into two parts. The first part is used to calibrate the model, and the second to validate it. This practice is known as 'Split-Sample' test. The length of calibration data depends upon the number of

parameters to be estimated. The general practice is to use half to two-third of the data for calibration and the remaining for validation.

3.2.9 Steps in Development of ANN Model

The steps followed in the development of Artificial Neural Model are summarized as:

- Step I: Identify parsimoniously all physically based input variables with their time memory that influence the output.
- Step II: All inputs and output sets for the calibration and verification are normalized.
- Step-III: Start with a three layered ANN model having only one hidden layer and the number of nodes in the hidden layer is approximately double of input models. The numbers of nodes in the input layer are equal to the number of input variables, whereas, the number of nodes in output layer is equal to the number of output variables.
- Step-IV: All the interconnecting weights are assigned a small value between - 0.5 to +0.5 through a random numbers generation program.
- Step-V: Select fixed or variable values of learning rate and / or momentum term depending upon the algorithm used for optimization.
- Step-VI: Select the learning process that is either pattern learning or batch learning processes.
- Step-VII: Execute the program, which performs:
- (a) feed forward calculation,
 - (b) error back propagation in the network, and
 - (c) Finally change the weight.
- Step-VIII: Estimate output for calibration and verification and apply performance evaluation criteria.
- Step-IX: Perform whole operation for maximum desired iterations.
- Step-X: Select the iteration that results in maximum generalization on the basis of performance evaluation criteria.
- Step-XI: For required generalization repeat the learning process by assigning more numbers of nodes in the hidden layer or by increasing the numbers of hidden layers.

3.3 PERFORMANCE EVALUATION CRITERIA

The performance evaluation criteria used in the present study are described below

3.3.1 Coefficient of determination (COD)

Coefficient of determination (COD) is used in the context of statistical models whose main purpose is the prediction of future outcomes on the basis of other related information. It is the proportion of variability in a data set that is accounted for by the statistical model (Steel and Torrie, 1960). It provides a measure of how well future outcomes are likely to be predicted by the model.

There are several different definitions of COD which are only sometimes equivalent. One class of such cases includes that of linear regression. In this case, if an intercept is included then COD is simply the square of the sample correlation coefficient between the outcomes and their predicted values, or in the case of simple linear regression, between the outcomes and the values of the single regressor being used for prediction. In such cases, the coefficient of determination ranges from 0 to 1. Important cases where the computational definition of COD can yield negative values, depending on the definition used, arise where the predictions which are being compared to the corresponding outcomes have not been derived from a model-fitting procedure using those data, and where linear regression is conducted without including an intercept. Additionally, negative values of COD may occur when fitting non-linear trends to data. (Cameron, 1997). In these instances, the mean of the data provide a fit to the data that is superior to that of the trend under this goodness of fit analysis.

The square of the multiple correlation coefficients COD or R^2 is defined as

$$COD = \frac{SSR}{SS_y} = 1 - \frac{SSE}{SS_y} \quad (3.9)$$

Where $SS_y =$ sum of square about the mean $= \Sigma(y - \bar{y})^2$

$SSE =$ sum of square about the regression $= \Sigma(y - y_{est})^2$

$SSR =$ sum of square due to regression $= \Sigma(y_{est} - \bar{y})^2$

i.e., $SS_y = SSE + SSR$

$y =$ the observed values of dependent variable,

$\bar{y} =$ the average value of dependent variable,

$y_{est} =$ the compute values of the dependent variable

The stronger the linear association between y and y_{est} , it will yield a large value of COD and vice-versa. Unfortunately, wherever comparing a subset model to a

large model including the subset, COD value larger than that for the subset model. However, for fixed number of independent variables COD can be used to compare different models with a large value of COD indicating the preferred model.

COD is a statistic that will give some information about the goodness of fit of a model. In regression, the COD coefficient of determination is a statistical measure of how well the regression line approximates the real data points. An COD of 1.0 indicates that the regression line perfectly fits the data.

Values of COD outside the range 0 to 1 can occur where it is used to measure the agreement between observed and modelled values and where the "modelled" values are not obtained by linear regression and depending on which formulation of COD is used. If the first formula above is used, values can never be greater than one. If the second expression is used, there are no constraints on the values obtainable.

In many (but not all) instances where COD is used, the predictors are calculated by ordinary least-squares regression: that is, by minimizing SSE. In this case COD increases as we increase the number of variables in the model (COD will not decrease). This illustrates a drawback to one possible use of COD, where one might try to include more variables in the model until "there is no more improvement". This leads to the alternative approach of looking at the adjusted COD. The explanation of this statistic is almost the same as COD but it penalizes the statistic as extra variables are included in the model. For cases other than fitting by ordinary least squares, the COD statistic can be calculated as above and may still be a useful measure. If fitting is by weighted least squares or generalized least squares, alternative versions of COD can be calculated appropriate to those statistical frameworks, while the "raw" COD may still be useful if it is more easily interpreted. Values for COD can be calculated for any type of predictive model, which need not have a statistical basis.

3.3.2 Nash-Sutcliffe Efficiency (NSE)

The Nash–Sutcliffe model efficiency coefficient is used to assess the predictive power of hydrological models. It is defined as:

$$NSE = 1 - \frac{\sum_{i=1}^n (O_i - P_i)^2}{\sum_{i=1}^n (O_i - \bar{O}_i)^2} \quad (3.10)$$

Where, n= total number of data sets;

O_i = Observed peak floods for i^{th} data set,

P_i = Predicted peak flood for i^{th} data set,

\bar{O}_i = Mean of observed peak flood for i^{th} data set,

NSEs can range from $-\infty$ to 1. An efficiency of 1 (NSE = 1) corresponds to a perfect match of predicted to the observed data. An efficiency of 0 (NSE = 0) indicates that the model predictions are as accurate as the mean of the observed data, whereas an efficiency less than zero (NSE < 0) occurs when the observed mean is a better predictor than the model or, in other words, when the residual variance (described by the numerator in the expression above), is larger than the data variance (described by the denominator).

Essentially, the closer the model efficiency (NSE) is to 1, the more accurate the model is. This method can be used to describe the predictive accuracy of other models as long as there is observed data to compare the model results to.

3.3.3 Root Mean Square Error (RMSE)

The Root Mean Square Error (RMSE) is a frequently used measure of the differences between values predicted by a model or an estimator and the values actually observed from the thing being modelled or estimated. It is expressed as

$$RMSE = \sqrt{\frac{1}{n} \sum_1^n (O_i - P_i)^2} \quad (3.11)$$

Where, n = total number of data sets;

O_i = Observed peak floods for i^{th} data set,

P_i = Predicted peak flood for i^{th} data set,

RMSE indicates the discrepancy between the observed and predicted values. A RMSE value close to zero indicates better performance of the model. The best fit between observed and predicted values, which is unlikely to occur, would have RMSE as 0.

STUDY AREA AND DATA AVAILABILITY

This chapter describes the study area and availability of data. The study area chosen for the present work is the deltaic region of Mahanadi River basin in India for application and testing of the proposed methodology. A brief of the Mahanadi basin is given as follows.

4.1 Mahanadi Basin

The Mahanadi basin extends over an area of 1,41,600 km² which is nearly 4.3% of the total geographical area of the country. It lies between east longitudes 80°30' to 86°50' and north latitudes 19°21' to 23°35'. It is bounded on the north by the Central India hills, on the south and east by the Eastern Ghats and on the west by the Maikala range. The upper basin is a saucer shaped and mostly lies in Chhattisgarh state. The basin lies in the States of Orissa, Bihar, Chhattisgarh, and Maharashtra. The basin is circular in shape with a diameter of about 400 km and an exit passage of about 160 km length and 60 km breadth. The state wise distribution of the drainage area is given in Table 1. Fig 4.1 depicts Mahanadi basin showing different zones.

Table 4.1: State wise distribution of drainage area of Mahanadi River

State	Drainage area(km ²)
Chhattisgarh	74,970
Odisha	65,600
Bihar	650
Maharashtra	250
Madhya Pradesh	130
Total	141,600

Source: Water Resources Department, Government of Odisha (2007).

Physiographically, the basin can be divided into four regions, namely, the northern plateau, the Eastern Ghats, the coastal plain and the erosional plains of central table land. The first two are hilly regions. The coastal plain is the delta area which is highly fertile. The central table land is the central interior region of the basin, traversed by the river and its tributaries. The basin has a culturable area of about 79,900km² which is about 57% of the basin area and four percent of the total culturable area of the country.

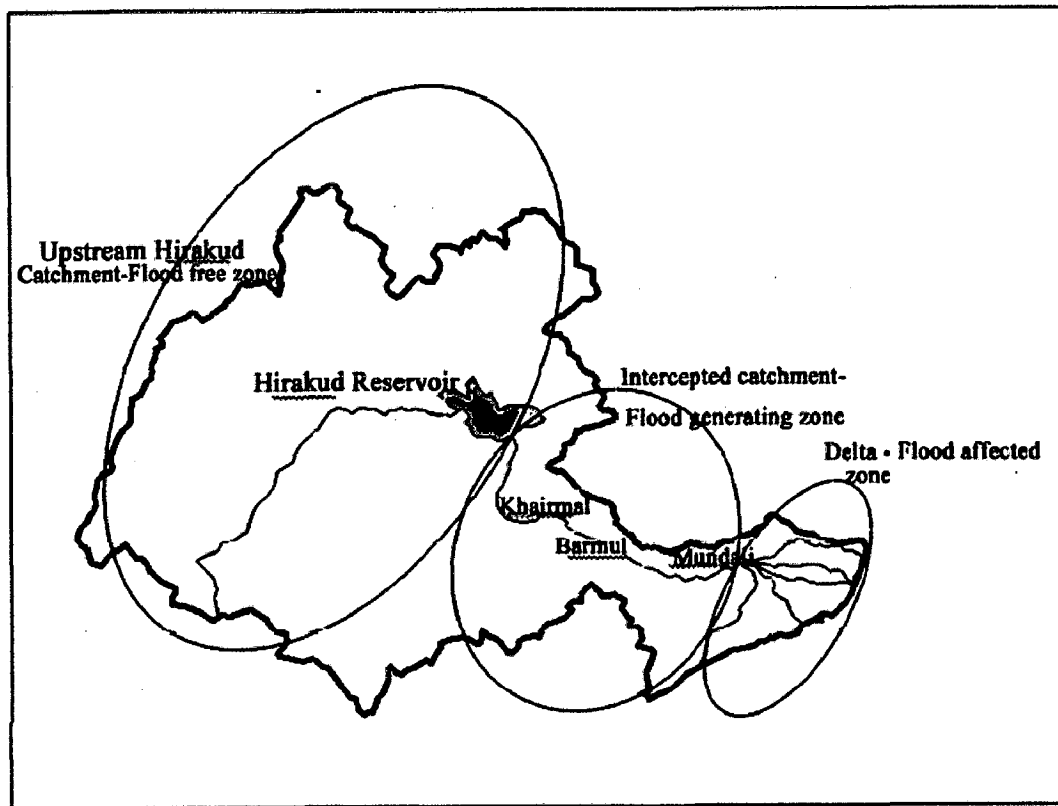


Fig 4.1: Mahanadi basin showing different zones (Source: Kar et al. 2010)

It originates from the Amarkantak hills of the Bastar Plateau near Pharsiya village in Raipur district of Chhatisgarh. The river traverses a total distance of 851 km (in Orissa - 494 km.) and falls into the Bay of Bengal. Mahanadi is a major river basin of eastern India comprising a catchment of 141600 sq. km. Its major part is occupied by Chhatisgarh and Orissa States. The basin lying in the South West monsoon tract is exposed to myriad hydro-climatic variations. The reservoir Hirakud which drains nearly 83000 sq. km. is the prime flood moderation structure in the basin, and the catchment of about 50000 sq. km. remains unregulated. Both the Hirakud release and intercepted catchment cause the flood damage to about 9000 sq. km. of delta.

Mahanadi is a major east flowing river of India and known for its large water volume and flood havocs. Mahanadi is the sixth largest river of our country and is said to be the lifeline of two states like Odisha and Chhatisgarh. Simultaneously, it is dangerous for the disastrous floods it carried during different periods of time. Basin receives 1088 mm of rainfall during the South-West monsoon (mid June to mid-October). Due to heavy rainfall the delta of the basin (Fig.4.1) the river downstream of Mundali is subjected to annual floods, which are aggravated by high tides and

heavy rainfall directly on the delta. Floods of recent time like those of 1980,1982,2001,2008 are still in the mind of the people of this basin. As the slope of basin is more flat on part of Odisha (carrying 46% of the total catchment) devastation due to floods are more here. Although, some reservoirs and storage structures are now planned or are to come up in both the states in order to control the flood as well as increase irrigation capacities.

4.2 Climate of Mahanadi Basin

To the north, in the region of the Mahanadi River the climate is predominantly sub-tropical with summer temperatures of around 29°C and winter temperatures of 21°C. The normal time of onset of monsoon over the basin is the first week of June. The bulk of the precipitation (800 to over 1,600 mm) over the basin falls in the period from July to September while during January to February, precipitation received is less than 50 mm.

The meteorology and climatology of the catchment are significantly influenced by the geographical location of the catchment with respect to the Bay of Bengal, where from most of the weather systems originate. Also, the orography of the Eastern Ghats, influence the rainfall pattern over the catchment to a great extent. The southwest monsoon normally sets over this area in the first week of June and withdraws in the first week of October. The south-west monsoon (June-October) accounts for nearly 91% of the annual rainfall. December is the driest month contributing less than 10% of annual rainfall.

4.2.1 Rainfall

The normal (1901-60) annual rainfall of the Mahanadi catchment is 141.7 cm. The average normal annual rainfall of the catchment above Hirakud is 139.6 cm and the corresponding value for catchment below Hirakud is 145.8 cm. Historical records show that the highest monthly and annual rainfalls were 1,405.9mm in June 1936 and 3,669.8mm in 1944 respectively at Bulandarpara. Besides the observatories maintained by IMD, about 200 rain gauge stations are maintained by the concerned States. Although distribution of the stations is fairly even, their number is not sufficient considering the hilly terrain which occupies the major part of the catchment. Rainfall data at some of the observatories and rain gauge stations are available from past 80 years.

4.2.2 Temperature

In the Mahanadi catchment, May is the hottest month and December the coldest. The diurnal range of temperature is the maximum during February and March; it is less during July and August. At Raipur and Sambalpur, the temperature varies from 12°C to 40°C while at Cuttack, it varies from 14 °C to 40°C. Temperature variation at Puri which is closer to sea is from 16 °C to 32°C.

4.2.3 Evaporation

Pan evaporation is being observed at four stations in the Mahanadi basin, namely, Labhandi, Hirakud, Bolangir and Cuttack. Out of these, long-term pan evaporation data is available for Labhandi and Cuttack stations. The average monthly pan evaporation of these stations is given in Table 4.2

Table 4.2 Pan Evaporation data (cm) of two stations in Mahanadi basin

Month	Station	
	Labhandi	Cuttack
January	3.0	3.3
February	4.9	4.4
March	6.8	5.3
April	10.9	6.6
May	14.6	7.5
June	11.8	5.6
July	5.7	3.9
August	4.9	3.4
September	4.1	3.9
October	3.7	3.6
November	3.0	3.3
December	2.4	3.0

Source: Jain (2007)

4.2.4 Soils and Land Use

The main soil types found in the basin are red and yellow soils. Mixed red and black soils occur in parts of the Bolangir, Sambalpur, and Sundargarh districts of Orissa. Laterite soil is found in the lower parts of Orissa. The deltaic soil is found in the coastal plains of the Mahanadi. Black soil and sandy soil with “Kankar” are the main soils found in the part of basin lying in Chhattisgarh. Except in the Chhattisgarh and coastal plains, the basin has an extensive area under forests. Forest and

agriculture are the main stay of the people in the interior parts of the basin. The Chhattisgarh and coastal plains, with a high incidence of rainfall, are predominantly rice growing areas.

4.3 Mahanadi Delta Region

Delta region of Mahanadi River basin in India forms study area (Fig. 4.2 & 4.3). It is located in the north-eastern part of coastal Orissa in India and lies between the longitudes $85^{\circ} 30' E$ and $86^{\circ} 52' E$ and the latitudes $19^{\circ} 40' N$ and $20^{\circ} 45' N$.

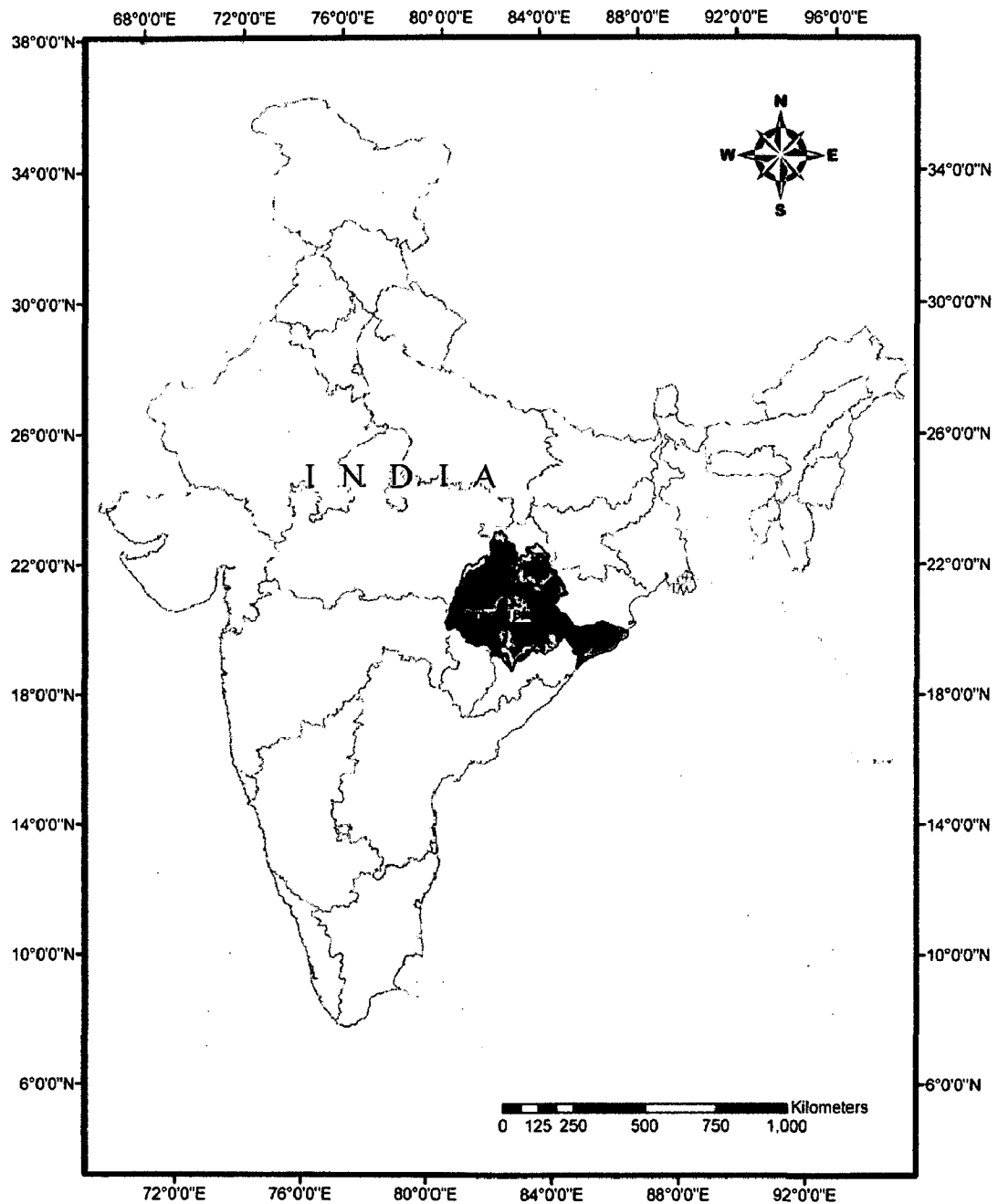


Fig.4.2 India Map showing Mahanadi basin

downstream end of the main course of the Mahanadi River as compared to others. The catchment area upstream of the delta receives heavy rainfall during the monsoon period as a result of which all the rivers in the delta flow full and flooding occurs.

Our study area lies between the longitudes $85^{\circ} 30' E$ and $86^{\circ} 25' E$ and the latitudes $19^{\circ} 40' N$ and $20^{\circ} 30' N$ of nearly 9000 km^2 . Which includes the distributaries Kathjodi, Kuakhai, Serua, Bharagavi, Kushabhadra, Daya, Devi and Kelue.

4.4 Data Acquisition

Three hourly stage and discharge (Table I.1, Appendix-I) is available at base station and forecasting station for a period of 2004-2009. The data is collected from Department of Water Resources, Government of Odisha. Peaks at base station i.e. at Khairmal and corresponding peaks at forecast station i.e. at Naraj are collected, and their travel times determined from the corresponding time series. Out of these, 65 peaks are considered for our analysis; total four cases are taken for calibration and validation. Again using 3 hourly stage forecasting model has been developed taking three cases in to consideration, Case-I using data of base station(Khairmal) as input, Case-II using the data of forecasting station(Naraj) as input and Case-III using the combination of data of Khairmal stage and Naraj stage as input in the model.

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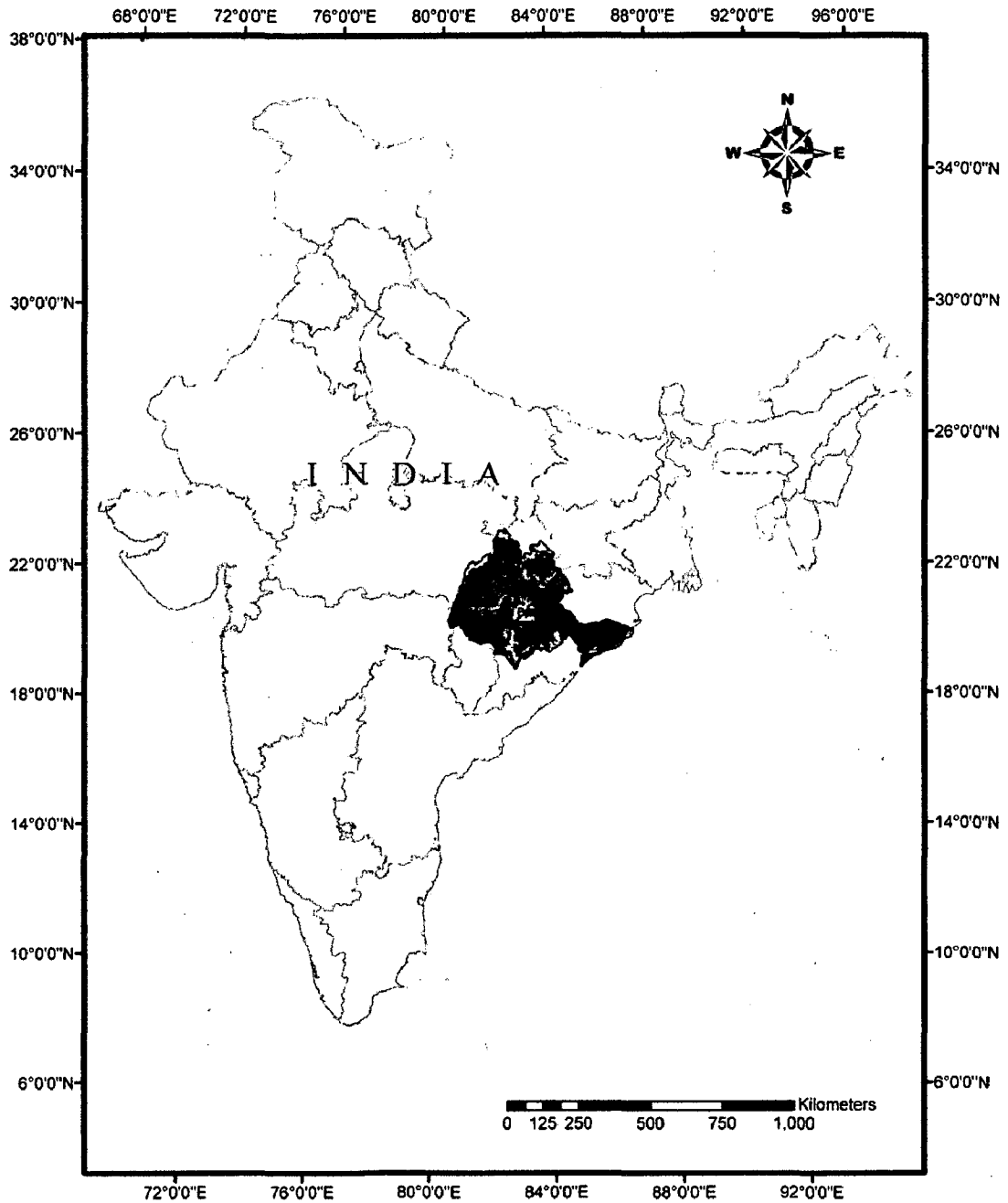


Fig.4.2 India Map showing Mahanadi basin

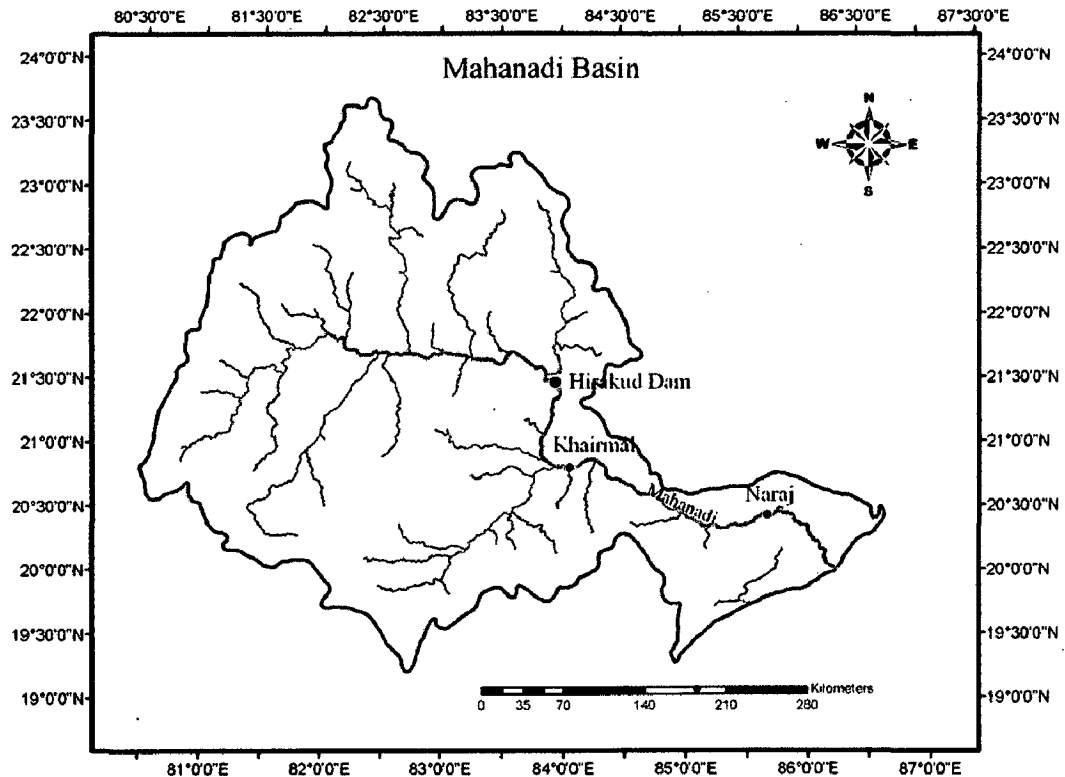


Fig 4.3 Mahanadi basin

The areal extent of the delta is about 6800 km² in which more than 80% of the total cropped area is affected by floods during the monsoon period. In the last five years, four severe floods have occurred in this region. The average surface elevation of the delta region ranges from 5m to 30m. The flooding in the delta region is due to the river Mahanadi and its distributaries. The downstream catchment has three main tributaries like Jeera, Ong and Tel with catchments 2383, 5128 and 25045 sq. km., respectively. So the contributions from the Tel catchment always remain predominant. Even the flood of 2008 is mainly due to the contribution of this tributary. It has produced a peak discharge of 33762 cumecs during 2008. The river Tel joins at Patharla to the main river Mahanadi and our base station Khairmal is at downstream of Patharla station. The other tributaries Ong and Jeera join also at the upstream of base station (Khairmal). The whole river from Khairmal is taken as one unit ignoring the contribution of further small tributaries.

The distributaries of the river Mahanadi include Kuakhai, Devi, Kathajodi, Kandal, Serua, Luna, Paika, Kushabhadra, Bhargavi, Chitrotpala, Daya and Biluakhai. The flooding problem is more severe in the rivers Devi, Kushabhadra and in the

downstream end of the main course of the Mahanadi River as compared to others. The catchment area upstream of the delta receives heavy rainfall during the monsoon period as a result of which all the rivers in the delta flow full and flooding occurs.

Our study area lies between the longitudes 85° 30' E and 86° 25' E and the latitudes 19° 40' N and 20° 30' N of nearly 9000 km². Which includes the distributaries Kathjodi, Kuakhai, Serua, Bharagavi, Kushabhadra, Daya, Devi and Kelue.

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As discussed in the previous chapters, the present work aims at to develop (a) conventional (i.e. statistical) model and (b) ANN based model for flood forecasting using stage data of Khairmal and Naraj gauging stations located on River Mahanadi in Odisha State. The performance of these models is evaluated using the criteria of Coefficient of Determination (COD), Nash-Sutcliffe Efficiency (NSE), and Root Mean Square Error (RMSE) for comparison purpose. Thus, the following text discusses the results of both the proposed statistical and ANN-based models.

5.1 Statistical Model Development

The flood forecasting is based on the stage values of upstream stations as input data. Here, forecasting models are proposed for peak stages by establishing a peak to peak correlation at the two gauging sites. Secondly, three hourly stages are correlated through multiple-linear regression analysis.

5.1.1 Peak to peak correlation

The statistical approach is applied for development of a relationship between the peak stage values at Khairmal and Naraj gauging sites. Flood peaks have been derived by drawing time series of Khairmal and Naraj stage as shown in Figs 5.1-5.5. One peak of Naraj is taken corresponding to Khairmal peak stage, and thus, 65 peaks are derived from these time series graph. The whole available data are split into two sets, calibration and validation. Total four cases (Table 5.1) are considered as follows:

Table 5.1 Cases considered based on number of peaks in calibration and validation

Case	Number of peaks considered	
	Calibration	Validation
I	35	30
II	45	20
III	50	15
IV	55	10

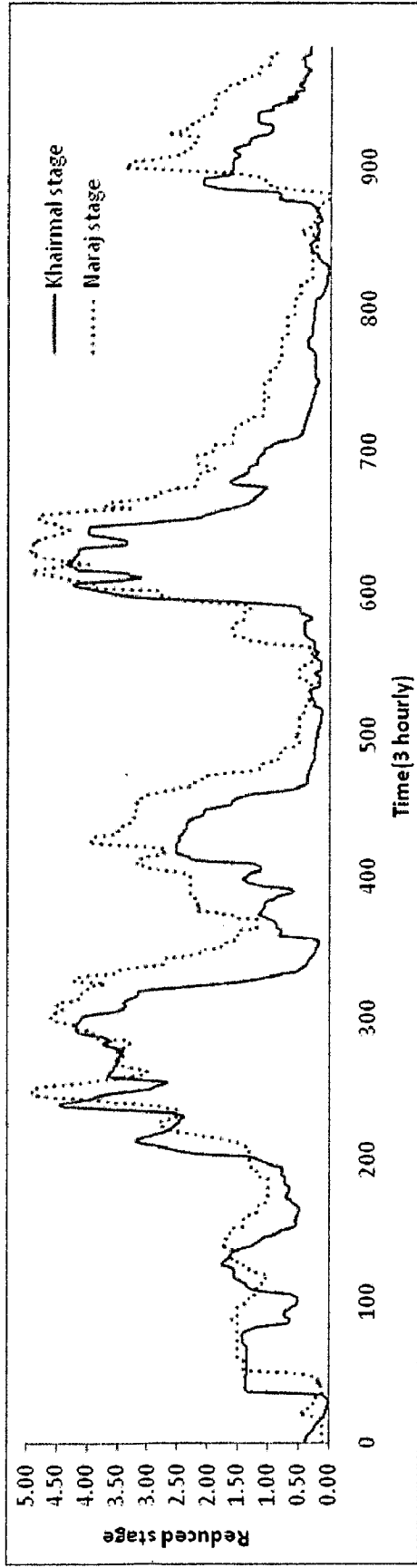


Fig. 5.1 Time series of Khairmal and Naraj stages for the year 2005

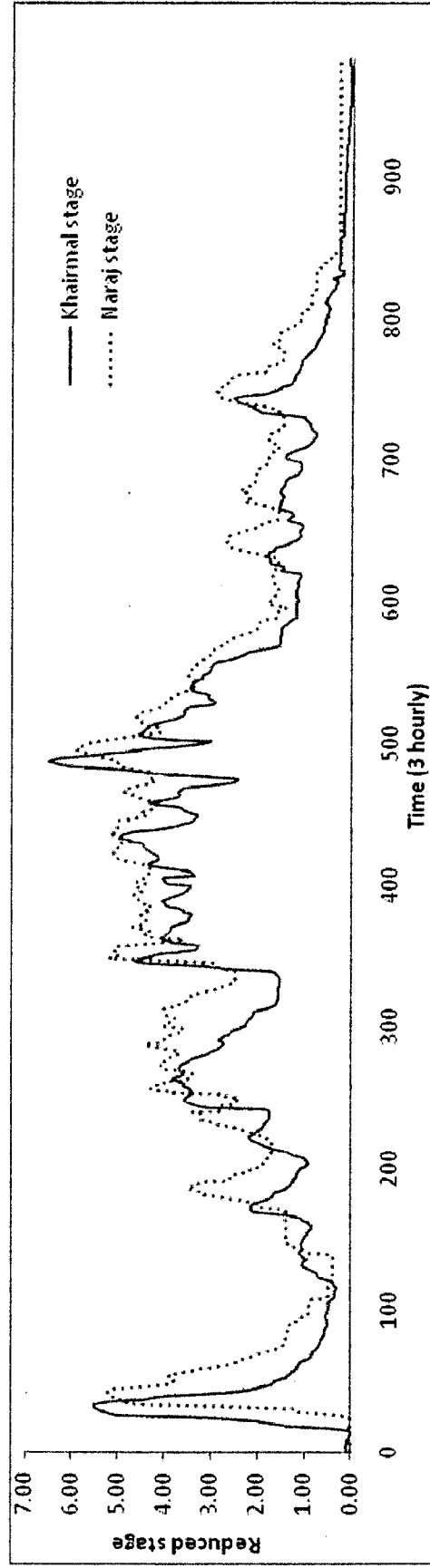


Fig. 5.2 Time series of Khairmal and Naraj stages for the year 2006

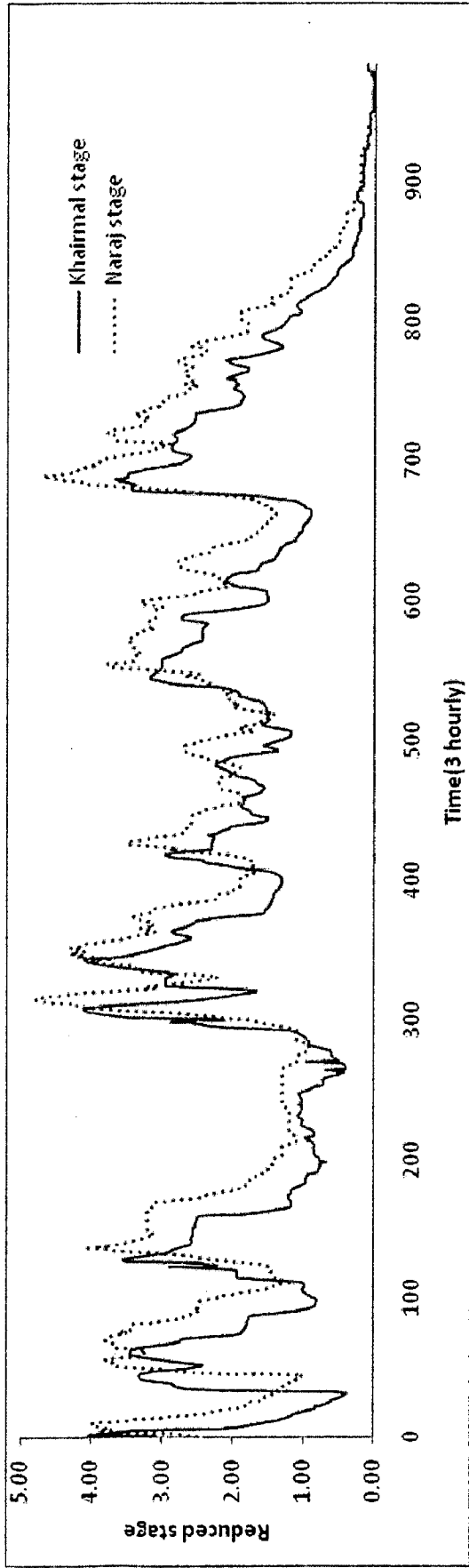


Fig. 5.3 Time series of Khairmal and Naraj stages for the year 2007

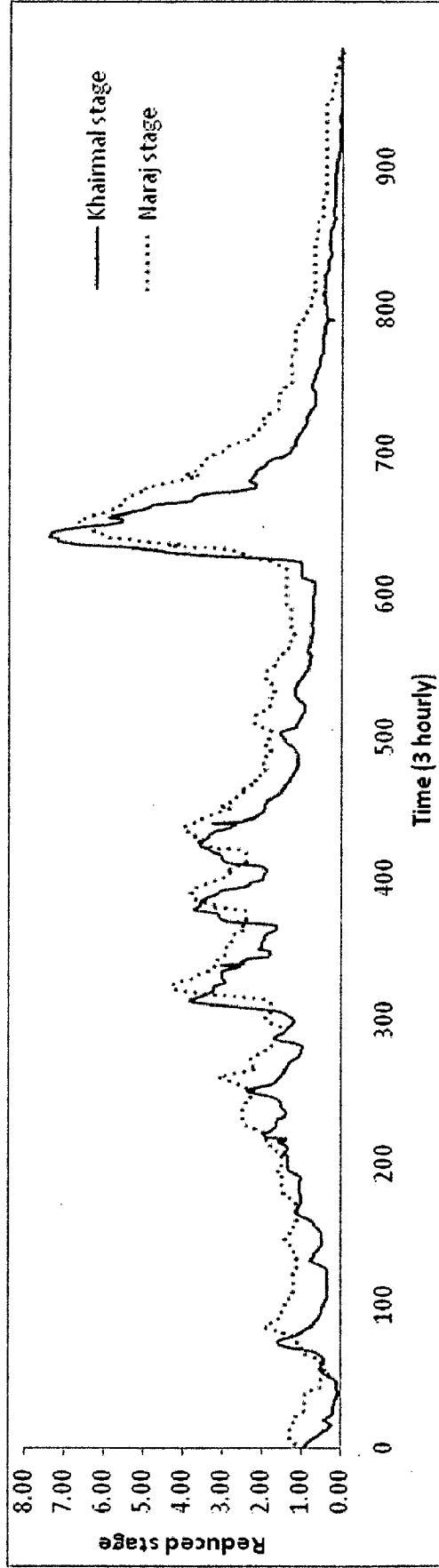


Fig. 5.4 Time series of Khairmal and Naraj stages for the year 2008

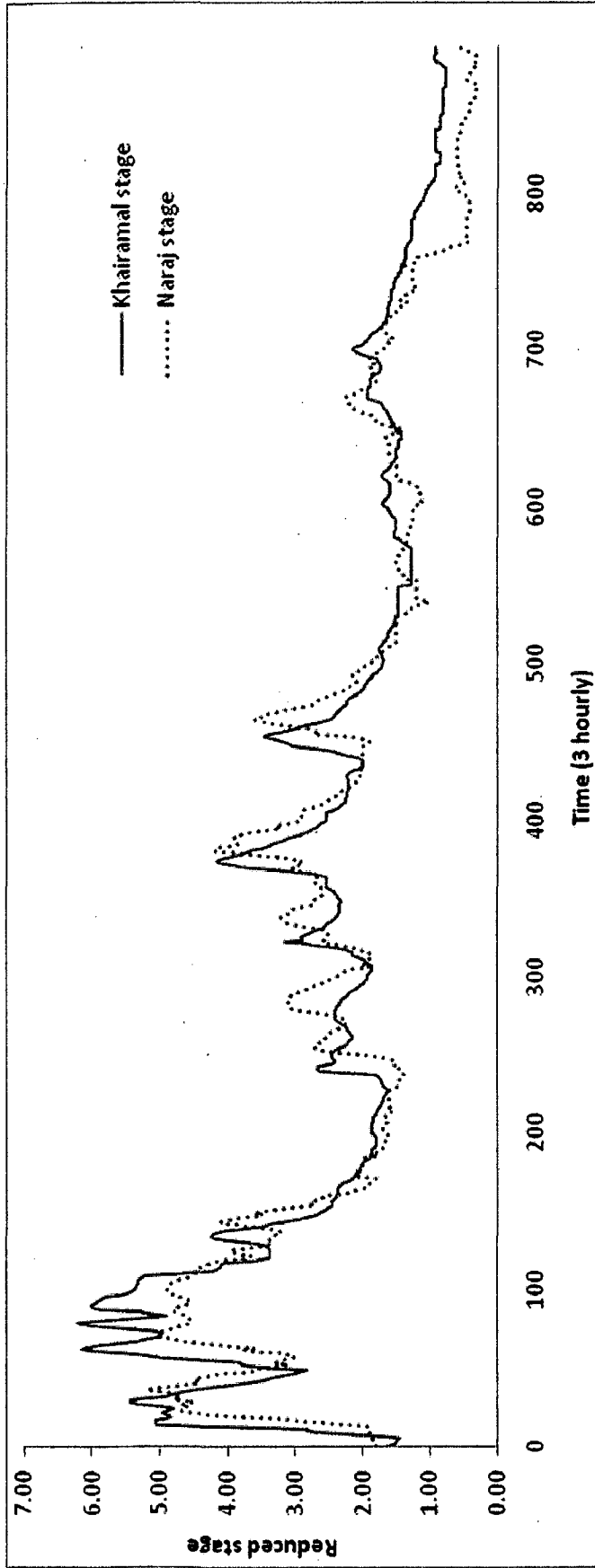


Fig. 5.5 Time series of Khairamal and Naraj stages for the year 2009

Table 5.2 Development of peak to peak stage (Khairmal to Naraj) linear relationship (statistical method)

Case	Equation	COD		RMSE (m)		NSE	
		Calibration	Validation	Calibration	Validation	Calibration	Validation
1	2	3	4	5	6	7	8
I	$H_N=0.87*H_K-65.38$	0.86	0.89	0.49	0.34	0.86	0.88
II	$H_N=0.86*H_K-65.03$	0.86	0.90	0.45	0.39	0.86	0.89
III	$H_N=0.88*H_K-66.47$	0.86	0.92	0.44	0.39	0.86	0.89
IV	$H_N=0.88*H_K-66.95$	0.87	0.96	0.43	0.46	0.87	0.83

Notations: H_N = Stage at Naraj (Forecasting Station) and H_K = Stage at Khairmal (Base Station)

Table 5.2 describes the statistical results of Case-I to Case-IV, and these are depicted in Figs 5.6 - 5.9 showing the Line of Perfect Fit (LPF) between forecast and observed peak stages of Naraj. It is seen from these figures that for Case-III majority of the forecast peak stages are relatively close to the Line of Perfect Fit. The proposed peak to peak flood forecasting models for delta region of Mahanadi basin show the values of COD and NSE in the ranges of 0.86 to 0.87 and 0.86 to 0.87, respectively, in calibration. Values of COD and NSE vary in the ranges of 0.89 to 0.96 and 0.83 to 0.89 in validation. RMSE varies from 0.43 to 0.49 in calibration, and 0.34 to 0.46 in validation. Out of these four cases, model performance in Case-III is better than the others yielding COD, RMSE, and NSE as 0.86, 0.44, and 0.86, respectively, in calibration, and 0.92, 0.39, and 0.89 in validation. The performance of models in Case-I and Case-II is poorer than in Case-III, i.e their CODs are lower, and RMSEs higher, than those of Case-III. In Case-IV, model performance is better in calibration, but poor in validation, and therefore, it is not selected. Finally Case-III model is selected as the preferred model among all these models.

Column 2 of Table 5.2 describes the forecasting equation for each case. These simple equations although not so much accurate, but useful in emergency where lead time is very less for flood forecasting by other methods, as other methods require more data.

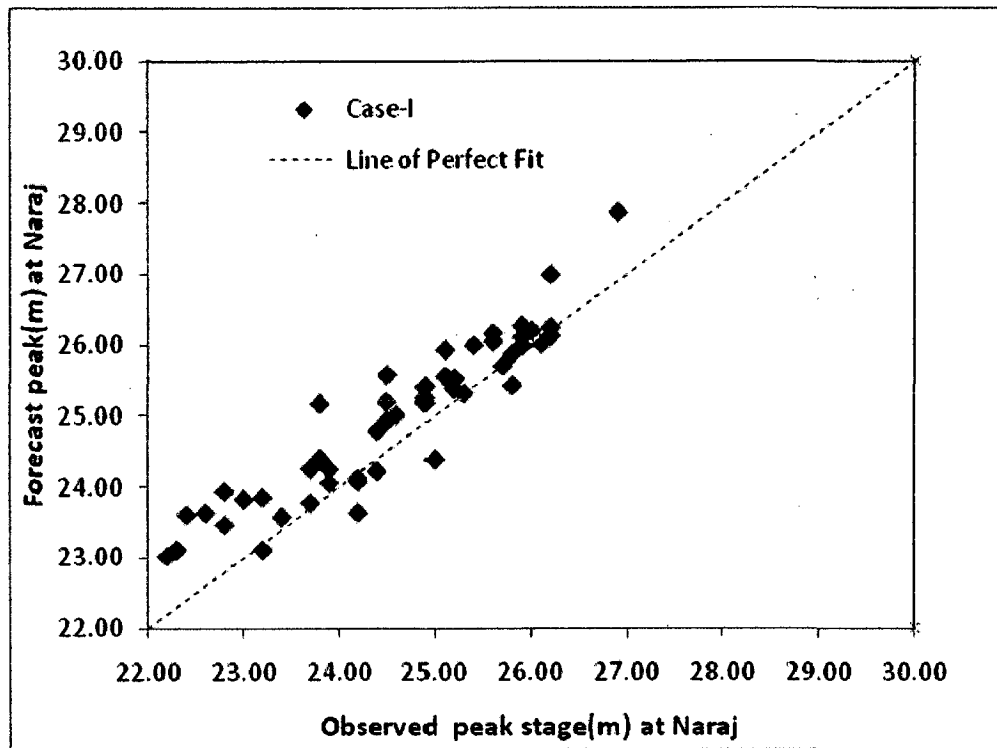


Fig. 5.6 (a) Forecast and observed peaks for Case-I in calibration

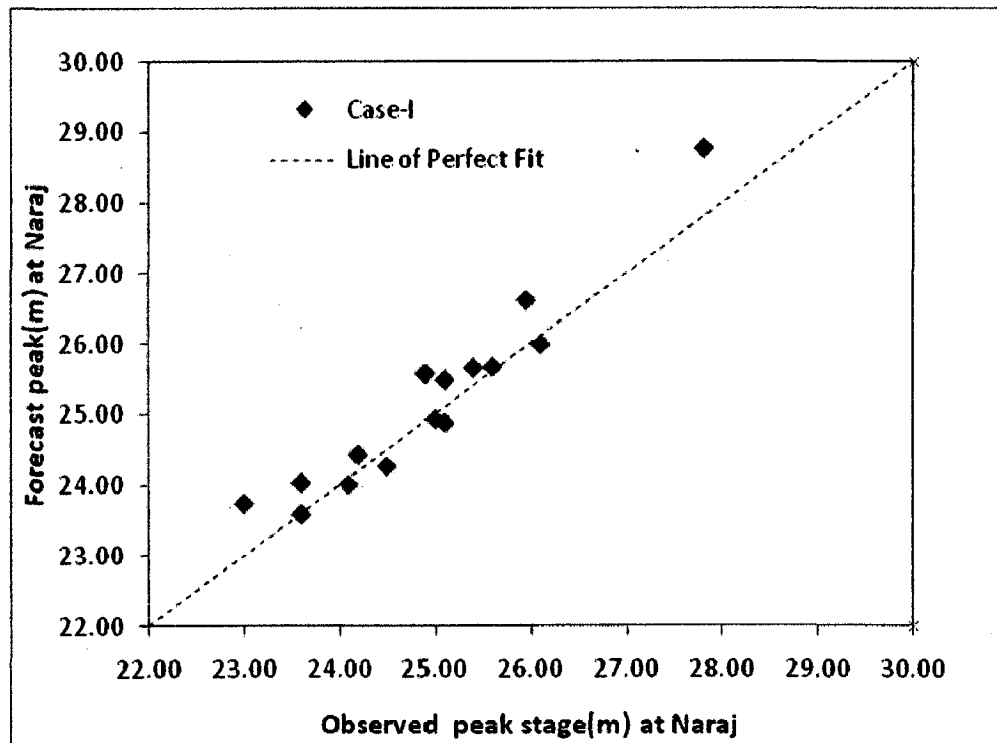


Fig. 5.6 (b) Forecast and observed peaks for Case-I in validation

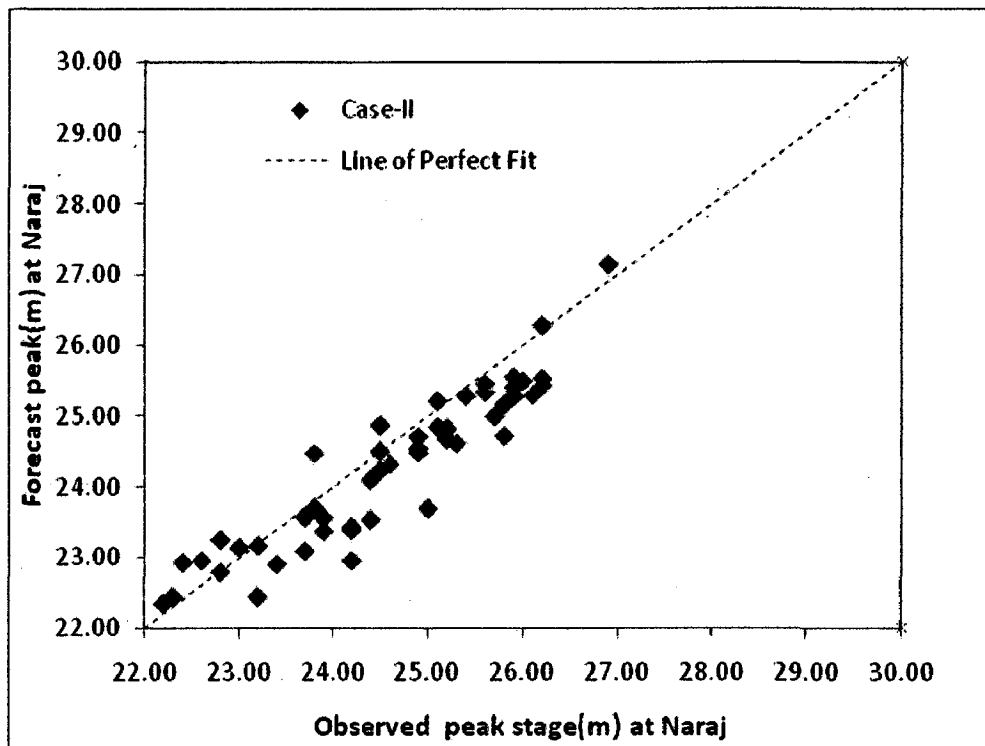


Fig. 5.7 (a) Forecast and observed peaks for Case-II in calibration

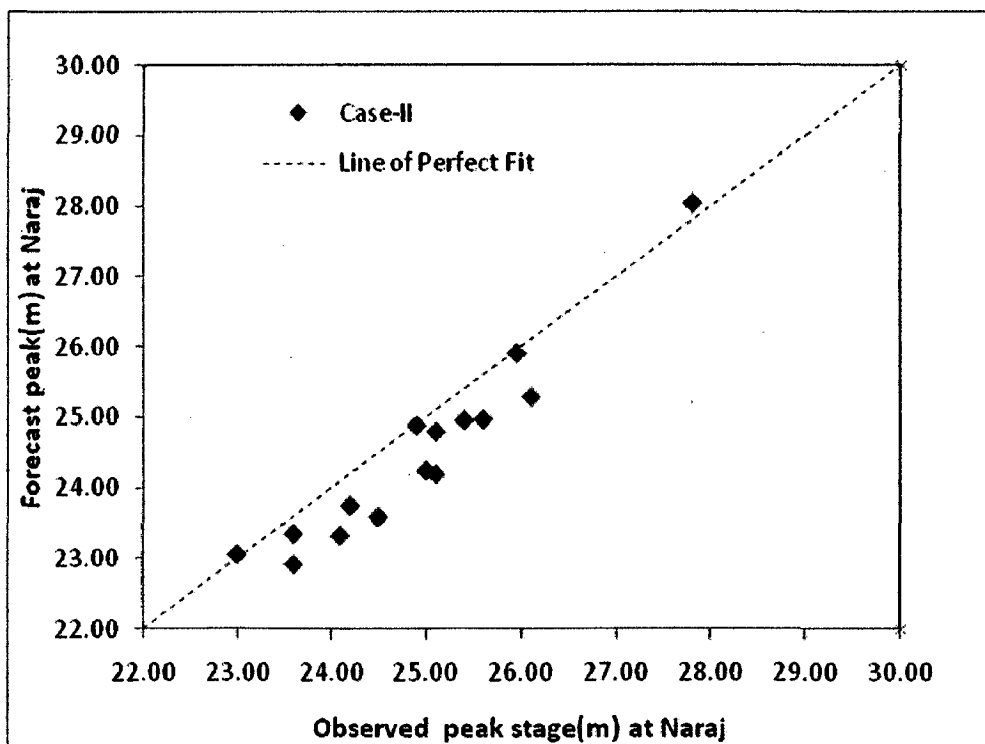


Fig. 5.7 (b) Forecast and observed peaks for Case-II in validation

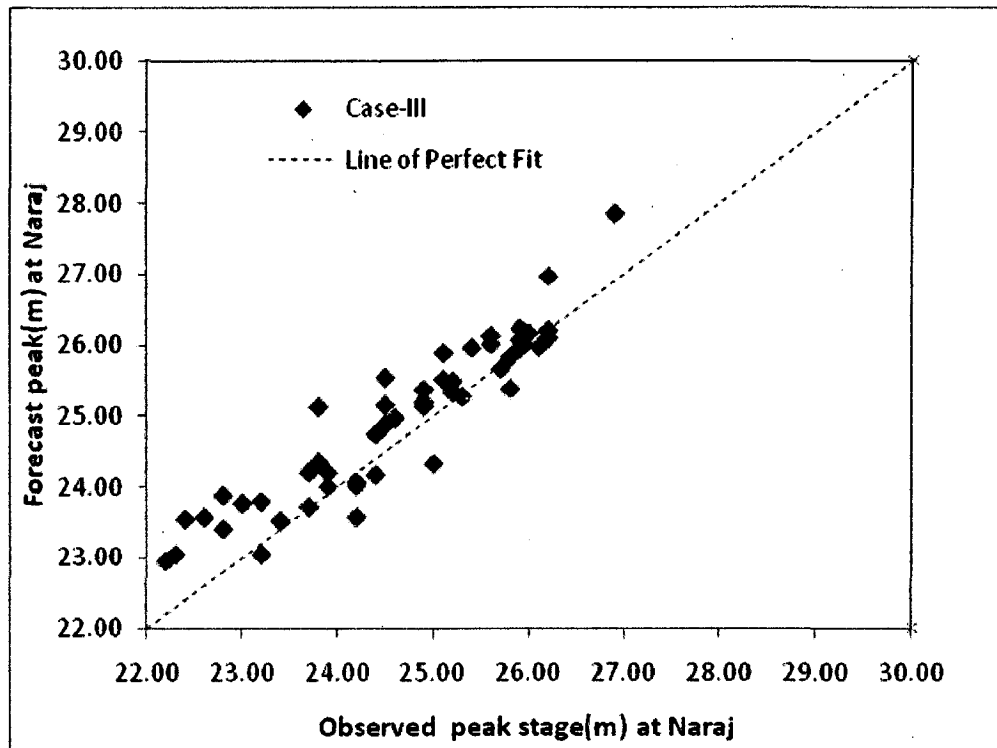


Fig. 5.8 (a) Forecast and observed peaks for Case-III in calibration

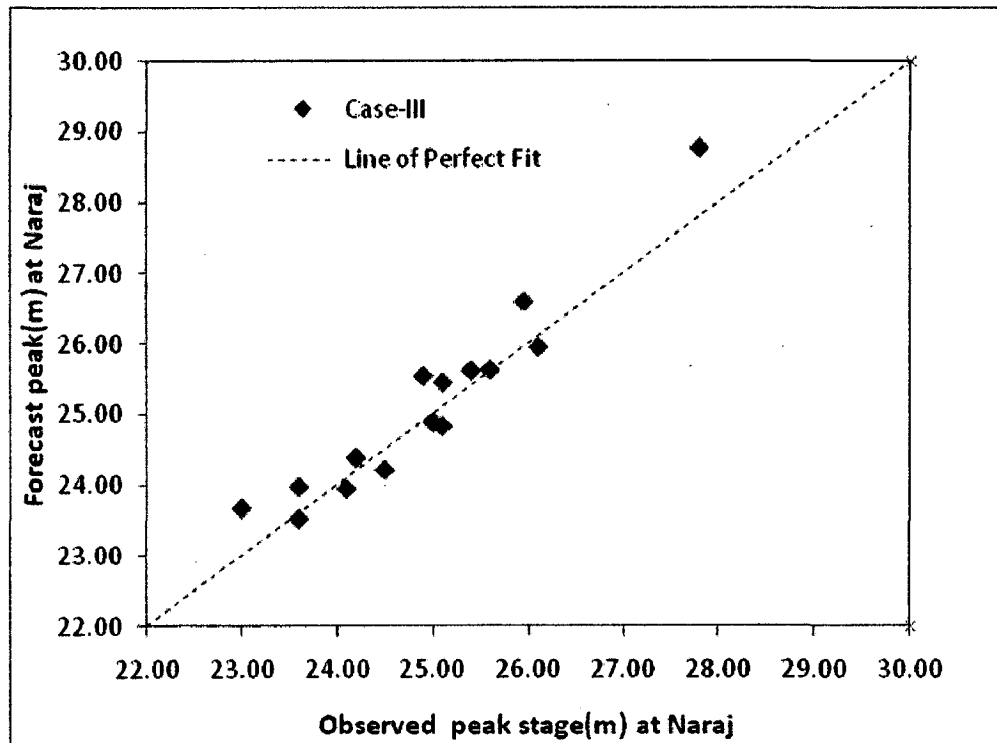


Fig. 5.8 (b) Forecast and observed peaks for Case-III in validation

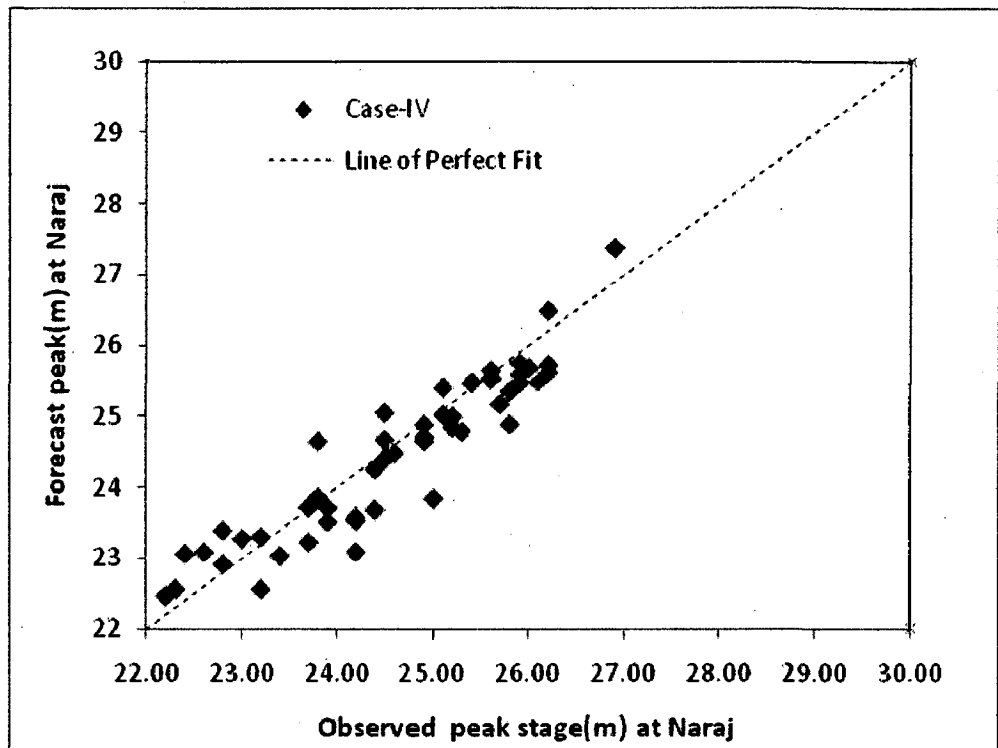


Fig. 5.9 (a) Forecast and observed peaks for Case-IV in calibration

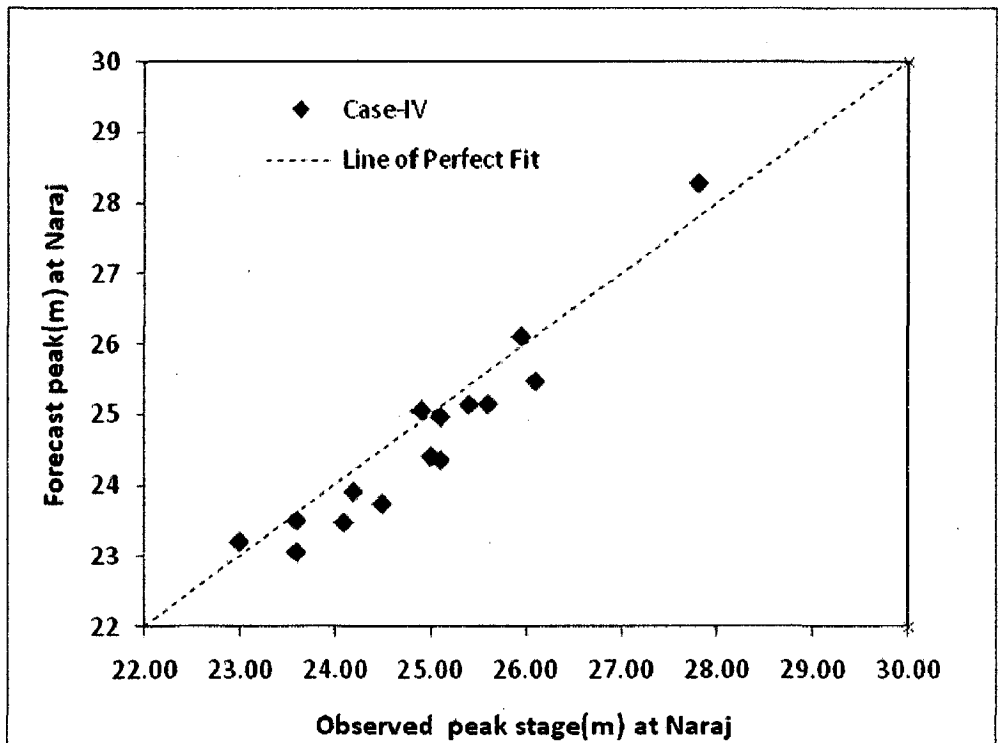


Fig. 5.9 (b) Forecast and observed peaks for Case-IV in validation

A major limitation of these equations is that these can be used in limited range of stage variation only. For example, if stage at Khairmal (H_K) is zero, the resulting stage at Naraj (H_N) is negative which is impossible and undesirable as well. Thus, these equations are valid only when H_N is greater than or equal to zero.

In all the years, the computed peak stages were compared with the observed peak stages and these are given in Table 5.3. For performance evaluation, the relative error (%) was computed as:

$$\text{Relative error(\%)} = \frac{(H_o - H_c)}{H_o} * 100 \quad (5.1)$$

Where, H_o and H_c correspond to the observed and computed stage values, respectively.

Table 5.3 Observed and computed (annual) peak stages and relative errors (peak to peak)

Year	Observed peak(m)	Computed peak(m)	Relative error(%)
2005	26.00	25.83	0.66
2006	26.90	27.52	-2.31
2007	25.90	25.63	1.05
2008	27.80	28.43	-2.28
2009	26.10	25.63	1.81

It is apparent from Table 5.3 that the relative errors for five years range from -2.28 % to 1.81 %. The sufficiently low values of errors are indicative of the satisfactory model performance. Here '+' values indicate that the computed values are lower than the observed ones and vice versa for '-' values. It is also apparent from the table that the high stages yield relatively high relative errors.

5.1.2 Three-hourly Continuous Stage Forecasting

Here three hourly continuous stages are correlated through multiple-linear regression analysis. In this, the influencing values or predictor variables corresponding to different lags are considered for establishment of a statistical correlation using EXCEL 2007. The dataset from 2005 to 2007 was used for model formulation, and the dataset from 2008 to 2009 for model validation.

The input vector is selected generally by trial and error method (Maier and Dandy, 2000). Determination of the number of antecedent stage values involves the computation of lags of stage values that have significant influence on the forecasted

stage. These influencing values corresponding to different lags can be identified through statistical analysis of the data series by avoiding the trial and error procedure. The statistical parameter such as cross correlation function (CCF) can be used for this purpose. Therefore, on the basis of cross correlation function of the data series, the input vector has been selected for the flood forecasting model in the present study.

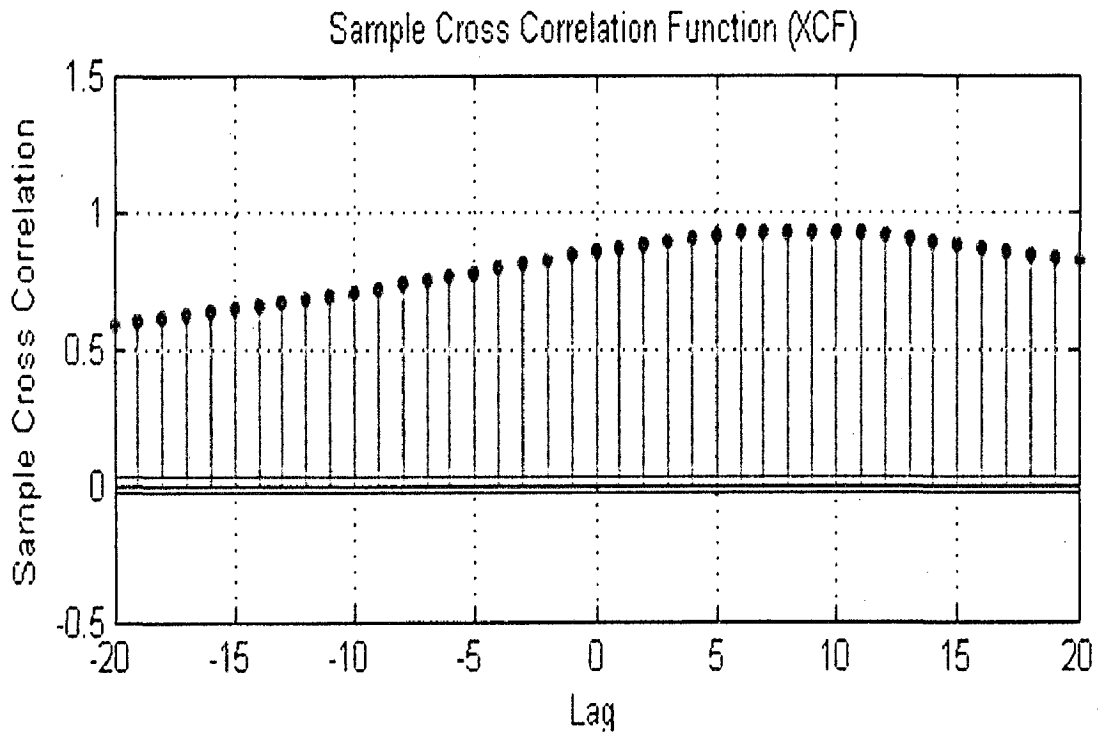


Fig 5.10: Sample cross correlation plot

Fig 5.10, the cross correlation plot between the three hourly stages at Khairmal site suggests the model input vector of stage series of Naraj site. This plot indicates the stage with 8(times 3) hr lag influences the stage at Naraj more than that due to any other lag time. To refine the model accordingly different model structures have been considered for forecasting the stage at Naraj. Total three cases were considered, Case-I: considers Khairmal stage only, Case-II: considers previous stage of Naraj only, and Case-III: considers combination of Khairmal and previous Naraj stages.

In the employment of statistical approach, different combination of relations between stages of Khairmal and Naraj were suggested and these are shown in Table 5.4.

Table 5.4 Model Formulations

Model No	Model
Case I Forecasting by taking Khairmal stage only	
M1	$H_N = f(H_{K(t-8)})$
M2	$H_N = f(H_{K(t-8)}, H_{K(t-7)})$
M3	$H_N = f(H_{K(t-9)}, H_{K(t-8)}, H_{K(t-7)})$
M4	$H_N = f(H_{K(t-9)}, H_{K(t-8)}, H_{K(t-7)}, H_{K(t-6)})$
M5	$H_N = f(H_{K(t-10)}, H_{K(t-9)}, H_{K(t-8)}, H_{K(t-7)}, H_{K(t-6)})$
Case II Forecasting by taking previous Naraj stages only	
M6	$H_N = f(H_{N(t-1)})$
M7	$H_N = f(H_{N(t-1)}, H_{N(t-2)})$
M8	$H_N = f(H_{N(t-1)}, H_{N(t-2)}, H_{N(t-3)})$
M9	$H_N = f(H_{N(t-1)}, H_{N(t-2)}, H_{N(t-3)}, H_{N(t-4)})$
Case III Forecasting by taking Khairmal and previous Naraj stage	
M10	$H_N = f(H_{K(t-8)}, H_{N(t-1)})$

In this Table, total ten models are taken into consideration with three cases. Case-I forecasting by taking Khairmal stage only, under this case total five models are formulated with different combinations keeping 8(times 3) hr lag data as centre point derived from the sample cross correlation plot (Fig 5.10). Case-II forecasts by taking previous Naraj stage only. Under this case, four models are considered. Case-III forecasts by taking Khairmal stage and previous Naraj stage. While formulating these models number of input parameters is also taken into consideration, so that model with minimum number of input parameters could be recommended.

Table 5.5 Performance of Statistical Models

Model	COD		RMSE (m)		NSE	
	Calibration	Validation	Calibration	Validation	Calibration	Validation
Case-I						
M1	0.51	0.60	0.96	0.80	0.51	0.58
M2	0.54	0.64	0.94	0.76	0.54	0.62
M3	0.54	0.64	0.94	0.76	0.54	0.62
M4	0.55	0.66	0.91	0.74	0.56	0.63
M5	0.55	0.66	0.91	0.74	0.56	0.63
Case-II						
M6	0.99	0.99	0.12	0.09	0.99	0.99
M7	0.99	0.99	0.11	0.08	0.99	0.99
M8	0.99	0.99	0.11	0.08	0.99	0.99
M9	0.99	0.99	0.11	0.08	0.99	0.99
Case-III						
M10	0.99	0.99	0.12	0.09	0.99	0.99

These models are calibrated using the three hourly stage data from 2005 to 2007, and validated on the dataset from 2008 to 2009. The model performance is evaluated using COD, RMSE, and NSE. It is seen in Table 5.5 that the values of COD and NSE vary in the range of 0.51 to 0.99 and 0.51 to 0.99, respectively, in calibration for the models suggested and these values vary in the range of 0.51 to 0.99 and 0.58 to 0.99 in model validation. RMSE varies from 0.11 to 0.96 in calibration, and from 0.09 to 0.80 in validation.

Model M2 is seen to have performed better than all other models with the values of COD, RMSE, and NSE resulting as 0.54, 0.94, and 0.54, respectively, in calibration, and 0.64, 0.76, and 0.62, respectively, in validation in Case I that considers Khairmal stage only. Model M1 performs poorer because its COD and NSE are less than the M2 and RMSE is more, and thus, M1 is not a preferred model. Performance of M2 and M3 is almost same but the number of input parameters in M2 is two whereas three in case of M3, and therefore, to reduce the number of input parameters in the model, M2 is taken as the best model. Models M4 and M5 show slightly better performance than model M2 but the number of input parameters is four and five respectively whereas M2 has only two input parameters. To reduce the number of parameters, M2 is given preference over others.

Among Models M6 to M9 with Naraj stage as inputs, Model M7 performs better than the others. In model M6, though COD and NSE are same but RMSE is more than M7, and therefore, M7 is preferred. The performance of M7 to M9 does not vary much but the number of input parameters in the forecasting model is 2, 3 and 4 respectively and thus, to reduce the number of parameters M7 is taken as the best model. In general, Model M7 is considered as more suitable model yielding the COD, RMSE, and NSE as 0.99, 0.11, and 0.99, respectively, in calibration, and 0.99, 0.08, and 0.99 in validation. It is observed that the inclusion of 3-hour previous stage in Models M6 to M9 increases the model performance significantly.

Model M10 is the combination of models M1 and M6, considering the Khairmal stage and Naraj stage. It yields COD, RMSE, and NSE as 0.99, 0.12, and 0.99 respectively in calibration and 0.99, 0.09, and 0.99 in validation. The performance of

M10 is almost same as M6 and M7, and therefore, no further investigation was carried out because other models have larger number of input parameters.

As above M2, M7 and M10 are the best models of Case-I, Case-II and Case-III respectively. Out of these three models M2 has very low COD, NSE and high RMSE values, and therefore, its performance compared to M7 and M10 is not good. The value of COD, NSE and RMSE are almost the same for M7 and M10 with equal number of input parameters but M7 with less input parameters depends on a single station data whereas M10 depends on two stations data. It is easy to collect the data from a single station rather than collecting from two or more stations in case of emergency or flood time, and thus, M7 is preferred over others with COD, RMSE, and NSE as 0.99, 0.11, and 0.99, respectively, in calibration, and 0.99, 0.08, and 0.99 in validation.

5.2 ANN Analysis

The data used in statistical model development were further used in development of a model based on the artificial neural network (ANN) architecture using MATLAB 2008 codes. The 3 hourly stage data of monsoon period for the year 2005 to 2007 (2951 values) are used for calibration and data of 2008-2009 (1849 values) are used for validation. The trial has been taken with a 3-layer feed forward network with back propagation error algorithm. Different combinations of feed forward network with changing transfer function, number of neurons and epochs varying at an increment of 20 are trailed. The combinations which are mostly as per performance criteria are noted. In all cases 'tansing' neurons are used in the first layer, 'purelin' in second layer and 'trainbr' remains the training function. Both 'tansing' and 'purelin' are better compatible with feed forward networks. Again the two layer sigmoid/linear network can represent any functional relationship inputs and outputs if the sigmoid layer has enough neurons (WMO, 1994). The 'trainbr' function updates the weight and bias values as per Levenberg-Marquardt optimization. It minimizes the combination of squared errors and weights and then determines the correct combination to produce a network that generalizes well as per Bayesian regularization process. It reduces the difficulty of determining the optimum network architecture also over-fitting of training dataset is prevented, whereas in other networks, generalization and early stopping is required for reducing over-fitting. The performance functions are set as COD, RMSE, and NSE.

Table 5.6 Performance criteria of ANN Models

Model	COD		RMSE (m)		NSE	
	Calibration	Validation	Calibration	Validation	Calibration	Validation
Case I						
M1	0.93	0.95	0.48	0.47	0.87	0.85
M2	0.93	0.95	0.47	0.46	0.88	0.85
M3	0.94	0.95	0.46	0.47	0.88	0.85
M4	0.94	0.95	0.45	0.47	0.89	0.85
M5	0.94	0.95	0.44	0.47	0.89	0.85
Case II						
M6	0.99	0.99	0.12	0.09	0.99	0.99
M7	0.99	0.99	0.11	0.08	0.99	0.99
M8	0.99	0.99	0.18	0.13	0.98	0.98
M9	0.99	0.99	0.18	0.13	0.98	0.98
Case III						
M10	0.99	0.99	0.11	0.08	0.99	0.99

Performance indices of the ANN models (M1 to M10) viz. COD, RMSE, and NSE are presented in Table 5.6 and these are used for model comparison. The values of COD and NSE are seen to vary in the range of 0.93 to 0.99 and 0.87 to 0.99, respectively, in calibration for the models suggested and these values vary in the range of 0.95 to 0.99 and 0.85 to 0.99 in model validation. RMSE varies from 0.11 to 0.48 in calibration, and from 0.08 to 0.47 in validation.

Model M2 is seen to have performed better than all other models with the values of COD, RMSE, and NSE resulting as 0.93, 0.47, and 0.88, respectively, in calibration, and 0.95, 0.46, and 0.85, respectively, in validation in Case I that considers Khairmal stage only. Model M1 performs poorer because its NSE is less than M2 in calibration and RMSE is more both in calibration and validation, and therefore, M1 is not a preferred model. Performance of M2 and M3 is almost the same, but the number input parameters in M2 is two whereas three in case of M3, and thus, to reduce number of input model parameters, M2 has been taken as the best model. Models M4 and M5 exhibit slightly better performance than model M2 but the number of input parameters is four and five respectively, whereas M2 has only two input parameters. For reasons of lesser number of parameters, M2 is taken as the best model.

Among Models M6 to M9 with Naraj stage as input, Model M7 performs better than the others; in model M6, though COD and NSE are the same but RMSE is more than

M7. The performance of M8 and M9 also deteriorates compared to M7 and the number of input parameters in the forecasting model is 3 and 4 respectively, and therefore, to reduce the number of parameters we select M7 as a more appropriate model. In general, Model M7 is considered as more suitable model yielding COD, RMSE, and NSE as 0.99, 0.11, and 0.99, respectively, in calibration, and 0.99, 0.08, and 0.99 in validation. It is observed that the inclusion of 3-hour previous stage of Naraj in Models M6 to M9 increases the model performance.

Model M10 is a combination of model M1 and M6, considering the Khairmal stage and Naraj stage. It yields COD, RMSE, and NSE as 0.99, 0.11, and 0.99, respectively, in calibration, and 0.99, 0.08, and 0.99 in validation. The performance of M10 is almost the same as M6 and M7, and therefore, further investigation was not desirable.

M2, M7 and M10 are the best models of Case-I, Case-II and Case-III respectively. Out of these three models M2 has very low COD, NSE and high RMSE values, and therefore, its performance as compared to M7 and M10 is not good. The value of COD, NSE and RMSE are almost same for M7 and M10 with equal number of input parameters but M7 input parameter depends on a single station data whereas M10 depends on two stations data. It is easy to collect the data from a single station rather than collecting from two or more stations in case of emergency flood time, and therefore, we select M7 as a preferable model over the other three cases with COD, RMSE, and NSE as 0.99, 0.11, and 0.99, respectively, in calibration, and 0.99, 0.08, and 0.99 in validation.

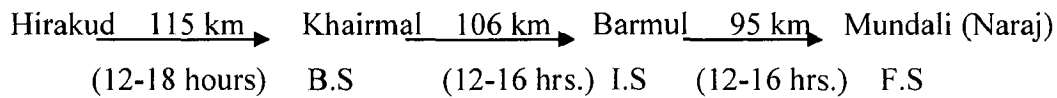
Optimal model structure decided on trial and error method. As per the inputs involved in the model, neurons in hidden layer kept varied from 1 to 6. The maximum performance obtained in M2, M7 and M10, with model structure 2-3-1, 2-2-1 and 2-2-1 respectively.

5.3 Model Comparison

Based on COD, RMSE and NSE the model performance is compared in both calibration and validation as shown in Tables 5.5 and 5.6. In Case-I, best statistical model yields COD, RMSE, and NSE as 0.54, 0.94, and 0.54 respectively in calibration, and 0.64, 0.76, and 0.62 in validation whereas the best ANN model yields COD, RMSE, and NSE as 0.93, 0.47, and 0.88 respectively in calibration, and 0.95, 0.46, and 0.88 in

validation. The performance of ANN model has been better as it has larger number of parameters and considers the process as non-linear whereas in statistical model, the process is considered as linear.

In Mahanadi deltaic part Department of Water Resources, Government of Orissa is forecasting flood by using time lag method, in which they are able to forecast the travel time only i.e. time taken by the Khairmal flood to reach the next intermediate station or forecast station. A schematic presentation shows the distance and travel time from Hirakud to Mundali presently being used for the official purposes of Department of Water Resources, Government of Orissa (WR Dept. Govt. of Orissa).



By adopting clustering method Kar et.al (2010) also proved that the travel time between the Khairmal and Munduli (u/s Naraj) stations varies from 24 to 37 hrs. By following the above travel time we can use the M2 ANN model for flood forecasting at Naraj site using the Khairmal stage only.

In Case-II, the performance of the statistical model and ANN model is almost the same, and therefore, in this case, the importance of the statistical model can't be ignored because it also gives encouraging results, and thus, the statistical model can also be used as a forecasting model instead of ANN model when model is formulated by considering previous stage of Naraj only. In Case-III also, the performance of statistical model is equivalent to ANN model, and therefore, we can use the statistical model instead of ANN model.

Figs. 5.11(a-c) and Figs. 5.12(a-b) show that ANN model M7 perform better than the counterpart statistical model requiring same input(s). Figs 5.11 (a-c) compares the stages for the year 2005, 2006 and 2007 respectively with observed stages, ANN forecasted stages and statistical forecasted stages in calibration. Figs 5.12 (a-b) compares the stages for the year 2008 and 2009 respectively with the observed stages, ANN forecasted stages and statistical forecasted stages in validation. It is observed in the above figs, ANN result

are more close to the observed than the statistical ones, therefore, ANN-based models have better than others in forecasting peak floods.

Table 5.7 Observed and computed peak stages and relative errors (3-hr continuous flow)

Year	Observed peak(m)	ANN peak(m)	Relative error (%)	Statistical peak(m)	Relative error (%)
2005	26.00	25.84	0.62	25.88	0.45
2006	26.90	26.60	1.10	26.88	0.08
2007	25.90	25.87	0.11	25.96	-0.25
2008	27.80	27.42	1.37	27.81	-0.04
2009	26.10	25.76	1.30	26.06	0.15

It is apparent from Table 5.7 that the relative errors ANN and statistical models for five years range from 0.62 % to 1.37 % and -0.25% to 0.45%. These sufficiently low values are indicative of satisfactory model performance. Here ‘+’ values indicate that the computed values are lower than the observed ones, and vice versa for ‘-’ values. It is also apparent from the table that the high stage yield relatively high relative errors.

5.4 Forecasting using the Recommended Model

Flood forecasting using the recommended model for different lead times of maximum lag 8 (times 3=24 hr) is shown in Table 5.8.

Table 5.8 Performance of the recommended ANN model M7 under different lead times

Maximum lag= 8(times 3=24 hr).

Lead Time	COD		RMSE		NSE	
	Calibration	Validation	Calibration	Validation	Calibration	Validation
3 hours	0.99	0.99	0.11	0.08	0.99	0.99
6 hours	0.98	0.99	0.25	0.19	0.97	0.98
9 hours	0.97	0.98	0.32	0.25	0.95	0.96
12 hours	0.96	0.97	0.37	0.29	0.93	0.95
15 hours	0.95	0.96	0.43	0.34	0.90	0.92
18 hours	0.94	0.95	0.48	0.38	0.88	0.91
21 hours	0.92	0.94	0.53	0.43	0.85	0.88
24 hours	0.91	0.93	0.58	0.47	0.82	0.85

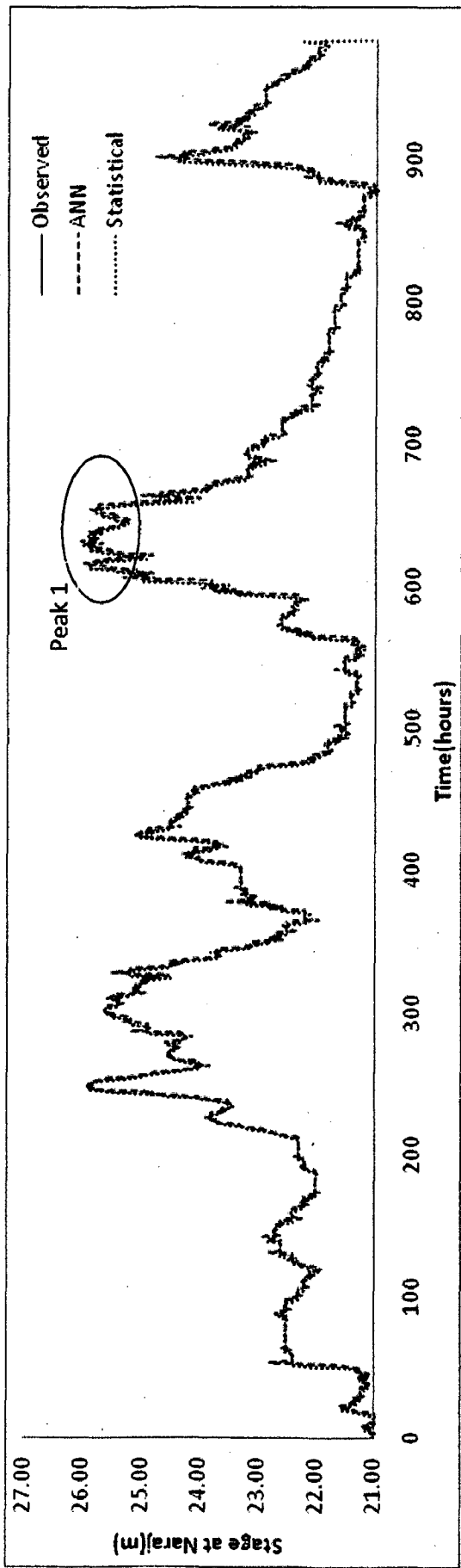


Fig. 5.11 (a) Comparison of stages in calibration for the year 2005 of M7

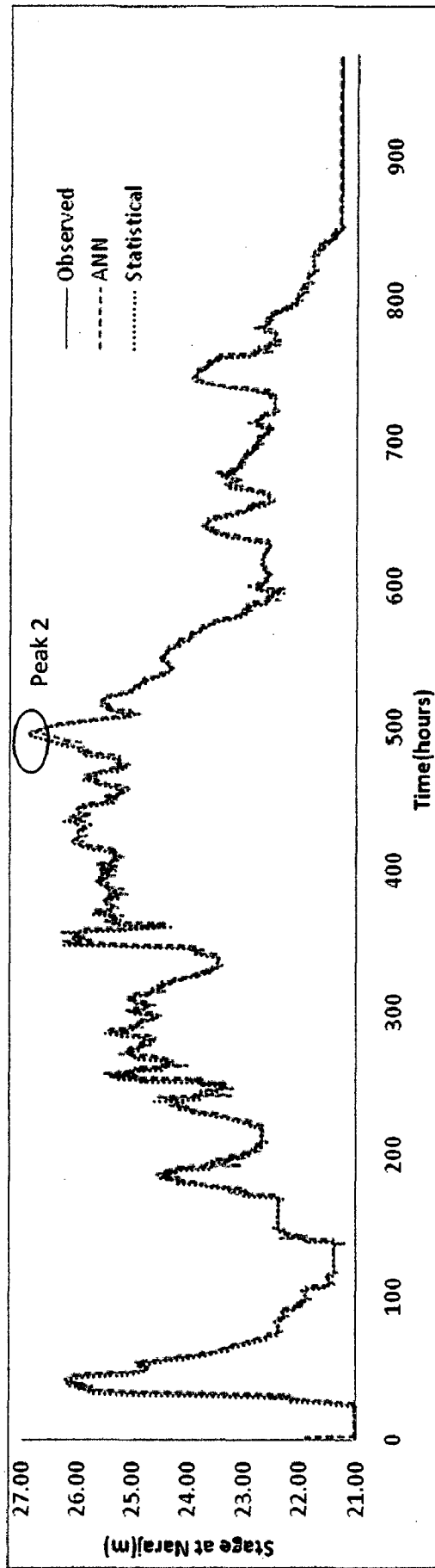


Fig. 5.11 (b) Comparison of stages in calibration for the year 2006 of M7

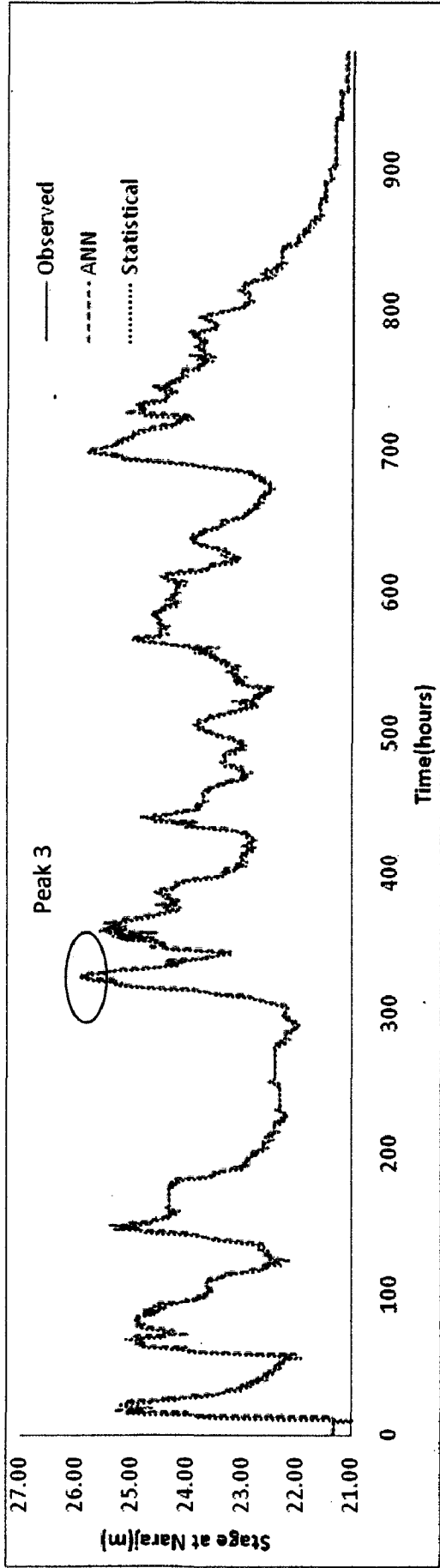


Fig. 5.11 (c) Comparison of stages in calibration for the year 2007 of M7

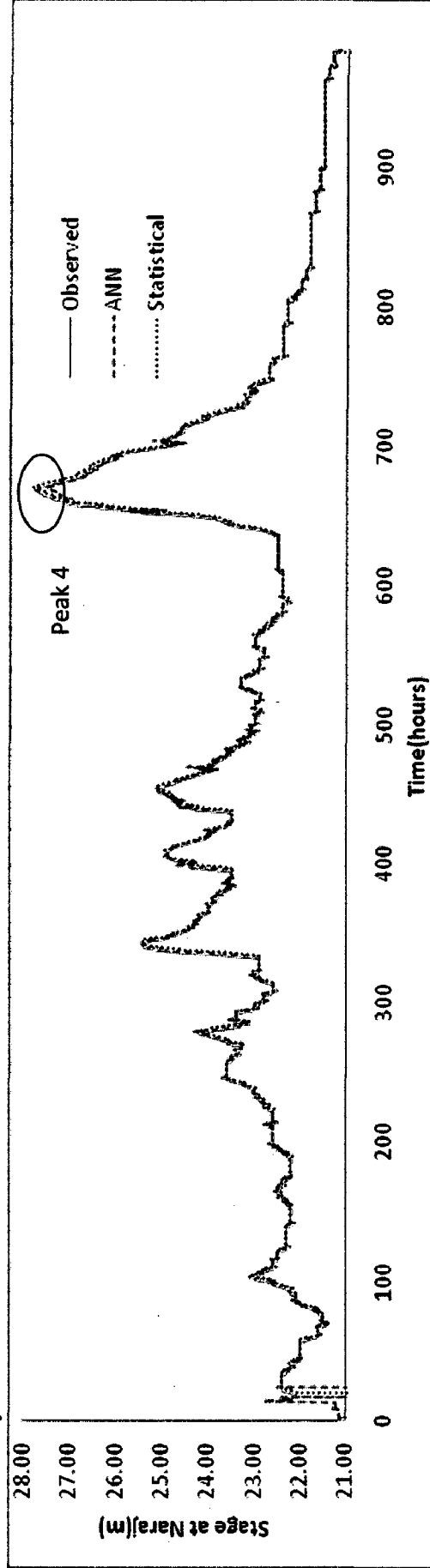


Fig. 5.12 (a) Comparison of stages in validation for the year 2008 of M7

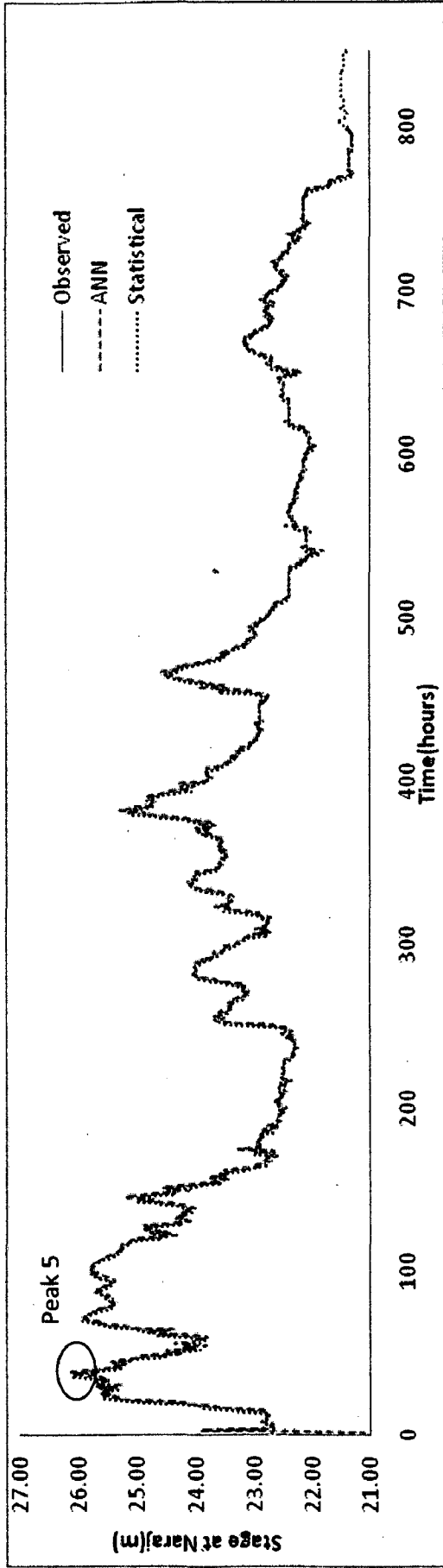


Fig. 5.12 (b) Comparison of stages in validation for the year 2009 of M7

In Table 5.8, the performance indices such as COD, RMSE and NSE values range from 0.91 to 0.99, 0.11 to 0.58 and 0.82 to 0.99 respectively in calibration and 0.93 to 0.99, 0.09 to 0.47 and 0.85 to 0.99 in validation. It is observed that as the lead time increases COD and NSE decrease and RMSE increases, and thus, the smaller the lead time the better the model results, and vice versa.

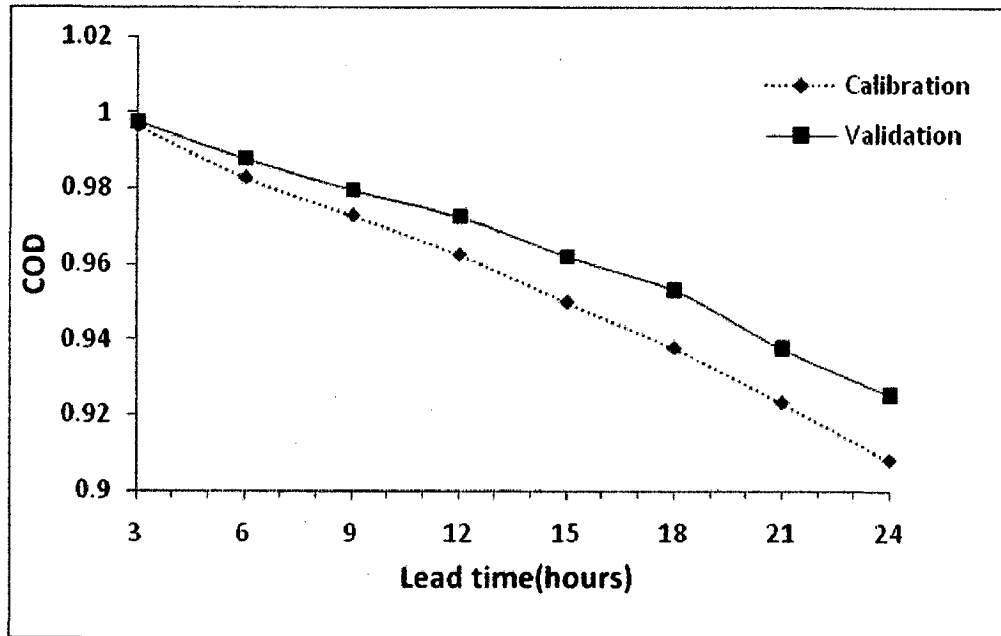


Fig. 5.13 Variation of COD with lead time in the recommended ANN model M7

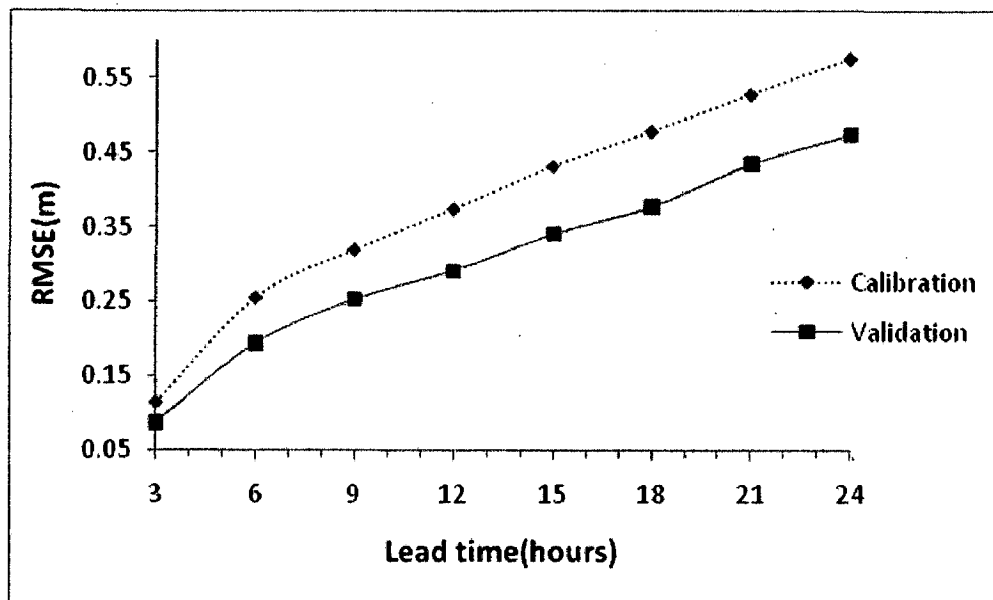


Fig. 5.14 Variation of RMSE with lead time in the recommended ANN model M7

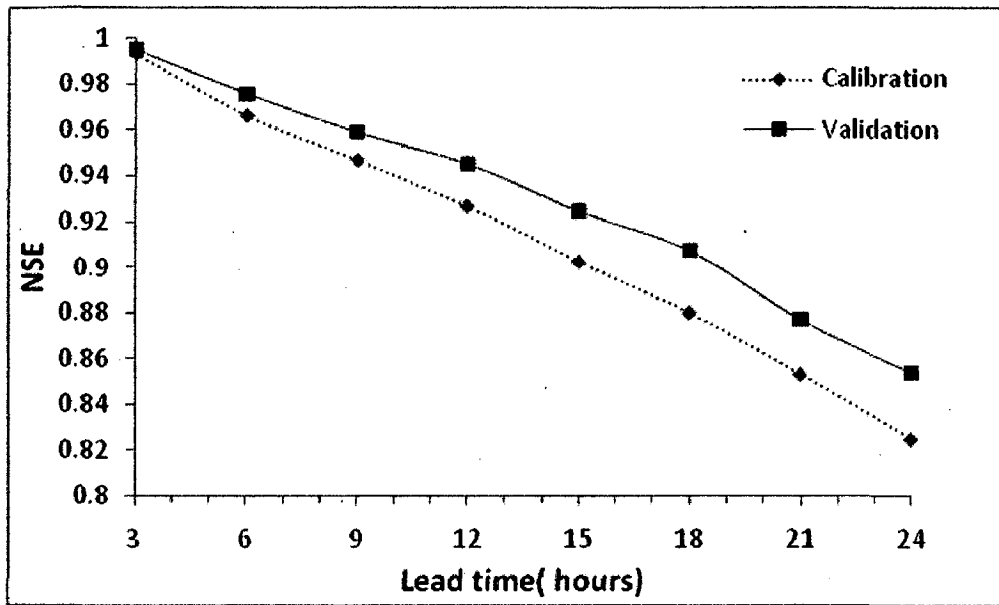


Fig. 5.15 Variation of NSE with lead time in the recommended ANN model M7

FigS 5.13 - 5.15 compare the calibration and validation performance results using COD, RMSE and NSE respectively of Case-II best ANN model. In Fig.5.13, it is seen that in calibration COD is less but in validation it is higher and as lead time increases, COD decreases. In Fig.5.14, it is observed that RMSE is almost the same in both calibration and validation. RMSE varies with lead time, as the latter increases then the former also increases. In Fig.5.15, it is observed that NSE in calibration is more than that in validation. NSE decreases with increasing lead time, and vice versa.

Mahanadi is a flood prone basin, controlling flood through moderation structure other than Hirakud reservoir is nearly impossible at present time. Therefore to control flood require non-structural measures like flood risk mapping, flood plain zoning, flood forecasting, flood proofing, flood insurance etc. At present this basin is not adequately supported by an efficient flood forecasting model for downstream part of Hirakud. Establishment of a physical based model requires lot of hydro-meteorological data. In this regard soft computing method like ANN application is a better alternative.

In this study attempt has been made to develop a flood forecasting model using stage of Khairmal site (base station) to forecast at Naraj site (forecast station). The main objectives of the study are to propose an ANN-based flood forecasting method for deltaic region of Mahanadi basin and to compare the forecasting results with those due to available conventional methods.

Drawing time series of Khairmal and Naraj stage total 65 peaks were derived. These 65 peaks were divided into two parts, one part for calibration and rest for validation. The best statistical model for peak to peak stage is derived by considering 50 peaks for calibration and 15 peaks for validation. This model yields COD, RMSE, and NSE as 0.86, 0.44, and 0.86, respectively, in calibration, and 0.92, 0.39, and 0.89 in validation.

The model is developed by basing on the criteria of cross correlation with the available 3 hourly continuous stage data for the period from 2005 to 2009. First three-year data were used for calibration, and rest two-year data for validation. Performance indices such as coefficient of determination (COD), root mean square (RMSE) and Nash-Sutcliffe Efficiency (NSE) were used for model selection. The forecasting obtained by both statistical and ANN methods is encouraging. The ANN method generally exhibits a better performance than the statistical method. The result at Naraj (Forecasting Station) with respect to Khairmal (Base Station) basing on the ANN network is best for taking the flood forecasting effectively because its NSE is 99% , RMSE is 0.11 m, and COD is 0.99.

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APPENDIX-I

Table I.1 Data used for study.

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
1	01.07.05	3	101.28	21.00	33	05.07.05	3	100.96	21.20	65	09.07.05	3	102.24	22.50	97	13.07.05	3	102.24	22.50	97	13.07.05	3	101.49	22.40
2		6	101.28	21.00	34		6	100.99	21.20	66		6	102.24	22.50	98		6	102.24	22.50	98		6	101.43	22.40
3		9	101.27	21.00	35		9	101.00	21.10	67		9	102.24	22.50	99		9	102.24	22.50	99		9	101.42	22.30
4		12	101.26	21.00	36		12	101.47	21.10	68		12	102.24	22.50	100		12	102.24	22.50	100		12	101.41	22.30
5		15	101.25	21.00	37		15	102.22	21.10	69		15	102.26	22.50	101		15	102.26	22.50	101		15	101.40	22.30
6		18	101.24	21.10	38		18	102.28	21.10	70		18	102.29	22.50	102		18	102.29	22.50	102		18	101.40	22.30
7		21	101.21	21.10	39		21	102.28	21.10	71		21	102.31	22.50	103		21	102.31	22.50	103		21	101.40	22.30
8		24	101.18	21.00	40		24	102.28	21.10	72		24	102.31	22.50	104		24	102.31	22.50	104		24	101.44	22.30
9	02.07.05	3	101.17	21.00	41	06.07.05	3	102.28	21.20	73	10.07.05	3	102.31	22.50	105	14.07.05	3	102.31	22.50	105	14.07.05	3	101.50	22.20
10		6	101.14	21.00	42		6	102.28	21.20	74		6	102.31	22.50	106		6	102.31	22.50	106		6	101.56	22.20
11		9	101.13	21.00	43		9	102.28	21.10	75		9	102.31	22.50	107		9	102.31	22.50	107		9	101.83	22.20
12		12	101.12	21.00	44		12	102.28	21.10	76		12	102.31	22.50	108		12	102.31	22.50	108		12	102.06	22.20
13		15	101.11	20.90	45		15	102.28	21.20	77		15	102.31	22.50	109		15	102.31	22.50	109		15	102.14	22.20
14		18	101.10	20.90	46		18	102.28	21.20	78		18	102.31	22.50	110		18	102.31	22.50	110		18	102.20	22.20
15		21	100.07	20.90	47		21	102.27	21.20	79		21	102.28	22.50	111		21	102.28	22.50	111		21	102.25	22.20
16		24	100.04	20.90	48		24	102.26	21.30	80		24	102.22	22.50	112		24	102.22	22.50	112		24	102.28	22.20
17	03.07.05	3	101.01	21.10	49	07.07.05	3	102.25	21.40	81	11.07.05	3	102.16	22.50	113	15.07.05	3	102.16	22.50	113	15.07.05	3	102.31	22.10
18		6	100.99	21.20	50		6	102.25	21.60	82		6	102.10	22.50	114		6	102.10	22.50	114		6	102.34	22.10
19		9	100.98	21.30	51		9	102.24	22.20	83		9	101.96	22.50	115		9	101.96	22.50	115		9	102.40	22.10
20		12	100.98	21.40	52		12	102.24	22.40	84		12	101.76	22.50	116		12	101.76	22.50	116		12	102.43	22.10
21		15	100.97	21.50	53		15	102.24	22.40	85		15	101.58	22.50	117		15	101.58	22.50	117		15	102.45	22.00
22		18	100.96	21.40	54		18	102.24	22.40	86		18	101.54	22.60	118		18	101.54	22.60	118		18	102.45	22.00
23		21	100.95	21.40	55		21	102.24	22.40	87		21	101.54	22.60	119		21	101.54	22.60	119		21	102.46	22.00
24		24	100.94	21.40	56		24	102.24	22.40	88		24	101.56	22.60	120		24	101.56	22.60	120		24	102.46	22.10
25	04.07.05	3	100.93	21.30	57	08.07.05	3	102.24	22.40	89	12.07.05	3	101.59	22.50	121	16.07.05	3	101.59	22.50	121	16.07.05	3	102.46	22.20
26		6	100.93	21.30	58		6	102.24	22.40	90		6	101.62	22.50	122		6	101.62	22.50	122		6	102.47	22.30
27		9	100.92	21.30	59		9	102.24	22.40	91		9	101.64	22.50	123		9	101.64	22.50	123		9	102.47	22.30
28		12	100.91	21.20	60		12	102.24	22.40	92		12	101.63	22.50	124		12	101.63	22.50	124		12	102.50	22.40
29		15	100.90	21.20	61		15	102.24	22.50	93		15	101.62	22.50	125		15	101.62	22.50	125		15	102.59	22.40
30		18	100.90	21.20	62		18	102.24	22.50	94		18	101.59	22.50	126		18	101.59	22.50	126		18	102.65	22.40
31		21	100.90	21.20	63		21	102.24	22.50	95		21	101.56	22.50	127		21	101.56	22.50	127		21	102.66	22.40
32		24	100.93	21.20	64		24	102.24	22.50	96		24	101.53	22.50	128		24	101.53	22.50	128		24	102.64	22.40

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
129	17.07.05	3	102.61	22.60	166		18	101.38	22.20	203		9	102.23	22.30	240		24	105.33	24.20
130		6	102.58	22.60	167		21	101.38	22.20	204		12	102.78	22.30	241	31.07.05	3	105.23	24.60
131		9	102.55	22.60	168		24	101.41	22.20	205		15	103.14	22.30	242		6	105.06	24.70
132		12	102.54	22.60	169	22.07.05	3	101.44	22.10	206		18	103.27	22.30	243		9	104.93	24.90
133		15	102.53	22.60	170		6	101.47	22.10	207		21	103.39	22.30	244		12	104.81	25.50
134		18	102.52	22.60	171		9	101.50	22.00	208		24	103.50	22.30	245		15	104.72	25.70
135		21	102.49	22.60	172		12	101.53	22.00	209	27.07.05	3	103.59	22.30	246		18	104.58	25.90
136		24	102.43	22.60	173		15	101.56	22.00	210		6	103.68	22.30	247		21	104.40	25.90
137	18.07.05	3	102.37	22.60	174		18	101.59	22.00	211		9	103.82	22.40	248		24	104.19	25.90
138		6	102.31	22.60	175		21	101.60	22.00	212		12	103.97	22.50	249	01.08.05	3	104.01	25.90
139		9	102.23	22.70	176		24	101.59	22.00	213		15	104.08	22.60	250		6	103.84	25.90
140		12	102.16	22.80	177	23.07.05	3	101.58	22.00	214		18	104.08	22.70	251		9	103.81	25.80
141		15	102.12	22.70	178		6	101.57	22.00	215		21	104.06	22.80	252		12	103.78	25.70
142		18	102.09	22.70	179		9	101.56	22.00	216		24	104.00	22.90	253		15	103.69	25.40
143		21	102.06	22.70	180		12	101.55	22.00	217	28.07.05	3	103.92	23.10	254		18	103.60	25.20
144		24	102.03	22.70	181		15	101.55	22.00	218		6	103.83	23.20	255		21	103.57	25.00
145	19.07.05	3	102.00	22.70	182		18	101.58	22.00	219		9	103.77	23.30	256		24	103.74	24.90
146		6	101.97	22.70	183		21	101.61	22.00	220		12	103.66	23.50	257	02.08.05	3	104.12	24.70
147		9	101.88	22.70	184		24	101.62	22.00	221		15	103.60	23.60	258		6	104.47	24.50
148		12	101.79	22.70	185	24.07.05	3	101.62	22.00	222		18	103.54	23.70	259		9	104.54	24.30
149		15	101.75	22.60	186		6	101.62	22.00	223		21	103.50	23.70	260		12	104.54	24.20
150		18	101.72	22.60	187		9	101.62	22.00	224		24	103.47	23.80	261		15	104.52	24.00
151		21	101.66	22.60	188		12	101.63	22.10	225	29.07.05	3	103.44	23.80	262		18	104.49	24.00
152		24	101.57	22.60	189		15	101.66	22.20	226		6	103.41	23.80	263		21	104.47	24.00
153	20.07.05	3	101.50	22.40	190		18	101.69	22.20	227		9	103.38	23.80	264		24	104.46	24.00
154		6	101.45	22.40	191		21	101.68	22.20	228		12	103.37	23.70	265	03.08.05	3	104.45	24.20
155		9	101.44	22.40	192		24	101.68	22.20	229		15	103.37	23.60	266		6	104.44	24.30
156		12	101.43	22.40	193	25.07.05	3	101.67	22.20	230		18	103.34	23.60	267		9	104.41	24.40
157		15	101.46	22.40	194		6	101.66	22.20	231		21	103.31	23.50	268		12	104.41	24.50
158		18	101.45	22.40	195		9	101.66	22.20	232		24	103.31	23.50	269		15	104.41	24.50
159		21	101.44	22.40	196		12	101.77	22.30	233	30.07.05	3	103.38	23.50	270		18	104.41	24.50
160		24	101.43	22.40	197		15	101.89	22.30	234		6	103.45	23.50	271		21	104.40	24.50
161	21.07.05	3	101.42	22.30	198		18	101.91	22.30	235		9	103.82	23.50	272		24	104.38	24.50
162		6	101.41	22.30	199		21	101.97	22.30	236		12	104.33	23.50	273	04.08.05	3	104.37	24.50
163		9	101.41	22.20	200		24	102.03	22.30	237		15	104.81	23.70	274		6	104.35	24.40
164		12	101.40	22.20	201	26.07.05	3	102.09	22.30	238		18	105.26	23.80	275		9	104.34	24.40
165		15	101.39	22.20	202		6	102.15	22.30	239		21	105.33	24.00	276		12	104.32	24.40

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
277		15	104.31	24.50	314		6	104.17	25.10	351		21	101.09	22.70	388		12	101.55	23.30
278		18	104.34	24.50	315		9	104.09	25.10	352		24	101.08	22.70	389		15	101.51	23.30
279		21	104.41	24.40	316		12	104.06	25.10	353	14.08.05	3	101.07	22.70	390		18	101.48	23.30
280		24	104.50	24.30	317		15	104.06	25.10	354		6	101.07	22.70	391		21	101.55	23.30
281	05.08.05	3	104.59	24.30	318		18	104.06	25.10	355		9	101.06	22.50	392		24	101.66	23.30
282		6	104.64	24.30	319		21	104.01	25.00	356		12	101.17	22.50	393	19.08.05	3	101.98	23.30
283		9	104.58	24.30	320		24	103.78	25.00	357		15	101.46	22.50	394		6	102.08	23.30
284		12	104.49	24.30	321	10.08.05	3	103.48	25.00	358		18	101.71	22.50	395		9	102.17	23.30
285		15	104.54	24.80	322		6	103.24	24.90	359		21	101.71	22.50	396		12	102.26	23.30
286		18	104.57	24.90	323		9	102.97	24.90	360		24	101.69	22.50	397		15	102.28	23.30
287		21	104.66	24.90	324		12	102.70	24.70	361	15.08.05	3	101.69	22.50	398		18	102.31	23.30
288		24	104.81	24.90	325		15	102.43	24.70	362		6	101.69	22.50	399		21	102.31	23.30
289	06.08.05	3	104.96	24.90	326		18	102.25	25.20	363		9	101.70	22.20	400		24	102.28	23.30
290		6	105.06	24.90	327		21	102.13	25.20	364		12	101.73	22.20	401	20.08.05	3	102.25	23.30
291		9	105.08	25.00	328		24	102.01	25.20	365		15	101.76	22.20	402		6	102.22	23.30
292		12	105.08	25.20	329	11.08.05	3	101.89	25.20	366		18	101.76	22.20	403		9	102.14	23.40
293		15	105.08	25.20	330		6	101.77	25.00	367		21	101.76	22.20	404		12	102.06	23.50
294		18	105.08	25.20	331		9	101.65	24.70	368		24	101.79	22.20	405		15	102.04	23.70
295		21	105.08	25.20	332		12	101.47	24.50	369	16.08.05	3	101.82	22.20	406		18	102.04	23.90
296		24	105.08	25.30	333		15	101.41	24.50	370		6	101.85	22.20	407		21	102.04	24.00
297	07.08.05	3	105.05	25.50	334		18	101.38	24.50	371		9	101.90	22.50	408		24	102.07	24.00
298		6	105.02	25.50	335		21	101.35	24.40	372		12	101.96	22.60	409	21.08.05	3	102.12	24.10
299		9	105.01	25.60	336		24	101.32	24.20	373		15	102.00	22.60	410		6	102.21	24.20
300		12	105.00	25.60	337	12.08.05	3	101.29	24.00	374		18	102.08	22.80	411		9	102.86	24.10
301		15	104.99	25.60	338		6	101.26	23.80	375		21	102.03	22.80	412		12	103.10	24.10
302		18	104.93	25.60	339		9	101.26	23.70	376		24	102.03	23.20	413		15	103.17	24.10
303		21	104.81	25.60	340		12	101.24	23.70	377	17.08.05	3	102.00	23.20	414		18	103.20	24.10
304		24	104.61	25.50	341		15	101.23	23.70	378		6	101.97	23.20	415		21	103.26	23.80
305	08.08.05	3	104.46	25.40	342		18	101.22	23.70	379		9	101.96	23.10	416		24	103.35	23.80
306		6	104.38	25.40	343		21	101.19	23.70	380		12	101.96	23.10	417	22.08.05	3	103.41	23.70
307		9	104.30	25.40	344		24	101.16	23.40	381		15	101.96	23.20	418		6	103.42	23.70
308		12	104.29	25.40	345	13.08.05	3	101.14	23.20	382		18	101.93	23.20	419		9	103.42	23.70
309		15	104.27	25.50	346		6	101.14	23.10	383		21	101.88	23.20	420		12	103.42	23.80
310		18	104.29	25.50	347		9	101.12	23.10	384		24	101.82	23.20	421		15	103.42	24.10
311		21	104.31	25.50	348		12	101.11	23.10	385	18.08.05	3	101.79	23.20	422		18	103.42	24.50
312		24	104.27	25.20	349		15	101.11	22.80	386		6	101.76	23.30	423		21	103.42	24.80
313	09.08.05	3	104.21	25.20	350		18	101.10	22.80	387		9	101.67	23.30	424		24	103.42	25.00

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
425	23.08.05	3	103.39	24.90	462		18	101.46	23.50	499		9	101.10	21.60	536		24	101.08	21.30
426		6	103.36	24.90	463		21	101.40	23.50	500		12	101.09	21.60	537	06.09.05	3	101.08	21.30
427		9	103.36	24.90	464		24	101.34	23.30	501		15	101.09	21.50	538		6	101.08	21.30
428		12	103.36	24.90	465	28.08.05	3	101.29	23.30	502		18	101.09	21.50	539		9	101.08	21.50
429		15	103.36	24.60	466		6	101.26	23.30	503		21	101.09	21.50	540		12	101.07	21.50
430		18	103.34	24.50	467		9	101.26	23.20	504		24	101.09	21.50	541		15	101.07	21.50
431		21	103.33	24.50	468		12	101.26	23.20	505	02.09.05	3	101.08	21.50	542		18	101.12	21.50
432		24	103.31	24.50	469		15	101.25	23.10	506		6	101.08	21.50	543		21	101.13	21.50
433	24.08.05	3	103.30	24.50	470		18	101.25	23.00	507		9	101.07	21.50	544		24	101.12	21.50
434		6	103.28	24.50	471		21	101.25	23.00	508		12	101.06	21.50	545	07.09.05	3	101.08	21.50
435		9	103.26	24.50	472		24	101.25	23.00	509		15	101.05	21.50	546		6	101.05	21.50
436		12	103.25	24.40	473	29.08.05	3	101.24	22.80	510		18	101.05	21.50	547		9	101.04	21.50
437		15	103.26	24.40	474		6	101.24	22.60	511		21	101.05	21.50	548		12	101.04	21.50
438		18	103.26	24.30	475		9	101.23	22.30	512		24	101.04	21.50	549		15	101.04	21.30
439		21	103.26	24.30	476		12	101.22	22.20	513	03.09.05	3	101.04	21.50	550		18	101.04	21.30
440		24	103.23	24.30	477		15	101.21	22.10	514		6	101.03	21.50	551		21	101.04	21.30
441	25.08.05	3	103.19	24.30	478		18	101.20	22.10	515		9	101.03	21.50	552		24	101.05	21.30
442		6	103.13	24.20	479		21	101.19	22.10	516		12	101.02	21.40	553	08.09.05	3	101.09	21.30
443		9	103.04	24.20	480		24	101.18	22.10	517		15	101.02	21.40	554		6	101.12	21.30
444		12	103.00	24.20	481	30.08.05	3	101.17	21.90	518		18	101.05	21.40	555		9	101.13	21.20
445		15	102.97	24.20	482		6	101.16	21.90	519		21	101.09	21.40	556		12	101.12	21.20
446		18	102.97	24.20	483		9	101.15	21.80	520		24	101.15	21.40	557		15	101.11	21.30
447		21	102.93	24.20	484		12	101.15	21.80	521	04.09.05	3	101.17	21.40	558		18	101.10	21.30
448		24	102.81	24.20	485		15	101.14	21.80	522		6	101.14	21.40	559		21	101.11	21.30
449	26.08.05	3	102.70	24.20	486		18	101.13	21.80	523		9	101.15	21.40	560		24	101.14	21.30
450		6	102.58	24.20	487		21	101.13	21.80	524		12	101.16	21.40	561	09.09.05	3	101.15	21.30
451		9	102.52	24.20	488		24	101.13	21.80	525		15	101.17	21.30	562		6	101.15	21.40
452		12	102.50	24.20	489	31.08.05	3	101.13	21.80	526		18	101.18	21.30	563		9	101.15	21.80
453		15	102.49	24.10	490		6	101.13	21.80	527		21	101.18	21.30	564		12	101.15	22.10
454		18	102.47	24.10	491		9	101.13	21.60	528		24	101.18	21.30	565		15	101.15	22.10
455		21	102.42	24.10	492		12	101.12	21.60	529	05.09.05	3	101.21	21.30	566		18	101.15	22.30
456		24	102.33	24.10	493		15	101.12	21.60	530		6	101.24	21.30	567		21	101.19	22.30
457	27.08.05	3	102.24	24.10	494		18	101.12	21.50	531		9	101.24	21.30	568		24	101.23	22.40
458		6	102.17	24.00	495		21	101.12	21.50	532		12	101.20	21.30	569	10.09.05	3	101.26	22.50
459		9	101.94	23.90	496		24	101.12	21.50	533		15	101.14	21.30	570		6	101.29	22.60
460		12	101.72	23.80	497	01.09.05	3	101.11	21.50	534		18	101.08	21.30	571		9	101.30	22.60
461		15	101.56	23.70	498		6	101.11	21.50	535		21	101.08	21.30	572		12	101.31	22.60

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	
573		15	101.31	22.60	610		6	104.16	25.30	647		21	104.56	25.50	684		12	102.29	23.10						
574		18	101.31	22.60	611		9	104.01	25.50	648		24	104.16	25.50	685		15	102.24	23.10						
575		21	101.31	22.60	612		12	104.18	25.60	649	20.09.05	3	103.85	25.60	686		18	102.24	22.90						
576		24	101.31	22.60	613		15	104.24	25.90	650		6	103.69	25.70	687		21	102.24	22.90						
577	11.09.05	3	101.31	22.60	614		18	104.24	25.90	651		9	103.36	25.70	688		24	102.24	22.90						
578		6	101.31	22.60	615		21	104.56	25.90	652		12	103.18	25.80	689	25.09.05	3	102.22	23.00						
579		9	101.31	22.50	616		24	105.06	25.80	653		15	103.02	25.80	690		6	102.19	23.10						
580		12	101.26	22.50	617	16.09.05	3	105.11	25.70	654		18	102.99	25.80	691		9	102.11	23.20						
581		15	101.20	22.40	618		6	105.11	25.50	655		21	102.94	25.80	692		12	102.10	23.20						
582		18	101.20	22.40	619		9	105.19	25.20	656		24	102.85	25.50	693		15	102.10	23.20						
583		21	101.23	22.40	620		12	105.25	25.00	657	21.09.05	3	102.77	25.30	694		18	102.10	23.20						
584		24	101.29	22.40	621		15	105.25	25.20	658		6	102.71	25.00	695		21	102.10	23.20						
585	12.09.05	3	101.35	22.40	622		18	105.21	25.40	659		9	102.58	24.60	696		24	102.08	23.20						
586		6	101.38	22.40	623		21	105.15	25.50	660		12	102.46	24.30	697	26.09.05	3	102.05	23.10						
587		9	101.38	22.40	624		24	105.12	25.70	661		15	102.39	24.70	698		6	102.02	23.00						
588		12	101.38	22.30	625	17.09.05	3	105.12	25.80	662		18	102.31	24.70	699		9	101.99	23.00						
589		15	101.38	22.30	626		6	105.11	25.90	663		21	102.25	24.70	700		12	101.98	22.90						
590		18	101.41	22.30	627		9	105.08	25.90	664		24	102.21	24.60	701		15	101.98	22.90						
591		21	101.56	22.30	628		12	105.05	25.80	665	22.09.05	3	102.18	24.40	702		18	101.98	22.90						
592		24	101.84	22.30	629		15	105.05	26.00	666		6	102.15	24.20	703		21	101.94	22.90						
593	13.09.05	3	102.18	22.70	630		18	105.05	25.90	667		9	102.15	24.00	704		24	101.85	22.90						
594		6	102.49	23.00	631		21	105.04	25.90	668		12	102.12	23.90	705	27.09.05	3	101.85	22.70						
595		9	103.06	23.40	632		24	104.96	25.90	669		15	102.09	23.90	706		6	101.82	22.60						
596		12	103.71	23.40	633	18.09.05	3	104.66	25.90	670		18	102.06	23.80	707		9	101.74	22.60						
597		15	104.09	23.70	634		6	104.30	25.90	671		21	102.03	23.80	708		12	101.63	22.60						
598		18	104.31	23.70	635		9	104.27	25.80	672		24	102.00	23.70	709		15	101.51	22.60						
599		21	104.46	23.80	636		12	104.27	25.90	673	23.09.05	3	101.97	23.60	710		18	101.42	22.60						
600		24	104.58	23.80	637		15	104.27	25.80	674		6	101.94	23.50	711		21	101.38	22.60						
601	14.09.05	3	104.71	23.80	638		18	104.35	25.80	675		9	101.93	23.30	712		24	101.35	22.60						
602		6	104.81	23.80	639		21	104.52	25.70	676		12	102.38	23.20	713	28.09.05	3	101.35	22.60						
603		9	104.88	24.50	640		24	104.61	25.60	677		15	102.51	23.20	714		6	101.35	22.60						
604		12	105.05	25.00	641	19.09.05	3	104.83	25.50	678		18	102.56	23.20	715		9	101.34	22.60						
605		15	105.12	25.00	642		6	104.88	25.40	679		21	102.54	23.20	716		12	101.34	22.60						
606		18	105.15	25.00	643		9	104.88	25.40	680		24	102.49	23.20	717		15	101.33	22.50						
607		21	105.04	24.90	644		12	104.88	25.30	681	24.09.05	3	102.44	23.20	718		18	101.33	22.50						
608		24	104.70	25.10	645		15	104.88	25.30	682		6	102.41	23.20	719		21	101.32	22.50						
609	15.09.05	3	104.38	25.10	646		18	104.86	25.40	683		9	102.35	23.20	720		24	101.31	22.40						

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721	29.09.05	3	101.30	22.40	758		18	101.14	21.90	795		9	101.17	21.70	832		24	100.98	21.30
722		6	101.29	2.30	759		21	101.14	21.90	796		12	101.17	21.60	833	13.10.05	3	101.01	21.30
723		9	101.29	22.30	760		24	101.14	21.90	797		15	101.17	21.60	834		6	101.04	21.30
724		12	101.28	22.30	761	04.10.05	3	101.14	21.90	798		18	101.17	21.60	835		9	101.07	21.30
725		15	101.27	22.10	762		6	101.14	21.90	799		21	101.16	21.60	836		12	101.10	21.30
726		18	101.26	22.10	763		9	101.14	21.80	800		24	101.16	21.60	837		15	101.10	21.30
727		21	101.25	22.10	764		12	101.14	21.80	801	09.10.05	3	101.15	21.60	838		18	101.10	21.30
728		24	101.24	22.10	765		15	101.14	21.80	802		6	101.14	21.60	839		21	101.12	21.30
729	30.09.05	3	101.23	22.10	766		18	101.14	21.80	803		9	101.14	21.60	840		24	101.15	21.30
730		6	101.23	22.10	767		21	101.14	21.80	804		12	101.14	21.60	841	14.10.05	3	101.18	21.30
731		9	101.22	22.10	768		24	101.14	21.80	805		15	101.14	21.60	842		6	101.21	21.30
732		12	101.22	22.10	769	05.10.05	3	101.14	21.80	806		18	101.14	21.60	843		9	101.22	21.30
733		15	101.21	22.10	770		6	101.16	21.80	807		21	101.11	21.60	844		12	101.24	21.20
734		18	101.21	22.10	771		9	101.19	21.80	808		24	101.08	21.50	845		15	101.24	21.20
735		21	101.20	22.10	772		12	101.22	21.80	809	10.10.05	3	101.05	21.50	846		18	101.21	21.20
736		24	101.19	22.10	773		15	101.25	21.80	810		6	101.02	21.50	847		21	101.18	21.20
737	01.10.05	3	101.18	22.00	774		18	101.25	21.80	811		9	101.01	21.50	848		24	101.15	21.20
738		6	101.17	22.00	775		21	101.25	21.80	812		12	101.01	21.50	849	15.10.05	3	101.15	21.20
739		9	101.17	22.10	776		24	101.25	21.80	813		15	101.00	21.50	850		6	101.15	21.20
740		12	101.16	22.10	777	06.10.05	3	101.25	21.80	814		18	101.00	21.50	851		9	101.12	21.20
741		15	101.15	22.10	778		6	101.25	21.80	815		21	100.99	21.50	852		12	101.12	21.30
742		18	101.15	22.10	779		9	101.25	21.80	816		24	100.98	21.50	853		15	101.10	21.50
743		21	101.14	22.10	780		12	101.22	21.70	817	11.10.05	3	100.97	21.50	854		18	101.10	21.50
744		24	101.13	22.10	781		15	101.19	21.70	818		6	100.96	21.50	855		21	101.10	21.50
745	02.10.05	3	101.13	22.10	782		18	101.18	21.70	819		9	100.95	21.40	856		24	101.10	21.40
746		6	101.12	22.10	783		21	101.18	21.70	820		12	100.95	21.40	857	16.10.05	3	101.12	21.40
747		9	101.11	22.10	784		24	101.18	21.70	821		15	100.94	21.30	858		6	101.12	21.30
748		12	101.10	22.00	785	07.10.05	3	101.18	21.70	822		18	100.94	21.30	859		9	101.12	21.30
749		15	101.10	22.00	786		6	101.18	21.70	823		21	100.94	21.30	860		12	101.12	21.30
750		18	101.10	22.00	787		9	101.18	21.70	824		24	100.94	21.30	861		15	101.07	21.30
751		21	101.12	22.00	788		12	101.18	21.70	825	12.10.05	3	100.93	21.30	862		18	101.04	21.20
752		24	101.13	22.00	789		15	101.18	21.70	826		6	100.93	21.30	863		21	101.04	21.20
753	03.10.05	3	101.14	22.00	790		18	101.18	21.70	827		9	100.93	21.30	864		24	101.07	21.20
754		6	101.14	22.00	791		21	101.17	21.70	828		12	100.92	21.30	865	17.10.05	3	101.07	21.20
755		9	101.14	22.00	792		24	101.17	21.70	829		15	100.92	21.30	866		6	101.10	21.20
756		12	101.14	22.00	793	08.10.05	3	101.17	21.70	830		18	100.92	21.30	867		9	101.10	21.20
757		15	101.14	21.90	794		6	101.17	21.70	831		21	100.95	21.30	868		12	101.12	21.20

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
869		15	101.12	21.20	906		6	102.49	23.80	943		21	101.76	22.90	980		12	101.24	21.90					
870		18	101.15	21.20	907		9	102.41	23.60	944		24	101.72	22.90	981		15	101.24	21.90					
871		21	101.15	21.20	908		12	102.41	23.50	945	27.10.05	3	101.56	22.90	982		18	101.24	21.90					
872		24	101.16	21.20	909		15	102.41	23.50	946		6	101.63	22.90	983		21	101.24	21.90					
873	18.10.05	3	101.21	21.00	910		18	102.49	23.40	947		9	101.47	22.90	984	01.07.06	3	100.76	21.00					
874		6	101.22	21.20	911		21	102.51	23.40	948		12	101.63	22.90	985		6	100.77	21.00					
875		9	101.35	21.10	912		24	102.49	23.40	949		15	101.46	22.90	986		9	100.78	21.00					
876		12	101.63	21.10	913	23.10.05	3	102.41	23.30	950		18	101.48	22.90	987		12	100.77	21.00					
877		15	101.74	21.00	914		6	102.35	23.30	951		21	101.48	22.80	988		15	100.76	21.00					
878		18	101.74	21.00	915		9	102.24	23.30	952		24	101.48	22.80	989		18	100.76	21.00					
879		21	101.72	21.00	916		12	102.24	23.30	953	28.10.05	3	101.35	22.70	990		21	100.76	21.00					
880		24	101.72	21.00	917		15	102.24	23.20	954		6	101.35	22.70	991		24	100.73	21.00					
881	19.10.05	3	101.74	21.10	918		18	102.23	23.20	955		9	101.35	22.70	992	02.07.06	3	100.70	21.00					
882		6	101.76	21.30	919		21	102.22	23.20	956		12	101.41	22.70	993		6	100.69	21.00					
883		9	102.19	21.60	920		24	102.15	23.20	957		15	101.41	22.60	994		9	100.69	21.00					
884		12	102.58	21.70	921	24.10.05	3	102.10	23.20	958		18	101.41	22.50	995		12	100.68	21.00					
885		15	102.77	22.00	922		6	101.94	23.50	959		21	101.35	22.50	996		15	100.67	21.00					
886		18	102.85	22.00	923		9	101.90	23.70	960		24	101.35	22.50	997		18	100.67	21.00					
887		21	102.99	22.00	924		12	101.88	23.60	961	29.10.05	3	101.34	22.40	998		21	100.70	21.00					
888		24	102.99	22.00	925		15	101.85	23.40	962		6	101.34	22.30	999		24	100.93	21.00					
889	20.10.05	3	102.99	22.00	926		18	101.85	23.40	963		9	101.34	22.30	1000	03.07.06	3	101.33	21.00					
890		6	102.99	22.10	927		21	101.85	23.30	964		12	101.29	22.20	1001		6	102.03	21.00					
891		9	102.99	22.10	928		24	101.85	23.30	965		15	101.29	22.20	1002		9	102.17	21.00					
892		12	102.97	22.20	929	25.10.05	3	101.90	23.30	966		18	101.29	22.20	1003		12	102.40	21.00					
893		15	102.77	22.30	930		6	102.08	23.30	967		21	101.24	22.20	1004		15	102.52	21.00					
894		18	102.58	22.40	931		9	102.10	23.20	968		24	101.24	22.20	1005		18	102.81	21.00					
895		21	102.55	22.70	932		12	102.11	23.20	969	30.10.05	3	101.29	22.20	1006		21	103.22	21.00					
896		24	102.56	23.00	933		15	102.11	23.10	970		6	101.34	22.10	1007		24	103.64	21.00					
897	21.10.05	3	102.53	23.50	934		18	102.11	23.10	971		9	101.34	22.00	1008	04.07.06	3	104.49	21.20					
898		6	102.51	23.90	935		21	102.11	23.10	972		12	101.34	22.00	1009		6	105.73	21.50					
899		9	102.51	24.40	936		24	102.10	23.10	973		15	101.34	22.00	1010		9	105.90	21.80					
900		12	102.51	24.40	937	26.10.05	3	102.10	23.00	974		18	101.34	22.00	1011		12	106.00	22.20					
901		15	102.51	24.30	938		6	102.05	22.90	975		21	101.35	22.00	1012		15	106.08	22.20					
902		18	102.51	24.30	939		9	101.85	22.90	976		24	101.38	22.00	1013		18	106.14	22.20					
903		21	102.51	24.30	940		12	101.85	22.90	977	31.10.05	3	101.29	21.90	1014		21	106.17	23.00					
904		24	102.50	24.00	941		15	101.85	22.90	978		6	101.24	21.90	1015		24	106.17	24.10					
905	22.10.05	3	102.49	23.90	942		18	101.85	22.90	979		9	101.24	21.90	1016	05.07.06	3	106.17	25.30					

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
1017		6	105.96	25.80	1054		21	101.46	22.70	1091		12	101.04	21.50	1128	19.07.06	3	101.75	22.30
1018		9	105.69	25.80	1055		24	101.43	22.60	1092		15	101.02	21.50	1129		6	101.74	22.30
1019		12	105.11	25.80	1056	10.07.06	3	101.40	22.60	1093		18	101.02	21.50	1130		9	101.74	22.40
1020		15	104.94	26.00	1057		6	101.37	22.50	1094		21	101.02	21.50	1131		12	101.72	22.40
1021		18	104.81	26.00	1058		9	101.35	22.40	1095		24	101.01	21.50	1132		15	101.70	22.40
1022		21	104.42	26.20	1059		12	101.33	22.40	1096	15.07.06	3	101.00	21.50	1133		18	101.67	22.40
1023		24	103.81	26.20	1060		15	101.32	22.40	1097		6	100.98	21.50	1134		21	101.67	22.40
1024	06.07.06	3	103.40	26.20	1061		18	101.30	22.40	1098		9	100.98	21.50	1135		24	101.64	22.40
1025		6	103.02	26.20	1062		21	101.29	22.40	1099		12	100.98	21.40	1136	20.07.06	3	101.61	22.40
1026		9	102.84	26.20	1063		24	101.27	22.40	1100		15	101.03	21.40	1137		6	101.60	22.40
1027		12	102.72	26.10	1064	11.07.06	3	101.24	22.40	1101		18	101.03	21.40	1138		9	101.57	22.40
1028		15	102.62	25.80	1065		6	101.23	22.40	1102		21	101.06	21.40	1139		12	101.54	22.40
1029		18	102.48	25.40	1066		9	101.23	22.40	1103		24	101.12	21.40	1140		15	101.53	22.40
1030		21	102.38	25.10	1067		12	101.22	22.40	1104	16.07.06	3	101.20	21.40	1141		18	101.52	22.40
1031		24	102.33	24.90	1068		15	101.22	22.30	1105		6	101.32	21.40	1142		21	101.52	22.40
1032	07.07.06	3	102.30	24.80	1069		18	101.21	22.30	1106		9	101.38	21.40	1143		24	101.55	22.40
1033		6	102.24	24.80	1070		21	101.20	22.30	1107		12	101.38	21.40	1144	21.07.06	3	101.58	22.40
1034		9	102.14	24.80	1071		24	101.18	22.30	1108		15	101.40	21.40	1145		6	101.61	22.40
1035		12	102.05	24.80	1072	12.07.06	3	101.17	22.30	1109		18	101.41	21.40	1146		9	101.69	22.40
1036		15	102.02	24.90	1073		6	101.17	22.30	1110		21	101.46	21.40	1147		12	101.75	22.40
1037		18	101.99	24.80	1074		9	101.16	22.30	1111		24	101.50	21.40	1148		15	101.81	22.40
1038		21	101.96	24.60	1075		12	101.16	22.10	1112	17.07.06	3	101.64	21.40	1149		18	101.93	22.40
1039		24	101.92	24.40	1076		15	101.20	22.10	1113		6	101.71	21.40	1150		21	102.07	22.40
1040	08.07.06	3	101.86	24.30	1077		18	101.20	22.10	1114		9	101.71	21.40	1151		24	102.41	22.40
1041		6	101.83	24.00	1078		21	101.20	22.00	1115		12	101.71	21.40	1152	22.07.06	3	102.74	22.40
1042		9	101.82	23.90	1079		24	101.19	22.00	1116		15	101.69	21.40	1153		6	102.82	22.40
1043		12	101.80	23.70	1080	13.07.06	3	101.18	21.90	1117		18	101.67	21.40	1154		9	102.81	22.70
1044		15	101.79	23.60	1081		6	101.17	21.90	1118		21	101.60	21.40	1155		12	102.79	23.00
1045		18	101.78	23.50	1082		9	101.16	21.90	1119		24	101.67	21.40	1156		15	102.79	23.00
1046		21	101.76	23.40	1083		12	101.15	21.90	1120	18.07.06	3	101.70	21.40	1157		18	102.79	23.00
1047		24	101.68	23.30	1084		15	101.15	21.90	1121		6	101.75	21.40	1158		21	102.77	23.00
1048	09.07.06	3	101.59	23.30	1085		18	101.15	21.90	1122		9	101.77	21.40	1159		24	102.66	23.20
1049		6	101.54	23.20	1086		21	101.14	21.90	1123		12	101.77	21.90	1160	23.07.06	3	102.56	23.40
1050		9	101.53	23.10	1087		24	101.14	21.90	1124		15	101.77	21.90	1161		6	102.45	23.60
1051		12	101.51	23.00	1088	14.07.06	3	101.13	21.90	1125		18	101.75	22.00	1162		9	102.36	23.75
1052		15	101.50	22.90	1089		6	101.10	21.90	1126		21	101.75	22.10	1163		12	102.34	23.90
1053		18	101.48	22.80	1090		9	101.07	21.60	1127		24	101.75	22.20	1164		15	102.33	24.20

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
1165		18	102.30	24.20	1202		9	102.79	22.70	1239		24	104.17	25.30	1276		15	103.30	24.90
1166		21	102.21	24.20	1203		12	102.84	22.80	1240	02.08.06	3	104.24	25.30	1277		18	103.28	24.80
1167		24	102.12	24.40	1204		15	102.87	22.90	1241		6	104.24	25.00	1278		21	103.24	24.70
1168	24.07.06	3	102.06	24.50	1205		18	102.87	22.90	1242		9	104.24	25.00	1279		24	103.20	24.60
1169		6	102.05	24.40	1206		21	102.81	23.00	1243		12	104.33	25.00	1280	07.08.06	3	103.14	24.60
1170		9	101.97	24.40	1207		24	102.75	23.00	1244		15	104.42	24.50	1281		6	103.06	24.60
1171		12	101.97	24.40	1208	29.07.06	3	102.72	23.20	1245		18	104.51	24.50	1282		9	102.99	24.80
1172		15	101.96	24.20	1209		6	102.69	23.30	1246		21	104.46	24.50	1283		12	102.94	25.00
1173		18	101.90	24.20	1210		9	102.63	23.40	1247		24	104.37	24.40	1284		15	102.92	25.00
1174		21	101.88	23.60	1211		12	102.57	23.60	1248	03.08.06	3	104.28	24.40	1285		18	102.90	25.00
1175		24	101.86	23.60	1212		15	102.54	23.70	1249		6	104.25	24.40	1286		21	102.89	24.80
1176	25.07.06	3	101.85	23.60	1213		18	102.52	23.90	1250		9	104.28	24.50	1287		24	102.87	24.80
1177		6	101.84	23.60	1214		21	102.52	24.00	1251		12	104.34	24.60	1288	08.08.06	3	102.84	24.80
1178		9	101.83	23.60	1215		24	102.48	24.00	1252		15	104.34	25.00	1289		6	102.79	24.80
1179		12	101.82	23.30	1216	30.07.06	3	102.45	24.20	1253		18	104.34	25.00	1290		9	102.79	25.00
1180		15	101.81	23.30	1217		6	102.42	24.20	1254		21	104.33	25.00	1291		12	102.78	25.00
1181		18	101.80	23.30	1218		9	102.42	24.20	1255		24	104.30	25.10	1292		15	102.78	25.00
1182		21	101.77	23.10	1219		12	102.42	24.20	1256	04.08.06	3	104.27	25.10	1293		18	102.75	25.00
1183		24	101.71	23.10	1220		15	102.42	24.20	1257		6	104.18	25.10	1294		21	102.62	25.00
1184	26.07.06	3	101.65	22.90	1221		18	102.42	24.20	1258		9	104.16	24.90	1295		24	102.50	25.00
1185		6	101.61	22.90	1222		21	102.42	24.40	1259		12	104.14	24.90	1296	09.08.06	3	102.40	24.70
1186		9	101.59	22.90	1223		24	102.47	23.80	1260		15	104.05	24.90	1297		6	102.33	24.70
1187		12	101.60	22.80	1224	31.07.06	3	102.56	23.80	1261		18	103.96	24.80	1298		9	102.28	24.70
1188		15	101.63	22.80	1225		6	103.76	23.80	1262		21	103.87	24.80	1299		12	102.27	24.60
1189		18	101.65	22.80	1226		9	103.91	23.80	1263		24	103.78	24.70	1300		15	102.26	24.50
1190		21	101.70	22.70	1227		12	104.02	23.80	1264	05.08.06	3	103.69	24.70	1301		18	102.25	24.50
1191		24	101.84	22.70	1228		15	104.13	23.50	1265		6	103.58	24.70	1302		21	102.25	24.50
1192	27.07.06	3	101.94	22.70	1229		18	104.20	23.50	1266		9	103.52	24.90	1303		24	102.24	24.50
1193		6	102.00	22.70	1230		21	104.24	23.50	1267		12	103.51	25.00	1304	10.08.06	3	102.24	24.30
1194		9	102.06	22.70	1231		24	104.21	23.40	1268		15	103.46	25.30	1305		6	102.24	24.30
1195		12	102.21	22.70	1232	01.08.06	3	104.18	23.40	1269		18	103.44	25.40	1306		9	102.24	24.20
1196		15	102.33	22.70	1233		6	104.15	23.60	1270		21	103.40	25.40	1307		12	102.24	24.10
1197		18	102.44	22.70	1234		9	104.12	23.80	1271		24	103.44	25.10	1308		15	102.24	24.00
1198		21	102.52	22.70	1235		12	104.12	23.80	1272	06.08.06	3	103.53	25.10	1309		18	102.23	23.80
1199		24	102.58	22.70	1236		15	104.11	24.90	1273		6	103.50	25.00	1310		21	102.23	23.80
1200	28.07.06	3	102.64	22.70	1237		18	104.10	24.90	1274		9	103.44	25.00	1311		24	102.22	23.70
1201		6	102.72	22.70	1238		21	104.11	25.30	1275		12	103.39	24.90	1312	11.08.06	3	102.22	23.60

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
1313		6	102.22	23.60	1350		21	104.56	25.40	1387		12	104.71	25.50	1424	25.08.06	3	104.42	26.00					
1314		9	102.22	23.50	1351		24	104.54	25.50	1388		15	104.65	25.40	1425		6	104.30	26.00					
1315		12	102.21	23.50	1352	16.08.06	3	104.54	25.60	1389		18	104.02	25.40	1426		9	104.18	26.00					
1316		15	102.21	23.50	1353		6	104.54	25.70	1390		21	104.05	25.40	1427		12	104.09	26.00					
1317		18	102.21	23.50	1354		9	104.46	25.50	1391		24	104.08	25.30	1428		15	104.05	26.00					
1318		21	102.23	23.50	1355		12	104.37	25.40	1392	21.08.06	3	104.11	25.30	1429		18	104.02	25.80					
1319		24	102.26	23.50	1356		15	104.28	25.40	1393		6	104.26	25.30	1430		21	103.99	25.60					
1320	12.08.06	3	102.29	23.50	1357		18	104.20	25.40	1394		9	104.46	25.30	1431		24	103.96	25.50					
1321		6	102.37	23.50	1358		21	104.17	25.40	1395		12	104.69	25.40	1432	26.08.06	3	103.96	25.40					
1322		9	102.80	23.50	1359		24	104.17	25.40	1396		15	104.89	25.40	1433		6	104.12	25.50					
1323		12	103.39	23.70	1360	17.08.06	3	104.16	25.50	1397		18	105.04	25.50	1434		9	104.19	25.50					
1324		15	103.60	23.80	1361		6	104.13	25.50	1398		21	105.01	25.60	1435		12	104.24	25.40					
1325		18	103.83	23.90	1362		9	104.10	25.50	1399		24	104.94	25.80	1436		15	104.27	25.30					
1326		21	104.43	23.90	1363		12	104.11	25.50	1400	22.08.06	3	104.85	25.90	1437		18	104.30	25.30					
1327		24	105.03	23.90	1364		15	104.28	25.30	1401		6	104.83	26.00	1438		21	104.41	25.30					
1328	13.08.06	3	105.30	24.00	1365		18	104.26	25.40	1402		9	104.83	26.00	1439		24	104.76	25.20					
1329		6	105.30	24.70	1366		21	104.40	25.40	1403		12	104.83	26.10	1440	27.08.06	3	105.01	25.20					
1330		9	105.21	25.40	1367		24	104.59	25.40	1404		15	104.86	26.10	1441		6	104.95	25.20					
1331		12	105.11	26.20	1368	18.08.06	3	104.66	25.30	1405		18	104.90	26.10	1442		9	104.80	25.40					
1332		15	104.95	26.00	1369		6	104.66	25.40	1406		21	104.96	26.00	1443		12	104.60	25.50					
1333		18	104.87	26.00	1370		9	104.69	25.50	1407		24	105.02	26.00	1444		15	104.46	25.60					
1334		21	104.75	26.00	1371		12	104.71	25.50	1408	23.08.06	3	105.08	26.00	1445		18	104.38	25.70					
1335		24	104.41	26.00	1372		15	104.65	25.50	1409		6	105.11	26.00	1446		21	104.36	25.70					
1336	14.08.06	3	104.17	26.10	1373		18	104.58	25.60	1410		9	105.12	26.00	1447		24	104.37	25.80					
1337		6	103.99	26.00	1374		21	104.49	25.60	1411		12	105.13	26.00	1448	28.08.06	3	104.40	25.90					
1338		9	103.97	26.00	1375		24	104.41	25.60	1412		15	105.13	26.00	1449		6	104.36	25.80					
1339		12	103.96	26.00	1376	19.08.06	3	104.32	25.65	1413		18	105.18	25.90	1450		9	104.30	25.80					
1340		15	103.94	26.00	1377		6	104.26	25.50	1414		21	105.46	25.90	1451		12	104.27	25.70					
1341		18	104.23	25.20	1378		9	104.21	25.50	1415		24	105.46	25.90	1452		15	104.06	25.60					
1342		21	104.50	25.00	1379		12	104.18	25.50	1416	24.08.06	3	105.64	26.00	1453		18	103.75	25.50					
1343		24	104.60	24.70	1380		15	104.16	25.50	1417		6	105.60	26.10	1454		21	103.47	25.30					
1344	15.08.06	3	104.66	24.60	1381		18	104.14	25.60	1418		9	105.54	26.10	1455		24	103.26	25.30					
1345		6	104.68	25.20	1382		21	104.11	25.50	1419		12	105.46	26.20	1456	29.08.06	3	103.15	25.20					
1346		9	104.68	25.40	1383		24	104.59	25.50	1420		15	105.32	26.00	1457		6	103.12	25.30					
1347		12	104.66	25.40	1384	20.08.06	3	104.66	25.40	1421		18	104.94	26.00	1458		9	103.11	25.30					
1348		15	104.63	25.40	1385		6	104.66	25.60	1422		21	104.70	26.00	1459		12	103.55	25.30					
1349		18	104.59	25.30	1386		9	104.69	25.60	1423		24	104.52	26.00	1460		15	104.00	25.30					

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
1461		18	104.55	25.30	1498		9	104.70	25.60	1535		24	103.70	24.45	1572		15	101.87	22.60					
1462		21	104.97	25.30	1499		12	104.58	25.60	1536	08.09.06	3	103.69	24.40	1573		18	101.87	22.60					
1463		24	105.27	25.50	1500		15	104.44	25.60	1537		6	103.67	24.40	1574		21	101.87	22.60					
1464	30.08.06	3	105.47	25.70	1501		18	104.38	25.60	1538		9	103.65	24.40	1575		24	101.87	22.60					
1465		6	105.86	25.90	1502		21	104.29	25.60	1539		12	103.63	24.30	1576	13.09.06	3	101.87	22.60					
1466		9	106.34	25.90	1503		24	104.26	25.60	1540		15	103.55	24.25	1577		6	101.87	22.50					
1467		12	106.76	26.00	1504	04.09.06	3	104.26	25.50	1541		18	103.41	24.20	1578		9	101.87	22.50					
1468		15	107.02	26.00	1505		6	104.26	25.40	1542		21	103.26	24.20	1579		12	101.87	22.40					
1469		18	107.18	26.00	1506		9	104.26	25.30	1543		24	103.17	24.20	1580		15	101.86	22.60					
1470		21	107.15	26.00	1507		12	104.22	25.20	1544	09.09.06	3	103.09	24.10	1581		18	101.86	22.80					
1471		24	107.02	26.10	1508		15	104.19	25.10	1545		6	103.03	24.00	1582		21	101.85	22.80					
1472	31.08.06	3	106.80	26.30	1509		18	104.13	25.05	1546		9	102.97	24.00	1583		24	101.84	22.80					
1473		6	106.46	26.40	1510		21	103.80	25.05	1547		12	102.91	24.00	1584	14.09.06	3	101.83	22.70					
1474		9	106.09	26.50	1511		24	103.62	25.00	1548		15	102.76	24.00	1585		6	101.86	22.70					
1475		12	105.88	26.60	1512	05.09.06	3	103.59	24.90	1549		18	102.61	23.90	1586		9	101.87	22.70					
1476		15	105.58	26.70	1513		6	103.63	24.90	1550		21	102.46	23.90	1587		12	101.87	22.65					
1477		18	105.32	26.80	1514		9	103.72	24.90	1551		24	102.34	23.80	1588		15	101.86	22.65					
1478		21	105.12	26.90	1515		12	103.75	24.85	1552	10.09.06	3	102.22	23.80	1589		18	101.86	22.60					
1479		24	104.80	26.90	1516		15	103.75	24.85	1553		6	102.22	23.80	1590		21	101.86	22.60					
1480	01.09.06	3	104.44	26.90	1517		18	103.71	24.75	1554		9	102.22	23.70	1591		24	101.86	22.60					
1481		6	104.17	26.80	1518		21	103.84	24.65	1555		12	102.22	23.65	1592	15.09.06	3	101.85	22.60					
1482		9	103.91	26.70	1519		24	104.09	24.60	1556		15	102.22	23.65	1593		6	101.84	22.60					
1483		12	103.75	26.60	1520	06.09.06	3	104.11	24.50	1557		18	102.22	23.55	1594		9	101.84	22.65					
1484		15	103.69	26.50	1521		6	104.11	24.45	1558		21	102.21	23.50	1595		12	101.83	22.65					
1485		18	104.49	26.30	1522		9	104.11	24.40	1559		24	102.20	23.40	1596		15	101.83	22.70					
1486		21	104.89	26.10	1523		12	104.11	24.35	1560	11.09.06	3	102.19	23.30	1597		18	101.83	22.70					
1487		24	105.09	25.90	1524		15	104.09	24.35	1561		6	102.19	23.20	1598		21	101.83	22.70					
1488	02.09.06	3	105.21	25.70	1525		18	104.07	24.35	1562		9	102.19	23.10	1599		24	101.80	22.70					
1489		6	105.21	25.50	1526		21	104.05	24.35	1563		12	102.19	23.10	1600	16.09.06	3	101.79	22.70					
1490		9	105.17	25.30	1527		24	103.97	24.40	1564		15	102.19	23.00	1601		6	101.78	22.70					
1491		12	105.12	25.10	1528	07.09.06	3	103.88	24.40	1565		18	102.18	23.00	1602		9	101.78	22.70					
1492		15	105.10	25.10	1529		6	103.87	24.45	1566		21	102.14	23.00	1603		12	101.82	22.70					
1493		18	105.08	25.10	1530		9	103.87	24.50	1567		24	102.09	23.00	1604		15	102.08	22.70					
1494		21	105.00	25.30	1531		12	103.85	24.50	1568	12.09.06	3	102.04	23.00	1605		18	102.00	22.65					
1495		24	104.99	25.40	1532		15	103.79	24.50	1569		6	101.99	22.90	1606		21	102.16	22.65					
1496	03.09.06	3	104.93	25.50	1533		18	103.73	24.45	1570		9	101.93	22.90	1607		24	102.13	22.65					
1497		6	104.78	25.50	1534		21	103.72	24.45	1571		12	101.87	22.65	1608	17.09.06	3	102.13	22.60					

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
1609		6	102.34	22.60	1646		21	102.00	22.60	1683		12	102.07	22.80	1720	01.10.06	3	102.80	22.90					
1610		9	102.43	22.60	1647		24	102.15	22.60	1684		15	102.11	22.80	1721		6	102.90	23.10					
1611		12	102.43	22.60	1648	22.09.06	3	102.25	22.70	1685		18	102.12	22.80	1722		9	103.08	23.30					
1612		15	102.43	22.60	1649		6	102.25	22.80	1686		21	102.08	22.80	1723		12	103.16	23.50					
1613		18	102.44	22.60	1650		9	102.24	22.90	1687		24	102.02	22.70	1724		15	103.19	23.60					
1614		21	102.47	22.70	1651		12	102.22	23.00	1688	27.09.06	3	101.96	22.70	1725		18	103.22	23.70					
1615		24	102.47	22.90	1652		15	102.21	23.20	1689		6	101.90	22.70	1726		21	103.14	23.80					
1616	18.09.06	3	102.47	23.00	1653		18	102.20	23.30	1690		9	101.81	22.70	1727		24	102.99	23.90					
1617		6	102.47	23.10	1654		21	102.19	23.30	1691		12	101.72	22.60	1728	02.10.06	3	102.62	23.90					
1618		9	102.47	23.30	1655		24	102.18	23.20	1692		15	101.65	22.60	1729		6	102.49	23.90					
1619		12	102.34	23.40	1656	23.09.06	3	102.17	23.20	1693		18	101.60	22.60	1730		9	102.40	23.90					
1620		15	102.32	23.50	1657		6	102.16	23.20	1694		21	101.57	22.60	1731		12	102.31	23.90					
1621		18	102.28	23.60	1658		9	102.18	23.20	1695		24	101.54	22.80	1732		15	102.24	23.90					
1622		21	102.16	23.60	1659		12	102.20	23.20	1696	28.09.06	3	101.53	22.80	1733		18	102.22	23.90					
1623		24	102.05	23.70	1660		15	102.20	23.40	1697		6	101.51	22.80	1734		21	102.20	23.90					
1624	19.09.06	3	101.98	23.70	1661		18	102.20	23.40	1698		9	101.48	22.80	1735		24	102.06	23.80					
1625		6	101.92	23.70	1662		21	102.20	23.30	1699		12	101.45	22.80	1736	03.10.06	3	102.00	23.70					
1626		9	101.86	23.70	1663		24	102.17	23.30	1700		15	101.44	22.80	1737		6	101.97	23.70					
1627		12	101.83	23.70	1664	24.09.06	3	102.14	23.20	1701		18	101.45	22.70	1738		9	101.96	23.70					
1628		15	101.81	23.70	1665		6	102.13	23.20	1702		21	101.48	22.70	1739		12	101.94	23.70					
1629		18	101.77	23.70	1666		9	102.12	23.20	1703		24	101.51	22.60	1740		15	101.92	23.60					
1630		21	101.79	23.60	1667		12	102.11	23.10	1704	29.09.06	3	101.54	22.50	1741		18	101.91	23.60					
1631		24	101.81	23.50	1668		15	102.10	23.10	1705		6	101.55	22.50	1742		21	101.90	23.50					
1632	20.09.06	3	101.81	23.40	1669		18	102.09	23.10	1706		9	101.57	22.50	1743		24	101.88	23.50					
1633		6	101.81	23.30	1670		21	102.06	23.10	1707		12	101.58	22.50	1744	04.10.06	3	101.87	23.30					
1634		9	101.78	23.20	1671		24	101.89	23.10	1708		15	101.59	22.50	1745		6	101.84	22.90					
1635		12	101.75	23.10	1672	25.09.06	3	101.83	23.10	1709		18	101.61	22.50	1746		9	101.82	22.80					
1636		15	101.74	23.00	1673		6	101.82	23.00	1710		21	101.64	22.50	1747		12	101.81	22.80					
1637		18	101.76	23.00	1674		9	101.80	23.00	1711		24	101.67	22.50	1748		15	101.80	22.80					
1638		21	101.86	22.90	1675		12	101.78	23.00	1712	30.09.06	3	101.70	22.50	1749		18	101.79	22.80					
1639		24	101.98	22.90	1676		15	101.76	23.00	1713		6	101.71	22.50	1750		21	101.78	22.60					
1640	21.09.06	3	102.04	22.70	1677		18	101.76	23.00	1714		9	102.02	22.50	1751		24	101.77	22.60					
1641		6	102.04	22.60	1678		21	101.76	22.90	1715		12	102.29	22.50	1752	05.10.06	3	101.77	22.60					
1642		9	101.99	22.60	1679		24	101.76	22.90	1716		15	102.62	22.60	1753		6	101.76	22.50					
1643		12	101.94	22.60	1680	26.09.06	3	101.76	22.80	1717		18	102.67	22.60	1754		9	101.73	22.50					
1644		15	101.94	22.60	1681		6	101.84	22.80	1718		21	102.70	22.60	1755		12	101.70	22.50					
1645		18	101.95	22.60	1682		9	101.95	22.80	1719		24	102.80	22.80	1756		15	101.67	22.50					

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
1757		18	101.64	22.50	1794		9	101.25	21.90	1831		24	100.94	21.40	1868		15	100.86	21.30
1758		21	101.61	22.50	1795		12	101.24	21.90	1832	15.10.06	3	100.94	21.30	1869		18	100.86	21.30
1759		24	101.58	22.50	1796		15	101.24	21.90	1833		6	100.94	21.30	1870		21	100.86	21.30
1760	06.10.06	3	101.55	22.50	1797		18	101.21	21.90	1834		9	100.94	21.30	1871		24	100.86	21.30
1761		6	101.52	22.50	1798		21	101.20	21.90	1835		12	100.94	21.30	1872	20.10.06	3	100.86	21.30
1762		9	101.49	22.70	1799		24	101.18	21.90	1836		15	100.94	21.30	1873		6	100.86	21.30
1763		12	101.47	22.70	1800	11.10.06	3	101.17	21.90	1837		18	100.94	21.30	1874		9	100.86	21.30
1764		15	101.46	22.70	1801		6	101.14	21.90	1838		21	100.94	21.30	1875		12	100.86	21.30
1765		18	101.45	22.70	1802		9	101.11	21.80	1839		24	100.94	21.30	1876		15	100.86	21.30
1766		21	101.44	22.70	1803		12	101.08	21.80	1840	16.10.06	3	100.90	21.30	1877		18	100.86	21.30
1767		24	101.43	22.60	1804		15	101.06	21.80	1841		6	100.90	21.30	1878		21	100.86	21.30
1768	07.10.06	3	101.42	22.60	1805		18	101.04	21.80	1842		9	100.90	21.30	1879		24	100.86	21.30
1769		6	101.39	22.60	1806		21	101.03	21.80	1843		12	100.90	21.30	1880	21.10.06	3	100.86	21.30
1770		9	101.36	22.60	1807		24	101.02	21.80	1844		15	100.90	21.30	1881		6	100.86	21.30
1771		12	101.35	22.60	1808	12.10.06	3	101.02	21.80	1845		18	100.90	21.30	1882		9	100.86	21.30
1772		15	101.32	22.60	1809		6	101.01	21.80	1846		21	100.90	21.30	1883		12	100.86	21.30
1773		18	101.30	22.50	1810		9	101.10	21.80	1847		24	100.90	21.30	1884		15	100.86	21.30
1774		21	101.30	22.50	1811		12	101.10	21.80	1848	17.10.06	3	100.90	21.30	1885		18	100.86	21.30
1775		24	101.29	22.40	1812		15	100.99	21.80	1849		6	100.90	21.30	1886		21	100.83	21.30
1776	08.10.06	3	101.29	22.40	1813		18	100.90	21.80	1850		9	100.90	21.30	1887		24	100.83	21.30
1777		6	101.29	22.30	1814		21	100.90	21.80	1851		12	100.90	21.30	1888	22.10.06	3	100.83	21.30
1778		9	101.28	22.20	1815		24	100.90	21.80	1852		15	100.90	21.30	1889		6	100.83	21.30
1779		12	101.27	22.20	1816	13.10.06	3	100.90	21.70	1853		18	100.90	21.30	1890		9	100.83	21.30
1780		15	101.28	22.20	1817		6	100.99	21.70	1854		21	100.90	21.30	1891		12	100.83	21.30
1781		18	101.25	22.10	1818		9	100.98	21.70	1855		24	100.90	21.30	1892		15	100.83	21.30
1782		21	101.25	22.10	1819		12	100.97	21.70	1856	18.10.06	3	100.90	21.30	1893		18	100.83	21.30
1783		24	101.21	22.10	1820		15	100.97	21.70	1857		6	100.86	21.30	1894		21	100.83	21.30
1784	09.10.06	3	101.23	22.10	1821		18	100.94	21.60	1858		9	100.86	21.30	1895		24	100.83	21.30
1785		6	101.22	22.10	1822		21	100.96	21.60	1859		12	100.86	21.30	1896	23.10.06	3	100.83	21.30
1786		9	101.21	22.10	1823		24	100.96	21.60	1860		15	100.86	21.30	1897		6	100.83	21.30
1787		12	101.20	22.00	1824	14.10.06	3	100.96	21.50	1861		18	100.86	21.30	1898		9	100.83	21.30
1788		15	101.19	22.00	1825		6	100.95	21.50	1862		21	100.86	21.30	1899		12	100.83	21.30
1789		18	101.18	22.00	1826		9	100.95	21.50	1863		24	100.86	21.30	1900		15	100.83	21.30
1790		21	101.19	22.00	1827		12	100.95	21.40	1864	19.10.06	3	100.86	21.30	1901		18	100.83	21.30
1791		24	101.21	22.00	1828		15	100.95	21.40	1865		6	100.86	21.30	1902		21	100.83	21.30
1792	10.10.06	3	101.24	22.00	1829		18	100.95	21.40	1866		9	100.86	21.30	1903		24	100.83	21.30
1793		6	101.25	21.90	1830		21	100.95	21.40	1867		12	100.86	21.30	1904	24.10.06	3	100.83	21.30

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
1905		6	100.80	21.30	1942		21	100.74	21.30	1979		18	102.15	24.10	2016		9	103.37	24.70
1906		9	100.80	21.30	1943		24	100.74	21.30	1980		21	102.09	24.00	2017		12	103.35	24.80
1907		12	100.80	21.30	1944	29.10.06	3	100.74	21.30	1981		24	102.06	23.70	2018		15	103.52	24.80
1908		15	100.80	21.30	1945		6	100.74	21.30	1982	03.07.07	3	102.00	23.50	2019		18	103.70	24.80
1909		18	100.80	21.30	1946		9	100.74	21.30	1983		6	101.92	23.40	2020		21	103.88	24.80
1910		21	100.80	21.30	1947		12	100.74	21.30	1984		9	101.83	23.30	2021		24	104.04	24.90
1911		24	100.80	21.30	1948		15	100.74	21.30	1985		12	101.74	23.20	2022	08.07.07	3	104.16	24.90
1912	25.10.06	3	100.80	21.30	1949		18	100.74	21.30	1986		15	101.76	23.00	2023		6	104.28	24.90
1913		6	100.80	21.30	1950		21	100.74	21.30	1987		18	101.73	23.00	2024		9	104.35	24.40
1914		9	100.80	21.30	1951		24	100.74	21.30	1988		21	101.67	22.90	2025		12	104.35	24.40
1915		12	100.80	21.30	1952	30.10.06	3	100.74	21.30	1989		24	101.61	22.90	2026		15	104.35	24.30
1916		15	100.80	21.30	1953		6	100.74	21.30	1990	04.07.07	3	101.55	22.90	2027		18	104.35	24.30
1917		18	100.80	21.30	1954		9	100.74	21.30	1991		6	101.52	22.70	2028		21	104.34	24.40
1918		21	100.77	21.30	1955		12	100.74	21.30	1992		9	101.51	22.70	2029		24	104.22	24.60
1919		24	100.77	21.30	1956		15	100.74	21.30	1993		12	101.45	22.70	2030	09.07.07	3	104.07	24.80
1920	26.10.06	3	100.77	21.30	1957		18	100.74	21.30	1994		15	101.39	22.60	2031		6	103.92	24.80
1921		6	100.77	21.30	1958		21	100.74	21.30	1995		18	101.35	22.60	2032		9	103.77	24.80
1922		9	100.77	21.30	1959		24	100.74	21.30	1996		21	101.32	22.50	2033		12	103.70	24.80
1923		12	100.77	21.30	1960	31.10.06	3	100.77	21.30	1997		24	101.30	22.50	2034		15	103.67	24.90
1924		15	100.77	21.30	1961		6	100.77	21.30	1998	05.07.07	3	101.52	22.40	2035		18	103.67	24.90
1925		18	100.77	21.30	1962		9	100.77	21.30	1999		6	103.02	22.40	2036		21	103.63	24.90
1926		21	100.77	21.30	1963		12	100.77	21.30	2000		9	103.58	22.40	2037		24	103.46	24.90
1927		24	100.77	21.30	1964		15	100.77	21.30	2001		12	103.69	22.40	2038	10.07.07	3	103.18	24.80
1928	27.10.06	3	100.77	21.30	1965		18	100.77	21.30	2002		15	103.75	22.30	2039		6	102.92	24.70
1929		6	100.77	21.30	1966	01.07.07	3	104.00	23.60	2003		18	103.75	22.30	2040		9	102.82	24.60
1930		9	100.77	21.30	1967		6	104.94	23.80	2004		21	103.81	22.30	2041		12	102.79	24.70
1931		12	100.74	21.30	1968		9	104.74	23.90	2005		24	104.00	22.30	2042		15	102.78	24.50
1932		15	100.74	21.30	1969		12	104.47	24.80	2006	06.07.07	3	104.13	22.20	2043		18	102.76	24.50
1933		18	100.74	21.30	1970		15	104.29	25.00	2007		6	104.22	22.20	2044		21	102.75	24.50
1934		21	100.74	21.30	1971		18	103.09	24.80	2008		9	104.24	22.20	2045		24	102.74	24.50
1935		24	100.74	21.30	1972		21	102.88	24.90	2009		12	104.24	22.10	2046	11.07.07	3	102.72	24.50
1936	28.10.06	3	100.74	21.30	1973		24	102.74	25.00	2010		15	104.24	22.60	2047		6	102.71	24.20
1937		6	100.74	21.30	1974	02.07.07	3	102.62	25.05	2011		18	104.16	23.20	2048		9	102.71	24.10
1938		9	100.74	21.30	1975		6	102.50	25.10	2012		21	104.05	23.70	2049		12	102.71	24.00
1939		12	100.74	21.30	1976		9	102.38	25.05	2013		24	103.82	24.00	2050		15	102.70	23.80
1940		15	100.74	21.30	1977		12	102.27	24.60	2014	07.07.07	3	103.61	24.00	2051		18	102.70	23.80
1941		18	100.74	21.30	1978		15	102.21	24.50	2015		6	103.49	24.40	2052		21	102.69	23.70

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	
2053		24	102.61	23.70	2090		15	103.30	22.90	2127		6	102.62	24.30	2164		21	101.68	22.50				21	101.68	22.50
2054	12.07.07	3	102.33	23.60	2091		18	103.38	23.10	2128		9	102.47	24.30	2165		24	101.68	22.50				24	101.68	22.50
2055		6	102.16	23.60	2092		21	104.44	23.30	2129		12	102.32	24.30	2166	26.07.07	3	101.70	22.50				3	101.70	22.50
2056		9	102.00	23.60	2093		24	104.48	23.50	2130		15	102.18	24.30	2167		6	101.73	22.40				6	101.73	22.40
2057		12	101.89	23.55	2094	17.07.07	3	104.38	23.60	2131		18	102.11	24.20	2168		9	101.76	22.40				9	101.76	22.40
2058		15	101.82	23.60	2095		6	104.23	23.70	2132		21	102.08	24.20	2169		12	101.76	22.40				12	101.76	22.40
2059		18	101.76	23.60	2096		9	104.08	23.90	2133		24	102.08	24.20	2170		15	101.76	22.40				15	101.76	22.40
2060		21	101.73	23.60	2097		12	103.90	24.20	2134	22.07.07	3	102.08	24.20	2171		18	101.76	22.40				18	101.76	22.40
2061		24	101.73	23.60	2098		15	103.83	24.60	2135		6	102.08	24.00	2172		21	101.76	22.40				21	101.76	22.40
2062	13.07.07	3	101.73	23.60	2099		18	103.79	24.80	2136		9	102.11	23.80	2173		24	101.77	22.40				24	101.77	22.40
2063		6	101.72	23.60	2100		21	103.76	24.90	2137		12	102.13	23.60	2174	27.07.07	3	101.76	22.40				3	101.76	22.40
2064		9	101.72	23.50	2101		24	103.71	25.20	2138		15	102.13	23.50	2175		6	101.76	22.30				6	101.76	22.30
2065		12	101.76	23.40	2102	18.07.07	3	103.65	24.90	2139		18	102.13	23.40	2176		9	101.76	22.30				9	101.76	22.30
2066		15	101.82	23.30	2103		6	103.59	25.00	2140		21	102.12	23.40	2177		12	101.77	22.30				12	101.77	22.30
2067		18	101.85	23.30	2104		9	103.53	24.80	2141		24	102.09	23.30	2178		15	101.78	22.20				15	101.78	22.20
2068		21	101.88	23.10	2105		12	103.50	24.70	2142	23.07.07	3	102.09	23.20	2179		18	101.84	22.20				18	101.84	22.20
2069		24	101.90	23.00	2106		15	103.50	24.60	2143		6	102.09	23.00	2180		21	101.88	22.20				21	101.88	22.20
2070	14.07.07	3	101.93	22.90	2107		18	103.50	24.50	2144		9	102.07	23.00	2181		24	101.91	22.20				24	101.91	22.20
2071		6	101.93	22.70	2108		21	103.50	24.40	2145		12	102.03	23.00	2182	28.07.07	3	101.76	22.20				3	101.76	22.20
2072		9	101.93	22.60	2109		24	103.50	24.30	2146		15	101.97	22.90	2183		6	101.76	22.30				6	101.76	22.30
2073		12	101.91	22.60	2110	19.07.07	3	103.49	24.30	2147		18	101.93	22.90	2184		9	101.76	22.30				9	101.76	22.30
2074		15	101.91	22.50	2111		6	103.49	24.20	2148		21	101.89	22.90	2185		12	101.77	22.30				12	101.77	22.30
2075		18	101.90	22.50	2112		9	103.49	24.20	2149		24	101.89	22.90	2186		15	101.78	22.30				15	101.78	22.30
2076		21	101.94	22.30	2113		12	103.49	24.30	2150	24.07.07	3	101.89	22.90	2187		18	101.84	22.30				18	101.84	22.30
2077		24	102.18	22.30	2114		15	103.49	24.30	2151		6	101.89	22.80	2188		21	101.88	22.30				21	101.88	22.30
2078	15.07.07	3	102.54	22.40	2115		18	103.49	24.30	2152		9	101.88	22.80	2189		24	101.91	22.30				24	101.91	22.30
2079		6	102.77	22.40	2116		21	103.48	24.30	2153		12	101.86	22.80	2190	29.07.07	3	101.97	22.30				3	101.97	22.30
2080		9	102.85	22.50	2117		24	103.45	24.30	2154		15	101.86	22.70	2191		6	101.95	22.30				6	101.95	22.30
2081		12	102.86	22.50	2118	20.07.07	3	103.45	24.30	2155		18	101.76	22.70	2192		9	101.94	22.30				9	101.94	22.30
2082		15	102.86	22.50	2119		6	103.45	24.30	2156		21	101.70	22.60	2193		12	101.92	22.30				12	101.92	22.30
2083		18	102.86	22.50	2120		9	103.44	24.30	2157		24	101.70	22.60	2194		15	101.95	22.30				15	101.95	22.30
2084		21	102.86	22.60	2121		12	103.43	24.30	2158	25.07.07	3	101.69	22.60	2195		18	101.98	22.30				18	101.98	22.30
2085		24	102.86	22.60	2122		15	103.43	24.30	2159		6	101.68	22.60	2196		21	102.00	22.30				21	102.00	22.30
2086	16.07.07	3	102.96	22.60	2123		18	103.42	24.30	2160		9	101.68	22.60	2197		24	101.99	22.30				24	101.99	22.30
2087		6	103.24	22.60	2124		21	103.38	24.30	2161		12	101.68	22.60	2198	30.07.07	3	101.97	22.30				3	101.97	22.30
2088		9	103.81	22.60	2125		24	103.11	24.30	2162		15	101.68	22.50	2199		6	101.96	22.30				6	101.96	22.30
2089		12	103.14	22.70	2126	21.07.07	3	102.81	24.30	2163		18	101.60	22.50	2200		9	101.94	22.30				9	101.94	22.30

Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
2201		12	101.94	22.30	2238	04.08.07	3	101.48	22.20	2275		18	104.72	25.30	2312		9	104.34	25.40
2202		15	101.94	22.30	2239		6	101.51	22.20	2276		21	104.46	25.30	2313		12	104.27	25.30
2203		18	101.95	22.40	2240		9	101.51	22.10	2277		24	104.12	25.70	2314		15	104.18	25.20
2204		21	101.99	22.40	2241		12	101.52	22.10	2278	09.08.07	3	103.79	25.80	2315		18	104.09	25.20
2205		24	101.95	22.40	2242		15	101.53	22.10	2279		6	103.49	25.90	2316		21	104.01	25.40
2206	31.07.07	3	101.95	22.40	2243		18	101.54	22.00	2280		9	103.30	25.90	2317		24	103.95	25.30
2207		6	101.95	22.40	2244		21	101.61	22.00	2281		12	103.12	25.70	2318	14.08.07	3	103.89	25.20
2208		9	101.95	22.40	2245		24	101.70	22.00	2282		15	102.98	25.50	2319		6	103.83	25.20
2209		12	101.97	22.40	2246	05.08.07	3	101.78	22.00	2283		18	102.92	25.40	2320		9	103.71	25.00
2210		15	101.97	22.40	2247		6	101.84	22.10	2284		21	102.72	25.20	2321		12	103.68	24.90
2211		18	101.98	22.40	2248		9	101.85	22.10	2285		24	102.60	24.80	2322		15	103.59	24.70
2212		21	101.98	22.40	2249		12	101.85	22.10	2286	10.08.07	3	102.60	24.60	2323		18	103.53	24.60
2213		24	101.92	22.40	2250		15	101.85	22.20	2287		6	102.90	24.40	2324		21	103.53	24.50
2214	01.08.07	3	101.86	22.40	2251		18	101.88	22.20	2288		9	103.32	24.20	2325		24	103.62	24.40
2215		6	101.81	22.40	2252		21	101.89	22.20	2289		12	103.88	24.30	2326	15.08.07	3	103.72	24.30
2216		9	101.78	22.40	2253		24	101.93	22.20	2290		15	103.88	24.20	2327		6	103.78	24.20
2217		12	101.74	22.40	2254	06.08.07	3	101.97	22.20	2291		18	103.88	23.90	2328		9	103.80	24.20
2218		15	101.68	22.40	2255		6	102.00	22.20	2292		21	103.88	23.80	2329		12	103.74	24.40
2219		18	101.64	22.40	2256		9	102.03	22.20	2293		24	103.88	23.60	2330		15	103.64	24.40
2220		21	101.63	22.40	2257		12	102.14	22.20	2294	11.08.07	3	103.88	23.50	2331		18	103.60	24.30
2221		24	101.63	22.40	2258		15	102.46	22.20	2295		6	103.88	23.40	2332		21	103.55	24.20
2222	02.08.07	3	101.63	22.40	2259		18	103.03	22.30	2296		9	103.80	23.30	2333		24	103.52	24.30
2223		6	101.63	22.40	2260		21	103.23	22.40	2297		12	103.76	23.50	2334	16.08.07	3	103.49	24.30
2224		9	101.60	22.40	2261		24	103.35	22.50	2298		15	103.75	23.80	2335		6	103.46	24.30
2225		12	101.52	22.40	2262	07.08.07	3	103.45	22.60	2299		18	103.88	24.30	2336		9	103.43	24.30
2226		15	101.43	22.40	2263		6	103.54	22.70	2300		21	104.07	24.40	2337		12	103.28	24.40
2227		18	101.39	22.40	2264		9	103.80	22.80	2301		24	104.28	24.40	2338		15	103.18	24.50
2228		21	101.34	22.40	2265		12	103.04	22.90	2302	12.08.07	3	104.49	24.50	2339		18	102.96	24.50
2229		24	101.62	22.40	2266		15	103.23	23.20	2303		6	104.67	24.50	2340		21	102.89	24.50
2230	03.08.07	3	101.32	22.40	2267		18	104.40	23.40	2304		9	104.78	24.50	2341		24	102.49	24.40
2231		6	101.32	22.40	2268		21	104.55	23.60	2305		12	104.87	24.80	2342	17.08.07	3	102.46	24.30
2232		9	101.32	22.30	2269		24	104.70	23.70	2306		15	104.96	25.10	2343		6	102.46	24.20
2233		12	101.34	22.20	2270	08.08.07	3	104.85	24.00	2307		18	105.00	25.00	2344		9	102.44	24.20
2234		15	101.38	22.20	2271		6	104.97	24.50	2308		21	105.02	25.10	2345		12	102.42	24.20
2235		18	101.89	22.20	2272		9	105.02	24.80	2309		24	104.88	24.80	2346		15	102.41	24.10
2236		21	101.42	22.20	2273		12	105.02	25.10	2310	13.08.07	3	104.67	25.30	2347		18	102.40	24.00
2237		24	101.45	22.20	2274		15	104.90	25.30	2311		6	104.49	25.20	2348		21	102.39	23.90

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
2349		24	102.38	23.70	2386		15	103.40	23.70	2423		6	102.77	22.90	2460		21	102.37	23.80
2350	18.08.07	3	102.37	23.50	2387		18	103.23	24.00	2424		9	102.77	22.90	2461		24	102.49	23.80
2351		6	102.36	23.40	2388		21	103.23	23.90	2425		12	102.74	23.00	2462	01.09.07	3	102.46	23.70
2352		9	102.35	23.30	2389		24	103.23	24.10	2426		15	102.66	23.00	2463		6	102.40	23.60
2353		12	102.35	23.30	2390	23.08.07	3	103.23	24.30	2427		18	102.57	23.00	2464		9	102.34	23.60
2354		15	102.35	23.30	2391		6	103.23	24.60	2428		21	102.54	23.00	2465		12	102.28	23.50
2355		18	102.34	23.30	2392		9	103.23	24.60	2429		24	102.51	23.10	2466		15	102.20	23.40
2356		21	102.33	23.10	2393		12	103.22	24.60	2430	28.08.07	3	102.48	23.20	2467		18	102.16	23.30
2357		24	102.33	23.10	2394		15	103.21	24.40	2431		6	102.47	23.30	2468		21	102.11	23.20
2358	19.08.07	3	102.30	23.10	2395		18	103.20	24.30	2432		9	102.49	23.30	2469		24	102.11	23.10
2359		6	102.27	23.00	2396		21	103.20	24.20	2433		12	102.54	23.30	2470	02.09.07	3	102.10	23.00
2360		9	102.26	23.00	2397		24	103.29	24.00	2434		15	102.60	23.30	2471		6	102.09	22.90
2361		12	102.25	23.00	2398	24.08.07	3	103.16	23.90	2435		18	102.62	23.30	2472		9	102.11	22.80
2362		15	102.24	23.00	2399		6	103.13	23.80	2436		21	102.62	23.30	2473		12	102.20	22.80
2363		18	102.23	23.00	2400		9	103.07	23.80	2437		24	102.65	23.30	2474		15	102.35	23.00
2364		21	102.23	23.00	2401		12	103.01	23.80	2438	29.08.07	3	102.73	23.30	2475		18	102.44	23.00
2365		24	102.23	23.00	2402		15	102.98	23.80	2439		6	102.84	23.30	2476		21	102.52	22.90
2366	20.08.07	3	102.23	23.00	2403		18	102.97	23.70	2440		9	102.90	23.10	2477		24	102.48	22.80
2367		6	102.23	22.90	2404		21	102.95	23.70	2441		12	102.94	23.10	2478	03.09.07	3	102.45	22.80
2368		9	102.25	22.90	2405		24	102.83	23.70	2442		15	102.97	23.10	2479		6	102.42	22.70
2369		12	102.26	22.90	2406	25.08.07	3	102.66	23.70	2443		18	103.00	23.00	2480		9	102.41	22.70
2370		15	102.31	22.80	2407		6	102.51	23.70	2444		21	103.04	23.00	2481		12	102.42	22.60
2371		18	102.37	22.90	2408		9	102.44	23.70	2445		24	103.10	23.00	2482		15	102.43	22.60
2372		21	102.45	22.90	2409		12	102.43	23.70	2446	30.08.07	3	103.16	23.00	2483		18	102.44	22.60
2373		24	102.66	22.90	2410		15	102.43	23.70	2447		6	103.19	23.10	2484		21	102.44	22.50
2374	21.08.07	3	102.85	22.90	2411		18	102.53	23.70	2448		9	103.19	23.10	2485		24	102.44	22.60
2375		6	102.96	22.80	2412		21	102.64	23.60	2449		12	103.16	23.20	2486	04.09.07	3	102.44	22.80
2376		9	103.05	22.80	2413		24	102.68	23.60	2450		15	103.11	23.30	2487		6	102.44	22.90
2377		12	103.20	22.80	2414	26.08.07	3	102.68	23.50	2451		18	103.05	23.40	2488		9	102.44	23.00
2378		15	103.35	22.80	2415		6	102.68	23.50	2452		21	103.02	23.50	2489		12	102.46	23.10
2379		18	103.35	22.80	2416		9	102.74	23.40	2453		24	102.98	23.50	2490		15	102.47	23.10
2380		21	103.43	22.90	2417		12	102.79	23.30	2454	31.08.07	3	102.90	23.60	2491		18	102.50	23.00
2381		24	103.73	22.90	2418		15	102.82	23.30	2455		6	102.77	23.70	2492		21	102.53	23.10
2382	22.08.07	3	103.84	23.00	2419		18	102.80	23.10	2456		9	102.60	23.70	2493		24	102.56	23.10
2383		6	103.90	23.10	2420		21	102.77	23.00	2457		12	102.42	23.80	2494	05.09.07	3	102.61	23.10
2384		9	103.85	23.20	2421		24	102.77	23.00	2458		15	102.28	23.80	2495		6	102.67	23.20
2385		12	103.67	23.50	2422	27.08.07	3	102.77	23.00	2459		18	102.28	23.80	2496		9	102.75	23.20

S/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
2497		12	102.83	23.20	2534	10.09.07	3	103.49	24.50	2571		18	102.44	23.60	2608		9	102.04	23.00					
2498		15	102.84	23.20	2535		6	103.43	24.50	2572		21	102.45	23.60	2609		12	102.04	22.90					
2499		18	102.84	23.10	2536		9	103.36	24.60	2573		24	102.54	23.50	2610		15	102.04	22.90					
2500		21	102.86	23.20	2537		12	103.36	24.60	2574	15.09.07	3	102.62	23.40	2611		18	102.03	22.90					
2501		24	102.92	23.20	2538		15	103.36	24.60	2575		6	102.84	23.20	2612		21	102.01	22.80					
2502	06.09.07	3	102.98	23.30	2539		18	103.36	24.50	2576		9	102.90	23.20	2613		24	102.00	22.80					
2503		6	103.04	23.30	2540		21	103.36	24.50	2577		12	102.96	23.10	2614	20.09.07	3	101.97	22.80					
2504		9	103.28	23.40	2541		24	103.36	24.50	2578		15	103.00	23.20	2615		6	101.94	22.70					
2505		12	103.66	23.40	2542	11.09.07	3	103.36	24.40	2579		18	103.02	23.30	2616		9	101.94	22.70					
2506		15	103.82	23.50	2543		6	103.36	24.40	2580		21	103.02	23.30	2617		12	101.94	22.70					
2507		18	103.91	23.50	2544		9	103.36	24.30	2581		24	103.01	23.30	2618		15	101.92	22.70					
2508		21	103.98	23.60	2545		12	103.36	24.20	2582	16.09.07	3	102.98	23.30	2619		18	101.92	22.70					
2509		24	104.09	23.60	2546		15	103.36	24.30	2583		6	102.95	23.30	2620		21	101.90	22.70					
2510	07.09.07	3	104.09	23.70	2547		18	103.33	24.30	2584		9	102.90	23.40	2621		24	101.89	22.60					
2511		6	104.09	23.80	2548		21	103.30	24.30	2585		12	102.82	23.50	2622	21.09.07	3	101.87	22.60					
2512		9	104.06	23.60	2549		24	103.29	24.30	2586		15	102.73	23.60	2623		6	101.86	22.60					
2513		12	104.03	23.70	2550	12.09.07	3	103.39	24.30	2587		18	102.64	23.70	2624		9	101.85	22.60					
2514		15	104.00	24.00	2551		6	103.54	24.20	2588		21	102.58	23.80	2625		12	101.83	22.50					
2515		18	103.97	24.20	2552		9	103.64	24.20	2589		24	102.57	23.80	2626		15	101.82	22.50					
2516		21	103.96	24.40	2553		12	103.64	24.20	2590	17.09.07	3	102.56	23.90	2627		18	101.81	22.50					
2517		24	103.95	24.60	2554		15	103.64	24.20	2591		6	102.54	23.90	2628		21	101.81	22.50					
2518	08.09.07	3	103.94	24.80	2555		18	103.61	24.20	2592		9	102.53	23.90	2629		24	101.82	22.50					
2519		6	103.93	24.90	2556		21	103.46	24.20	2593		12	102.47	23.90	2630	22.09.07	3	101.85	22.50					
2520		9	103.93	24.90	2557		24	103.25	24.20	2594		15	102.41	23.80	2631		6	101.88	22.60					
2521		12	103.93	24.60	2558	13.09.07	3	103.05	24.20	2595		18	102.35	23.80	2632		9	101.91	22.60					
2522		15	103.93	24.50	2559		6	102.88	24.10	2596		21	102.33	23.70	2633		12	101.91	22.60					
2523		18	103.93	24.50	2560		9	102.76	24.10	2597		24	102.32	23.70	2634		15	101.92	22.70					
2524		21	103.90	24.50	2561		12	102.64	24.20	2598	18.09.07	3	102.30	23.60	2635		18	101.98	22.70					
2525		24	103.84	24.50	2562		15	102.53	24.30	2599		6	102.29	23.50	2636		21	102.01	22.80					
2526	09.09.07	3	103.78	24.50	2563		18	102.46	24.40	2600		9	102.29	23.40	2637		24	102.07	22.80					
2527		6	103.72	24.40	2564		21	102.44	24.40	2601		12	102.27	23.40	2638	23.09.07	3	102.29	22.90					
2528		9	103.66	24.40	2565		24	102.43	24.40	2602		15	102.26	23.40	2639		6	102.43	23.00					
2529		12	103.64	24.50	2566	14.09.07	3	102.42	24.30	2603		18	102.25	23.40	2640		9	102.56	23.20					
2530		15	103.64	24.50	2567		6	102.42	24.20	2604		21	102.23	23.30	2641		12	102.83	23.40					
2531		18	103.62	24.50	2568		9	102.42	24.00	2605		24	102.20	23.20	2642		15	103.35	23.60					
2532		21	103.59	24.50	2569		12	102.44	23.80	2606	19.09.07	3	102.16	23.10	2643		18	103.95	23.80					
2533		24	103.55	24.50	2570		15	102.44	23.70	2607		6	102.10	23.00	2644		21	104.36	24.00					

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
2645		24	104.36	24.30	2682		15	103.73	24.80	2719		6	102.86	23.60	2756		21	102.48	23.00					
2646	24.09.07	3	104.36	24.60	2683		18	103.76	24.80	2720		9	102.85	23.80	2757		24	102.42	23.00					
2647		6	104.36	24.90	2684		21	103.78	24.80	2721		12	102.89	23.70	2758	08.10.07	3	102.36	22.90					
2648		9	104.30	25.20	2685		24	103.78	24.90	2722		15	102.89	23.70	2759		6	102.30	22.90					
2649		12	104.36	25.20	2686	29.09.07	3	103.73	24.80	2723		18	102.89	23.70	2760		9	102.27	22.90					
2650		15	104.45	25.30	2687		6	103.67	24.80	2724		21	103.01	23.70	2761		12	102.24	22.90					
2651		18	104.54	25.50	2688		9	103.61	24.60	2725		24	102.99	23.70	2762		15	102.21	22.90					
2652		21	104.60	25.70	2689		12	103.58	24.50	2726	04.10.07	3	102.93	23.80	2763		18	102.20	22.90					
2653		24	104.41	25.80	2690		15	103.55	24.40	2727		6	102.87	23.80	2764		21	102.18	22.90					
2654	25.09.07	3	104.41	25.70	2691		18	103.52	24.40	2728		9	102.81	23.80	2765		24	102.17	22.90					
2655		6	104.41	25.60	2692		21	103.50	24.40	2729		12	102.75	23.80	2766	09.10.07	3	102.15	23.00					
2656		9	104.41	25.50	2693		24	103.49	24.40	2730		15	102.72	23.70	2767		6	102.14	23.00					
2657		12	104.33	25.40	2694	30.09.07	3	103.48	24.30	2731		18	102.71	23.70	2768		9	102.12	23.00					
2658		15	104.24	25.30	2695		6	103.47	24.30	2732		21	102.72	23.70	2769		12	102.06	23.00					
2659		18	104.18	25.30	2696		9	103.46	24.30	2733		24	102.80	23.70	2770		15	102.01	23.00					
2660		21	104.06	25.20	2697		12	103.46	24.50	2734	05.10.07	3	102.89	23.80	2771		18	101.98	23.00					
2661		24	103.91	25.20	2698		15	103.46	24.50	2735		6	102.96	23.80	2772		21	101.96	22.90					
2662	26.09.07	3	103.79	25.10	2699		18	103.46	24.40	2736		9	103.00	23.90	2773		24	101.96	22.90					
2663		6	103.67	25.00	2700		21	103.34	24.40	2737		12	103.03	23.90	2774	10.10.07	3	102.00	22.80					
2664		9	103.63	25.00	2701		24	103.22	24.30	2738		15	102.93	23.80	2775		6	102.03	22.70					
2665		12	103.60	25.00	2702	01.10.07	3	103.10	24.30	2739		18	102.78	23.70	2776		9	102.03	22.60					
2666		15	103.57	25.00	2703		6	102.96	24.30	2740		21	102.67	23.60	2777		12	102.02	22.50					
2667		18	103.54	24.90	2704		9	102.89	24.20	2741		24	102.58	23.50	2778		15	102.02	22.60					
2668		21	103.52	24.80	2705		12	102.85	24.10	2742	06.10.07	3	102.49	23.50	2779		18	101.99	22.60					
2669		24	103.55	24.70	2706		15	102.82	24.10	2743		6	102.40	23.50	2780		21	101.96	22.60					
2670	27.09.07	3	103.64	24.60	2707		18	102.82	24.10	2744		9	102.34	23.50	2781		24	101.93	22.60					
2671		6	103.73	24.40	2708		21	102.81	24.10	2745		12	102.28	23.50	2782	11.10.07	3	101.90	22.50					
2672		9	103.79	24.30	2709		24	102.80	24.10	2746		15	102.22	23.60	2783		6	101.87	22.40					
2673		12	103.79	24.20	2710	02.10.07	3	102.79	24.10	2747		18	102.22	23.70	2784		9	101.84	22.40					
2674		15	103.79	24.20	2711		6	102.78	24.00	2748		21	102.24	23.70	2785		12	101.79	22.30					
2675		18	103.79	24.10	2712		9	102.80	23.90	2749		24	102.31	23.70	2786		15	101.75	22.30					
2676		21	103.79	24.10	2713		12	102.81	23.80	2750	07.10.07	3	102.38	23.60	2787		18	101.70	22.30					
2677		24	103.79	24.00	2714		15	102.82	23.80	2751		6	102.42	23.50	2788		21	101.70	22.30					
2678	28.09.07	3	103.78	24.10	2715		18	102.88	23.80	2752		9	102.50	23.40	2789		24	101.64	22.30					
2679		6	103.75	24.70	2716		21	102.91	23.80	2753		12	102.52	23.30	2790	12.10.07	3	101.61	22.30					
2680		9	103.73	24.80	2717		24	102.91	23.70	2754		15	102.53	23.20	2791		6	101.58	22.30					
2681		12	103.73	24.80	2718	03.10.07	3	102.89	23.70	2755		18	102.51	23.10	2792		9	101.57	22.30					

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	
2793		12	101.56	22.30	2830	17.10.07	3	101.13	21.60	2867		18	101.09	21.30	2904		9	100.99	21.20				9	100.99	21.20
2794		15	101.54	22.30	2831		6	101.13	21.60	2868		21	101.09	21.30	2905		12	100.99	21.20				12	100.99	21.20
2795		18	101.51	22.30	2832		9	101.13	21.50	2869		24	101.09	21.30	2906		15	100.99	21.20				15	100.99	21.20
2796		21	101.51	22.30	2833		12	101.13	21.50	2870	22.10.07	3	101.09	21.30	2907		18	100.99	21.20				18	100.99	21.20
2797		24	101.48	22.30	2834		15	101.13	21.50	2871		6	101.09	21.30	2908		21	100.99	21.20				21	100.99	21.20
2798	13.10.07	3	101.46	22.20	2835		18	101.13	21.50	2872		9	101.09	21.30	2909		24	100.99	21.10				24	100.99	21.10
2799		6	101.46	22.20	2836		21	101.13	21.50	2873		12	101.09	21.30	2910	27.10.07	3	100.99	21.10				3	100.99	21.10
2800		9	101.45	22.10	2837		24	101.13	21.50	2874		15	101.09	21.30	2911		6	100.99	21.10				6	100.99	21.10
2801		12	101.45	22.00	2838	18.10.07	3	101.12	21.50	2875		18	101.09	21.30	2912		9	100.99	21.10				9	100.99	21.10
2802		15	101.44	22.00	2839		6	101.10	21.50	2876		21	101.09	21.30	2913		12	100.99	21.10				12	100.99	21.10
2803		18	101.44	22.00	2840		9	101.09	21.50	2877		24	101.06	21.30	2914		15	100.99	21.10				15	100.99	21.10
2804		21	101.42	22.00	2841		12	101.09	21.50	2878	23.10.07	3	101.06	21.30	2915		18	100.95	21.10				18	100.95	21.10
2805		24	101.39	22.00	2842		15	101.09	21.50	2879		6	101.06	21.30	2916		21	100.95	21.10				21	100.95	21.10
2806	14.10.07	3	101.36	22.00	2843		18	101.09	21.50	2880		9	101.06	21.30	2917		24	100.95	21.10				24	100.95	21.10
2807		6	101.33	21.90	2844		21	101.09	21.50	2881		12	101.06	21.30	2918	28.10.07	3	100.95	21.10				3	100.95	21.10
2808		9	101.30	21.90	2845		24	101.09	21.40	2882		15	101.06	21.30	2919		6	100.95	21.10				6	100.95	21.10
2809		12	101.27	21.90	2846	19.10.07	3	101.09	21.40	2883		18	101.06	21.30	2920		9	100.95	21.10				9	100.95	21.10
2810		15	101.26	21.80	2847		6	101.09	21.40	2884		21	101.06	21.30	2921		12	100.95	21.10				12	100.95	21.10
2811		18	101.25	21.80	2848		9	101.09	21.40	2885		24	101.06	21.30	2922		15	100.95	21.10				15	100.95	21.10
2812		21	101.24	21.80	2849		12	101.09	21.40	2886	24.10.07	3	101.06	21.30	2923		18	100.95	21.10				18	100.95	21.10
2813		24	101.24	21.80	2850		15	101.13	21.40	2887		6	101.06	21.30	2924		21	100.95	21.10				21	100.95	21.10
2814	15.10.07	3	101.24	21.80	2851		18	101.16	21.40	2888		9	101.02	21.30	2925		24	100.95	21.10				24	100.95	21.10
2815		6	101.24	21.80	2852		21	101.16	21.40	2889		12	101.02	21.20	2926	29.10.07	3	100.95	21.10				3	100.95	21.10
2816		9	101.24	21.70	2853		24	101.16	21.40	2890		15	101.02	21.20	2927		6	100.95	21.10				6	100.95	21.10
2817		12	101.23	21.70	2854	20.10.07	3	101.16	21.40	2891		18	101.02	21.20	2928		9	100.95	21.10				9	100.95	21.10
2818		15	101.23	21.70	2855		6	101.16	21.30	2892		21	101.02	21.20	2929		12	100.95	21.10				12	100.95	21.10
2819		18	101.23	21.60	2856		9	101.16	21.30	2893		24	101.02	21.20	2930		15	100.95	21.10				15	100.95	21.10
2820		21	101.19	21.60	2857		12	101.16	21.30	2894	25.10.07	3	101.02	21.20	2931		18	100.92	21.10				18	100.92	21.10
2821		24	101.20	21.60	2858		15	101.13	21.30	2895		6	101.02	21.20	2932		21	100.92	21.10				21	100.92	21.10
2822	16.10.07	3	101.20	21.60	2859		18	101.13	21.30	2896		9	101.02	21.20	2933		24	100.92	21.10				24	100.92	21.10
2823		6	101.16	21.60	2860		21	101.13	21.30	2897		12	101.02	21.20	2934	30.10.07	3	100.92	21.10				3	100.92	21.10
2824		9	101.16	21.60	2861		24	101.13	21.30	2898		15	100.99	21.20	2935		6	100.92	21.10				6	100.92	21.10
2825		12	101.16	21.60	2862	21.10.07	3	101.09	21.30	2899		18	100.99	21.20	2936		9	100.92	21.10				9	100.92	21.10
2826		15	101.16	21.60	2863		6	101.09	21.30	2900		21	100.99	21.20	2937		12	100.95	21.10				12	100.95	21.10
2827		18	101.16	21.60	2864		9	101.09	21.30	2901		24	100.99	21.20	2938		15	100.95	21.10				15	100.95	21.10
2828		21	101.15	21.60	2865		12	101.09	21.30	2902	26.10.07	3	100.99	21.20	2939		18	100.95	21.10				18	100.95	21.10
2829		24	101.14	21.60	2866		15	101.09	21.30	2903		6	100.99	21.20	2940		21	100.99	21.10				21	100.99	21.10

Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
2941		24	100.95	21.10	2978		18	101.02	22.00	3015		9	101.44	22.00	3052		24	101.22	22.50
2942	31.10.07	3	100.95	21.10	2979		21	100.98	22.00	3016		12	101.55	22.10	3053	14.07.08	3	101.22	22.40
2943		6	101.02	21.10	2980		24	100.98	22.00	3017		15	101.66	22.10	3054		6	101.19	22.30
2944		9	101.02	21.20	2981	05.07.08	3	100.98	22.00	3018		18	101.93	22.10	3055		9	101.19	22.30
2945		12	101.02	21.20	2982		6	100.98	22.00	3019		21	102.19	22.10	3056		12	101.19	22.30
2946		15	101.02	21.20	2983		9	100.95	22.00	3020		24	102.30	22.10	3057		15	101.19	22.30
2947		18	101.02	21.20	2984		12	100.95	22.00	3021	10.07.08	3	102.41	22.10	3058		18	101.19	22.30
2948		21	101.02	21.20	2985		15	100.95	22.00	3022		6	102.44	22.20	3059		21	101.19	22.30
2949	01.07.08	3	101.77	22.00	2986		18	100.92	22.00	3023		9	102.44	22.20	3060		24	101.19	22.30
2950		6	101.73	22.10	2987		21	100.92	22.00	3024		12	102.38	22.20	3061	15.07.08	3	101.19	22.30
2951		9	101.70	22.20	2988		24	100.92	21.90	3025		15	102.27	22.20	3062		6	101.19	22.30
2952		12	101.66	22.30	2989	06.07.08	3	100.95	21.80	3026		18	102.12	22.30	3063		9	101.19	22.30
2953		15	101.62	22.40	2990		6	100.95	21.70	3027		21	102.00	22.40	3064		12	101.19	22.30
2954		18	101.59	22.40	2991		9	100.95	21.60	3028		24	101.93	22.50	3065		15	101.19	22.30
2955		21	101.52	22.40	2992		12	100.95	21.60	3029	11.07.08	3	101.88	22.60	3066		18	101.19	22.30
2956		24	101.44	22.40	2993		15	100.95	21.60	3030		6	101.83	22.60	3067		21	101.19	22.30
2957	02.07.08	3	101.39	22.40	2994		18	100.95	21.60	3031		9	101.77	22.70	3068		24	101.19	22.30
2958		6	101.34	22.40	2995		21	100.95	21.60	3032		12	101.70	22.90	3069	16.07.08	3	101.19	22.30
2959		9	101.32	22.40	2996		24	100.98	21.60	3033		15	101.62	23.00	3070		6	101.19	22.30
2960		12	101.27	22.40	2997	07.07.08	3	101.05	21.60	3034		18	101.59	23.00	3071		9	101.19	22.20
2961		15	101.22	22.40	2998		6	101.16	21.60	3035		21	101.55	22.90	3072		12	101.19	22.20
2962		18	101.16	22.40	2999		9	101.24	21.50	3036		24	101.52	22.90	3073		15	101.19	22.20
2963		21	101.12	22.40	3000		12	101.29	21.40	3037	12.07.08	3	101.48	22.80	3074		18	101.24	22.20
2964		24	101.06	22.40	3001		15	101.32	21.50	3038		6	101.44	22.80	3075		21	101.29	22.20
2965	03.07.08	3	101.16	22.30	3002		18	101.34	21.50	3039		9	101.42	22.70	3076		24	101.37	22.20
2966		6	101.22	22.30	3003		21	101.39	21.50	3040		12	101.39	22.60	3077	17.07.08	3	101.44	22.20
2967		9	101.27	22.20	3004		24	101.37	21.50	3041		15	101.37	22.60	3078		6	101.55	22.20
2968		12	101.27	22.20	3005	08.07.08	3	101.34	21.50	3042		18	101.37	22.60	3079		9	101.62	22.20
2969		15	101.24	22.20	3006		6	101.32	21.50	3043		21	101.34	22.60	3080		12	101.62	22.20
2970		18	101.19	22.20	3007		9	101.29	21.50	3044		24	101.33	22.60	3081		15	101.59	22.20
2971		21	101.12	22.20	3008		12	101.27	21.60	3045	13.07.08	3	101.32	22.60	3082		18	101.55	22.20
2972		24	101.09	22.10	3009		15	101.27	21.60	3046		6	101.32	22.50	3083		21	101.55	22.20
2973	04.07.08	3	101.05	22.10	3010		18	101.27	21.60	3047		9	101.29	22.50	3084		24	101.52	22.20
2974		6	101.05	22.00	3011		21	101.27	21.70	3048		12	101.29	22.50	3085	18.07.08	3	101.48	22.20
2975		9	101.05	22.00	3012		24	101.29	21.80	3049		15	101.27	22.50	3086		6	101.44	22.30
2976		12	101.02	22.00	3013	09.07.08	3	101.34	21.90	3050		18	101.24	22.50	3087		9	101.42	22.30
2977		15	101.02	22.00	3014		6	101.39	22.00	3051		21	101.24	22.50	3088		12	101.39	22.30

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
3089		15	101.37	22.40	3126		6	101.88	22.50	3163		21	102.44	22.90	3200		12	103.14	23.30
3090		18	101.34	22.40	3127		9	101.90	22.50	3164		24	102.27	22.90	3201		15	102.99	23.50
3091		21	101.32	22.40	3128		12	101.90	22.60	3165	28.07.08	3	102.23	23.00	3202		18	102.81	23.60
3092		24	101.32	22.40	3129		15	101.90	22.60	3166		6	102.72	23.00	3203		21	102.63	23.60
3093	19.07.08	3	101.32	22.40	3130		18	101.90	22.60	3167		9	102.78	23.00	3204		24	102.57	23.70
3094		6	101.32	22.50	3131		21	101.90	22.60	3168		12	102.78	23.00	3205	02.08.08	3	102.50	23.80
3095		9	101.32	22.50	3132		24	101.90	22.60	3169		15	102.72	23.00	3206		6	102.47	23.90
3096		12	101.32	22.50	3133	24.07.08	3	101.90	22.60	3170		18	102.66	23.10	3207		9	102.44	24.00
3097		15	101.32	22.50	3134		6	101.90	22.60	3171		21	102.60	23.20	3208		12	102.41	24.10
3098		18	101.32	22.40	3135		9	101.90	22.60	3172		24	102.57	23.20	3209		15	102.38	24.20
3099		21	101.34	22.40	3136		12	101.88	22.60	3173	29.07.08	3	102.53	23.30	3210		18	102.38	24.00
3100		24	101.37	22.40	3137		15	101.88	22.60	3174		6	102.50	23.40	3211		21	102.34	23.90
3101	20.07.08	3	101.39	22.40	3138		18	101.88	22.60	3175		9	102.47	23.50	3212		24	102.30	23.70
3102		6	101.42	22.40	3139		21	101.88	22.60	3176		12	102.47	23.60	3213	03.08.08	3	102.27	23.50
3103		9	101.44	22.30	3140		24	101.93	22.60	3177		15	102.47	23.60	3214		6	102.23	23.30
3104		12	101.48	22.30	3141		3	102.00	22.60	3178		18	102.44	23.60	3215		9	102.23	23.30
3105		15	101.52	22.20	3142	25.07.08	6	102.08	22.70	3179		21	102.44	23.60	3216		12	102.19	23.20
3106		18	101.55	22.20	3143		9	102.16	22.60	3180		24	102.38	23.60	3217		15	102.19	23.40
3107		21	101.59	22.20	3144		12	102.19	22.60	3181	30.07.08	3	102.30	23.60	3218		18	102.16	23.40
3108		24	101.62	22.20	3145		15	102.19	22.60	3182		6	102.27	23.60	3219		21	102.16	23.40
3109	21.07.08	3	101.66	22.20	3146		18	102.19	22.60	3183		9	102.23	23.60	3220		24	102.08	23.40
3110		6	101.77	22.20	3147		21	102.19	22.60	3184		12	102.23	23.60	3221	04.08.08	3	102.02	23.40
3111		9	101.85	22.20	3148		24	102.19	22.60	3185		15	102.27	23.60	3222		6	101.97	23.40
3112		12	101.93	22.20	3149	26.07.08	3	102.19	22.60	3186		18	102.27	23.60	3223		9	101.93	23.40
3113		15	102.00	22.20	3150		6	102.19	22.60	3187		21	102.34	23.60	3224		12	101.90	23.30
3114		18	102.00	22.20	3151		9	102.19	22.60	3188		24	102.38	23.60	3225		15	101.90	23.10
3115		21	101.97	22.20	3152		12	102.19	22.60	3189	31.07.08	3	102.38	23.50	3226		18	101.88	23.00
3116		24	101.95	22.20	3153		15	102.19	22.60	3190		6	102.38	23.50	3227		21	101.85	23.00
3117	22.07.08	3	101.93	22.20	3154		18	102.23	22.70	3191		9	102.38	23.50	3228		24	101.85	23.00
3118		6	101.90	22.20	3155		21	102.27	22.70	3192		12	102.41	23.40	3229	05.08.08	3	101.83	23.00
3119		9	101.90	22.20	3156		24	102.27	22.70	3193		15	102.44	23.40	3230		6	101.83	22.90
3120		12	101.88	22.20	3157	27.07.08	3	102.23	22.80	3194		18	102.53	23.40	3231		9	101.85	22.80
3121		15	101.88	22.30	3158		6	102.19	22.80	3195		21	102.63	23.40	3232		12	101.93	22.80
3122		18	101.88	22.30	3159		9	102.19	22.80	3196		24	102.78	23.40	3233		15	102.02	22.80
3123		21	101.88	22.40	3160		12	102.23	22.80	3197	01.08.08	3	102.99	23.30	3234		18	102.27	22.80
3124		24	101.88	22.40	3161		15	102.27	22.90	3198		6	103.17	23.30	3235		21	102.50	22.80
3125	23.07.08	3	101.88	22.50	3162		18	102.34	22.90	3199		9	103.24	23.30	3236		24	102.50	22.80

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
3237	06.08.08	3	102.47	22.70	3274		18	103.91	25.30	3311		9	102.63	23.60	3348		24	102.84	24.20
3238		6	102.44	22.60	3275		21	103.78	25.30	3312		12	102.53	23.60	3349	20.08.08	3	102.81	24.10
3239		9	102.34	22.60	3276		24	103.78	25.10	3313		15	102.47	23.50	3350		6	102.81	24.00
3240		12	102.30	22.60	3277	11.08.08	3	103.81	24.90	3314		18	102.47	23.50	3351		9	102.81	24.00
3241		15	102.27	22.60	3278		6	103.85	24.90	3315		21	102.50	23.60	3352		12	102.78	24.00
3242		18	102.23	22.60	3279		9	103.85	24.80	3316		24	102.60	23.60	3353		15	102.78	23.90
3243		21	102.19	22.60	3280		12	103.85	24.70	3317	16.08.08	3	103.05	23.60	3354		18	102.75	24.00
3244		24	102.16	22.60	3281		15	103.85	24.60	3318		6	103.66	23.60	3355		21	102.75	23.90
3245	07.08.08	3	102.12	22.70	3282		18	103.85	24.50	3319		9	103.81	23.50	3356		24	102.78	23.80
3246		6	102.08	22.80	3283		21	103.85	24.40	3320		12	103.91	23.50	3357	21.08.08	3	102.87	23.70
3247		9	102.05	22.90	3284		24	103.72	24.40	3321		15	103.94	23.50	3358		6	102.99	23.60
3248		12	102.05	22.90	3285	12.08.08	3	103.54	24.40	3322		18	103.94	23.50	3359		9	103.57	23.60
3249		15	102.08	23.00	3286		6	103.39	24.30	3323		21	103.94	23.50	3360		12	103.72	23.50
3250		18	102.12	23.00	3287		9	103.91	24.30	3324		24	104.03	23.50	3361		15	103.81	23.50
3251		21	102.16	23.00	3288		12	103.33	24.30	3325	17.08.08	3	104.33	23.50	3362		18	103.85	23.50
3252		24	102.23	23.00	3289		15	103.39	24.30	3326		6	104.55	23.70	3363		21	103.85	23.50
3253	08.08.08	3	102.30	22.90	3290		18	103.33	24.20	3327		9	104.55	24.00	3364		24	103.88	23.50
3254		6	102.38	22.90	3291		21	103.27	24.20	3328		12	104.49	24.40	3365	22.08.08	3	103.91	23.50
3255		9	102.53	22.90	3292		24	103.21	24.20	3329		15	104.42	24.40	3366		6	103.94	23.50
3256		12	102.87	22.90	3293	13.08.08	3	102.69	24.20	3330		18	104.42	24.30	3367		9	104.06	23.50
3257		15	103.27	22.90	3294		6	102.67	24.10	3331		21	104.42	24.40	3368		12	104.15	23.60
3258		18	103.63	22.90	3295		9	102.66	24.00	3332		24	104.39	24.60	3369		15	104.21	23.90
3259		21	104.09	22.90	3296		12	102.65	24.00	3333	18.08.08	3	104.33	24.70	3370		18	104.30	24.30
3260		24	104.42	22.90	3297		15	102.64	24.00	3334		6	104.27	24.80	3371		21	104.39	24.30
3261	09.08.08	3	104.64	22.90	3298		18	102.93	24.00	3335		9	104.21	24.90	3372		24	104.42	24.50
3262		6	104.64	22.90	3299		21	102.90	24.00	3336		12	104.09	24.90	3373	23.08.08	3	104.45	24.60
3263		9	104.64	23.00	3300		24	102.87	24.00	3337		15	103.97	24.90	3374		6	104.49	24.70
3264		12	104.58	23.30	3301	14.08.08	3	102.87	24.00	3338		18	103.94	24.90	3375		9	104.40	24.60
3265		15	104.49	23.60	3302		6	102.87	23.90	3339		21	103.94	24.90	3376		12	104.33	24.70
3266		18	104.36	24.00	3303		9	102.85	23.90	3340		24	103.78	24.90	3377		15	104.24	24.70
3267		21	104.24	24.60	3304		12	102.81	23.90	3341	19.08.08	3	103.51	24.80	3378		18	104.21	24.80
3268		24	104.18	24.80	3305		15	102.78	23.90	3342		6	103.33	24.80	3379		21	104.18	24.80
3269	10.08.08	3	104.12	25.10	3306		18	102.78	23.80	3343		9	103.24	24.70	3380		24	104.12	24.80
3270		6	104.09	25.30	3307		21	102.81	23.80	3344		12	103.17	24.60	3381	24.08.08	3	104.06	24.90
3271		9	104.09	25.40	3308		24	102.78	23.80	3345		15	103.14	24.50	3382		6	104.00	25.00
3272		12	104.09	25.40	3309	15.08.08	3	102.75	23.80	3346		18	103.02	24.40	3383		9	103.78	25.10
3273		15	104.03	25.40	3310		6	102.72	23.70	3347		21	102.87	24.30	3384		12	103.66	25.10

SI No	Date	Time (hrs)	Stage at Khairimal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairimal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairimal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairimal (m)	Stage at Naraj (m)
3385		15	103.60	25.10	3422		6	102.08	23.10	3459		21	101.93	23.30	3496		12	101.70	22.90
3386		18	103.54	25.00	3423		9	102.05	23.10	3460		24	101.90	23.30	3497		15	101.70	22.90
3387		21	104.10	24.90	3424		12	102.02	23.10	3461	03.09.08	3	101.90	23.30	3498		18	101.66	22.80
3388		24	103.39	24.80	3425		15	102.00	23.00	3462		6	101.88	23.30	3499		21	101.66	22.80
3389	25.08.08	3	103.30	24.70	3426		18	101.97	23.10	3463		9	101.85	23.30	3500		24	101.66	22.80
3390		6	103.21	24.70	3427		21	101.95	23.10	3464		12	101.83	23.20	3501	08.09.08	3	101.66	22.70
3391		9	103.11	24.60	3428		24	101.95	23.10	3465		15	101.80	23.20	3502		6	101.66	22.70
3392		12	103.05	24.50	3429	30.08.08	3	101.95	23.10	3466		18	101.80	23.10	3503		9	101.66	22.70
3393		15	102.99	24.40	3430		6	101.95	23.00	3467		21	101.80	23.00	3504		12	101.62	22.60
3394		18	102.93	24.30	3431		9	101.93	23.00	3468		24	101.80	23.00	3505		15	101.62	22.60
3395		21	102.87	24.20	3432		12	101.93	23.00	3469	04.09.08	3	101.80	23.00	3506		18	101.66	22.60
3396		24	102.84	24.10	3433		15	101.93	23.00	3470		6	101.80	22.90	3507		21	101.70	22.60
3397	26.08.08	3	102.81	24.00	3434		18	101.93	23.00	3471		9	101.83	22.90	3508		24	101.70	22.50
3398		6	102.78	23.90	3435		21	101.93	23.00	3472		12	101.88	22.90	3509	09.09.08	3	101.70	22.50
3399		9	102.78	24.20	3436		24	101.95	23.00	3473		15	101.93	22.90	3510		6	101.70	22.50
3400		12	102.78	24.00	3437	31.08.08	3	101.97	23.00	3474		18	101.95	22.90	3511		9	101.66	22.40
3401		15	102.78	24.00	3438		6	102.00	22.90	3475		21	101.97	22.90	3512		12	101.66	22.40
3402		18	102.75	23.90	3439		9	102.02	22.90	3476		24	102.00	22.90	3513		15	101.66	22.40
3403		21	102.75	23.90	3440		12	102.05	22.90	3477	05.09.08	3	102.02	22.90	3514		18	101.62	22.40
3404		24	102.70	23.90	3441		15	102.08	23.00	3478		6	102.05	22.80	3515		21	101.62	22.40
3405	27.08.08	3	102.63	23.80	3442		18	102.12	23.00	3479		9	102.05	22.80	3516		24	101.62	22.40
3406		6	102.57	23.70	3443		21	102.19	23.00	3480		12	102.05	22.80	3517	10.09.08	3	101.62	22.40
3407		9	102.50	23.70	3444		24	102.23	23.00	3481		15	102.05	22.80	3518		6	101.62	22.30
3408		12	102.44	23.60	3445	01.09.08	3	102.27	23.00	3482		18	102.02	22.80	3519		9	101.62	22.30
3409		15	102.38	23.60	3446		6	102.27	23.00	3483		21	102.02	22.80	3520		12	101.62	22.30
3410		18	102.38	23.60	3447		9	102.30	22.90	3484		24	102.00	22.80	3521		15	101.59	22.30
3411		21	102.38	23.50	3448		12	102.34	22.90	3485	06.09.08	3	101.97	22.90	3522		18	101.59	22.40
3412		24	102.34	23.60	3449		15	102.38	22.90	3486		6	101.95	23.00	3523		21	101.59	22.40
3413	28.08.08	3	102.30	23.50	3450		18	102.41	22.90	3487		9	101.93	23.00	3524		24	101.59	22.40
3414		6	102.27	23.40	3451		21	102.41	22.90	3488		12	101.90	23.00	3525	11.09.08	3	101.59	22.40
3415		9	102.23	23.40	3452		24	102.34	22.90	3489		15	101.88	23.00	3526		6	101.62	22.40
3416		12	102.19	23.30	3453	02.09.08	3	102.33	23.00	3490		18	101.85	23.00	3527		9	101.62	22.40
3417		15	102.16	23.20	3454		6	102.08	23.10	3491		21	101.83	23.00	3528		12	101.62	22.40
3418		18	102.16	23.30	3455		9	102.00	23.10	3492		24	101.80	23.00	3529		15	101.62	22.40
3419		21	102.14	23.30	3456		12	102.00	23.20	3493	07.09.08	3	101.77	23.00	3530		18	101.59	22.40
3420		24	102.12	23.30	3457		15	101.97	23.30	3494		6	101.73	23.00	3531		21	101.59	22.40
3421	29.08.08	3	102.08	23.20	3458		18	101.95	23.30	3495		9	101.70	22.90	3532		24	101.59	22.40

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
3533	12.09.08	3	101.59	22.40	3570		18	101.88	22.80	3607		9	106.13	27.00	3644		24	102.50	24.50
3534		6	101.59	22.40	3571		21	101.90	22.90	3608		12	105.95	26.90	3645	26.09.08	3	102.41	24.50
3535		9	101.59	22.40	3572		24	102.12	23.10	3609		15	105.80	26.80	3646		6	102.34	24.40
3536		12	101.59	22.40	3573	17.09.08	3	102.57	23.30	3610		18	105.70	26.80	3647		9	102.27	24.30
3537		15	101.59	22.40	3574		6	103.02	23.50	3611		21	105.70	26.70	3648		12	102.19	24.20
3538		18	101.59	22.40	3575		9	103.88	23.50	3612		24	105.52	26.70	3649		15	102.16	24.10
3539		21	101.59	22.40	3576		12	104.49	23.60	3613	22.09.08	3	105.05	26.60	3650		18	102.16	24.10
3540		24	101.59	22.40	3577		15	104.96	23.70	3614		6	104.73	26.60	3651		21	102.12	24.10
3541	13.09.08	3	101.59	22.50	3578		18	105.30	23.80	3615		9	104.61	26.60	3652		24	102.12	24.00
3542		6	101.59	22.50	3579		21	105.46	23.90	3616		12	104.61	26.50	3653	27.09.08	3	102.05	23.90
3543		9	101.59	22.50	3580		24	105.86	24.20	3617		15	104.58	26.50	3654		6	102.05	23.80
3544		12	101.59	22.50	3581	18.09.08	3	106.10	24.40	3618		18	104.49	26.40	3655		9	102.05	23.70
3545		15	101.59	22.50	3582		6	106.59	25.00	3619		21	104.30	26.30	3656		12	102.05	23.60
3546		18	101.59	22.50	3583		9	107.29	25.50	3620		24	104.03	26.20	3657		15	102.02	23.40
3547		21	101.59	22.50	3584		12	107.61	25.20	3621	23.09.08	3	103.47	26.10	3658		18	102.00	23.40
3548		24	101.55	22.50	3585		15	107.80	25.70	3622		6	103.33	26.00	3659		21	101.97	23.40
3549	14.09.08	3	101.55	22.50	3586		18	108.04	26.10	3623		9	103.08	26.10	3660		24	101.95	23.30
3550		6	101.55	22.50	3587		21	108.04	26.40	3624		12	103.02	26.00	3661	28.09.08	3	101.93	23.20
3551		9	101.55	22.50	3588		24	108.04	26.50	3625		15	103.02	25.90	3662		6	101.90	23.20
3552		12	101.55	22.50	3589	19.09.08	3	108.22	27.00	3626		18	103.05	25.80	3663		9	101.88	23.20
3553		15	101.55	22.50	3590		6	108.22	27.10	3627		21	103.17	25.60	3664		12	101.85	23.20
3554		18	101.55	22.50	3591		9	108.18	27.10	3628		24	103.21	25.40	3665		15	101.83	23.20
3555		21	101.52	22.50	3592		12	108.18	27.20	3629	24.09.08	3	103.14	25.20	3666		18	101.80	23.20
3556		24	101.55	22.50	3593		15	108.01	27.40	3630		6	103.11	25.00	3667		21	101.77	23.10
3557	15.09.08	3	101.62	22.50	3594		18	107.84	27.40	3631		9	103.11	24.90	3668		24	101.73	23.10
3558		6	101.73	22.50	3595		21	107.58	27.50	3632		12	103.08	24.70	3669	29.09.08	3	101.73	23.00
3559		9	101.84	22.50	3596		24	107.32	27.60	3633		15	103.05	25.00	3670		6	101.73	23.00
3560		12	101.85	22.50	3597	20.09.08	3	106.80	27.60	3634		18	103.05	25.00	3671		9	101.73	23.10
3561		15	101.88	22.50	3598		6	106.59	27.70	3635		21	103.05	24.90	3672		12	101.73	23.10
3562		18	101.88	22.50	3599		9	106.39	27.80	3636		24	102.99	24.80	3673		15	101.73	23.10
3563		21	101.88	22.50	3600		12	106.39	27.80	3637	25.09.08	3	102.90	24.80	3674		18	101.70	23.00
3564		24	101.88	22.50	3601		15	106.39	27.70	3638		6	102.84	24.70	3675		21	101.70	23.00
3565	16.09.08	3	101.88	22.50	3602		18	106.68	27.60	3639		9	102.78	24.70	3676		24	101.66	22.90
3566		6	101.88	22.50	3603		21	106.74	27.50	3640		12	102.75	24.60	3677	30.09.08	3	101.66	22.80
3567		9	101.88	22.60	3604		24	106.68	27.40	3641		15	102.72	24.60	3678		6	101.62	22.70
3568		12	101.85	22.60	3605	21.09.08	3	106.45	27.20	3642		18	102.66	24.60	3679		9	101.59	22.70
3569		15	101.85	22.70	3606		6	106.26	27.10	3643		21	102.60	24.60	3680		12	101.59	22.70

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
3681		15	101.55	22.70	3718		6	101.34	22.30	3755		21	101.27	21.90	3792		12	101.16	21.80
3682		18	101.55	22.70	3719		9	101.34	22.30	3756		24	101.29	21.90	3793		15	101.16	21.80
3683		21	101.55	22.70	3720		12	101.32	22.30	3757	10.10.08	3	101.29	21.90	3794		18	101.16	21.80
3684		24	101.55	22.70	3721		15	101.32	22.30	3758		6	101.32	21.80	3795		21	101.16	21.80
3685	01.10.08	3	101.55	22.70	3722		18	101.32	22.30	3759		9	101.32	21.80	3796		24	101.16	21.80
3686		6	101.55	22.70	3723		21	101.32	22.30	3760		12	101.29	21.80	3797	15.10.08	3	101.16	21.80
3687		9	101.55	22.70	3724		24	101.32	22.30	3761		15	101.29	21.80	3798		6	101.16	21.70
3688		12	101.52	22.70	3725	06.10.08	3	101.32	22.30	3762		18	101.27	21.80	3799		9	101.16	21.70
3689		15	101.52	22.70	3726		6	101.32	22.30	3763		21	101.27	21.80	3800		12	101.16	21.70
3690		18	101.52	22.60	3727		9	101.32	22.30	3764		24	101.27	21.80	3801		15	101.16	21.70
3691		21	101.55	22.60	3728		12	101.32	22.30	3765	11.10.08	3	101.27	21.80	3802		18	101.16	21.70
3692		24	101.59	22.60	3729		15	101.32	22.30	3766		6	101.27	21.80	3803		21	101.16	21.70
3693	02.10.08	3	101.62	22.60	3730		18	101.32	22.30	3767		9	101.27	21.80	3804		24	101.12	21.70
3694		6	101.62	22.50	3731		21	101.32	22.30	3768		12	101.27	21.80	3805	16.10.08	3	101.12	21.70
3695		9	101.62	22.40	3732		24	101.29	22.30	3769		15	101.29	21.80	3806		6	101.09	21.70
3696		12	101.62	22.40	3733	07.10.08	3	101.29	22.30	3770		18	101.29	21.80	3807		9	101.09	21.70
3697		15	101.62	22.40	3734		6	101.29	22.30	3771		21	101.29	21.80	3808		12	101.09	21.70
3698		18	101.59	22.40	3735		9	101.27	22.20	3772		24	101.27	21.80	3809		15	101.09	21.70
3699		21	101.59	22.40	3736		12	101.27	22.20	3773	12.10.08	3	101.27	21.80	3810		18	101.05	21.70
3700		24	101.55	22.40	3737		15	101.27	22.20	3774		6	101.24	21.80	3811		21	101.05	21.70
3701	03.10.08	3	101.55	22.40	3738		18	101.27	22.20	3775		9	101.24	21.80	3812		24	101.05	21.70
3702		6	101.52	22.40	3739		21	101.24	22.10	3776		12	101.22	21.80	3813	17.10.08	3	101.09	21.60
3703		9	101.52	22.40	3740		24	101.24	22.10	3777		15	101.22	21.80	3814		6	101.09	21.60
3704		12	101.48	22.40	3741		3	101.06	22.10	3778		18	101.19	21.80	3815		9	101.09	21.60
3705		15	101.48	22.40	3742	08.10.08	6	101.24	22.00	3779		21	101.19	21.80	3816		12	101.09	21.60
3706		18	101.48	22.40	3743		9	101.24	22.00	3780		24	101.19	21.80	3817		15	101.09	21.60
3707		21	101.44	22.40	3744		12	101.24	22.00	3781	13.10.08	3	101.19	21.80	3818		18	101.09	21.60
3708		24	101.44	22.40	3745		15	101.24	22.00	3782		6	101.19	21.80	3819		21	101.09	21.60
3709	04.10.08	3	101.42	22.40	3746		18	101.24	22.00	3783		9	101.19	21.80	3820		24	101.05	21.60
3710		6	101.39	22.40	3747		21	101.24	22.00	3784		12	101.16	21.80	3821	18.10.08	3	101.05	21.60
3711		9	101.39	22.40	3748		24	101.24	22.00	3785		15	101.16	21.80	3822		6	101.05	21.60
3712		12	101.39	22.40	3749	09.10.08	3	101.24	22.00	3786		18	101.12	21.80	3823		9	101.05	21.60
3713		15	101.39	22.40	3750		6	101.24	21.90	3787		21	101.12	21.80	3824		12	101.05	21.60
3714		18	101.39	22.40	3751		9	101.27	21.90	3788		24	101.12	21.80	3825		15	101.05	21.60
3715		21	101.37	22.40	3752		12	101.27	21.90	3789	14.10.08	3	101.16	21.80	3826		18	101.05	21.60
3716		24	101.37	22.40	3753		15	101.27	21.90	3790		6	101.16	21.80	3827		21	101.05	21.60
3717	05.10.08	3	101.34	22.40	3754		18	101.27	21.90	3791		9	101.16	21.80	3828		24	101.05	21.60

Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl/No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
3829	19.10.08	3	101.05	21.50	3866		18	100.92	21.50	3903		9	100.85	21.30	3940		6	101.93	22.80
3830		6	101.05	21.50	3867		21	100.92	21.50	3904		12	100.85	21.30	3941		9	102.30	22.80
3831		9	101.05	21.50	3868		24	100.92	21.50	3905		15	100.85	21.30	3942		12	102.41	22.80
3832		12	101.02	21.50	3869	24.10.08	3	100.92	21.50	3906		18	100.85	21.30	3943		15	102.41	22.80
3833		15	101.02	21.50	3870		6	100.92	21.50	3907		21	100.85	21.30	3944		18	103.06	22.80
3834		18	101.02	21.50	3871		9	100.92	21.50	3908		24	100.85	21.30	3945		21	103.94	23.00
3835		21	101.02	21.50	3872		12	100.92	21.50	3909	29.10.08	3	100.85	21.30	3946		24	104.65	23.30
3836		24	101.02	21.50	3873		15	100.92	21.50	3910		6	100.85	21.30	3947	14.07.09	3	104.65	23.50
3837	20.10.08	3	101.02	21.50	3874		18	100.92	21.50	3911		9	100.85	21.30	3948		6	104.65	23.80
3838		6	101.02	21.50	3875		21	100.92	21.50	3912		12	100.85	21.30	3949		9	104.52	24.00
3839		9	101.02	21.50	3876		24	100.88	21.50	3913		15	100.85	21.20	3950		12	104.42	24.20
3840		12	101.02	21.50	3877	25.10.08	3	100.88	21.50	3914		18	100.85	21.20	3951		15	104.45	24.80
3841		15	101.02	21.50	3878		6	100.88	21.50	3915		21	100.85	21.20	3952		18	104.52	25.10
3842		18	101.02	21.50	3879		9	100.92	21.50	3916		24	100.85	21.20	3953		21	104.55	25.30
3843		21	101.02	21.50	3880		12	100.92	21.50	3917	30.10.08	3	100.85	21.20	3954		24	104.52	25.50
3844		24	100.98	21.50	3881		15	100.92	21.50	3918		6	100.85	21.20	3955	15.07.09	3	104.45	25.60
3845	21.10.08	3	100.98	21.50	3882		18	100.92	21.50	3919		9	100.85	21.20	3956		6	104.39	25.60
3846		6	100.98	21.50	3883		21	100.92	21.50	3920		12	100.85	21.20	3957		9	104.49	25.50
3847		9	100.98	21.50	3884		24	100.92	21.50	3921		15	100.85	21.20	3958		12	104.70	25.60
3848		12	100.98	21.50	3885	26.10.08	3	100.92	21.50	3922		18	100.85	21.20	3959		15	104.91	25.50
3849		15	100.98	21.50	3886		6	100.88	21.50	3923		21	100.85	21.20	3960		18	105.02	25.40
3850		18	100.98	21.50	3887		9	100.88	21.50	3924		24	100.85	21.20	3961		21	105.02	25.60
3851		21	100.98	21.50	3888		12	100.88	21.50	3925	31.10.08	3	100.85	21.10	3962		24	105.02	25.70
3852		24	100.98	21.50	3889		15	100.88	21.50	3926		6	100.85	21.10	3963	16.07.09	3	104.73	25.60
3853	22.10.08	3	100.95	21.50	3890		18	100.88	21.50	3927		9	100.85	21.10	3964		6	104.52	25.60
3854		6	100.95	21.50	3891		21	100.88	21.50	3928		12	100.85	21.10	3965		9	104.36	25.65
3855		9	100.95	21.50	3892		24	100.88	21.50	3929		15	100.85	21.10	3966		12	104.27	25.75
3856		12	100.95	21.50	3893	27.10.08	3	100.88	21.40	3930		18	100.85	21.10	3967		15	104.15	25.90
3857		15	100.95	21.50	3894		6	100.88	21.40	3931		21	100.85	21.10	3968		18	104.03	26.10
3858		18	100.95	21.50	3895		9	100.85	21.40	3932		6	101.21	22.70	3969		21	103.88	26.00
3859		21	100.95	21.50	3896		12	100.85	21.40	3933		9	101.11	22.70	3970		24	103.69	25.80
3860		24	100.92	21.50	3897		15	100.85	21.40	3934		12	101.11	22.70	3971	17.07.09	3	103.50	25.60
3861	23.10.08	3	100.92	21.50	3898		18	100.85	21.40	3935		15	101.08	22.70	3972		6	103.33	25.40
3862		6	100.92	21.50	3899		21	100.85	21.40	3936		18	101.08	22.70	3973		9	103.17	25.30
3863		9	100.92	21.50	3900		24	100.85	21.40	3937		21	101.04	22.80	3974		12	103.05	25.40
3864		12	100.92	21.50	3901	28.10.08	3	100.85	21.40	3938		24	101.27	22.80	3975		15	102.99	25.35
3865		15	100.92	21.50	3902		6	100.85	21.30	3939	13.07.09	3	101.62	22.80	3976		18	102.90	25.20

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
3977		21	102.78	25.10	4014		12	104.99	25.50	4051	27.07.09	3	103.17	24.90	4088		18	102.05	23.65
3978		24	102.66	25.00	4015		15	104.70	25.50	4052		6	102.99	24.60	4089		21	102.02	23.60
3979	18.07.09	3	102.57	24.60	4016		18	104.49	25.55	4053		9	102.96	24.60	4090		24	102.00	23.50
3980		6	102.47	24.50	4017		21	104.85	25.60	4054		12	102.96	24.55	4091	01.08.09	3	101.97	23.50
3981		9	102.41	24.50	4018		24	104.85	25.65	4055		15	102.96	24.70	4092		6	101.97	23.50
3982		12	102.90	24.25	4019	23.07.09	3	105.46	25.70	4056		18	102.96	24.80	4093		9	101.95	23.20
3983		15	103.33	24.20	4020		6	105.55	25.70	4057		21	102.96	24.80	4094		12	101.95	23.10
3984		18	103.39	24.00	4021		9	105.58	25.65	4058		24	102.96	24.85	4095		15	101.95	23.00
3985		21	103.39	24.20	4022		12	105.61	25.55	4059	28.07.09	3	102.99	24.65	4096		18	101.95	22.90
3986		24	103.69	24.15	4023		15	105.55	25.50	4060		6	103.02	24.45	4097		21	101.95	22.80
3987	19.07.09	3	104.15	24.10	4024		18	105.52	25.45	4061		9	103.08	24.25	4098		24	101.93	22.80
3988		6	104.55	24.00	4025		21	105.49	25.45	4062		12	103.21	24.30	4099	02.08.09	3	101.90	22.80
3989		9	104.70	23.90	4026		24	105.46	25.50	4063		15	103.39	24.30	4100		6	101.88	22.80
3990		12	104.82	23.90	4027	24.07.09	3	105.43	25.55	4064		18	103.60	24.25	4101		9	101.83	22.75
3991		15	104.99	24.10	4028		6	105.36	25.70	4065		21	103.78	24.25	4102		12	101.77	22.70
3992		18	105.30	24.50	4029		9	105.17	25.70	4066		24	103.81	24.20	4103		15	101.73	22.70
3993		21	105.61	24.65	4030		12	105.08	25.80	4067	29.07.09	3	103.81	24.20	4104		18	101.70	23.00
3994		24	105.74	24.50	4031		15	105.02	25.80	4068		6	103.81	24.10	4105		21	101.70	22.95
3995	20.07.09	3	105.64	24.80	4032		18	104.99	25.80	4069		9	103.69	24.10	4106		24	101.66	22.95
3996		6	105.55	25.00	4033		21	104.96	25.80	4070		12	103.48	24.15	4107	03.08.09	3	101.66	22.95
3997		9	105.36	25.20	4034		24	104.96	25.80	4071		15	103.30	24.25	4108		6	101.62	22.95
3998		12	105.13	25.50	4035	25.07.09	3	104.94	25.80	4072		18	103.12	24.40	4109		9	101.62	22.95
3999		15	104.94	25.60	4036		6	104.91	25.75	4073		21	103.02	24.65	4110		12	101.62	22.90
4000		18	104.76	25.70	4037		9	104.91	25.70	4074		24	102.97	24.70	4111		15	101.59	22.90
4001		21	104.58	25.80	4038		12	104.91	25.65	4075	30.07.09	3	102.78	25.00	4112		18	101.59	22.90
4002		24	104.58	25.90	4039		15	104.88	25.60	4076		6	102.66	25.00	4113		21	101.59	22.90
4003	21.07.09	3	104.58	25.95	4040		18	104.85	25.50	4077		9	102.53	24.90	4114		24	101.55	22.85
4004		6	104.58	25.90	4041		21	104.82	25.45	4078		12	102.44	24.70	4115	04.08.09	3	101.52	22.85
4005		9	104.64	25.85	4042		24	104.33	25.40	4079		15	102.34	24.40	4116		6	101.48	22.85
4006		12	104.82	25.80	4043	26.07.09	3	104.15	25.35	4080		18	102.27	24.40	4117		9	101.48	22.70
4007		15	105.11	25.75	4044		6	103.81	25.35	4081		21	102.23	24.50	4118		12	101.48	22.75
4008		18	105.40	25.65	4045		9	103.75	25.30	4082		24	102.19	24.40	4119		15	101.44	22.70
4009		21	105.61	25.55	4046		12	103.72	25.30	4083	31.07.09	3	102.16	24.20	4120		18	101.44	22.65
4010		24	105.74	25.45	4047		15	103.69	25.25	4084		6	102.12	24.00	4121		21	101.44	22.60
4011	22.07.09	3	105.80	25.45	4048		18	103.69	25.20	4085		9	102.08	23.80	4122		24	101.41	22.60
4012		6	105.55	25.45	4049		21	103.69	25.15	4086		12	102.05	23.60	4123	05.08.09	3	101.41	22.60
4013		9	105.27	25.45	4050		24	103.51	25.10	4087		15	102.05	23.70	4124		6	101.39	22.60

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
4125		9	101.39	22.60	4162		24	101.27	22.35	4199		15	101.83	23.20	4236		6	101.44	23.10
4126		12	101.39	22.55	4163	10.08.09	3	101.29	22.35	4200		18	101.85	23.20	4237		9	101.44	22.90
4127		15	101.39	22.55	4164		6	101.29	22.35	4201		21	101.88	23.15	4238		12	101.44	22.80
4128		18	101.39	22.55	4165		9	101.32	22.35	4202		24	101.90	23.15	4239		15	101.44	22.90
4129		21	101.39	22.50	4166		12	101.32	22.30	4203	15.08.09	3	101.93	23.15	4240		18	101.48	22.85
4130		24	101.41	22.50	4167		15	101.34	22.30	4204		6	101.97	23.15	4241		21	101.52	22.85
4131	06.08.09	3	101.42	22.55	4168		18	101.37	22.30	4205		9	102.00	23.20	4242		24	101.55	22.85
4132		6	101.44	22.55	4169		21	101.39	22.30	4206		12	102.00	23.20	4243	20.08.09	3	101.62	22.80
4133		9	101.44	22.60	4170		24	101.59	22.30	4207		15	102.00	23.35	4244		6	101.66	22.80
4134		12	101.44	22.60	4171	11.08.09	3	101.95	22.30	4208		18	102.00	23.50	4245		9	101.73	22.80
4135		15	101.44	22.55	4172		6	102.23	22.35	4209		21	102.00	23.60	4246		12	101.73	22.75
4136		18	101.44	22.55	4173		9	102.27	22.35	4210		24	102.00	23.80	4247		15	101.73	22.80
4137		21	101.44	22.55	4174		12	102.23	22.35	4211	16.08.09	3	101.97	23.90	4248		18	101.80	22.90
4138		24	101.44	22.55	4175		15	102.16	22.45	4212		6	101.97	24.00	4249		21	101.85	22.90
4139	07.08.09	3	101.42	22.50	4176		18	102.05	22.40	4213		9	101.95	24.00	4250		24	101.97	23.00
4140		6	101.42	22.50	4177		21	102.00	22.40	4214		12	101.93	24.00	4251	21.08.09	3	102.16	23.20
4141		9	101.42	22.50	4178		24	102.00	22.40	4215		15	101.93	24.00	4252		6	102.34	23.30
4142		12	101.42	22.55	4179	12.08.09	3	102.02	22.45	4216		18	101.90	24.00	4253		9	102.41	23.50
4143		15	101.39	22.55	4180		6	102.05	22.55	4217		21	101.90	24.00	4254		12	102.75	23.50
4144		18	101.39	22.55	4181		9	102.05	22.65	4218		24	101.88	24.00	4255		15	102.47	23.45
4145		21	101.39	22.55	4182		12	102.05	23.00	4219	17.08.09	3	101.85	24.00	4256		18	102.47	23.45
4146		24	101.37	22.45	4183		15	102.05	23.30	4220		6	101.83	23.90	4257		21	102.50	23.45
4147	08.08.09	3	101.37	22.45	4184		18	102.02	23.50	4221		9	101.80	23.90	4258		24	102.47	23.45
4148		6	101.34	22.50	4185		21	102.00	23.50	4222		12	101.77	23.80	4259	22.08.09	3	102.41	23.40
4149		9	101.32	22.50	4186		24	101.95	23.60	4223		15	101.73	23.75	4260		6	102.34	23.40
4150		12	101.32	22.50	4187	13.08.09	3	101.90	23.60	4224		18	101.70	23.70	4261		9	102.27	23.45
4151		15	101.29	22.50	4188		6	101.85	23.60	4225		21	101.64	23.70	4262		12	102.23	23.50
4152		18	101.29	22.50	4189		9	101.83	23.60	4226		24	101.62	23.60	4263		15	102.16	23.60
4153		21	101.27	22.50	4190		12	101.80	23.50	4227	18.08.09	3	101.59	23.55	4264		18	102.16	23.80
4154		24	101.27	22.50	4191		15	101.77	23.45	4228		6	101.55	23.50	4265		21	102.12	23.90
4155	09.08.09	3	101.27	22.50	4192		18	101.73	23.45	4229		9	101.55	23.50	4266		24	102.08	24.00
4156		6	101.24	22.50	4193		21	101.73	23.45	4230		12	101.52	23.40	4267	23.08.09	3	102.05	24.05
4157		9	101.24	22.50	4194		24	101.73	23.45	4231		15	101.52	23.35	4268		6	102.02	24.10
4158		12	101.22	22.50	4195	14.08.09	3	101.77	23.40	4232		18	101.52	23.30	4269		9	102.00	24.10
4159		15	101.22	22.50	4196		6	101.77	23.40	4233		21	101.52	23.25	4270		12	101.97	24.05
4160		18	101.24	22.45	4197		9	101.80	23.35	4234		24	101.48	23.20	4271		15	101.95	24.00
4161		21	101.27	22.40	4198		12	101.83	23.30	4235	19.08.09	3	101.48	23.15	4272		18	101.95	24.00

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
4273		21	101.93	24.00	4310		12	103.42	24.70	4347	02.09.09	3	101.83	23.30	4384		18	102.96	22.90
4274		24	101.93	24.00	4311		15	103.36	24.80	4348		6	101.83	23.30	4385		21	103.05	23.00
4275	24.08.09	3	101.93	23.90	4312		18	103.24	25.10	4349		9	101.83	23.25	4386		24	103.02	23.20
4276		6	101.93	23.80	4313		21	103.09	25.10	4350		12	101.83	23.25	4387	07.09.09	3	102.93	23.60
4277		9	101.93	23.70	4314		24	103.02	25.10	4351		15	101.80	23.20	4388		6	102.81	23.55
4278		12	101.93	23.60	4315	29.08.09	3	102.96	24.90	4352		18	101.80	23.15	4389		9	102.72	23.65
4279		15	101.90	23.60	4316		6	102.93	24.80	4353		21	101.80	23.10	4390		12	102.63	23.70
4280		18	101.90	23.60	4317		9	102.87	24.75	4354		24	101.80	23.10	4391		15	102.57	23.85
4281		21	101.93	23.60	4318		12	102.81	24.75	4355	03.09.09	3	101.80	23.05	4392		18	102.47	24.00
4282		24	101.95	23.60	4319		15	102.75	24.75	4356		6	101.80	23.00	4393		21	102.41	24.20
4283	25.08.09	3	101.95	23.55	4320		18	102.69	24.80	4357		9	101.80	23.00	4394		24	102.30	24.30
4284		6	101.97	23.50	4321		21	102.63	24.80	4358		12	101.80	22.95	4395	08.09.09	3	102.19	24.40
4285		9	102.00	23.50	4322		24	102.53	24.70	4359		15	101.83	22.95	4396		6	102.12	24.50
4286		12	102.00	23.50	4323	30.08.09	3	102.47	24.60	4360		18	101.83	22.95	4397		9	102.05	24.50
4287		15	102.05	23.50	4324		6	102.41	24.50	4361		21	101.83	22.90	4398		12	102.02	24.40
4288		18	102.08	23.50	4325		9	102.38	24.30	4362		24	101.80	22.90	4399		15	102.00	24.30
4289		21	102.12	23.55	4326		12	102.34	24.20	4363	04.09.09	3	101.73	22.90	4400		18	101.97	24.30
4290		24	102.12	23.55	4327		15	102.30	24.10	4364		6	101.66	22.90	4401		21	101.95	24.20
4291	26.08.09	3	102.12	23.60	4328		18	102.27	24.20	4365		9	101.62	22.95	4402		24	101.93	24.10
4292		6	102.12	23.60	4329		21	102.23	24.20	4366		12	101.59	22.90	4403	09.09.09	3	101.90	23.95
4293		9	102.12	23.60	4330		24	102.19	24.00	4367		15	101.59	22.90	4404		6	101.88	23.85
4294		12	102.12	23.55	4331	31.08.09	3	102.16	23.90	4368		18	101.59	22.90	4405		9	101.85	23.70
4295		15	102.12	23.55	4332		6	102.12	23.80	4369		21	101.59	22.90	4406		12	101.83	23.65
4296		18	102.21	23.60	4333		9	102.12	23.80	4370		24	101.59	22.90	4407		15	101.83	23.55
4297		21	102.30	23.65	4334		12	102.12	23.80	4371	05.09.09	3	101.62	22.90	4408		18	101.83	23.55
4298		24	102.53	23.70	4335		15	102.12	23.80	4372		6	101.66	22.90	4409		21	101.80	23.50
4299	27.08.09	3	102.75	23.80	4336		18	102.12	23.80	4373		9	101.80	22.90	4410		24	101.77	23.45
4300		6	102.96	23.90	4337		21	102.12	23.80	4374		12	101.88	22.90	4411	10.09.09	3	101.73	23.40
4301		9	103.24	23.90	4338		24	102.05	23.80	4375		15	101.95	22.90	4412		6	101.70	23.35
4302		12	103.42	23.95	4339	01.09.09	3	102.00	23.70	4376		18	102.02	22.90	4413		9	101.66	23.30
4303		15	103.54	23.80	4340		6	101.95	23.60	4377		21	102.16	22.90	4414		12	101.62	23.20
4304		18	103.66	23.85	4341		9	101.93	23.55	4378		24	102.34	22.90	4415		15	101.59	23.15
4305		21	103.75	23.80	4342		12	101.90	23.50	4379	06.09.09	3	102.50	22.90	4416		18	101.55	23.15
4306		24	103.75	23.90	4343		15	101.88	23.45	4380		6	102.63	22.85	4417		21	101.55	23.10
4307	28.08.09	3	103.69	24.00	4344		18	101.85	23.40	4381		9	102.72	22.85	4418		24	101.55	23.05
4308		6	103.60	24.20	4345		21	101.85	23.40	4382		12	102.81	22.80	4419	11.09.09	3	101.52	23.00
4309		9	103.51	24.45	4346		24	101.85	23.35	4383		15	102.87	22.80	4420		6	101.52	23.00

Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	Sl No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
4569		21	101.09	22.50	4606		12	101.52	22.95	4643	09.10.09	3	101.42	22.55	4680		18	101.05	22.15					
4570		24	101.05	22.50	4607		15	101.52	22.90	4644		6	101.39	22.60	4681		21	101.05	22.15					
4571	30.09.09	3	101.05	22.50	4608		18	101.48	22.85	4645		9	101.37	22.60	4682		24	101.02	22.15					
4572		6	101.05	22.50	4609		21	101.48	22.80	4646		12	101.34	22.60	4683	14.10.09	3	101.02	22.15					
4573		9	101.05	22.50	4610		24	101.48	22.75	4647		15	101.32	22.65	4684		6	101.02	22.15					
4574		12	101.05	22.50	4611	05.10.09	3	101.48	22.75	4648		18	101.29	22.60	4685		9	101.02	22.15					
4575		15	101.02	22.50	4612		6	101.48	22.70	4649		21	101.27	22.55	4686		12	100.95	22.15					
4576		18	101.02	22.55	4613		9	101.48	22.70	4650		24	101.27	22.55	4687		15	101.02	22.15					
4577		21	101.02	22.55	4614		12	101.48	22.70	4651	10.10.09	3	101.24	22.55	4688		18	100.98	22.10					
4578		24	101.02	22.55	4615		15	101.44	22.75	4652		6	101.24	22.55	4689		21	100.98	22.10					
4579	01.10.09	3	101.05	22.45	4616		18	101.42	22.75	4653		9	101.24	22.50	4690		24	100.98	22.10					
4580		6	101.09	22.30	4617		21	101.37	22.80	4654		12	101.24	22.45	4691	15.10.09	3	100.95	22.10					
4581		9	101.09	22.30	4618		24	101.34	22.80	4655		15	101.22	22.40	4692		6	100.95	22.05					
4582		12	101.09	22.45	4619	06.10.09	3	101.34	22.80	4656		18	101.22	22.40	4693		9	100.95	21.90					
4583		15	101.12	22.50	4620		6	101.32	22.80	4657		21	101.22	22.40	4694		12	100.95	21.80					
4584		18	101.12	22.60	4621		9	101.32	22.75	4658		24	101.22	22.40	4695		15	100.95	21.70					
4585		21	101.12	22.70	4622		12	101.32	22.70	4659	11.10.09	3	101.22	22.40	4696		18	100.95	21.70					
4586		24	101.16	22.70	4623		15	101.34	22.70	4660		6	101.22	22.35	4697		21	100.95	21.65					
4587	02.10.09	3	101.16	22.70	4624		18	101.37	22.80	4661		9	101.19	22.25	4698		24	100.92	21.60					
4588		6	101.19	22.70	4625		21	101.37	22.80	4662		12	101.19	22.25	4699	16.10.09	3	100.92	21.50					
4589		9	101.19	22.70	4626		24	101.39	22.80	4663		15	101.19	22.25	4700		6	100.92	21.40					
4590		12	101.22	22.75	4627	07.10.09	3	101.48	22.80	4664		18	101.16	22.35	4701		9	100.88	21.30					
4591		15	101.22	22.80	4628		6	101.55	22.75	4665		21	101.16	22.30	4702		12	100.88	21.30					
4592		18	101.24	22.90	4629		9	101.62	22.75	4666		24	101.16	22.30	4703		15	100.85	21.35					
4593		21	101.24	22.95	4630		12	101.66	22.70	4667	12.10.09	3	101.16	22.25	4704		18	100.85	21.35					
4594		24	101.27	23.00	4631		15	101.70	22.65	4668		6	101.16	22.20	4705		21	100.85	21.35					
4595	03.10.09	3	101.27	23.05	4632		18	101.73	22.60	4669		9	101.16	22.20	4706		24	100.85	21.35					
4596		6	101.29	23.10	4633		21	101.73	22.55	4670		12	101.16	22.10	4707	17.10.09	3	100.85	21.35					
4597		9	101.29	23.10	4634		24	101.70	22.55	4671		15	101.16	22.10	4708		6	100.85	21.35					
4598		12	101.32	23.15	4635	08.10.09	3	101.62	22.55	4672		18	101.12	22.10	4709		9	100.85	21.35					
4599		15	101.37	23.15	4636		6	101.59	22.50	4673		21	101.12	22.15	4710		12	100.85	21.35					
4600		18	101.42	23.15	4637		9	101.55	22.50	4674		24	101.12	22.15	4711		15	100.85	21.35					
4601		21	101.52	23.15	4638		12	101.52	22.45	4675	13.10.09	3	101.12	22.15	4712		18	100.85	21.35					
4602		24	101.52	23.15	4639		15	101.52	22.45	4676		6	101.09	22.15	4713		21	100.85	21.35					
4603	04.10.09	3	101.52	23.10	4640		18	101.48	22.50	4677		9	101.09	22.15	4714		24	100.85	21.35					
4604		6	101.52	23.00	4641		21	101.48	22.50	4678		12	101.09	22.15	4715	18.10.09	3	100.85	21.35					
4605		9	101.52	23.00	4642		24	101.44	22.50	4679		15	101.05	22.15	4716		6	100.82	21.35					

SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)	SI No	Date	Time (hrs)	Stage at Khairmal (m)	Stage at Naraj (m)
4717		9	100.82	21.30	4745		21	100.50	21.45	4773		9	100.45	21.45	4801		21	100.36	21.20
4718		12	100.82	21.30	4746		24	100.50	21.45	4774		12	100.45	21.45	4802		24	100.36	21.25
4719		15	100.82	21.30	4747	22.10.09	3	100.50	21.45	4775		15	100.45	21.45	4803	29.10.09	3	100.36	21.30
4720		18	100.82	21.30	4748		6	100.50	21.45	4776		18	100.45	21.40	4804		6	100.36	21.35
4721		21	100.79	21.30	4749		9	100.50	21.45	4777		21	100.45	21.40	4805		9	100.36	22.00
4722		24	100.77	21.30	4750		12	100.50	21.50	4778		24	100.45	21.40	4806		12	100.36	21.70
4723	19.10.09	3	100.77	21.30	4751		15	100.45	21.50	4779	26.10.09	3	100.45	21.40	4807		15	100.36	21.30
4724		6	100.74	21.30	4752		18	100.45	21.50	4780		6	100.45	21.35	4808		18	100.36	21.30
4725		9	100.72	21.30	4753		21	100.45	21.50	4781		9	100.45	21.35	4809		21	100.36	21.30
4726		12	100.72	21.30	4754		24	100.45	21.50	4782		12	100.41	21.35	4810		24	100.36	21.30
4727		15	100.69	21.30	4755	23.10.09	3	100.45	21.50	4783		15	100.41	21.35	4811	30.10.09	3	100.36	21.30
4728		18	100.69	21.35	4756		6	100.45	21.50	4784		18	100.41	21.30	4812		6	100.36	21.25
4729		21	100.69	21.35	4757		9	100.45	21.50	4785		21	100.41	21.30	4813		9	100.41	21.20
4730		24	100.66	21.35	4758		12	100.45	21.50	4786		24	100.41	21.30	4814		12	100.45	21.25
4731	20.10.09	3	100.66	21.40	4759		15	100.50	21.50	4787	27.10.09	3	100.41	21.30	4815		15	100.50	21.25
4732		6	100.64	21.40	4760		18	100.50	21.50	4788		6	100.41	21.30	4816		18	100.50	21.20
4733		9	100.64	21.45	4761		21	100.50	21.50	4789		9	100.41	21.30	4817		21	100.54	21.20
4734		12	100.64	21.50	4762		24	100.50	21.50	4790		12	100.41	21.25	4818		24	100.54	21.20
4735		15	100.61	21.55	4763	24.10.09	3	100.50	21.50	4791		15	100.41	21.25	4819	31.10.09	3	100.54	21.20
4736		18	100.61	21.50	4764		6	100.50	21.50	4792		18	100.41	21.25	4820		6	100.50	21.25
4737		21	100.61	21.45	4765		9	100.50	21.50	4793		21	100.41	21.25	4821		9	100.50	21.30
4738		24	100.58	21.40	4766		12	100.50	21.50	4794		24	100.41	21.25	4822		12	100.50	21.35
4739	21.10.09	3	100.58	21.40	4767		15	100.50	21.45	4795	28.10.09	3	100.41	21.25	4823		15	100.50	21.40
4740		6	100.54	21.40	4768		18	100.50	21.45	4796		6	100.41	21.25	4824		18	99.59	21.45
4741		9	100.54	21.40	4769		21	100.50	21.45	4797		9	100.41	21.25	4825		21	99.59	21.50
4742		12	100.54	21.50	4770		24	100.50	21.45	4798		12	100.41	21.20					
4743		15	100.50	21.50	4771	25.10.09	3	100.50	21.45	4799		15	100.36	21.20					
4744		18	100.50	21.50	4772		6	100.50	21.45	4800		18	100.36	21.20					